

HIGH Q_0 RESEARCH: THE DYNAMICS OF FLUX TRAPPING IN SC NIOBIUM

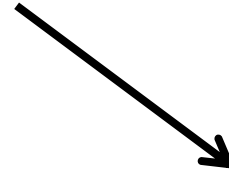
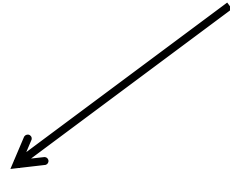
Julia Vogt, Oliver Kugeler and Jens Knobloch,
Helmholtz-Zentrum Berlin, Germany

$$G / Q_0 = R_{surface} = R_{BCS}(f, T) + R_{residual}(?)$$

- Trapped vortices under rf field (up to 100% of ambient field)
- Lossy oxides or metallic hydrides on surface
- Grain boundaries
- Precipitates
- Generation of hypersound
- Localized electron surface states
- ...

→ Surface treatment,
Bake out

TRAPPED VORTICES UNDER RF FIELD



Reduction of trapped vortices

- Shielding (earth field)
- Can we reduce pinning centers?
Impact niobium material properties
the trapping behavior?
- Are there additional ways to optimize
Meissner effect?
- Do temperature gradients generate
trapped flux?

Impact of trapped vortices on losses

$$R_{residual} \propto B_{applied}$$

→ *Phys Rev B 87, Gurevich and Ciovati (2012)*

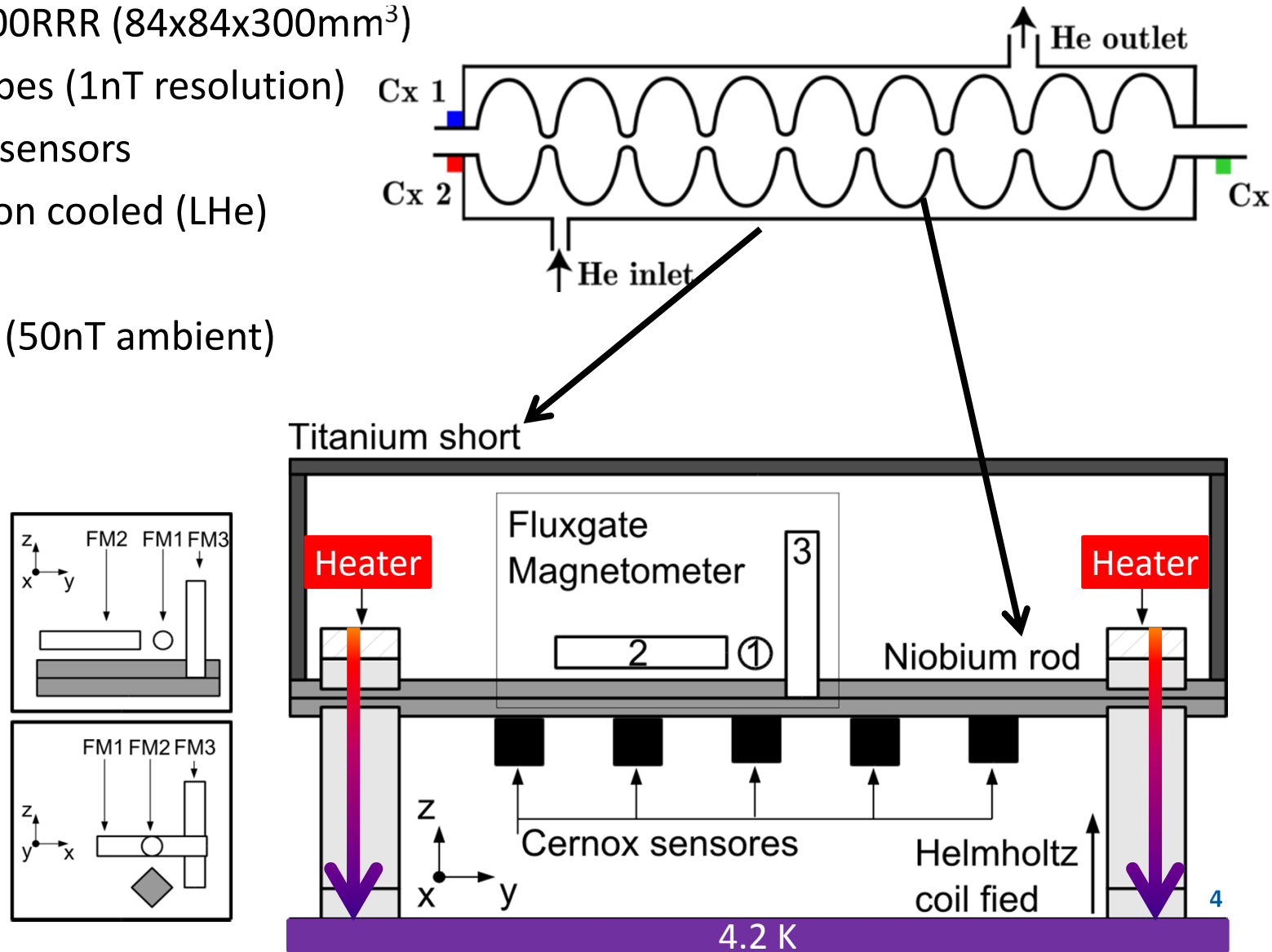
Empiric: $1\mu\text{T} \leftrightarrow 3.5\text{n}\Omega$ (TESLA)

→ *Phys. Rev. STAB 3, B. Aune, et al. (2000)*

→ *Vogt, Kugeler and Knobloch, PRSTAB (accepted for publication, Sept. 11, 2013)*

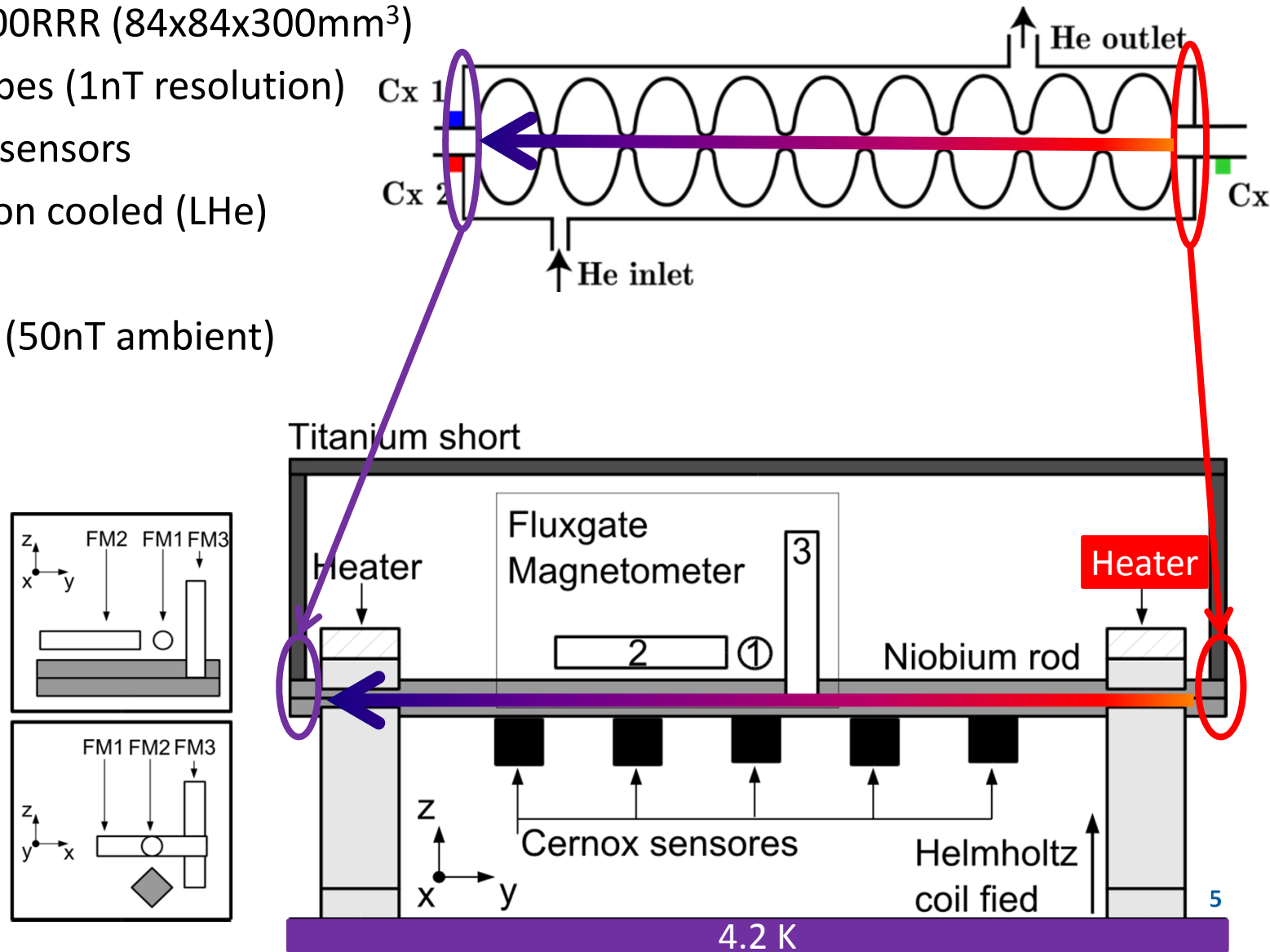
MODEL SYSTEM

- Mimics thermoelectric properties of cavity-tank system
- Nb rod 300RRR (84x84x300mm³)
- 3 FM probes (1nT resolution)
- 7 Cernox sensors
- Conduction cooled (LHe)
- 2 heaters
- Shielding (50nT ambient)

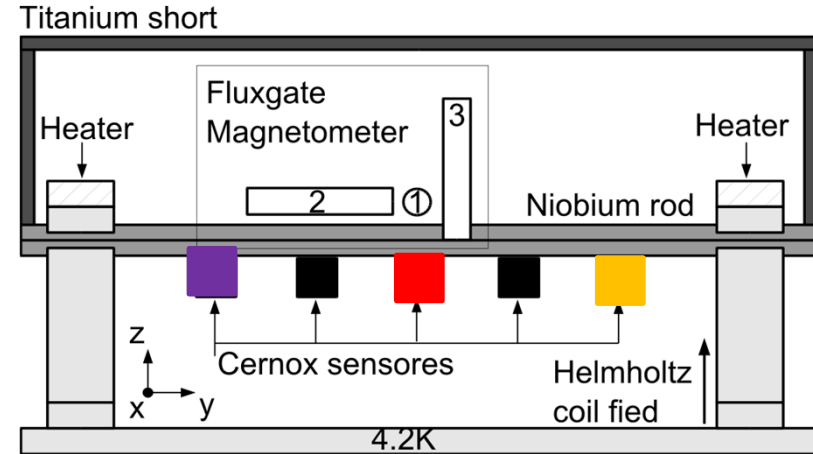
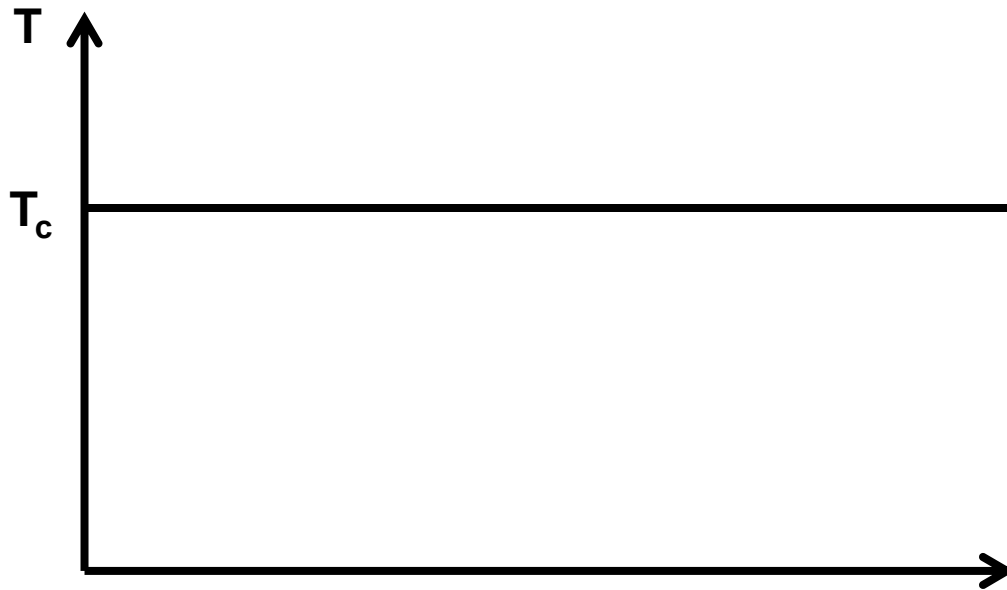


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MODEL SYSTEM: THERMOCURRENTS



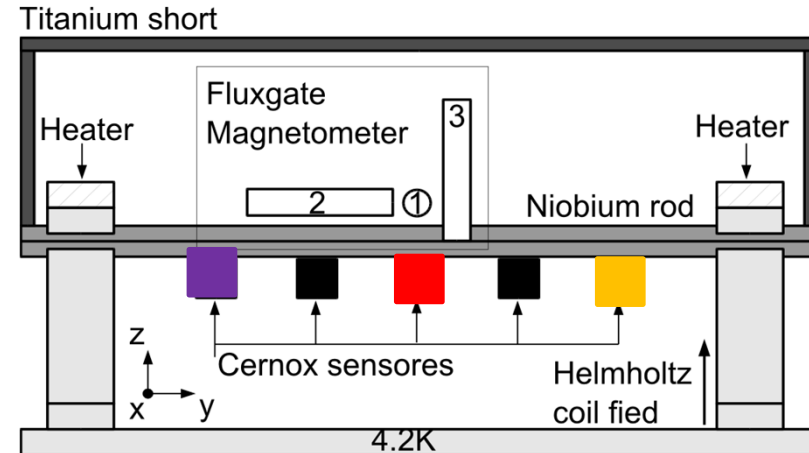
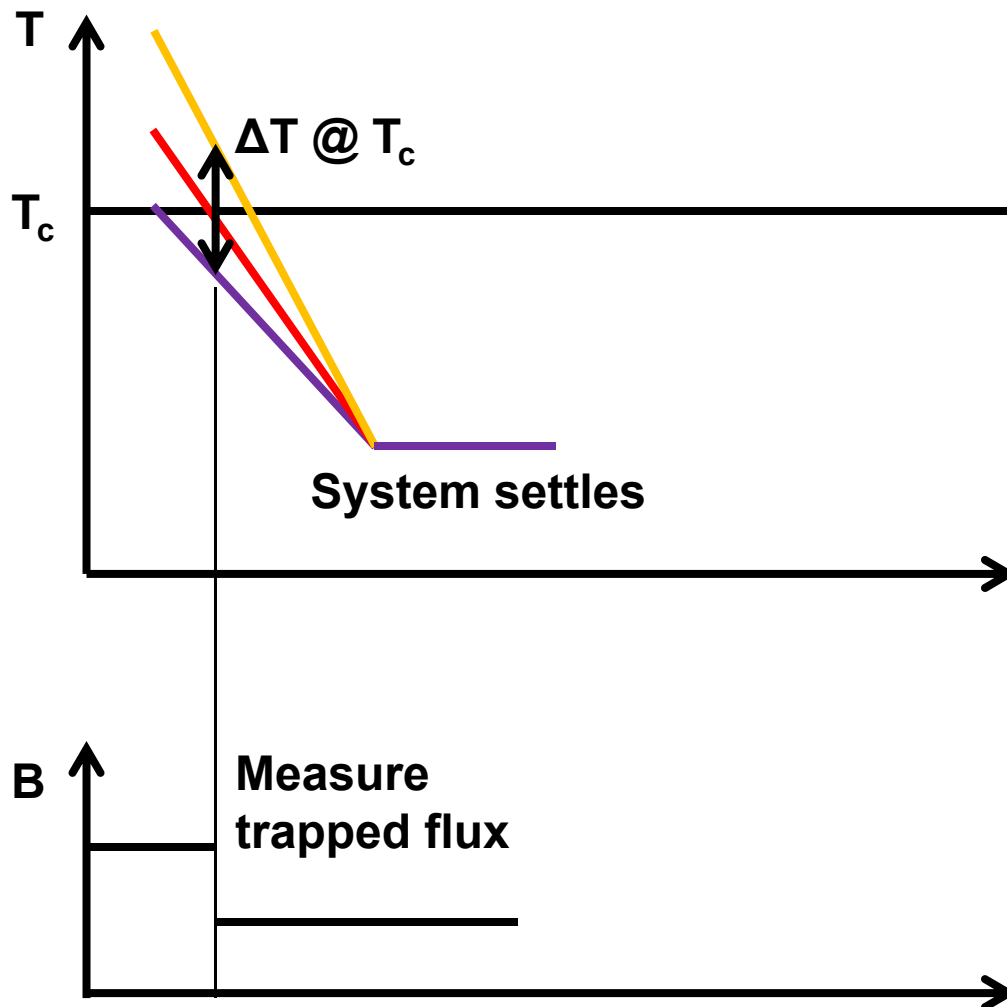
Two contact points on different temperatures

Level of trapped flux correlates with ΔT at the instance of phase Transition. Thermoelectric effect:

$$B \leftrightarrow I = \Delta V / R = \Delta S \cdot \Delta T / R$$

Thermopower of System $\Delta S = S_{Nb} - S_{Ti}$

MODEL SYSTEM: THERMOCURRENTS



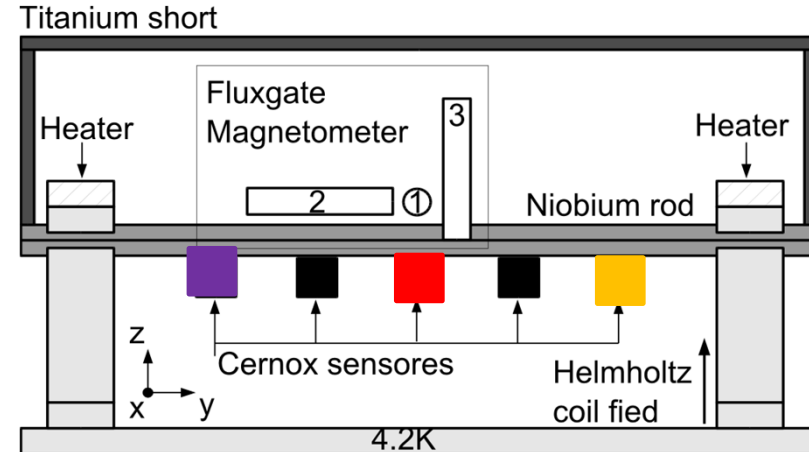
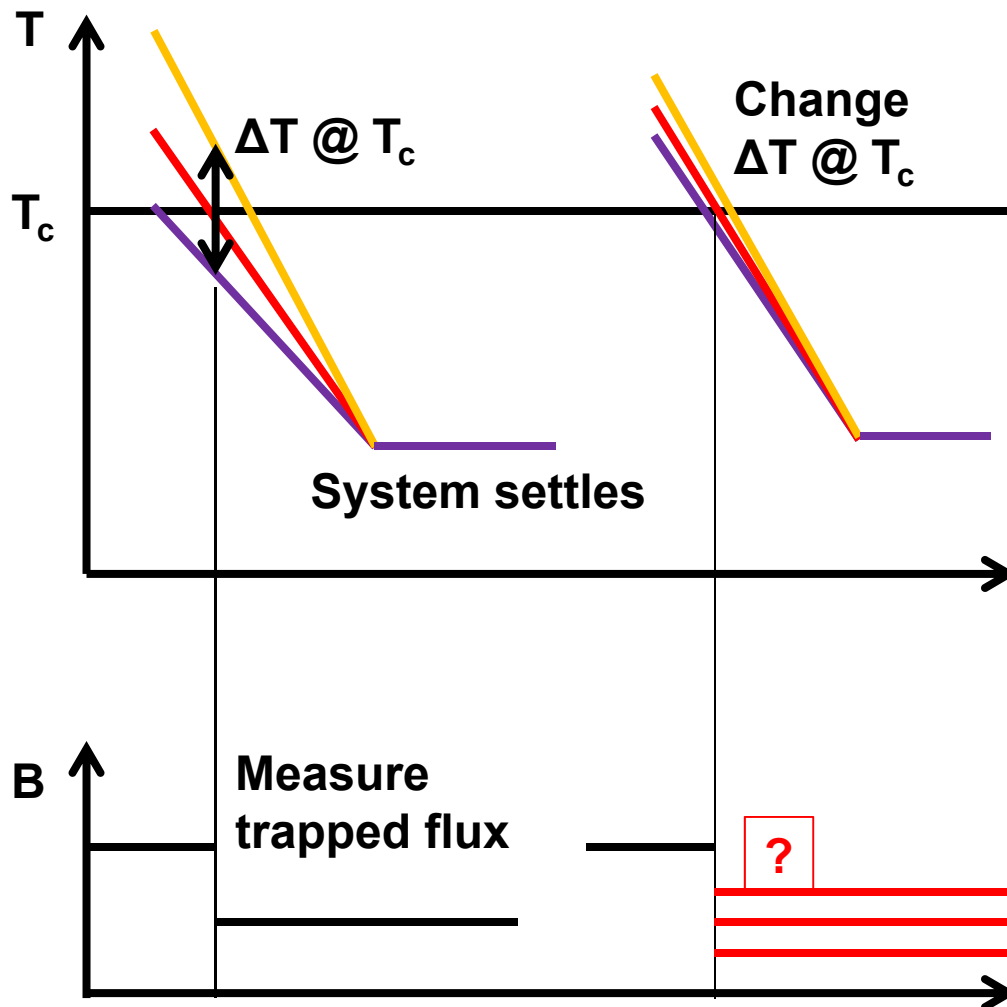
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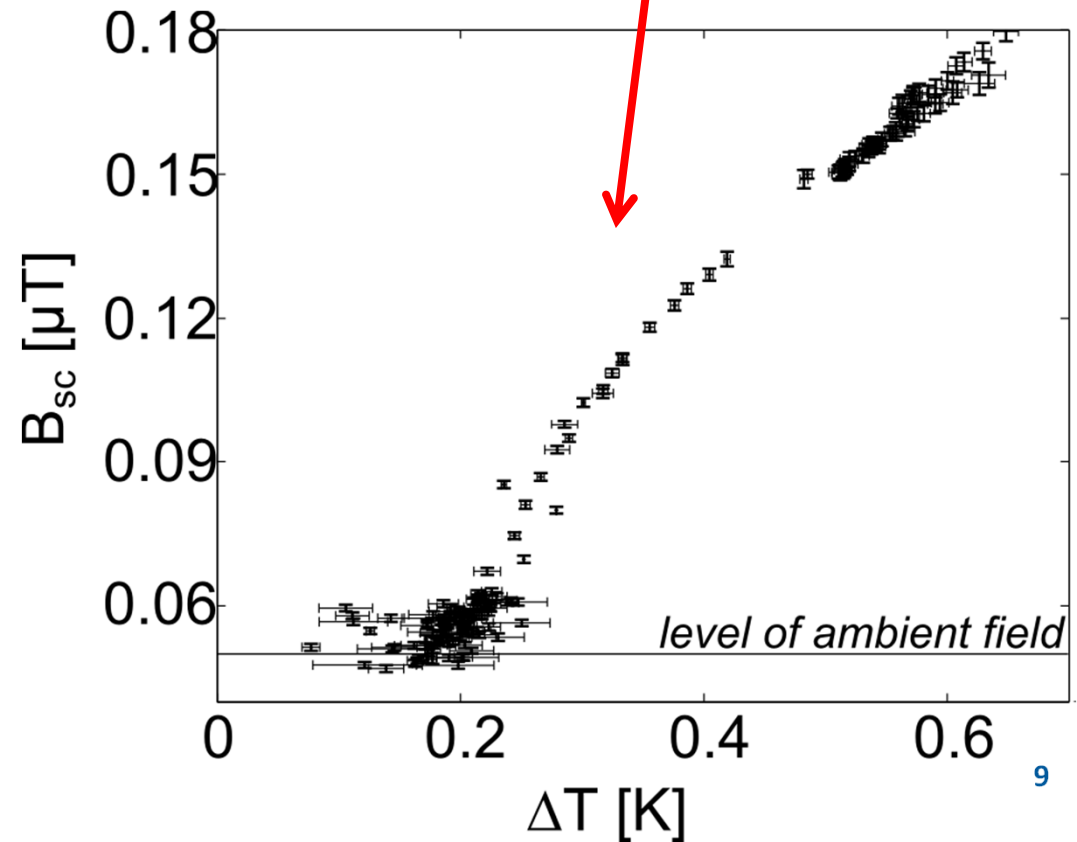
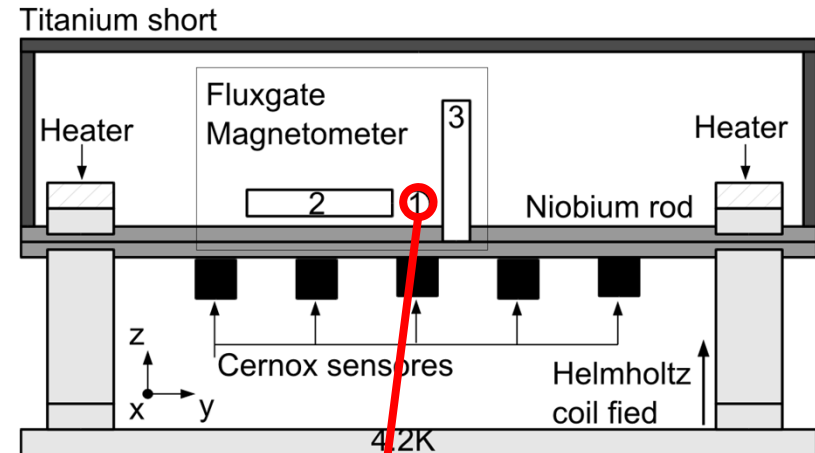
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$$B \leftrightarrow I = \Delta V / R = \Delta S \cdot \Delta T / R$$

Thermopower of System $\Delta S = S_{\text{Nb}} - S_{\text{Ti}}$

- Measure temperature difference during phase transition of Nb rod
- System settles
- Measure trapped flux



MODEL SYSTEM: THERMOCURRENTS

- Two contact points on different temperatures

Level of trapped flux correlates with ΔT at the instance of phase Transition. Thermoelectric effect:

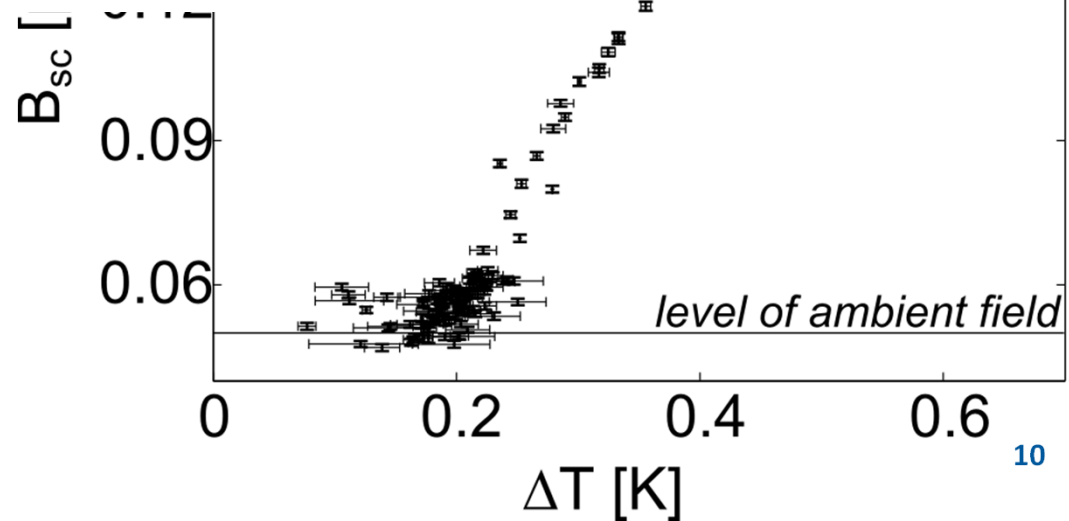
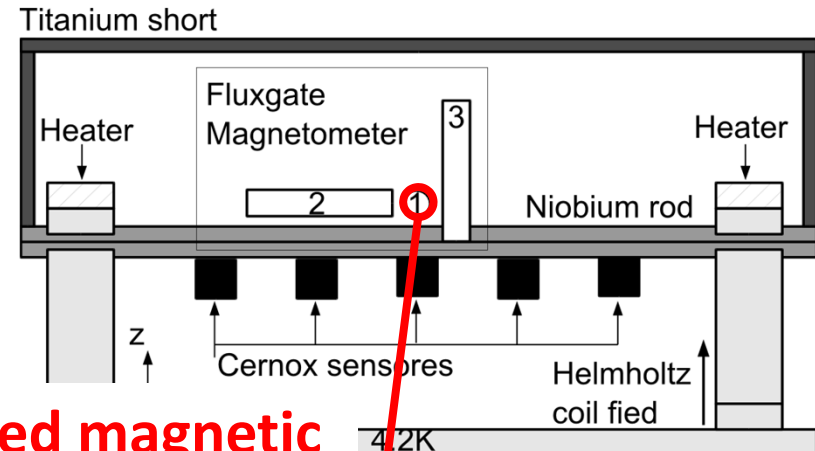
$$B \leftrightarrow I = \Delta V / R$$

Thermopower of S_i

- Measure temperature during phase transition
- System settles
- Measure trapped flux

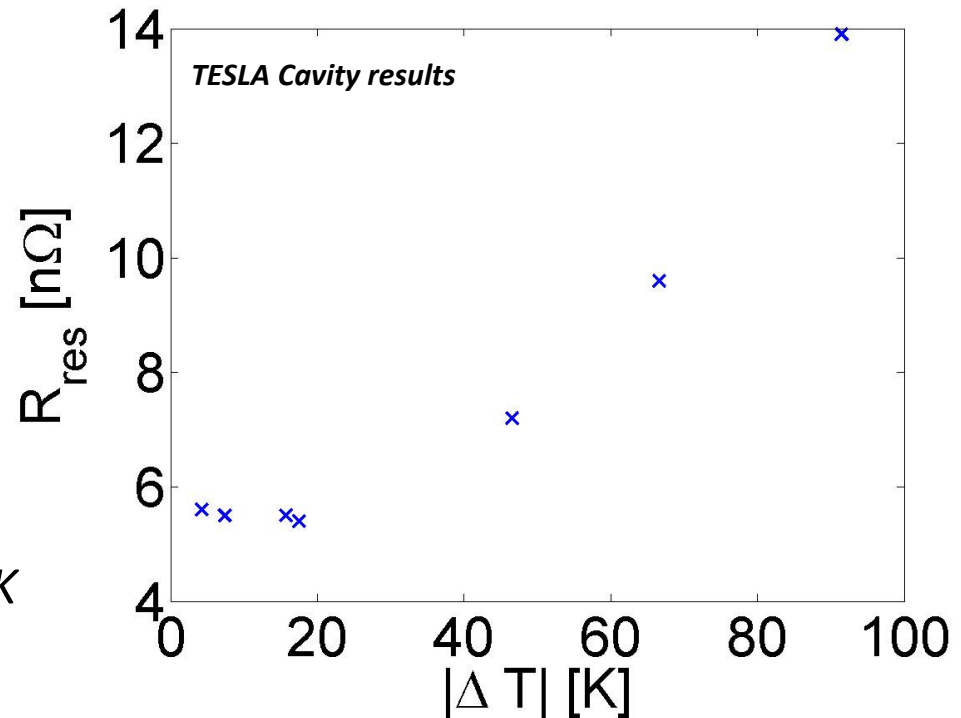
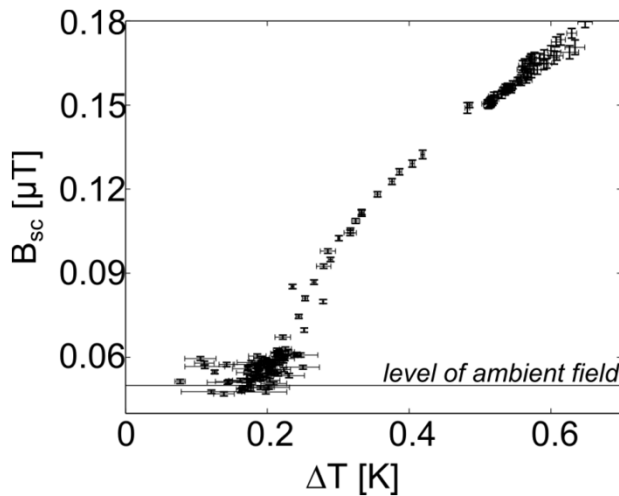
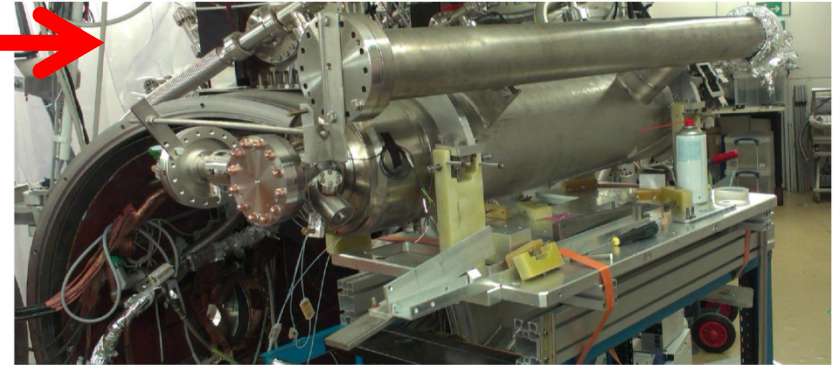
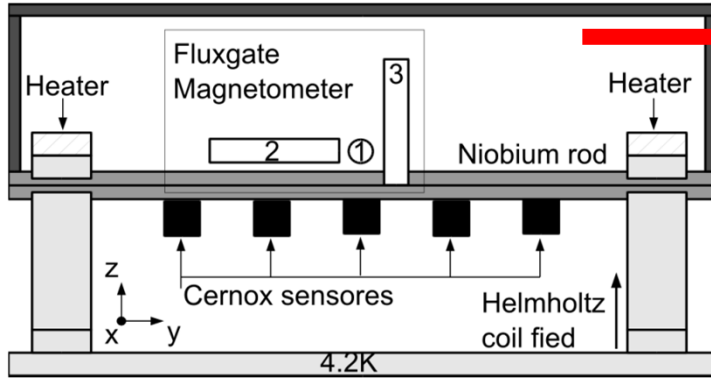
Thermoelectrically induced magnetic field gets trapped in sc niobium!

Is this measurement able to explain the observed variation in R_{res} ?



MODEL SYSTEM VS. DRESSED CAVITY: TEST 1

Titanium short



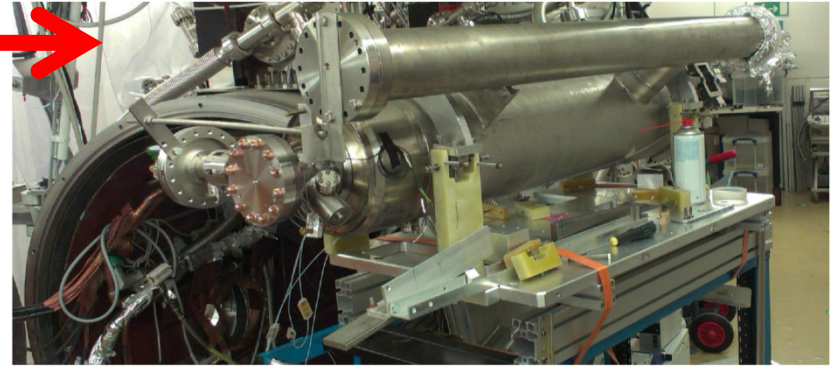
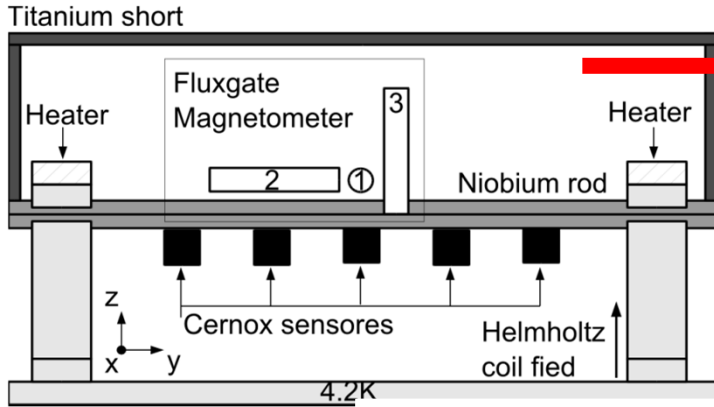
Model system: $B = 0.12 \mu T$ for $\Delta T = 0.6 K$

0.12 μT trapped in a TESLA Cavity:

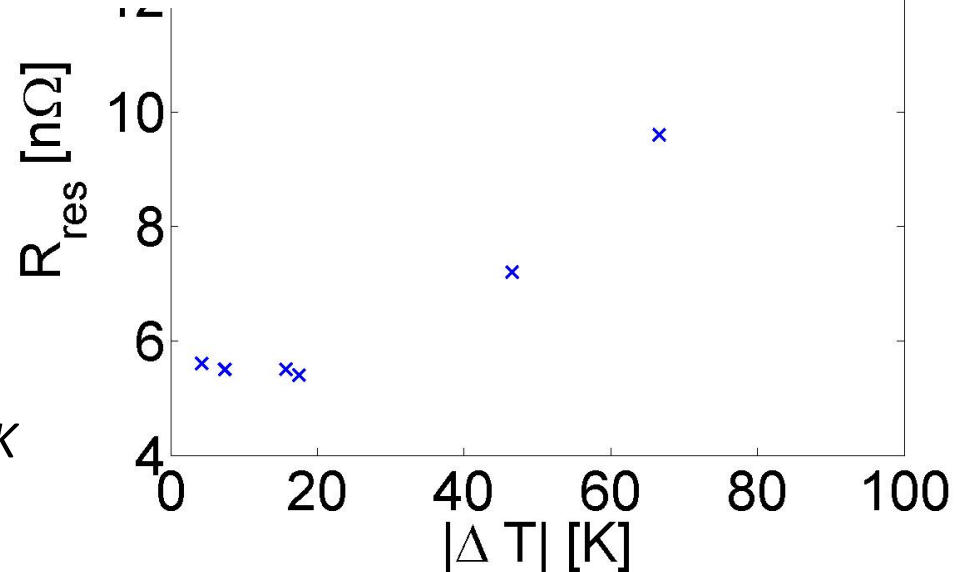
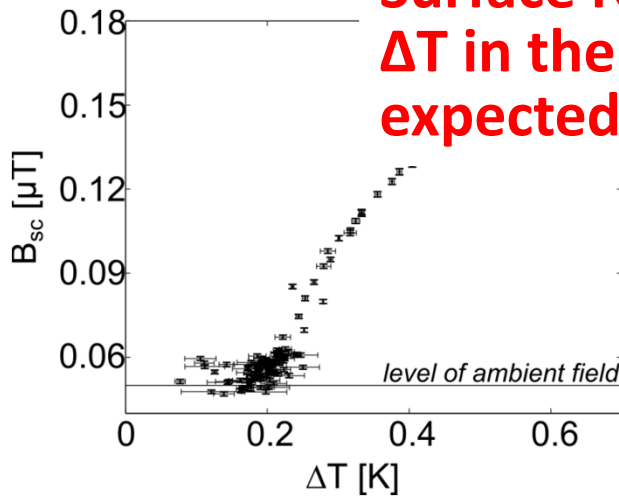
$$\rightarrow \Delta R_{res} = 0.4 n\Omega$$

→ Kugeler, Vogt and Knobloch, SRF2013, TUIOA0111

MODEL SYSTEM VS. DRESSED CAVITY: TEST 1



Surface resistance in the 10 nΩ range for ΔT in the 10's K range can reasonably be expected!



Model system: $B = 0.12\mu T$ for $\Delta T = 0.6K$

0.12μT trapped in a TESLA Cavity:

$$\rightarrow \Delta R_{res} = 0.4n\Omega$$

→ Kugeler, Vogt and Knobloch, SRF2013, TUIOA0112

MODEL SYSTEM VS. DRESSED CAVITY: TEST 2

Is this measurement able to explain the observed variation in R_{res} ?

$$B \leftrightarrow I = \Delta V / R = \Delta S \cdot \Delta T / R$$

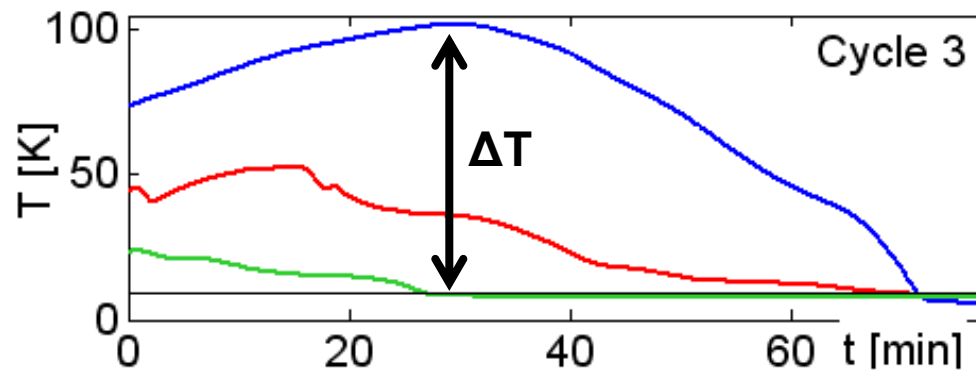
Thermopower: $\Delta S \approx 10 \mu\text{V/K}$

Literature is not consistent for titanium.
Independent measurement performed
in HoBiCaT.

Parameter of cavity-tank system @10K:
 $R \approx 100 \mu\Omega$ (dominated by titanium tank)

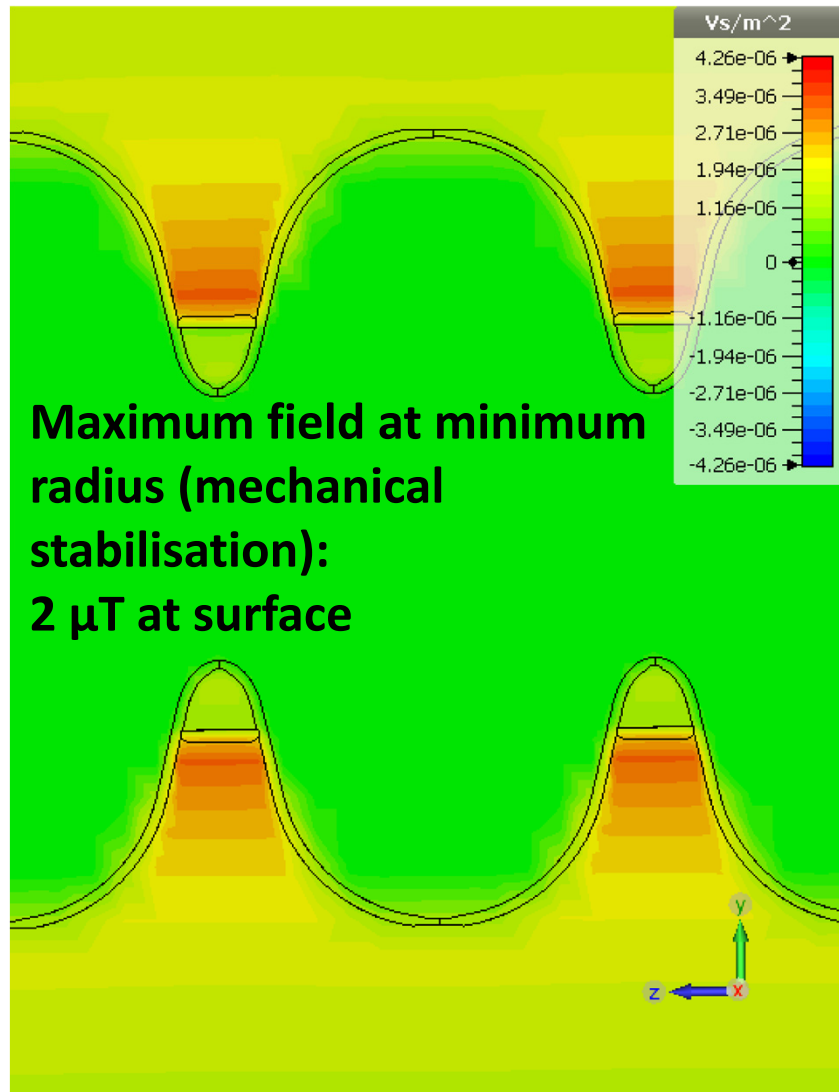
→ J. Milck, Tech. Rep., Hughes Aircraft Company (1970)

$$= 10 \mu\text{V/K} \cdot 100\text{K} / 100 \mu\Omega = 1\text{A}$$

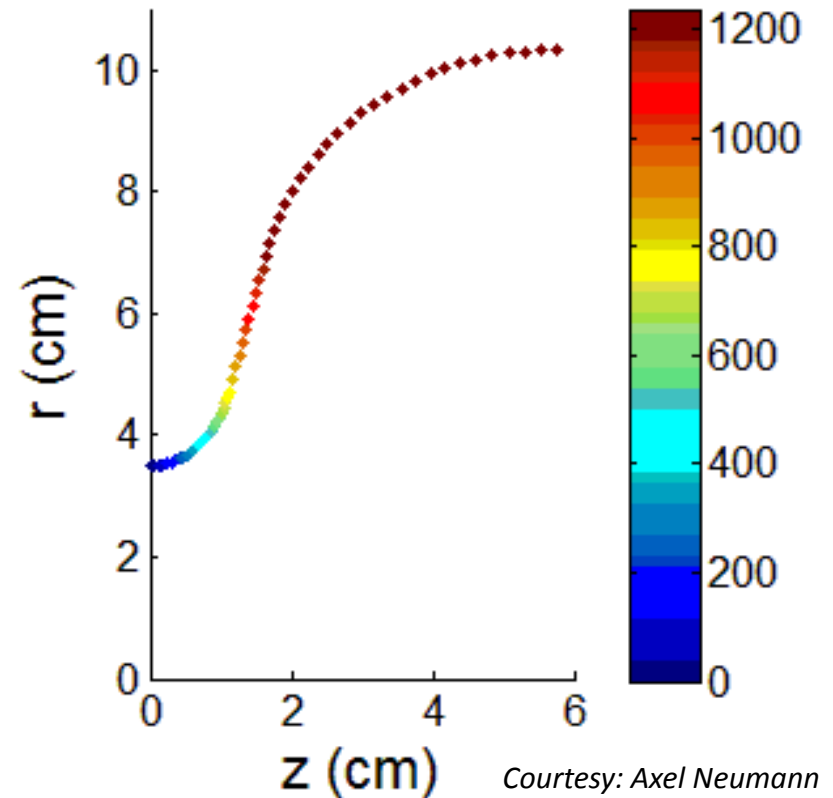


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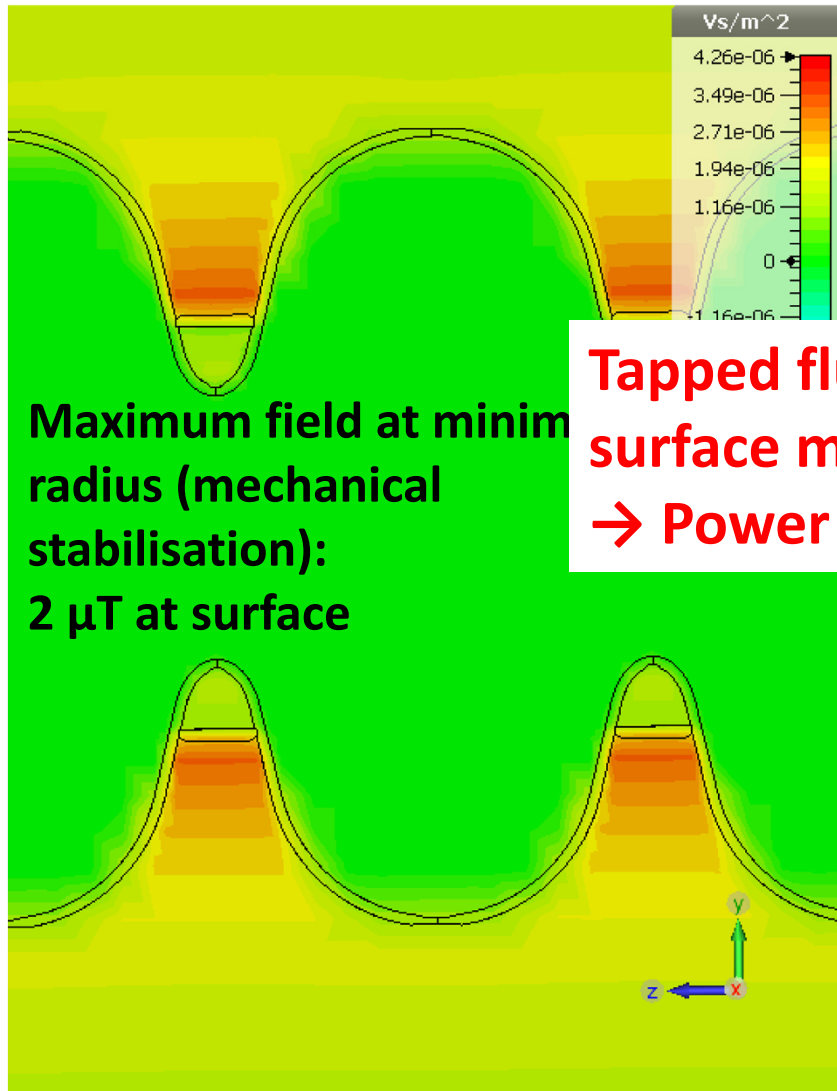


TESLA half cell, TM_{010} π -mode, surface H-field



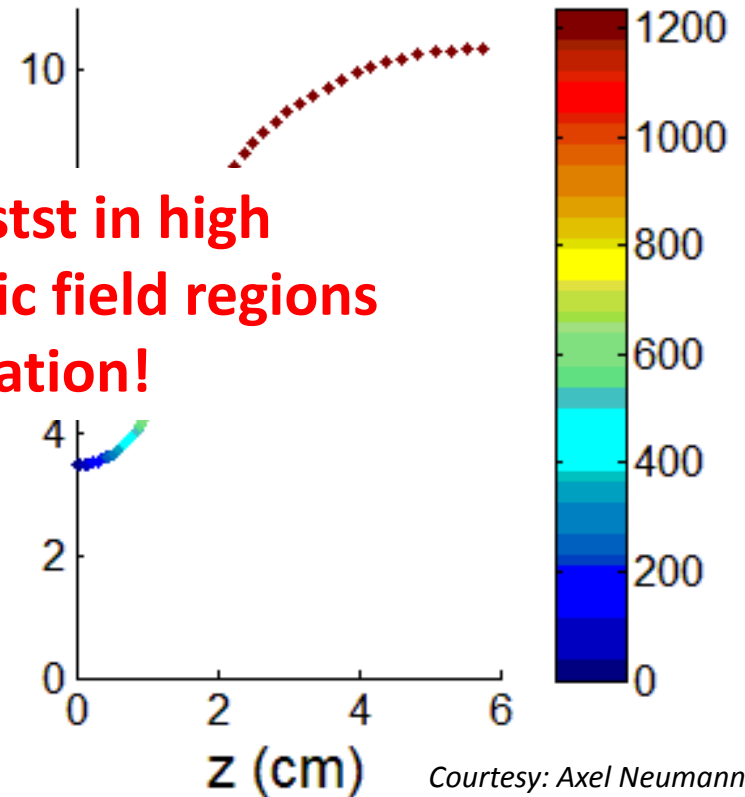
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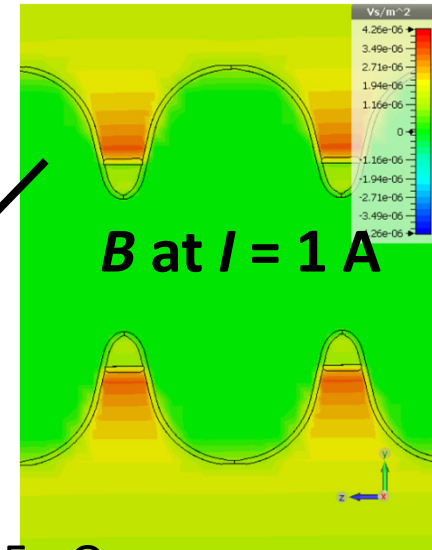
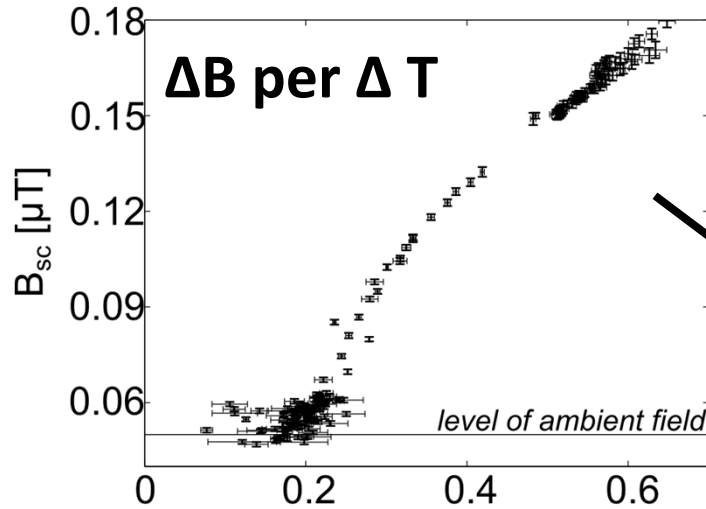
**Tapped flux existst in high
surface magnetic field regions
→ Power dissipation!**

TESLA half cell, TM_{010} π -mode, surface H-field



MODEL SYSTEM VS. DRESSED CAVITY: TEST 2

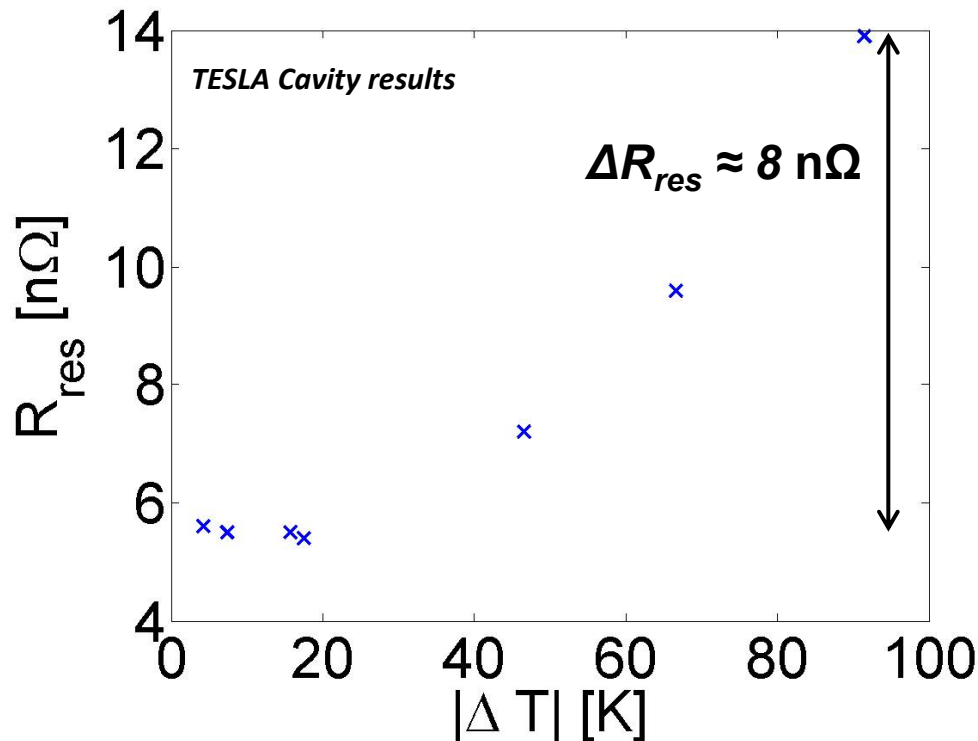
Model system results



2 μT trapped flux
for $\Delta T = 100 K$

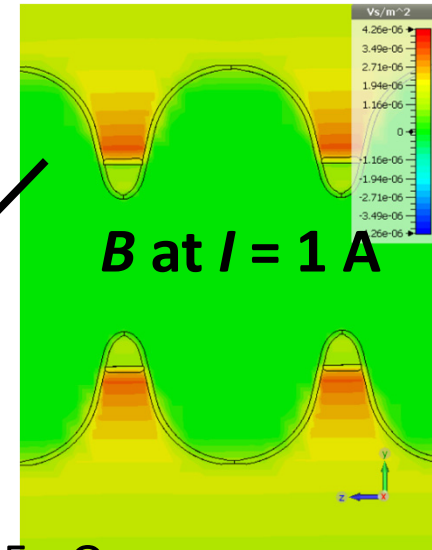
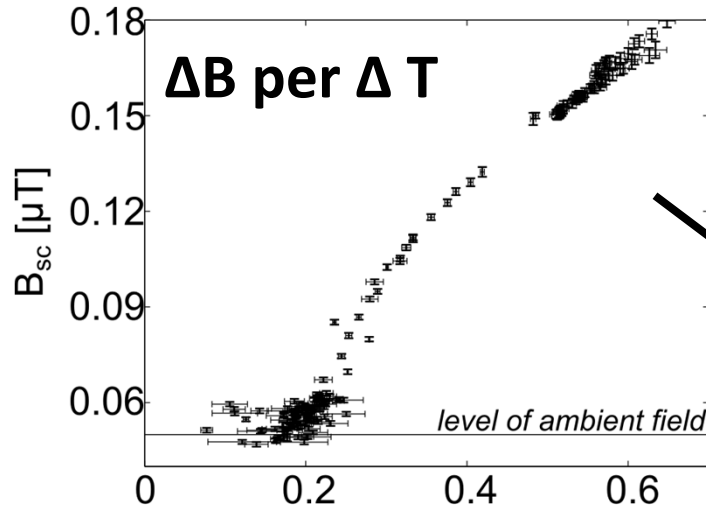
1 $\mu T \Leftrightarrow 3.5$ n Ω

cause 7 n Ω additional
surface resistance



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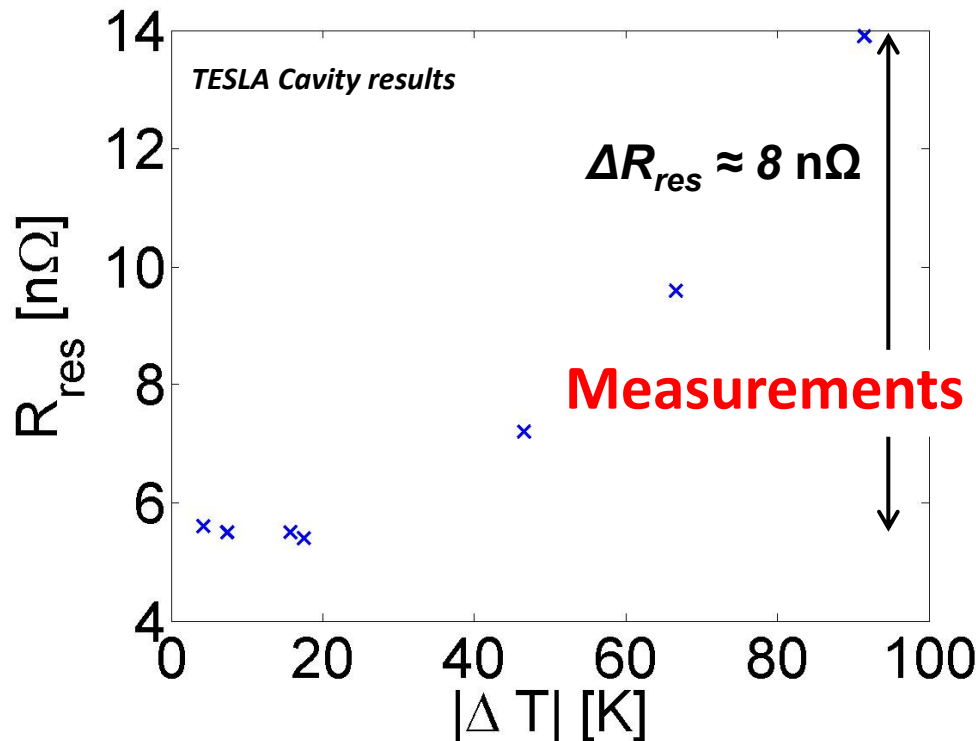


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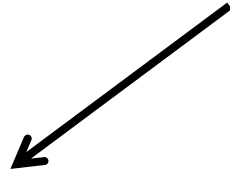
1 μT $\leftrightarrow$ 3.5 nΩ

**cause 7 nΩ additional
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Measurements are consistent!

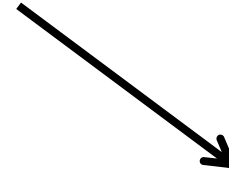


TRAPPED VORTICES UNDER RF FIELD



Reduction of trapped vortices

- Shielding (earth field)
- Do temperature gradients generate trapped flux?
- Can we reduce pinning centers?
Impact niobium material properties
the trapping behavior?
- Are there additional ways to optimize
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Impact of trapped vortices on losses

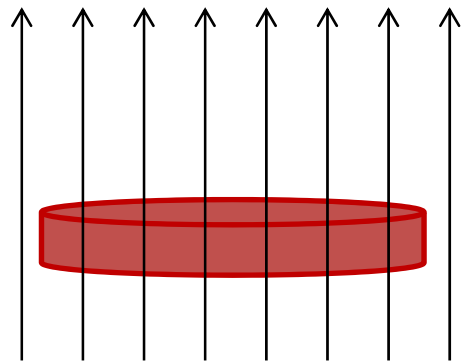
$$R_{residual} \propto B_{applied}$$

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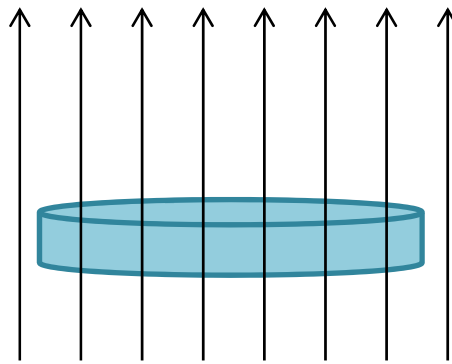
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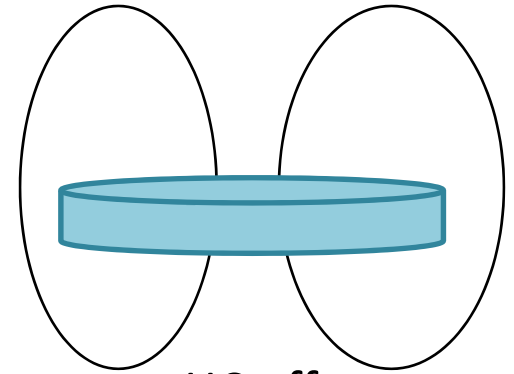
FLUX TRAPPING IN DISK-SHAPED NIOBIUM SAMPLES



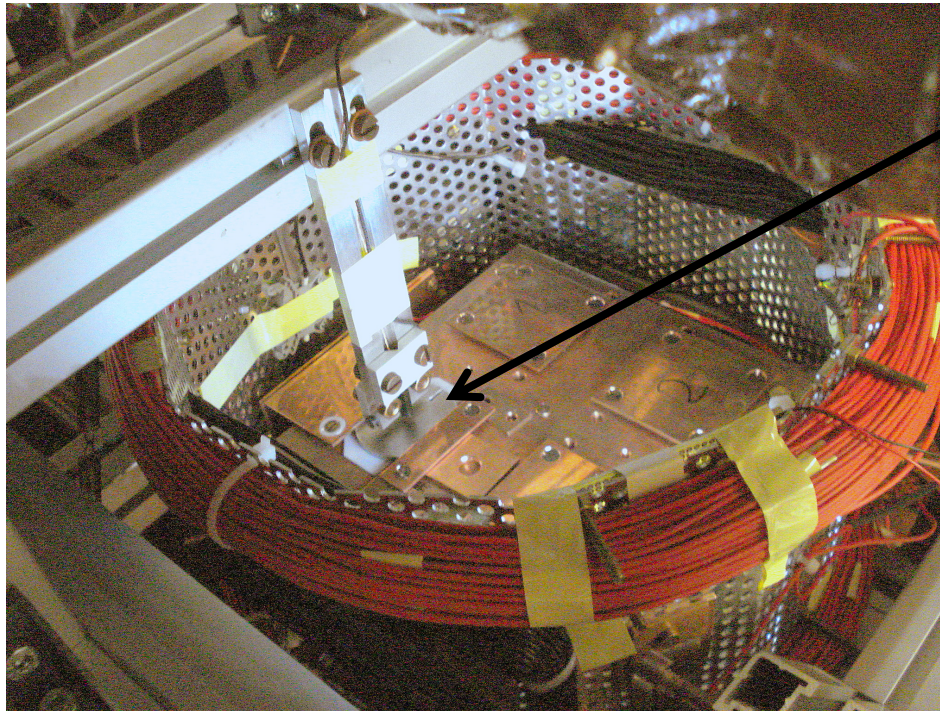
Helmholtz coil applies
magnetic field



Field cooled



HC off,
Measure magnetization



Sample

Courtesy: Sarah Aull

FLUX TRAPPING IN DISK-SHAPED NIOBIUM SAMPLES ($\approx 300\text{RRR}$)

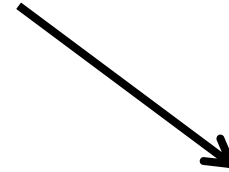
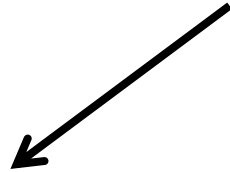
#	Crystal structure	Treatment	Fraction of trapped flux
1	Polycrystalline	None	100%
2	Polycrystalline	BCP	100%
3	Polycrystalline	BCP + 800°C bake out	$(83.1 \pm 0.8)\%$
4	Single crystal	BCP	$[(72.9 + 0.1 \ln v) \pm 0.8]\%$
5	Single crystal	BCP + 800°C bake out	$[(61.6 + 1.3 \ln v) \pm 0.8]\%$
6	Single crystal	BCP + 1200°C bake out	$[(42.1 + 0.13 \ln v) \pm 0.6]\%$

→ Aull, Kugeler and Knobloch, *PRSTAB* 15, 062001 (2012)

depends on cooling rate $v = \Delta T / \Delta t$

Consistant with results that Q's of large grain cavities are greater.
For example W. Singer, MOIOA03: "Large grain cavities on average have 60% higher Q"

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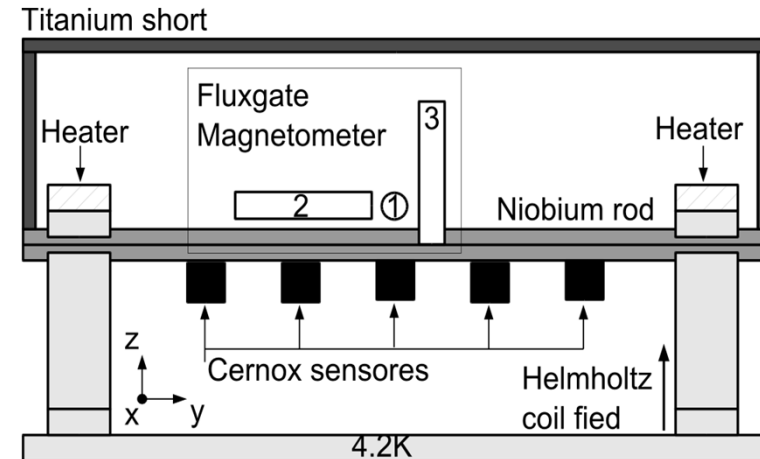
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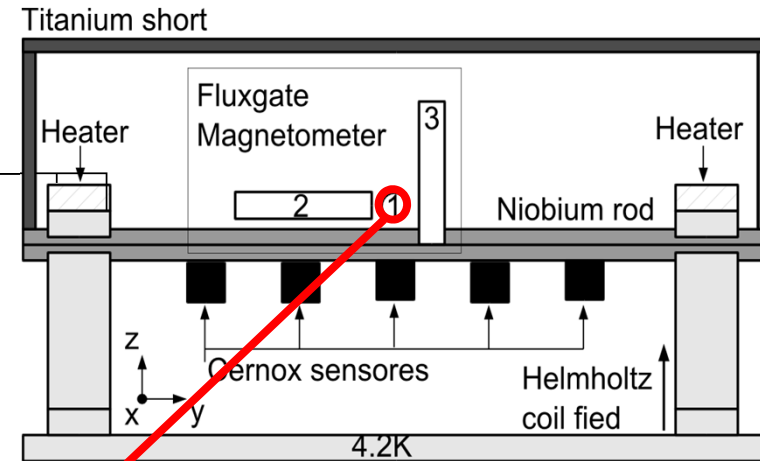
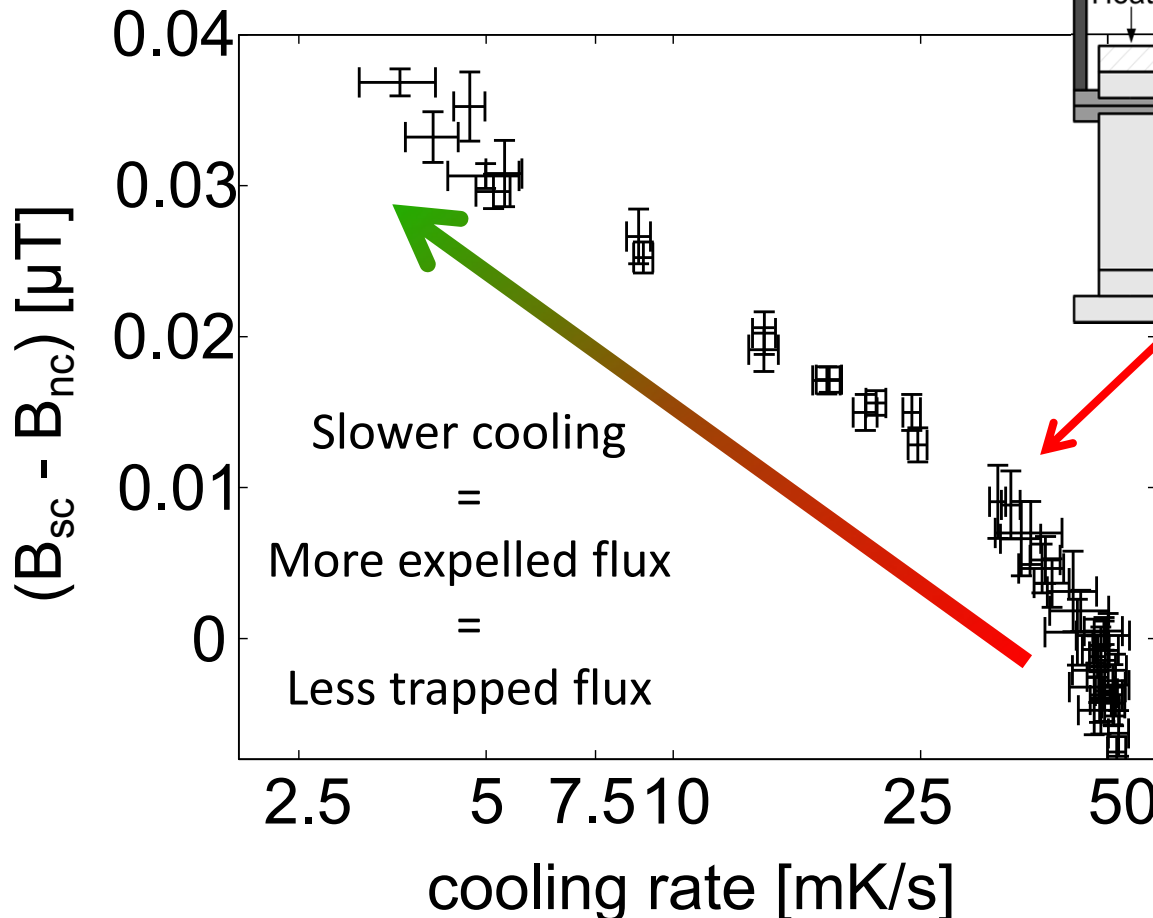
COOLING RATE

- Ambient field increased to $3\mu\text{T}$ ($0.3\mu\text{T}$ in FM1 direction)
- Vary cooling rate during isothermal cooldown ($\max \Delta T < 0.1\text{K}$)
- Slower transition supports Meissner effect
- Logarithmic correlation



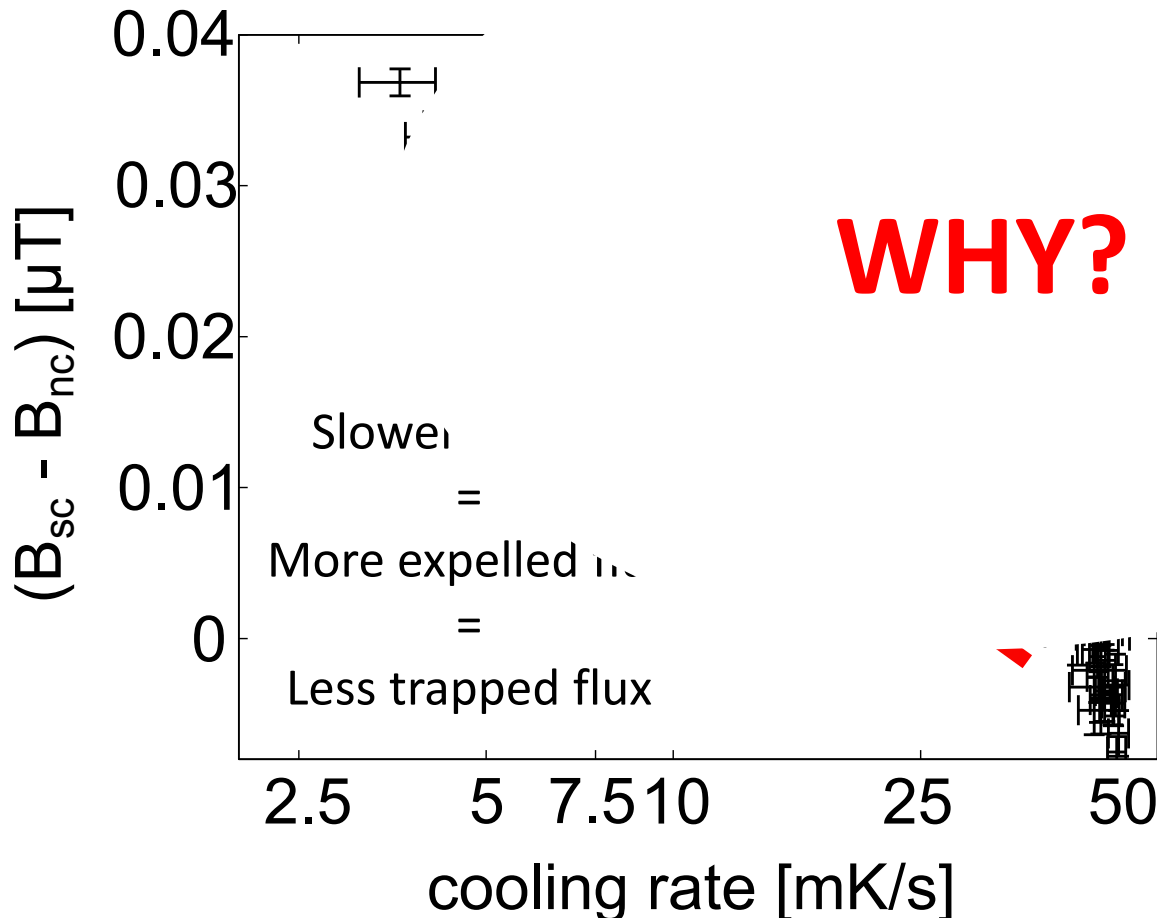
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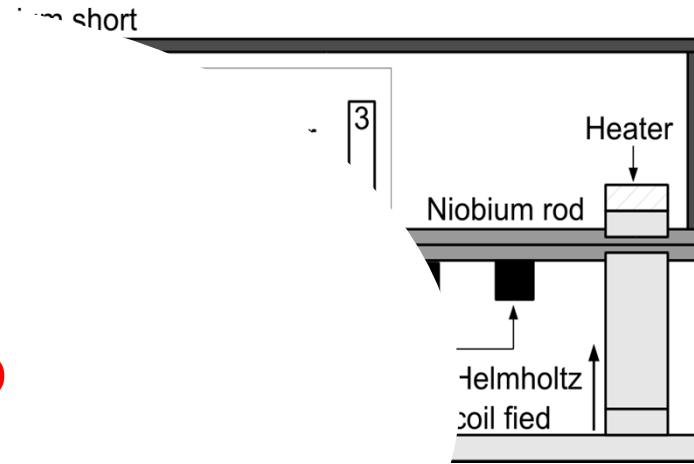


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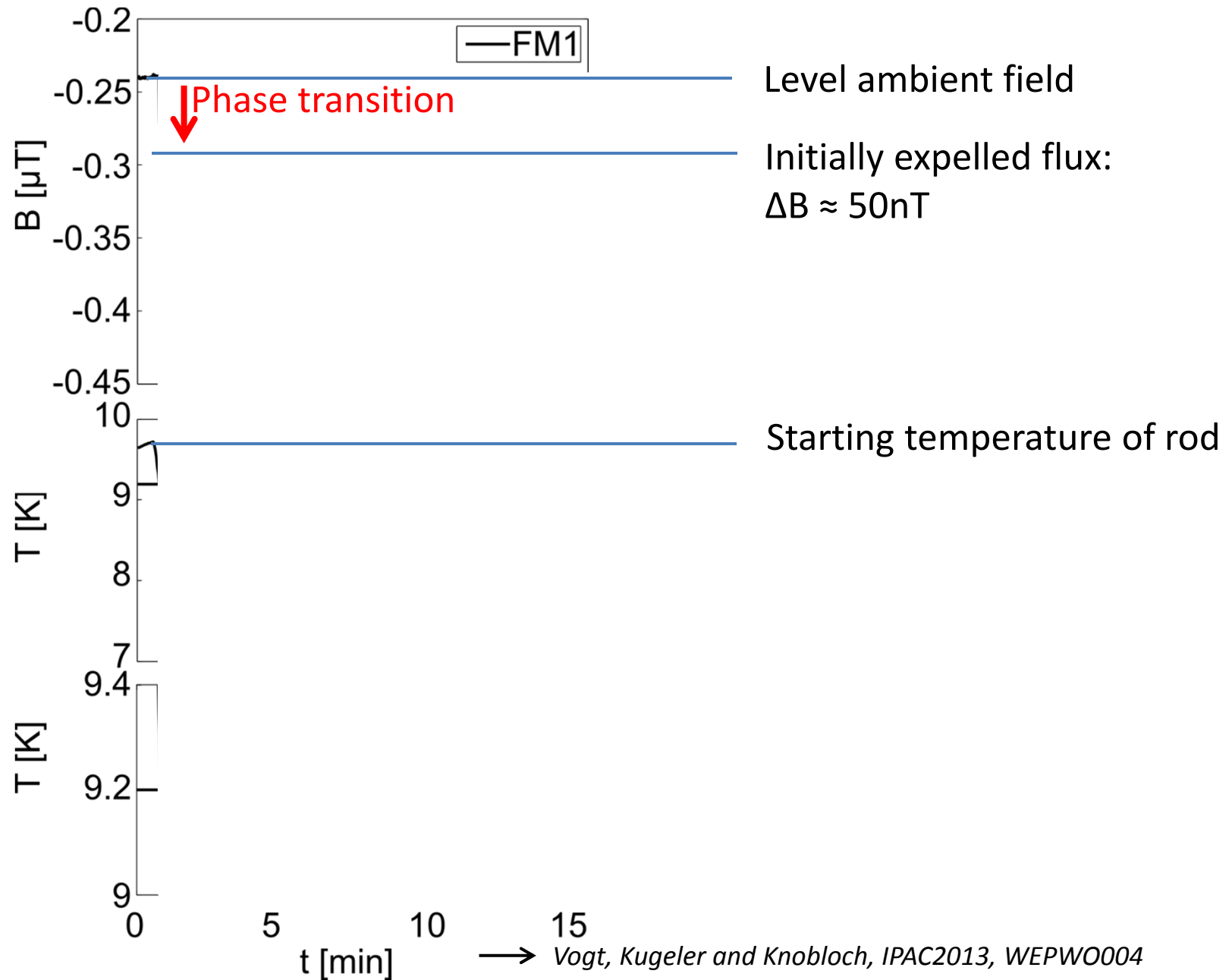
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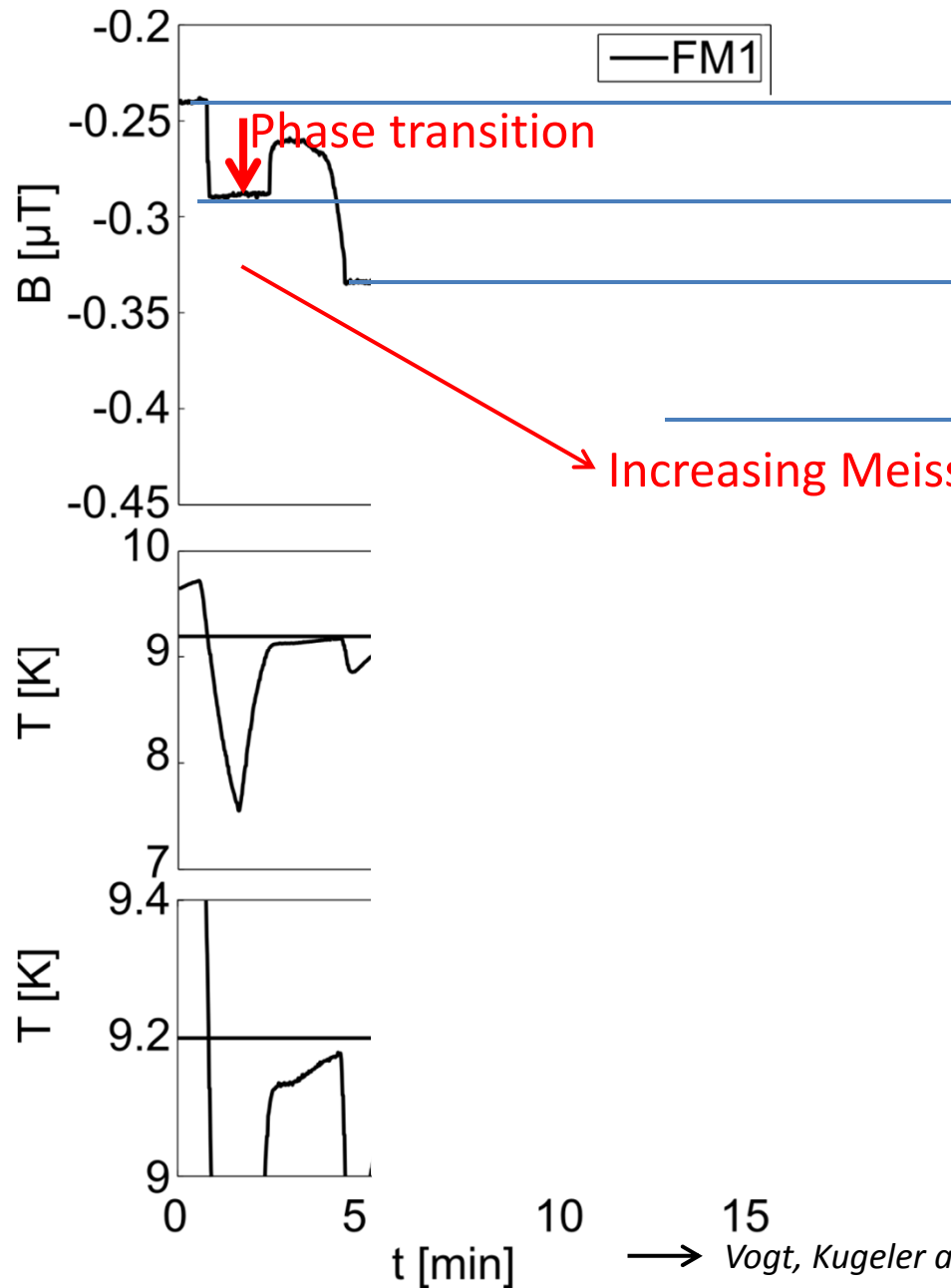
WHY?



INCREASED FLUX MOBILITY CLOSE TO TRANSITION TEMPERATURE



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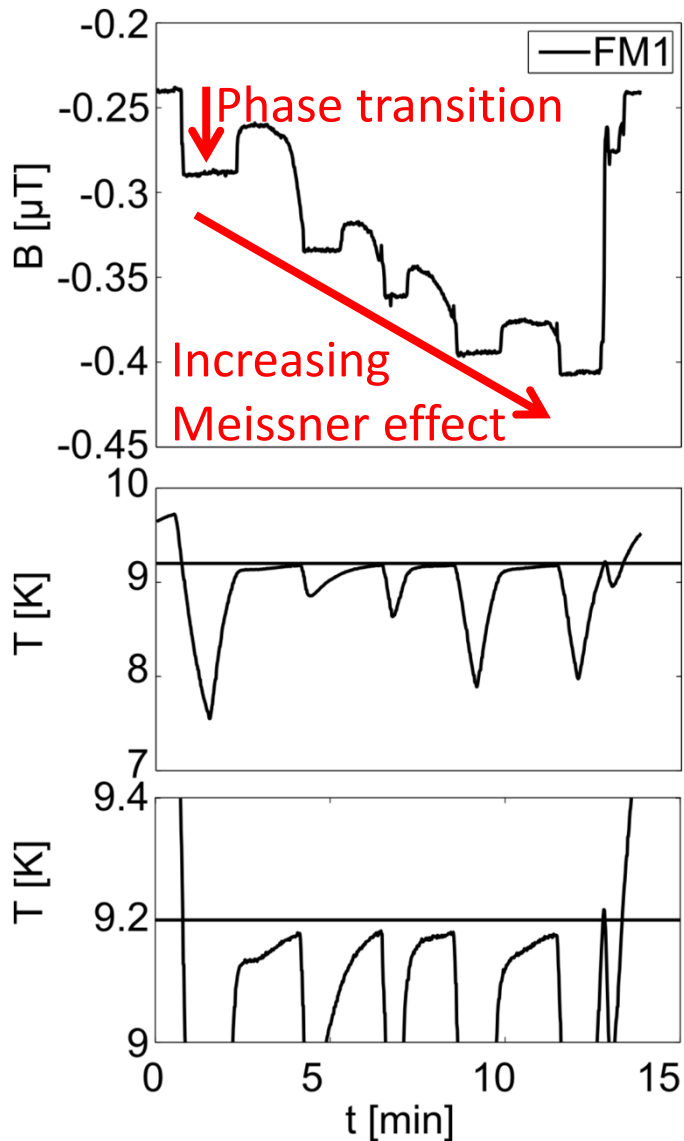
Level ambient field
Initially expelled flux:
 $\Delta B \approx 50\text{nT}$

Increased expelled flux

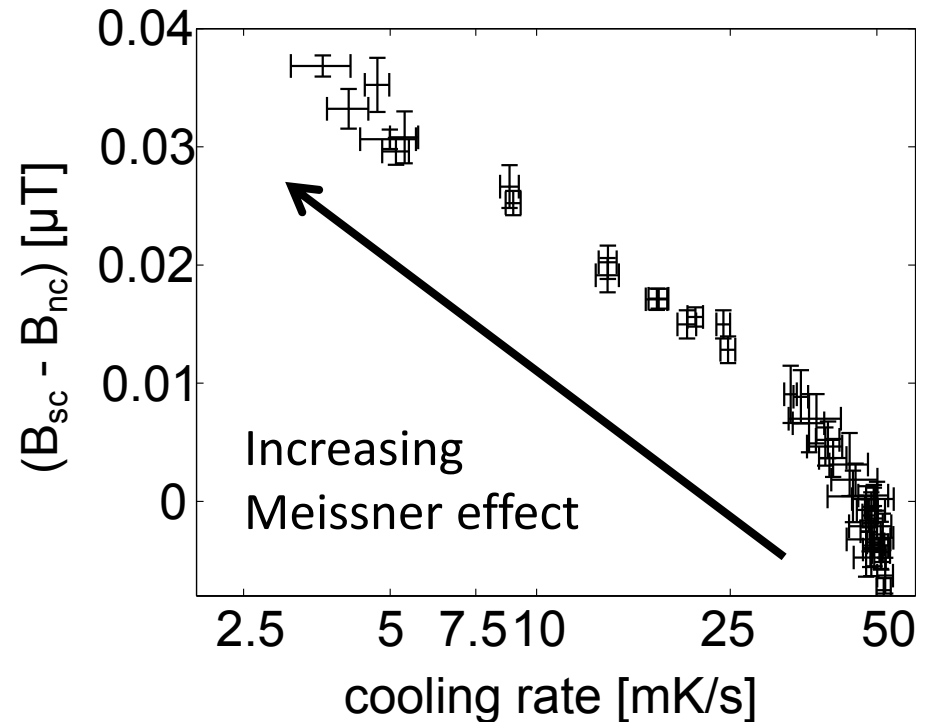
4 × more flux expelled
→ **Increasing Meissner effect**

Increased flux mobility close to transition temperature

INCREASED FLUX MOBILITY CLOSE TO TRANSITION TEMPERATURE



Slower coolingrate = niobium longer in region with increased flux mobility



***Sarah Aull et al., SRF2013, WEIOC01
RF measurements demonstrate that R_s
is impacted by the cooling rate***

SUMMARY

Do temperature gradients generate trapped flux?	Thermoelectrically induced magnetic fields exist and get trapped in sc niobium.	Avoid temperature gradients as you transition to the SC state!
Can we reduce pinning centers? Impact niobium material properties the trapping behavior?	Material defects and contaminants affect trapped flux	Use large grain material and/or high temperature treatment!
Are there additional ways to optimize Meissner effect?	Flux shows increased mobility close to transition temperature	Decrease cooling rate near T_c to take advantage of increased flux mobility!



- Cavity cooldown without ΔT (time to settle before transition or add cycling)
- Cool slowly and smoothly through T_c

THANK YOU FOR YOUR ATTENTION

Acknowledgement:

Hans-Peter Vogel and Peter vom Stein (RI), Peter Kneisel and Rong-Li Geng (J Lab), Enzo Palmieri (INFN-Legnaro) for providing the samples.

To our engineers André Frahm, Michael Schuster, Sascha Klauke, Dirk Pflückhahn, Stefan Rotterdam, Axel Hellwig for patient support and

MODEL SYSTEM VS. DRESSED CAVITY: TEST 2

Is this measurement able to explain the observed variation in R_{res} ?

$$B \leftrightarrow I = \Delta V / R = \Delta S \cdot \Delta T / R$$

Thermopower $\Delta S \approx 10 \mu\text{V/K}$
Literature is not consistent

Parameter of cavity-tank system @10K:
 $R \approx 100 \mu\Omega$ (dominated by titanium tank)

→ J. Milck, Tech. Rep., Hughes Aircraft Company (1970)

