



C-BAND HIGH POWER AMPLIFIER KLYSTRON DEVELOPED FOR LINEAR ELECTRON ACCELERATORS

Yury Paramonov

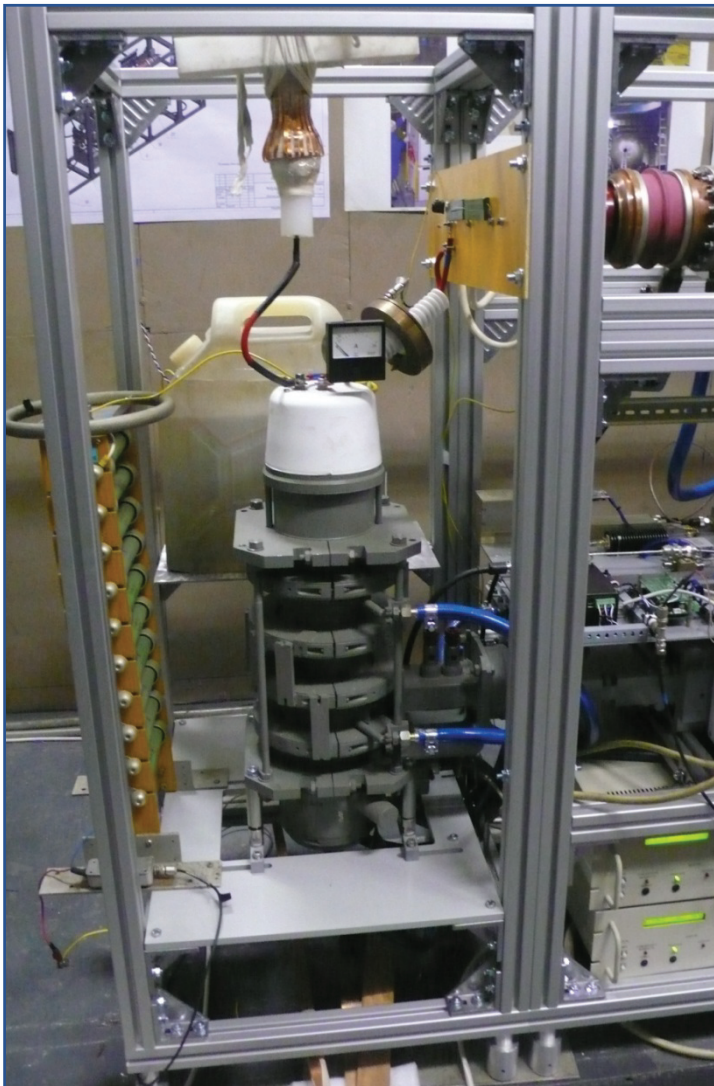


MICROWAVE TUBES FOR LINEAR ACCELERATORS

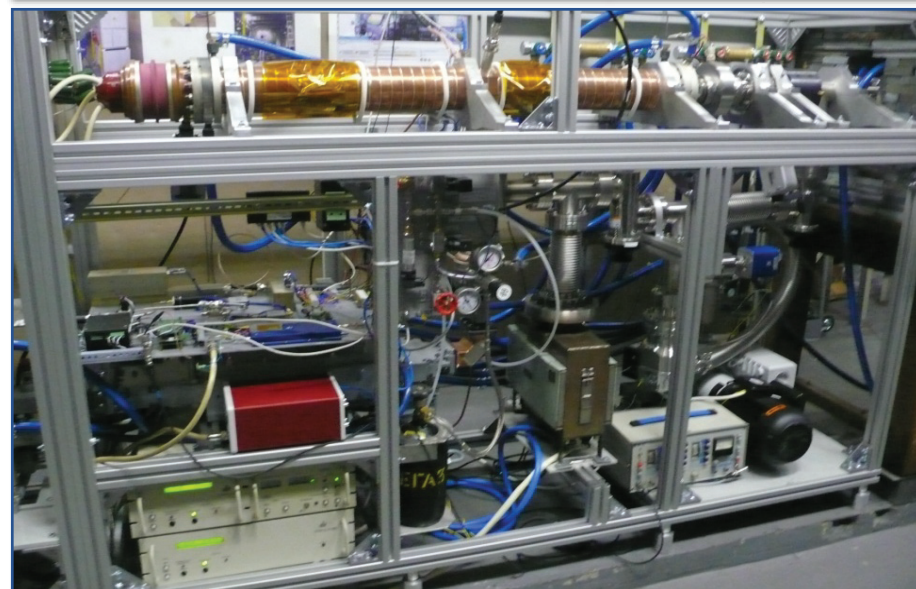
	Magnetron	CW klystron	Pulsed klystrons				
	MI-470	KU-399	KIU-40	KIU-111	KIU-147	KIU-147A	KIU-168
Center frequency, MHz	1885	2450	991	2450	2450	2856	2856
Output pulse power, MW	10	-	4.7	5	5	6	6
Output average/CW power, kW	30	25	70	5	25	25	5
Cathode voltage, kV	50	10	65	50	50	52	52
Number of electron beams	1	18	6	40			
Focusing	solenoid	permanent magnets	solenoid	permanent magnets			



LINEAR ACCELERATOR UELR-10-15 FOR STERILIZATION



Beam Energy, MeV	5 – 10
Electron Beam Average Power, kW	1 – 15
Pulse Repetition Rate, Hz	up to 400
Scan Length, mm	400 – 600
Scan Frequency, Hz	1 – 30
Microwave Tube	Klystron KIU-147A
Modulator	Solid State





C-BAND HIGH POWER AMPLIFIER KLYSTRON

Main parameters

Frequency –	5712 MHz
Cathode voltage –	45 kV
Pulse cathode current –	150 A
Output pulse power –	3 MW
Quality factor –	300 - 1000;
Focusing –	permanent magnets





Analogs

Type	efficiency, %	Mode
VKL-8271	50.0	140 kV, 125A, 2.5 MW (2.4)
VKL-8301	50.0	130 kV, 160 A, 10.0 MW (3.5)
VKS-8262D	40.0	130 кV, 105 A, 5.5 MW (2.2)
VKC-8313 (5712 MHz)	35.0	120 кV, 79 A, 3 MW (1.9)
TH-1801 (L, MBK, 6 beam) 2016	40.0 (60.0)	120 кV, 132 A 10 MW (3.2)



MAX efficiency (60 – 70%)

MAGIC2-D Simulations of High Efficiency Klystrons using the Core Oscillation Method

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Lancaster, United Kingdom
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Igor Syratcev
CERN
Geneva, Switzerland

Andrey Yu. Baikov
Moscow University of Finance & Law
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Richard Kowalczyk
SLAC National Accelerator Laboratory
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20MWp High-Efficiency L Band Multi-Beam Klystron for CLIC Drive Beam

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Thales Electron Devices, 2 rue M.Dassault, F-78414 Vélizy-Villacoublay, France

rodolphe.marchesin@thalesgroup.com

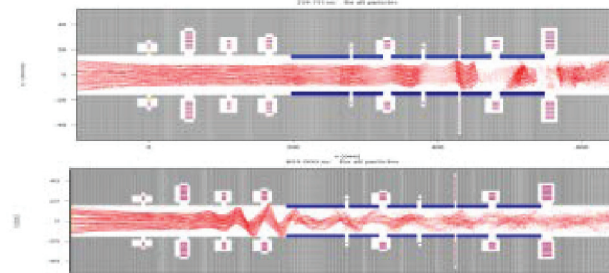


Fig. 5 - Simulation of beam breakup due to 6.7 GHz mode (top) and 4.2 GHz mode (bottom).

Comparison of 6 MW S-band pulsed BAC MBK with the existing SBKs

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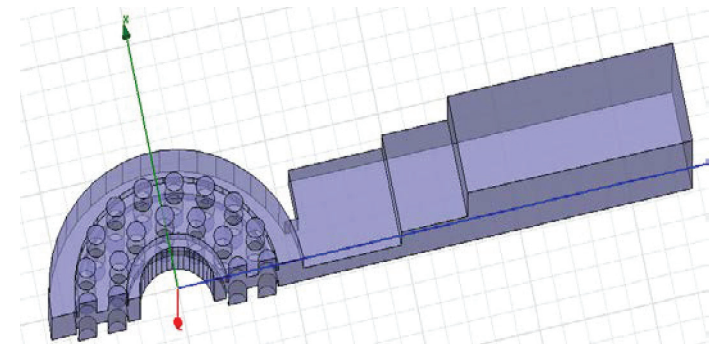
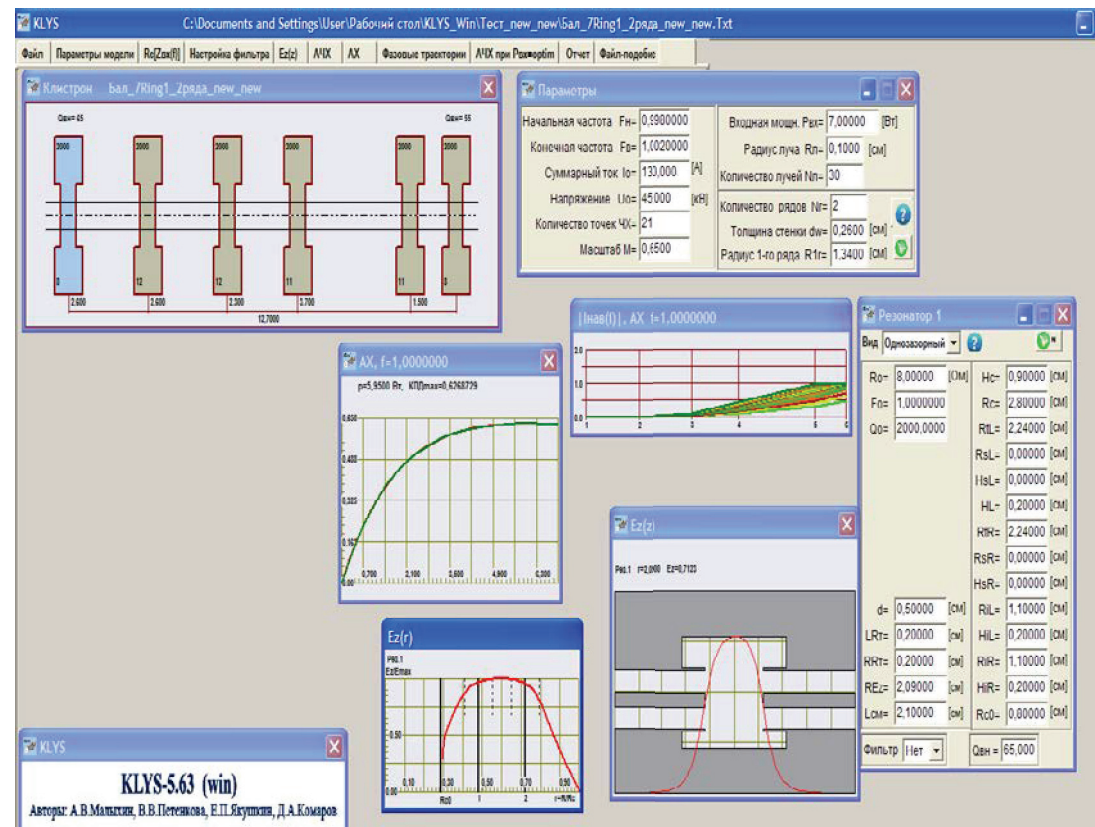
⁴JINR, Moscow region, Dubna, Joliot-Curie, 6, Russian Federation

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Test of a BAC Klystron

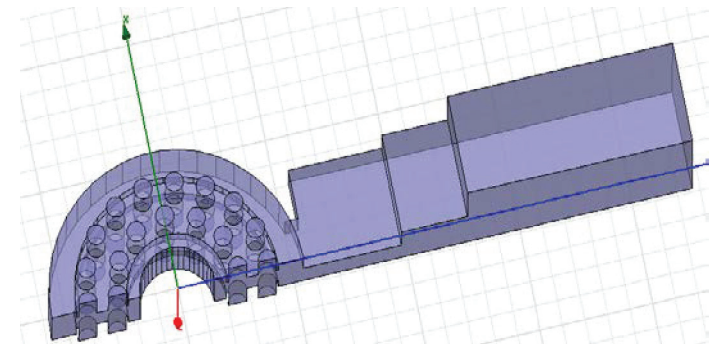
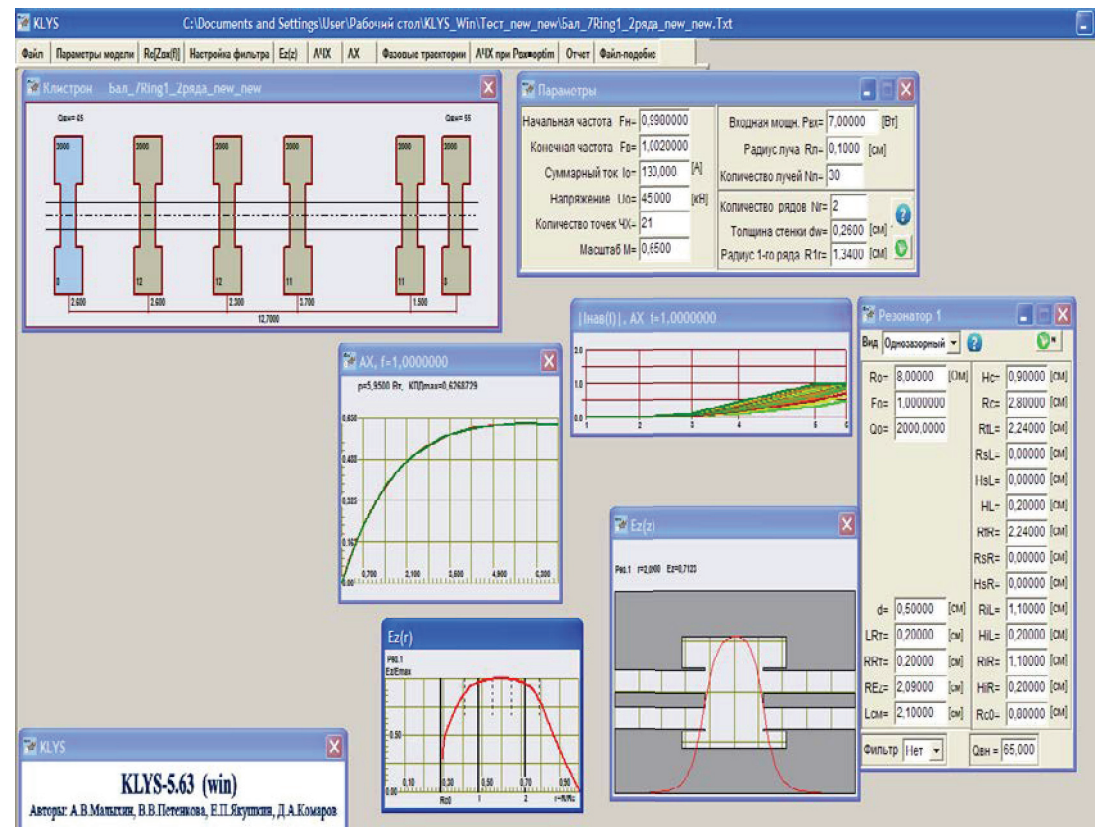
R. Kowalczyk, A. Haase, E. Jongewaard, M. Kemp
and J. Neilson
SLAC National Accelerator Laboratory
Menlo Park, CA

A. Jensen
Leidos
Billerica, MA





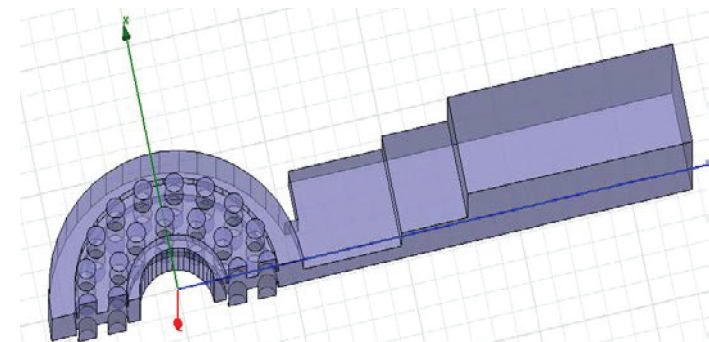
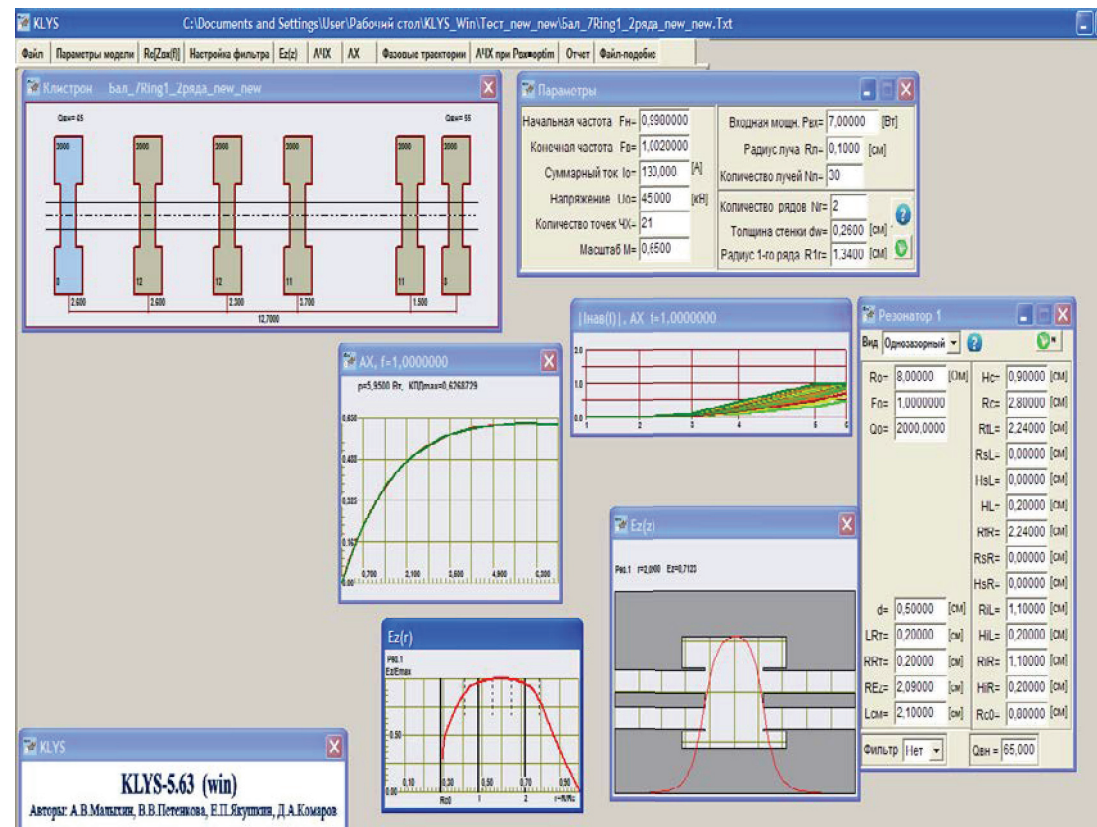
Design





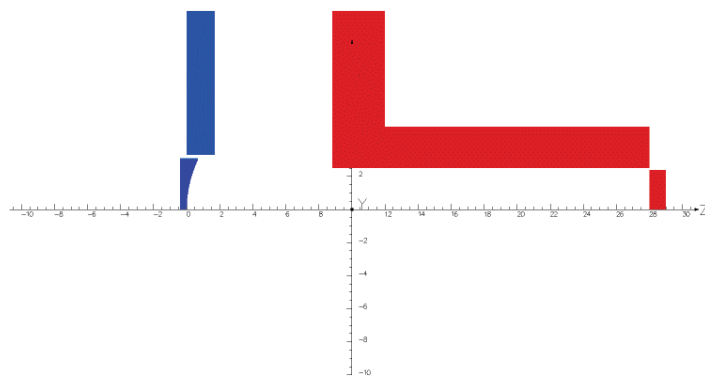
Design

Modeling output/input cavity

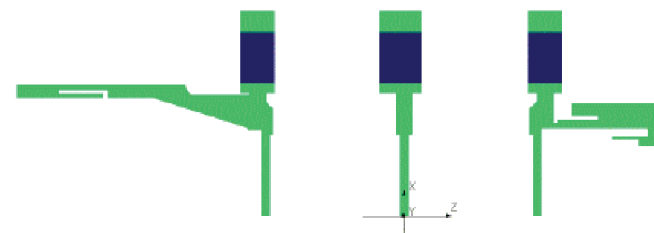




Electron gun



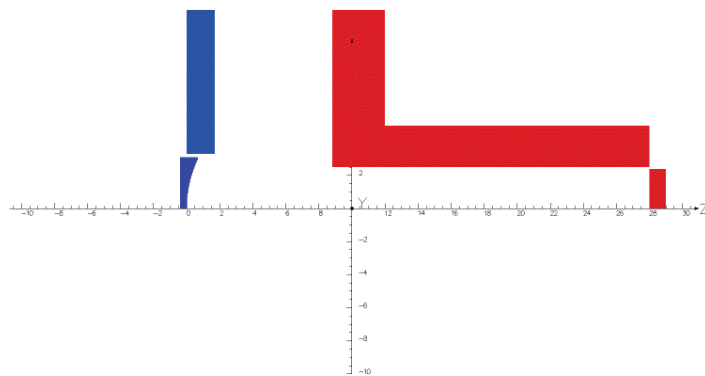
Focusing system



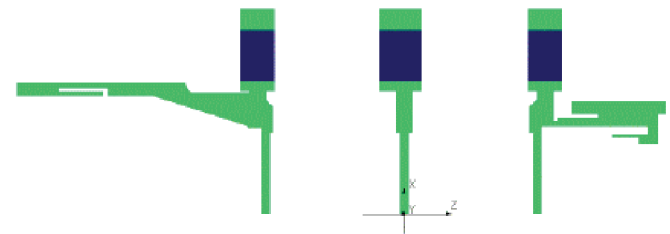


Calculation electron gun

Electron gun



Focusing system

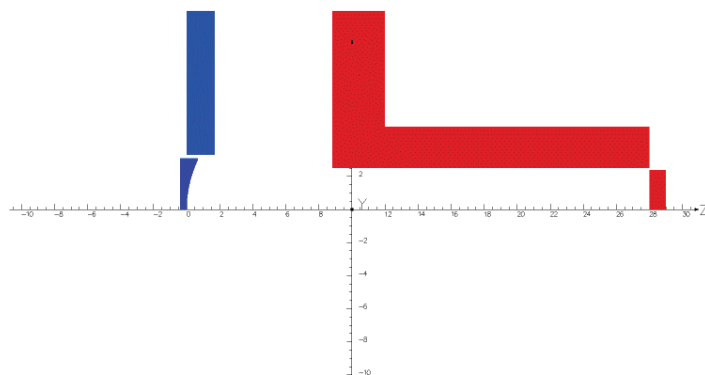




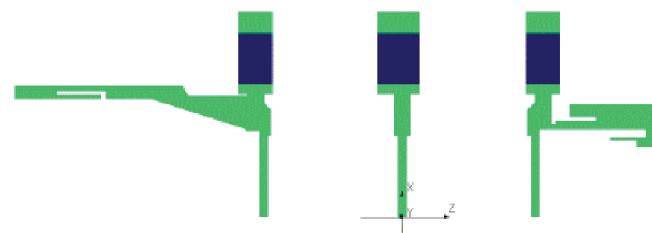
Calculation electron gun

Calculation focusing system

Electron gun



Focusing system



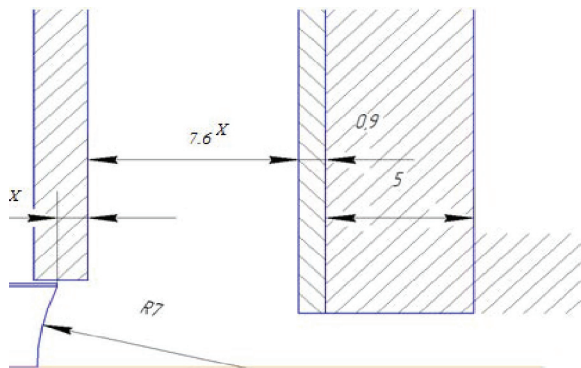


Calculation electron gun

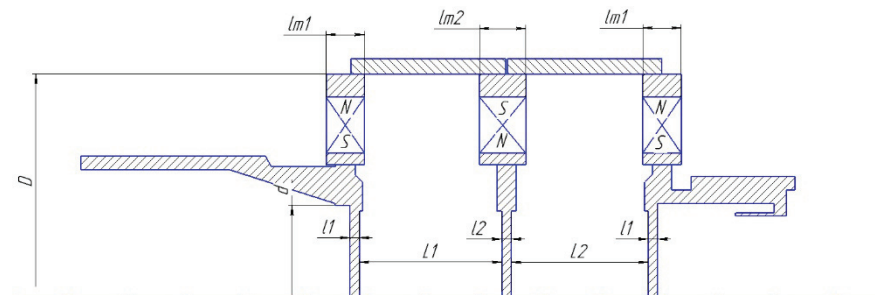
Preliminary design

Calculation focusing system

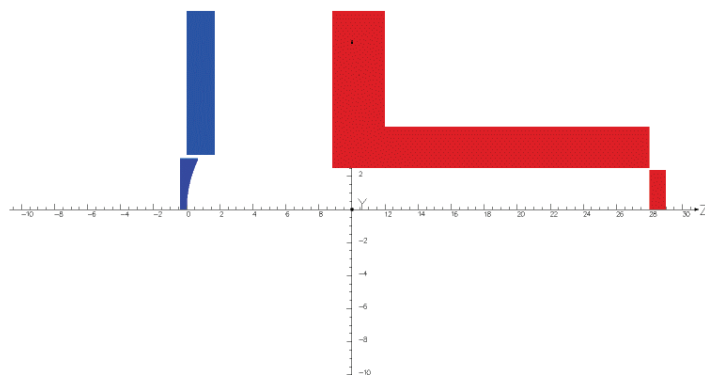
Electron gun



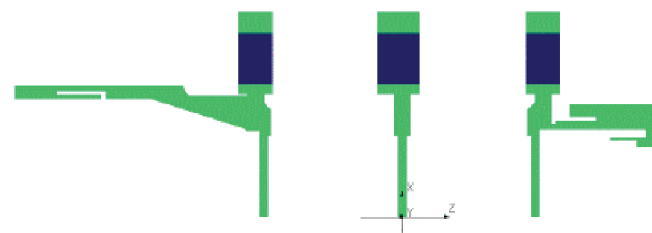
Magnetic system



Electron gun



Focusing system



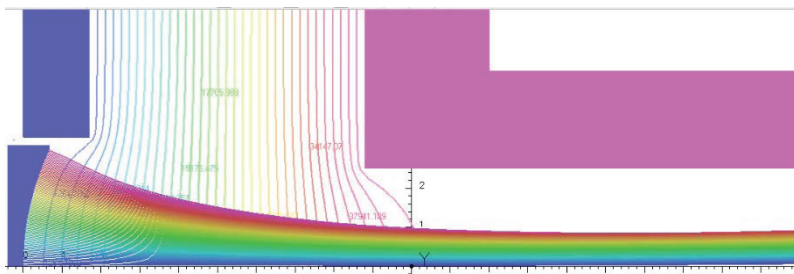


Calculation electron gun

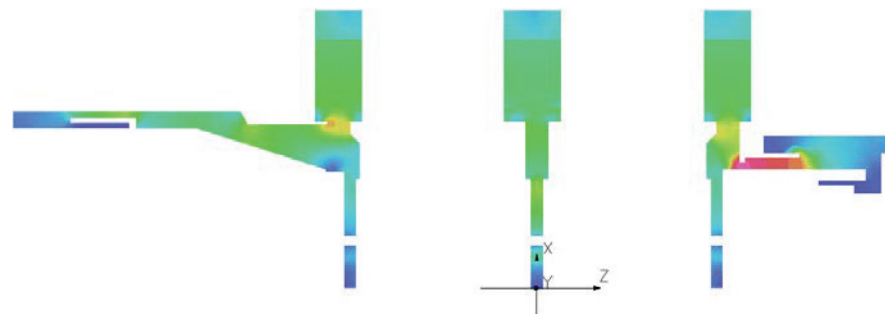
2D design

Calculation focusing system

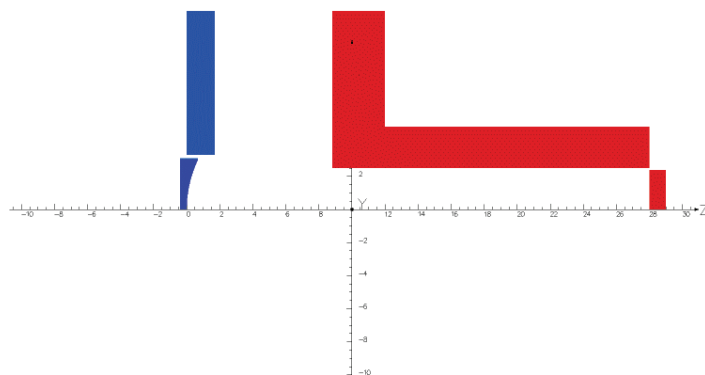
Electron gun



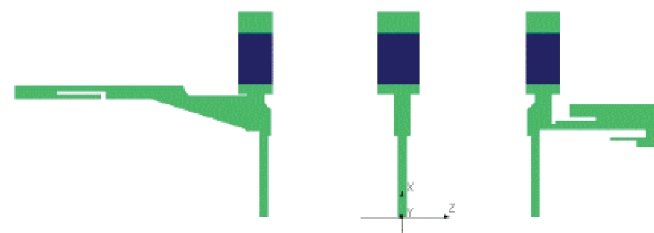
Focusing system



Electron gun



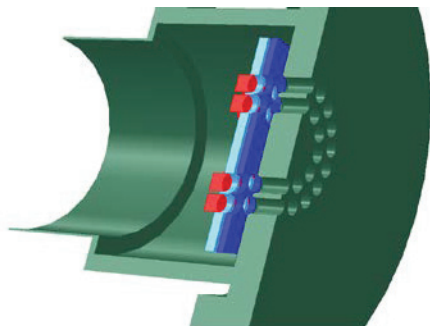
Focusing system



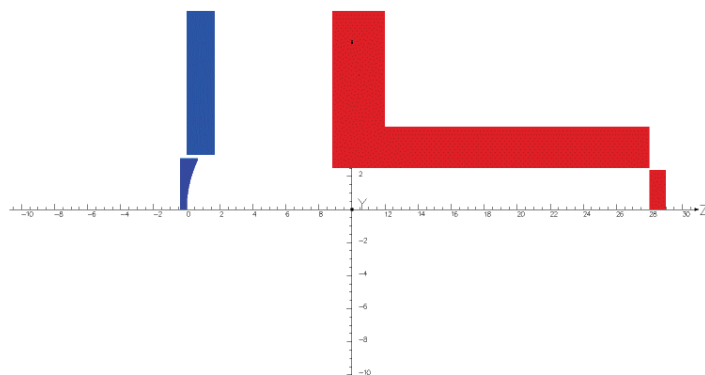


Calculation electron gun

Electron gun



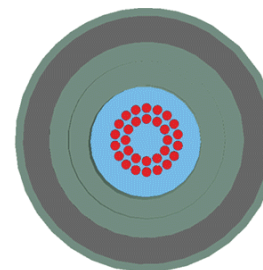
Electron gun



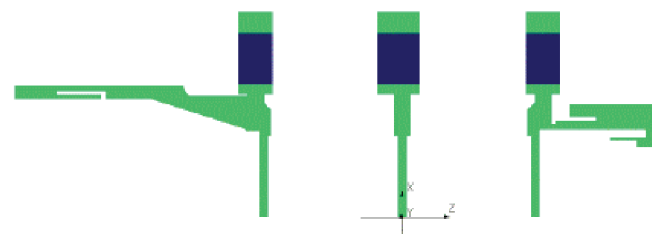
3D design

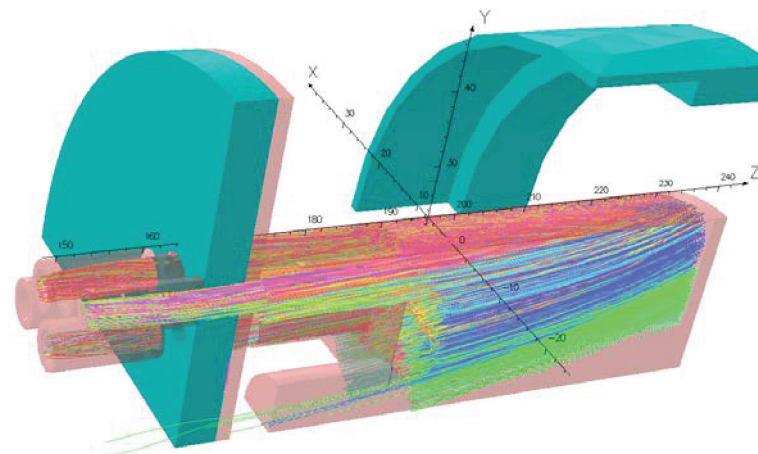
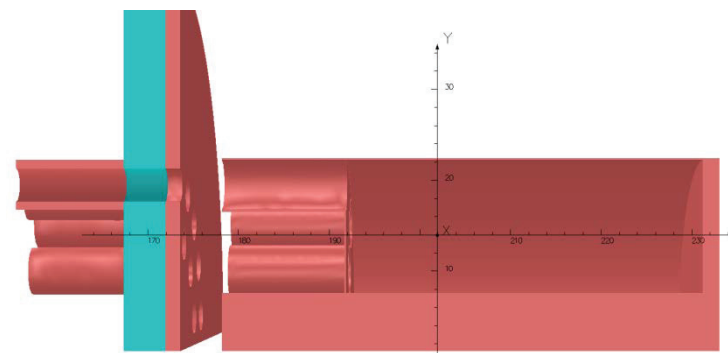
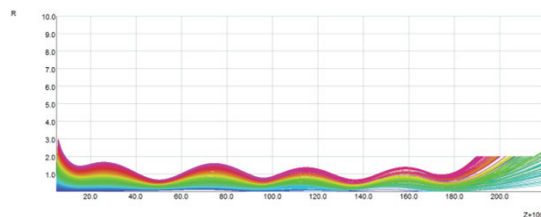
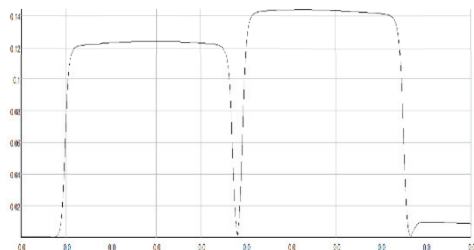
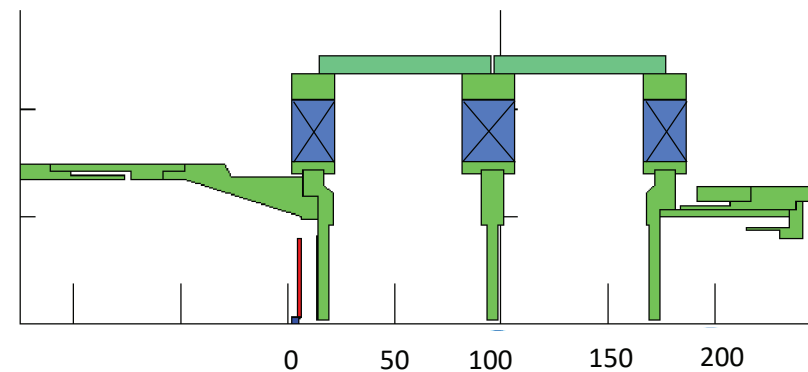
Calculation focusing system

Multi-beam focusing system



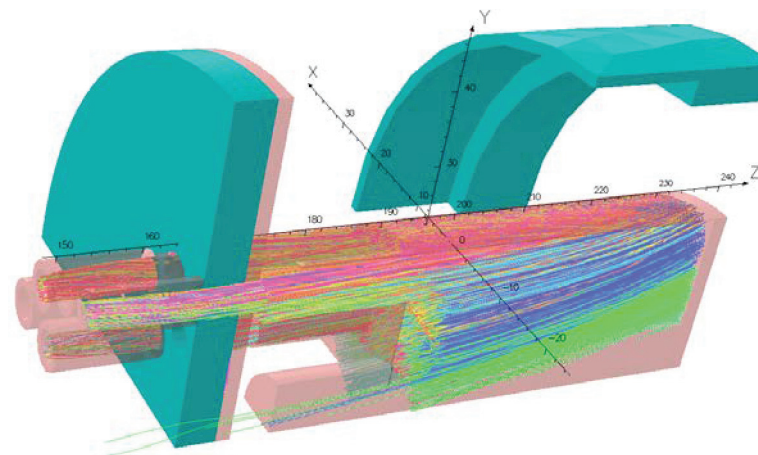
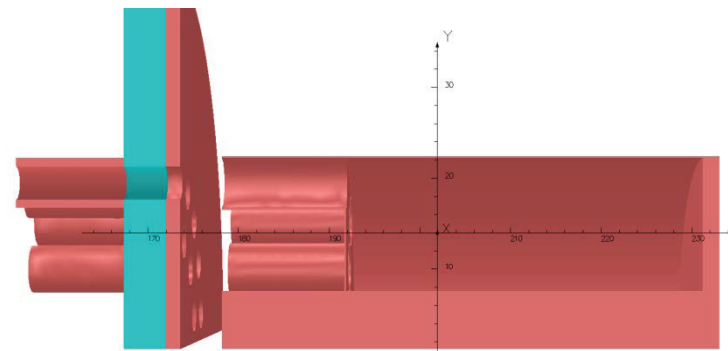
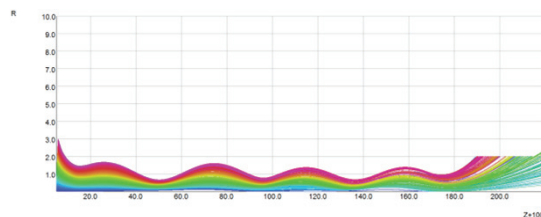
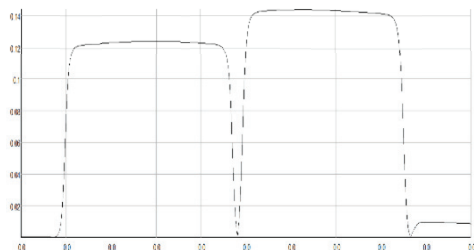
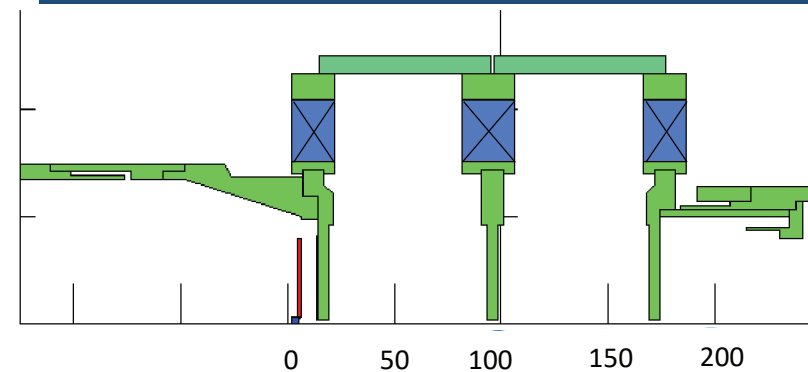
Focusing system





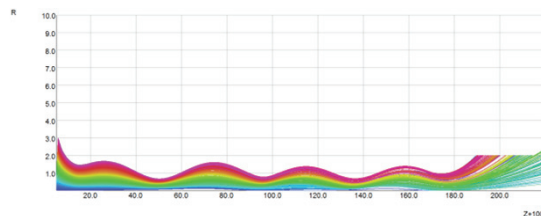
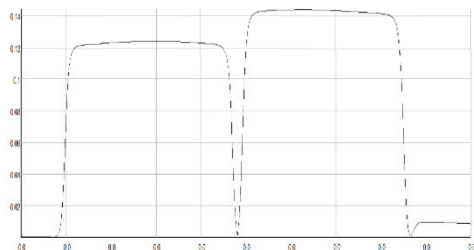
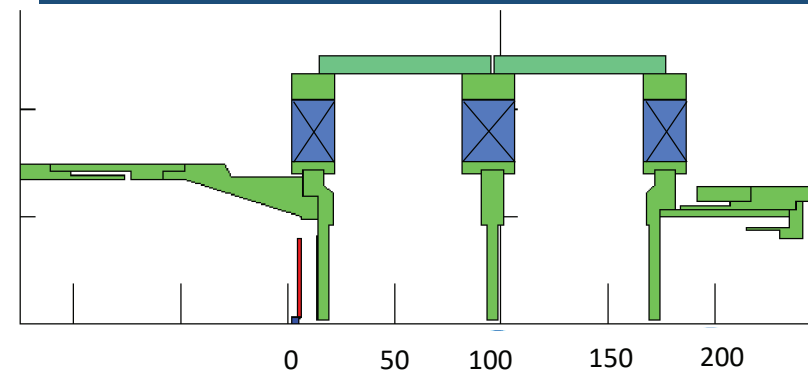


Electron beam path analysis

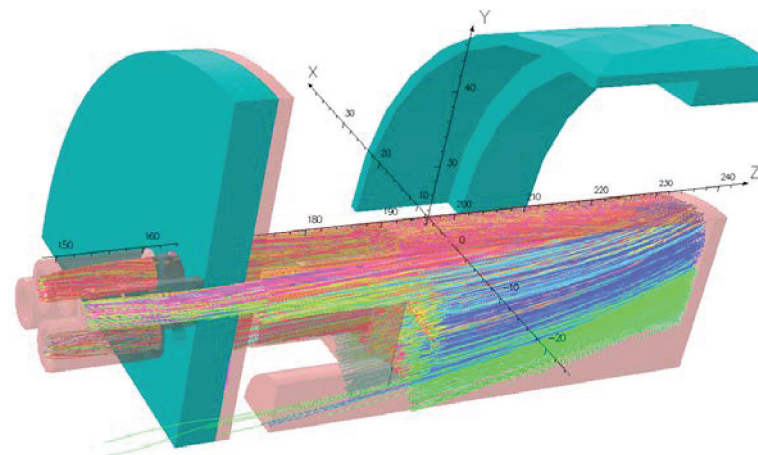
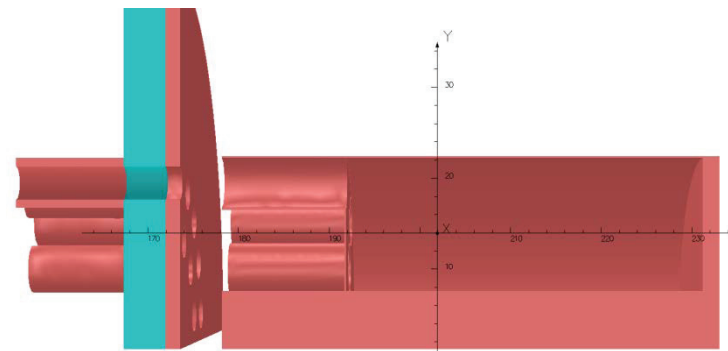




Electron beam path analysis

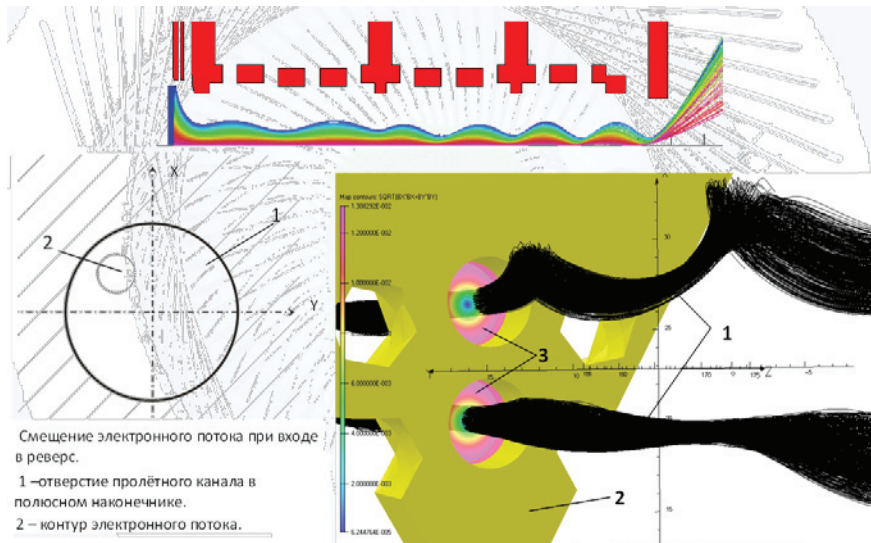


Collector calculation

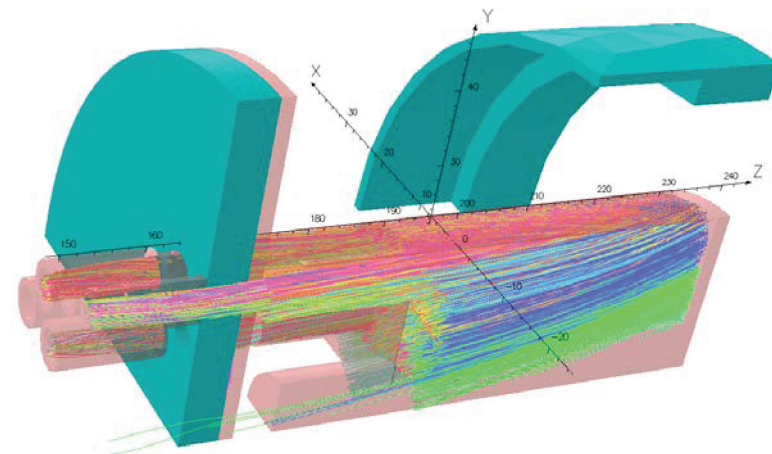
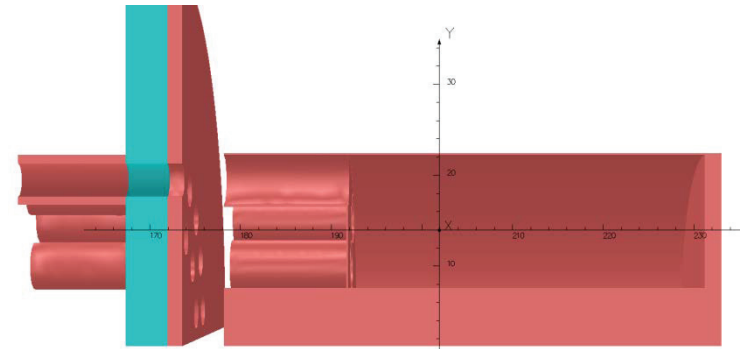


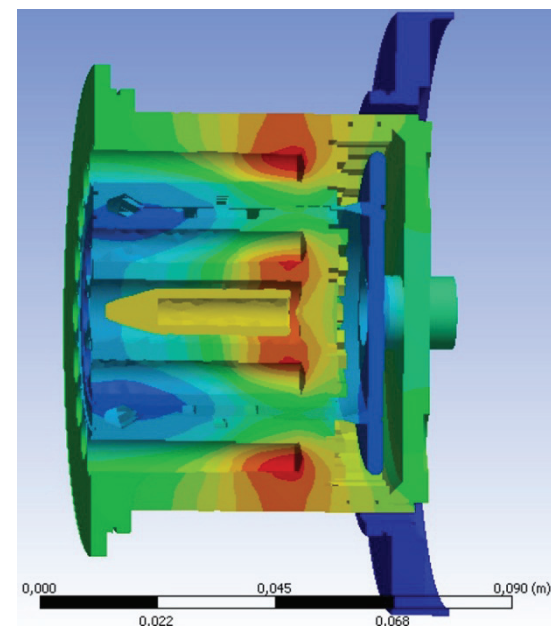
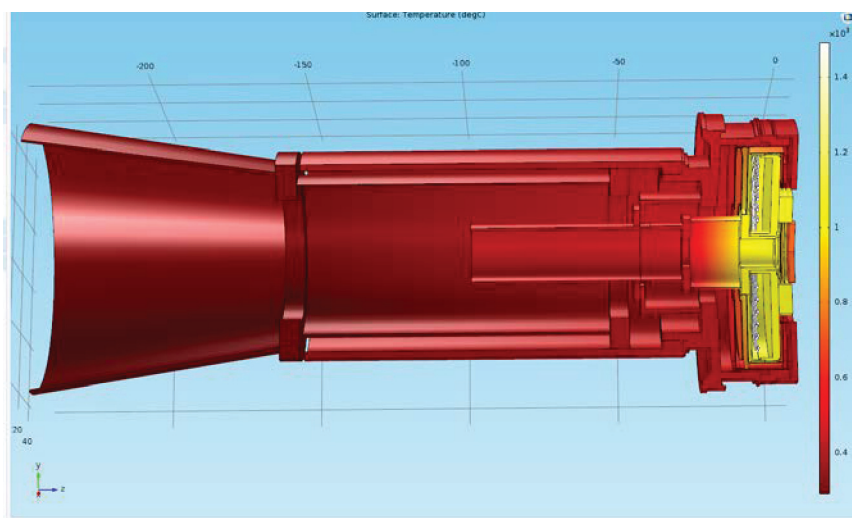
Electron beam path analysis

3D calculate multi-beam system



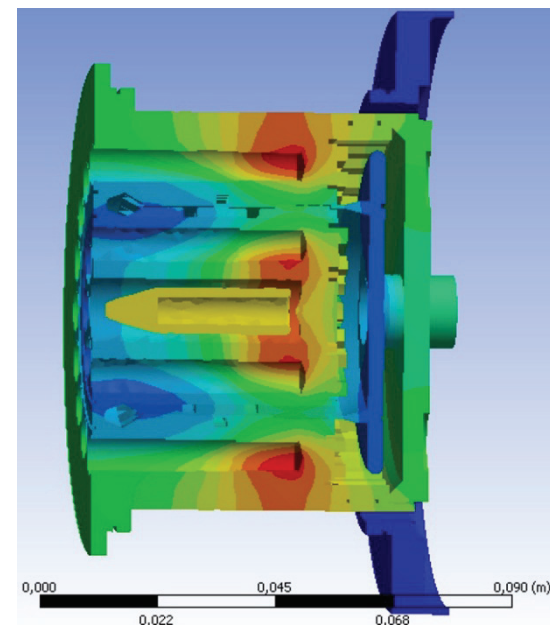
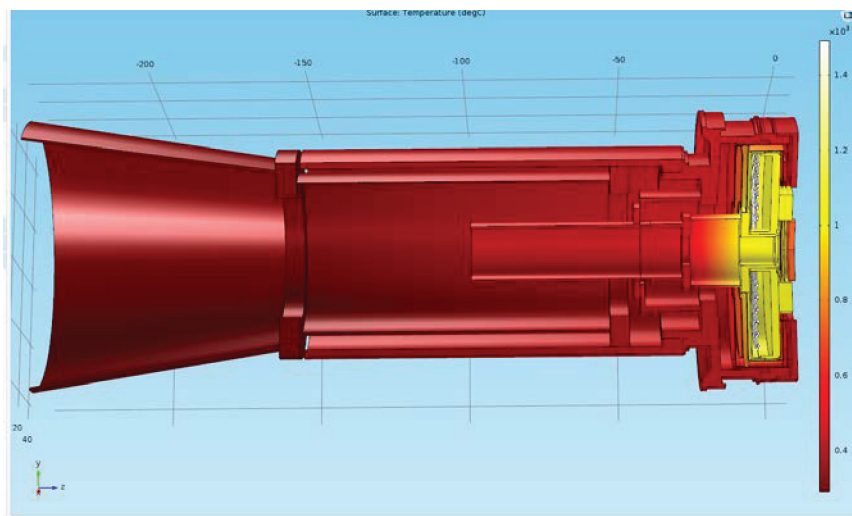
Collector calculation





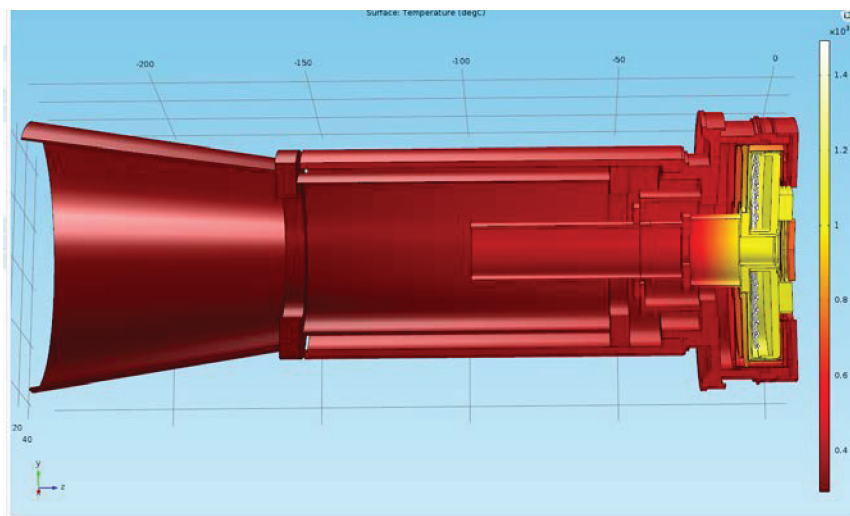


Calculation of thermal deformations in electron gun

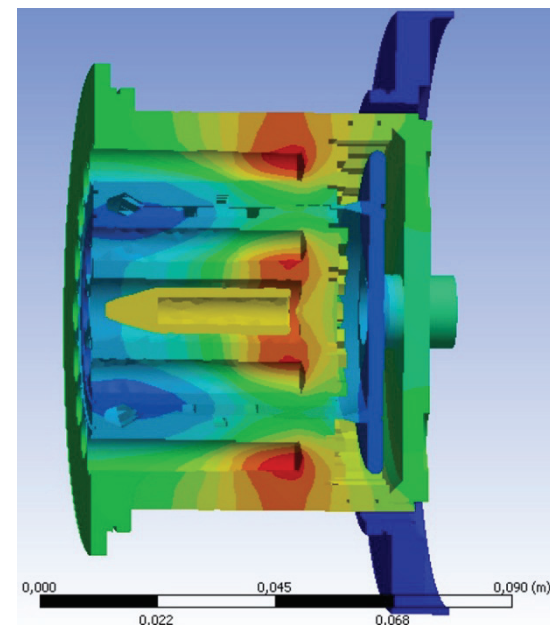




Calculation of thermal deformations in electron gun

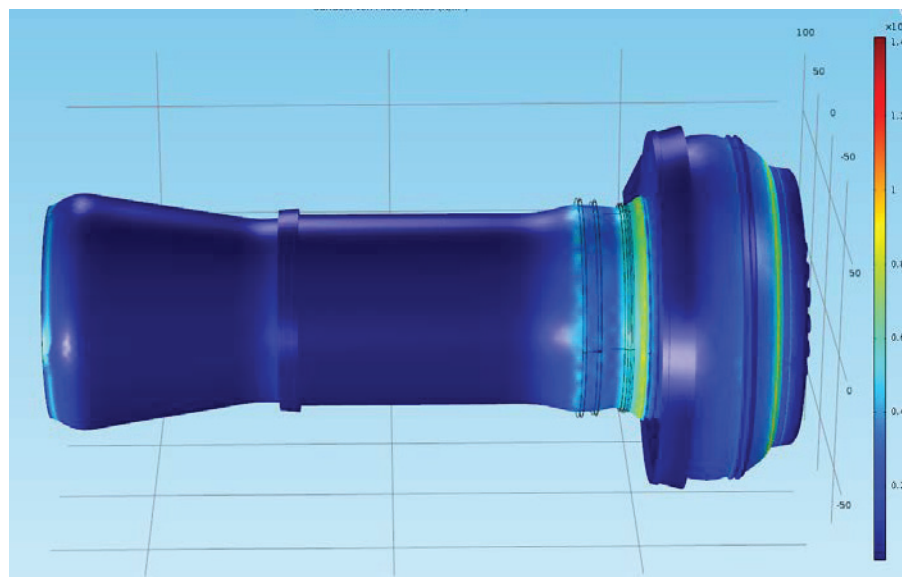


Calculation of thermal deformations in collector

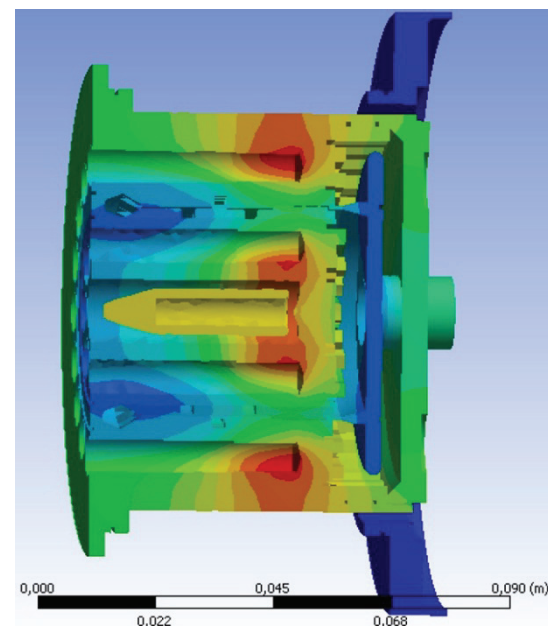




Calculation of thermal deformations in electron gun

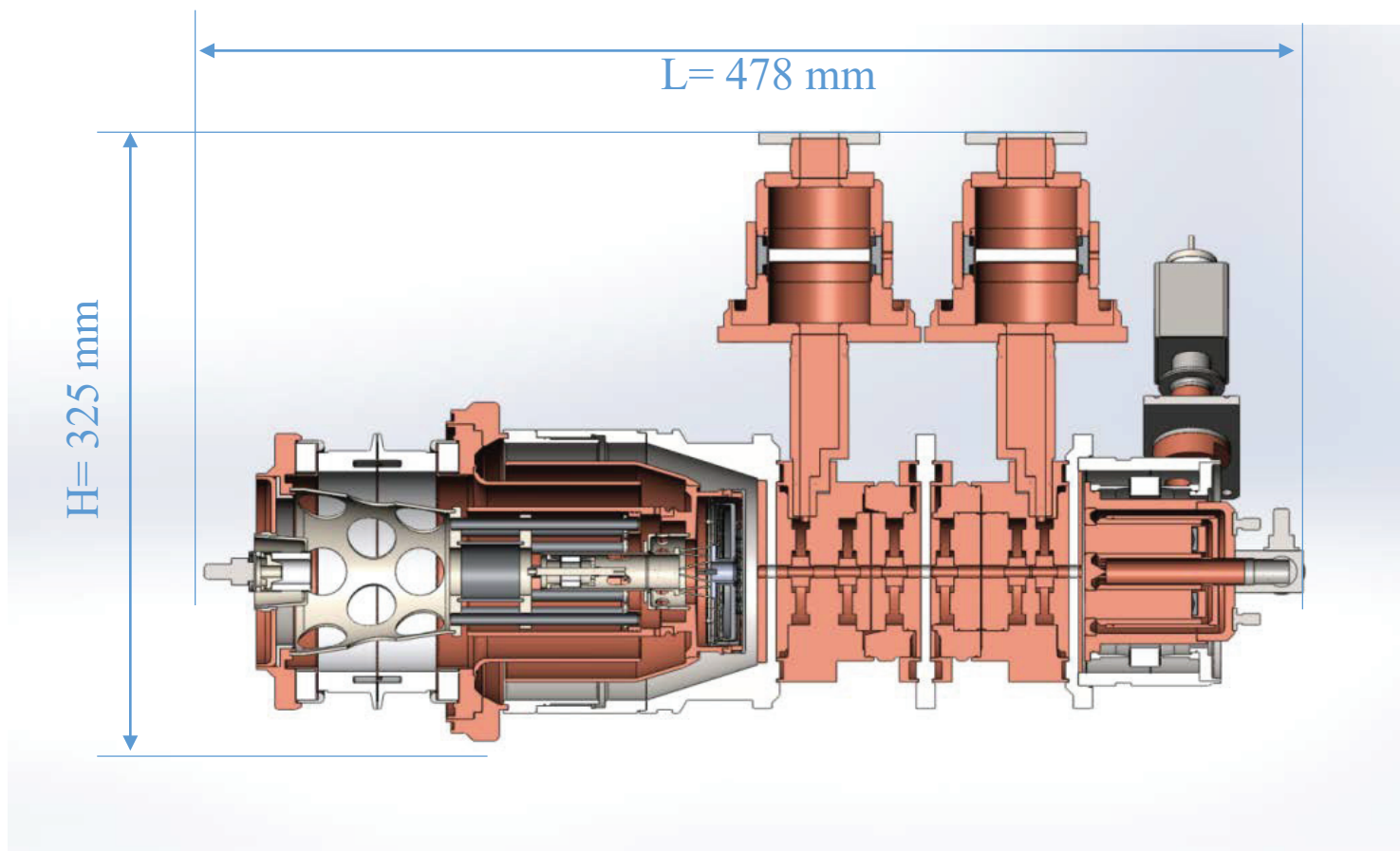


Calculation of thermal deformations in collector



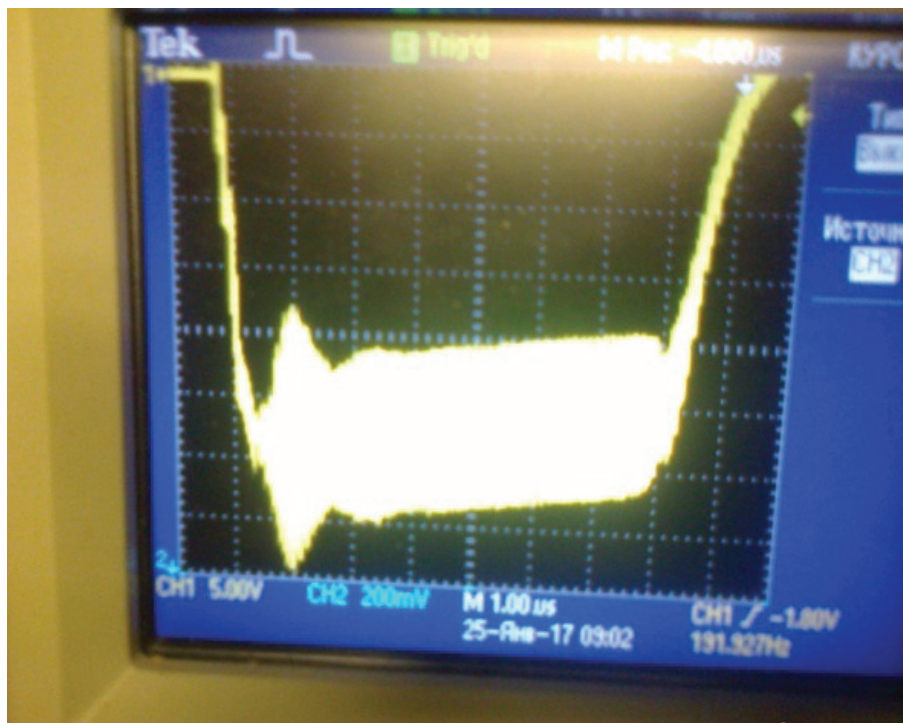


Solid model





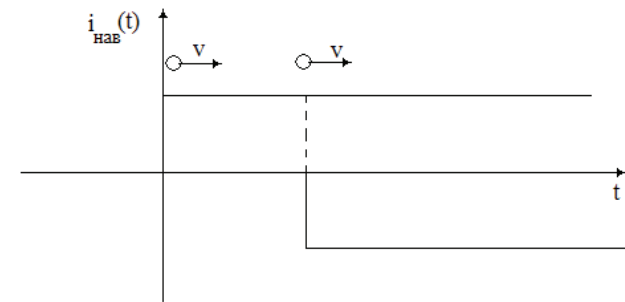
First test





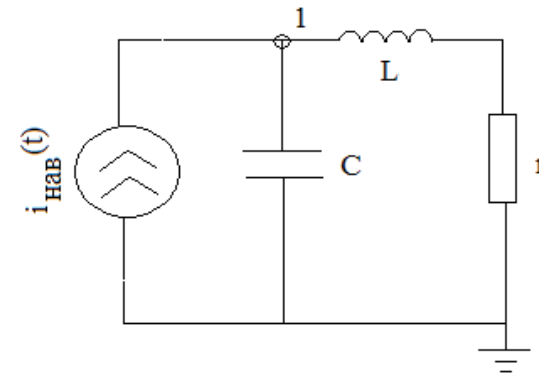
Analytical model

$$i_{ind}(t) = \frac{q \cdot v}{d} \cdot (\eta(t) - \eta(t - \tau))$$



induced current

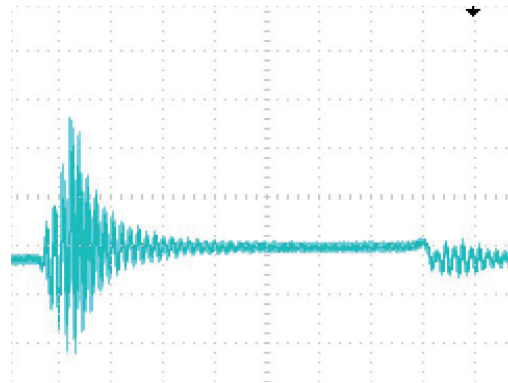
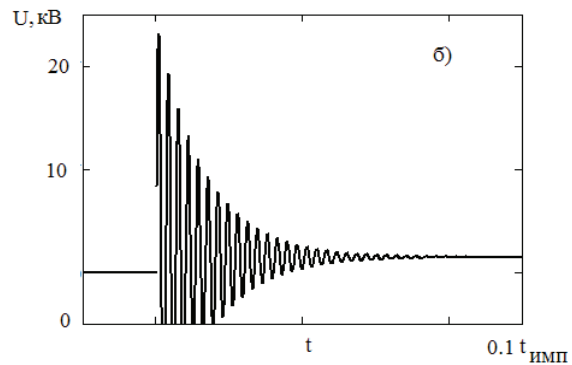
$$\varphi_1(s) \cdot \left(s \cdot C + \frac{1}{r + s \cdot L} \right) = I(s)$$



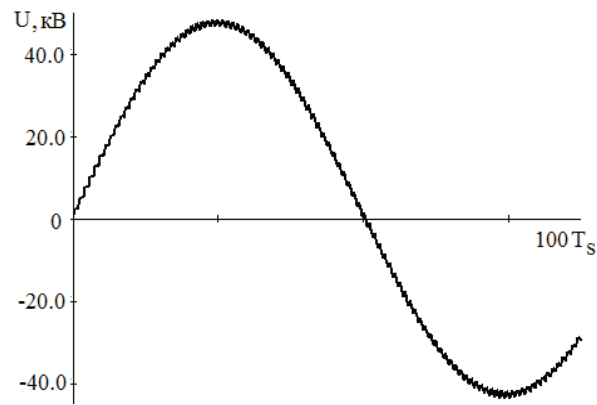
equivalent circuit



Results



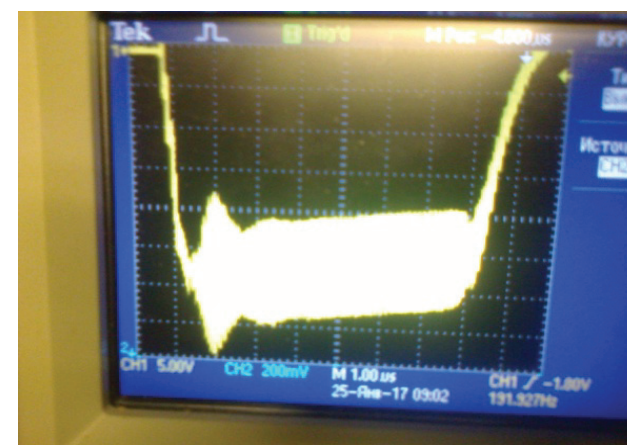
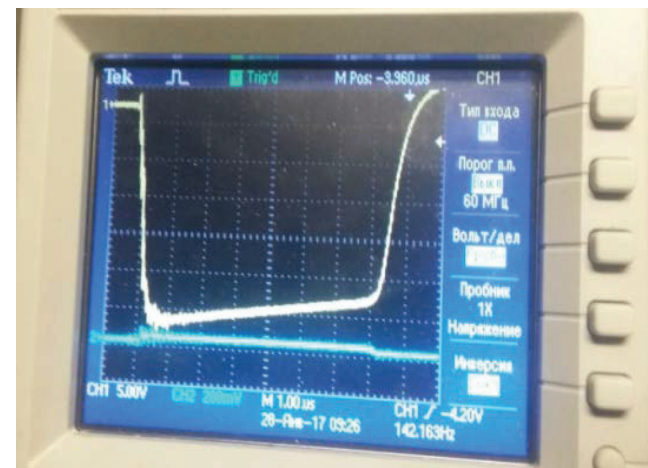
Induced current in static mode



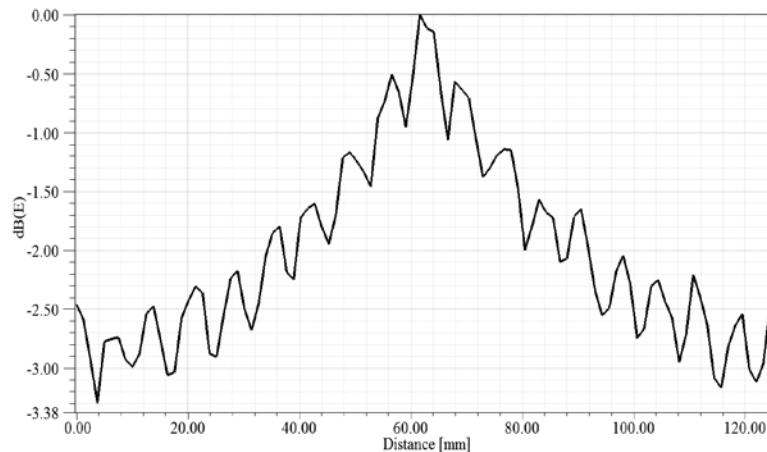
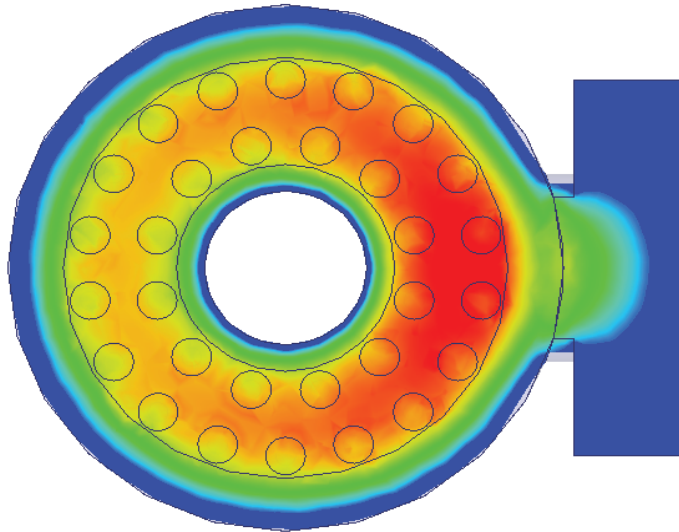
Induced current in dynamical mode



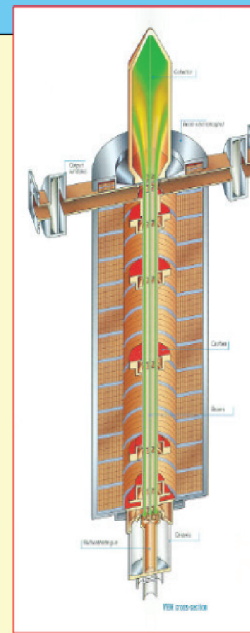
Effect of external electrical circuits



Optimization of the output cavity



RF Sources for VLLC - MBK option (2)



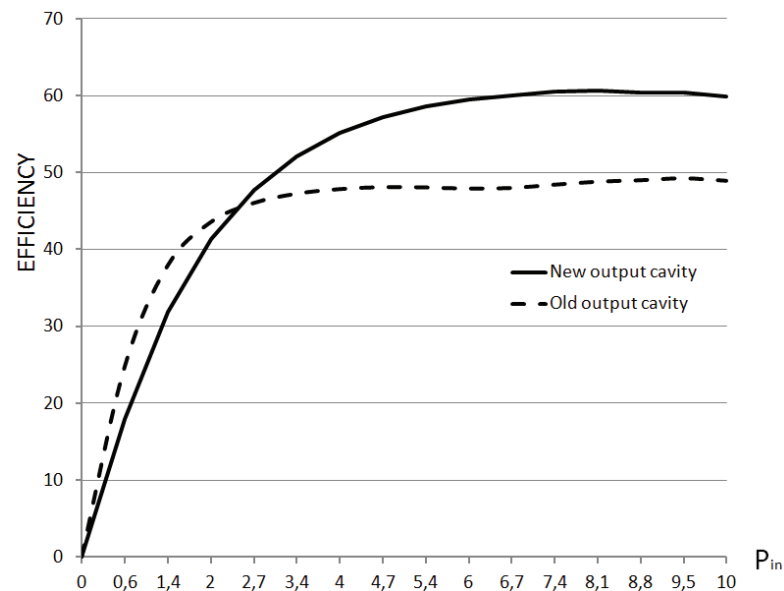
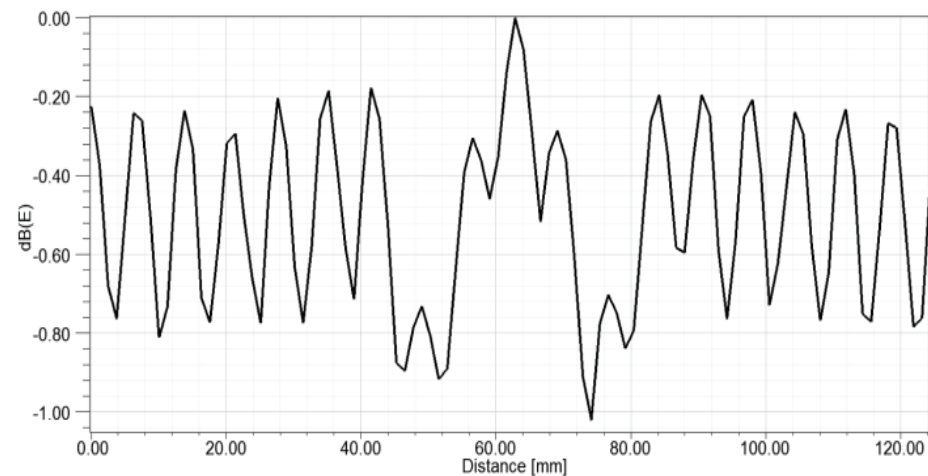
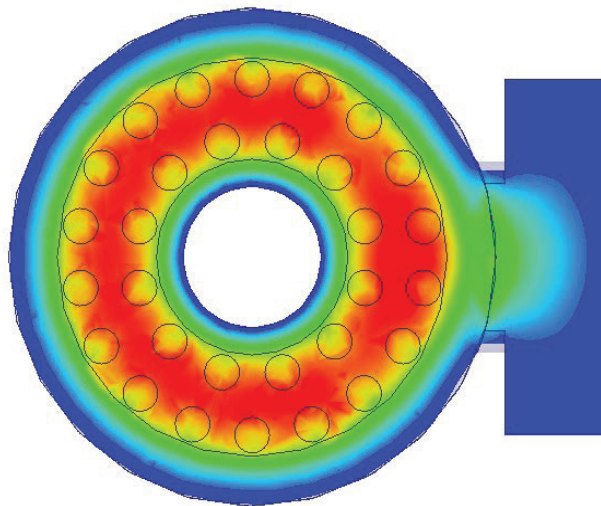
- MBK principle and technology are the ones of a conventional klystron .
- For the same RF power and comparable efficiency , the beam voltage is half of the klystron one .
- Pulsed MBK is able to operate in working areas (RF peak power + RF pulse duration + Efficiency) not accessible to the conventional klystron .
- In CW operation the expected advantage lies in the reduced voltage .

THALES ELECTRON

THALES



Optimization of the output cavity

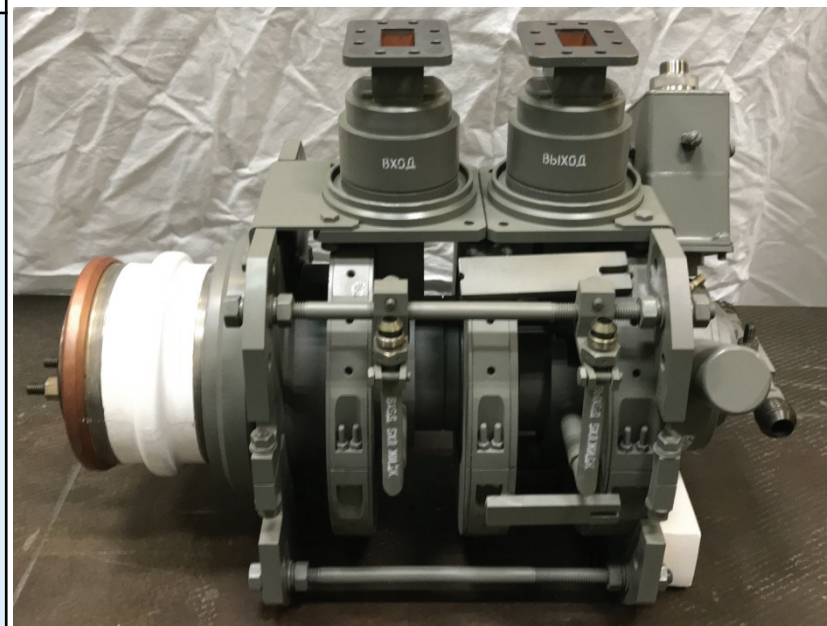


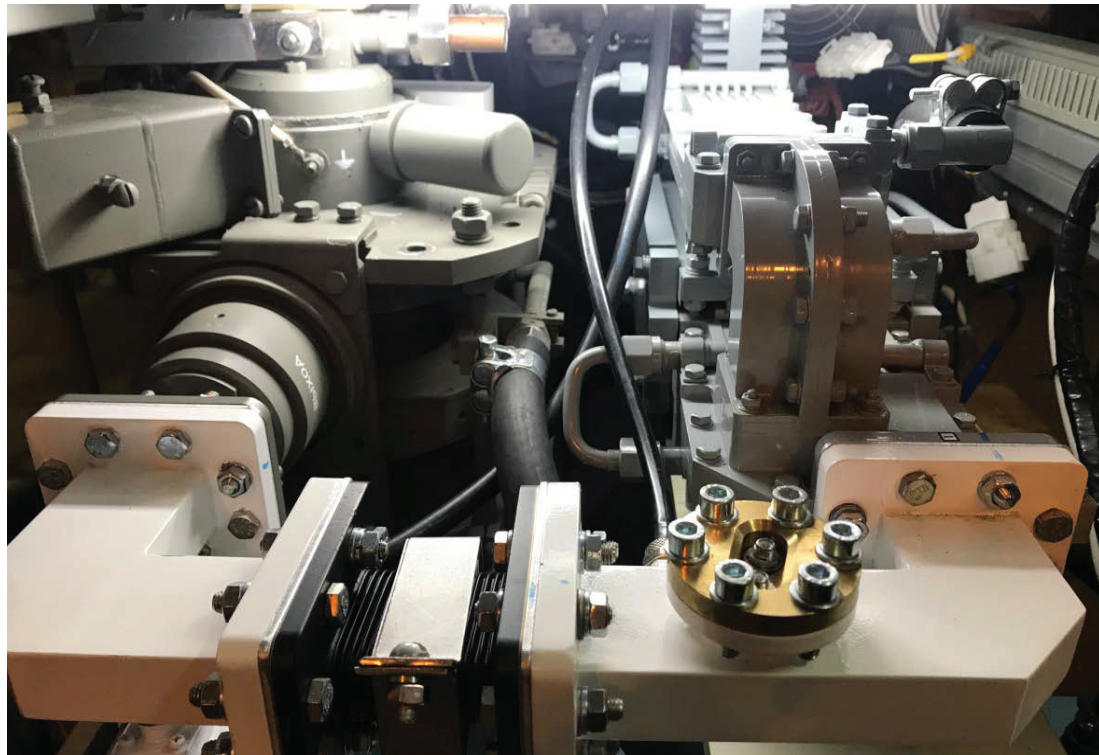


Conclusion

KILYSTRON KIU-271

Frequency –	5712 MHz
Cathode voltage –	45 kV
Pulse cathode current –	150 A
Output pulse power –	3,2 MW
Quality factor –	300 - 1000;
Focusing –	permanent magnets
Length -	478 mm



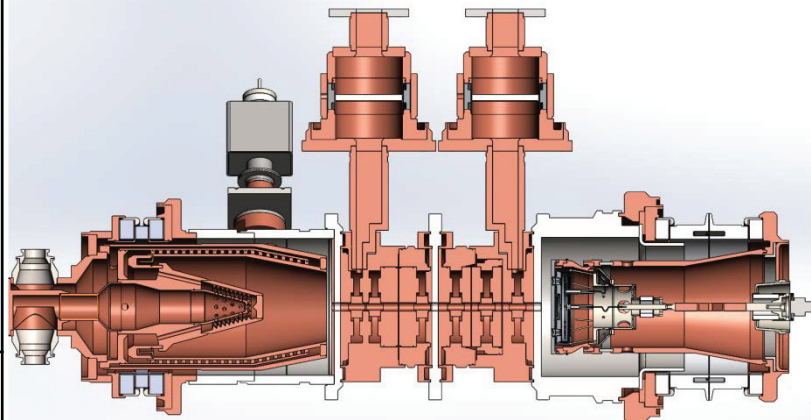
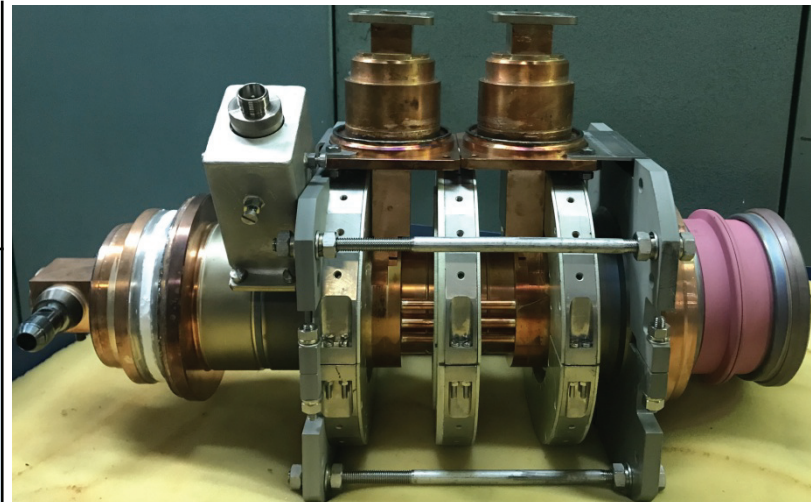




Conclusion

KLYSTRON KIU-273

Frequency –	5712 MHz
Cathode voltage –	45 kV
Pulse cathode current –	150 A
Output pulse power –	3,4 MW (+200 kW)
Quality factor –	300 - 1000;
Focusing –	permanent magnets
Length -	548 mm (+70 mm)





Thank You!

JSC «RPC «Toriy»

TORIY.RU



Since 1959