



Ultrahigh Vacuum in Superconducting Synchrotrons

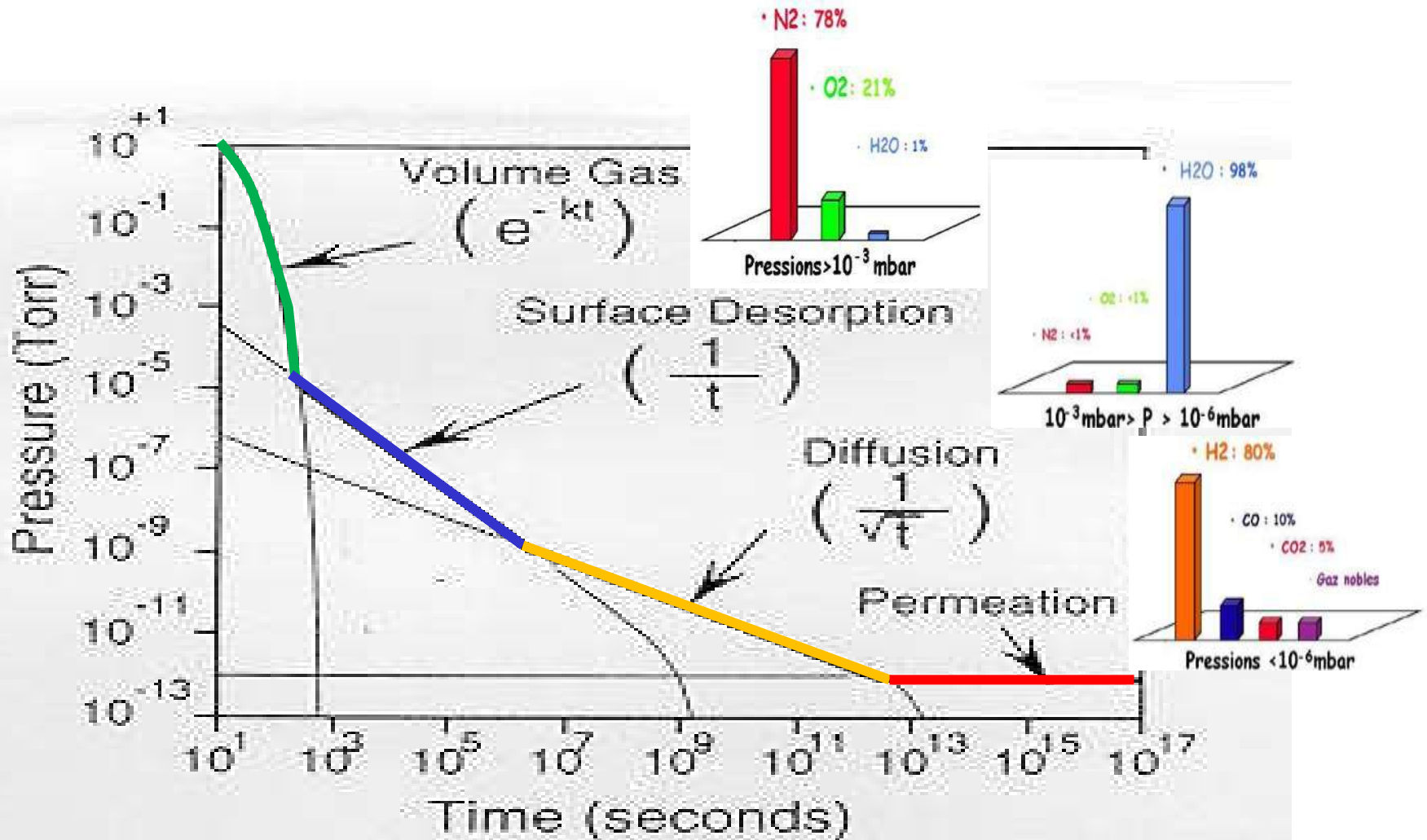
A.Smirnov, JINR, Dubna, Russia

Topics:

- Pumping & outgasing of hydrogen
- Cryogenic pumps & non evaporable getters for UHV
- Superconducting accelerators: LHC, RHIC, SIS100, Nuclotron
- Vacuum system for NICA Booster

Russian Particle Accelerator Conference
Obninsk, October 5 -10, 2014

Limiting mechanisms during pump down



Out gassing of Metals

- **Unbaked metals**

- Water is the main gas desorbed by unbaked metals.
- The outgassing rate of water decreases following a $1/t$ law: the outgassing of unbaked metals is not an intrinsic value.
- The water outgassing does not depend significantly on the nature of metals, on surface treatments and on temperature (for temperatures lower than 110 °C).
- At present no methods, except heating, exist to quickly remove water from unbaked metals.

- **Baked metals**

- Hydrogen is the main gas desorbed by baked metals.
- The value of the outgassing rate of hydrogen is stable at room temperature; when the thermal history is known the outgassing of hydrogen is an intrinsic property of metals.
- The diffusion model predicts values for the hydrogen outgassing that are in accord with experimental observations.
- Firing decrease the hydrogen outgassing rate by more than 2 orders of magnitude

Hydrogen diffusion in metals: Firing

CERN unpublished results

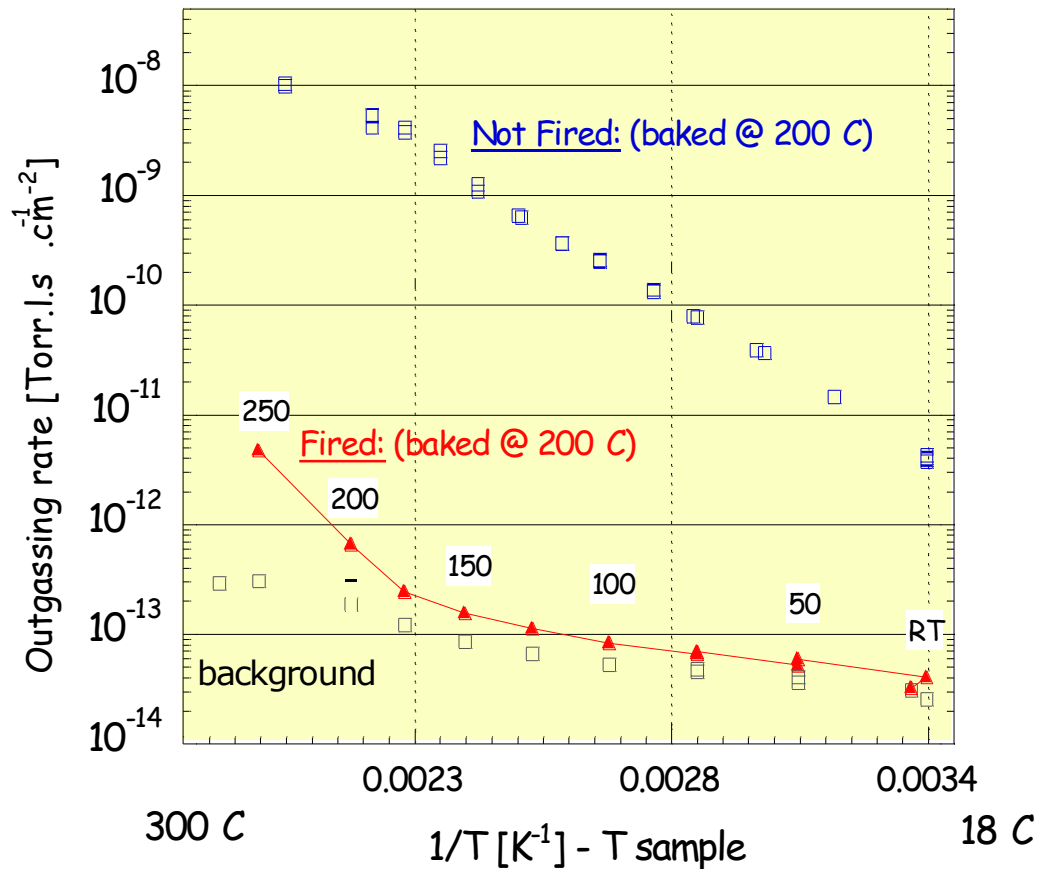
Material: 316LN

Wall thickness: 2 mm

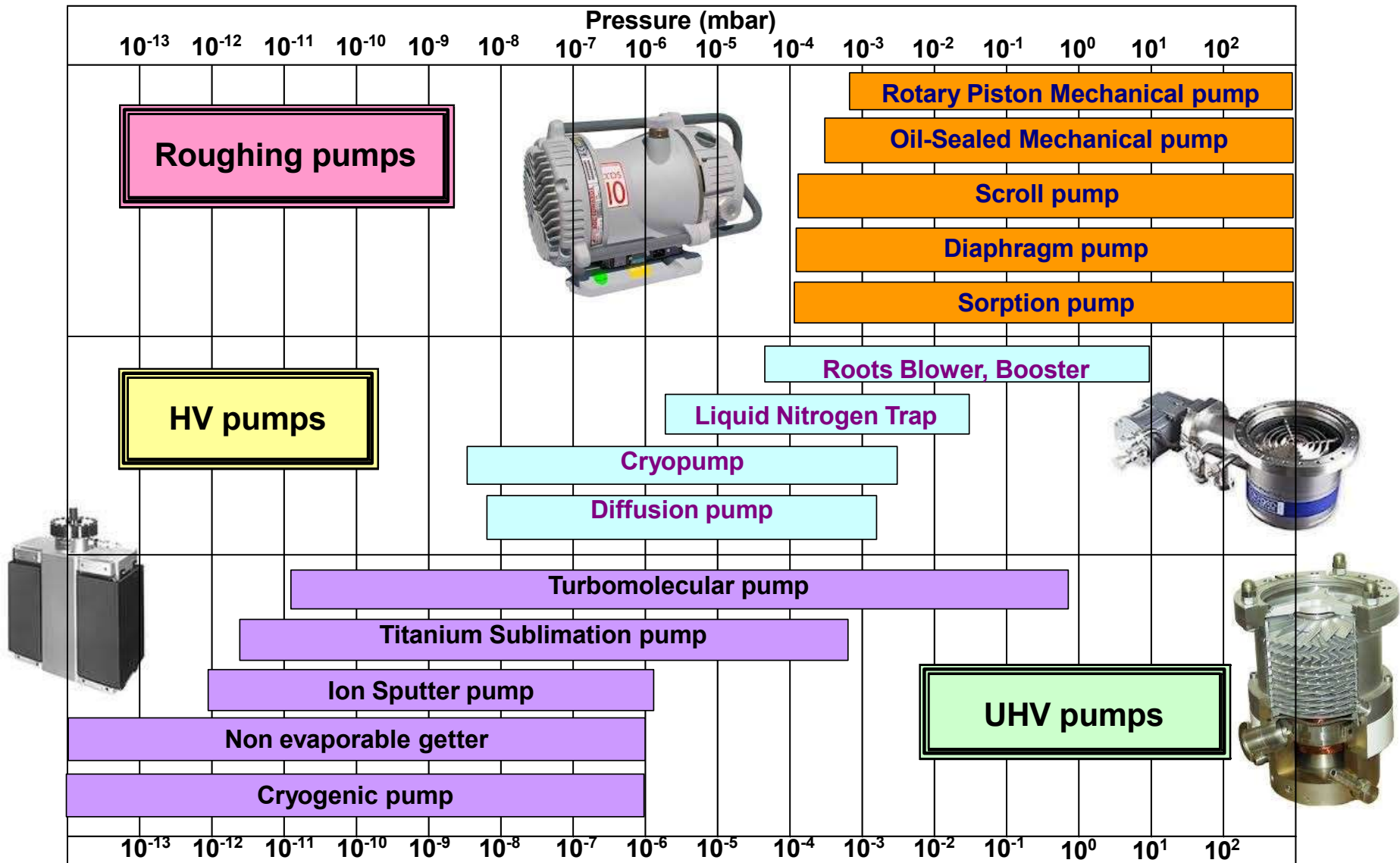
Vacuum firing:

950 °C x 2 h, 10^{-5} Torr H_2

For the fired chambers, the outgassing rate is limited by the background signal. The result was so intriguing that the experiment was repeated in a second system. On both systems, the upper limit at RT is 10^{-14} Torr.l.s $^{-1}$.cm $^{-2}$.



Pressure Ranges of Vacuum Pumps



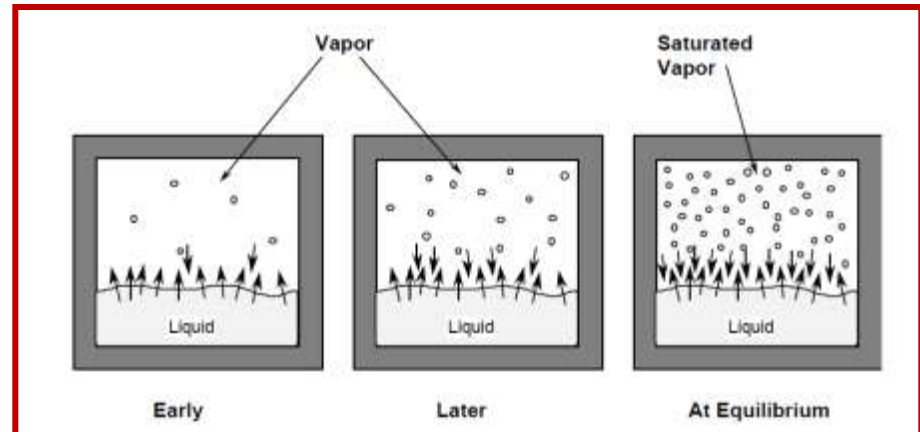
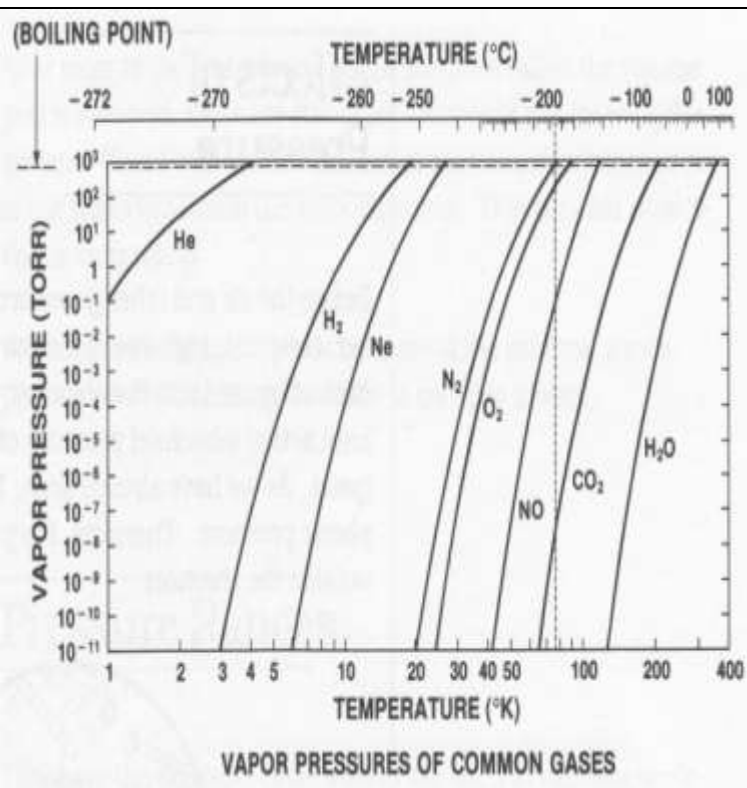
Cryopumping

Cryopumping relies on three different pumping mechanisms:

1. **Cryocondensation:** is based on the mutual attraction of **similar** molecules at low temperature:
 - a. the key property is the **saturated vapour pressure**, i.e. the pressure of the gas phase in equilibrium with the condensate at a given temperature. It limits the attainable pressure.
 - b. Only Ne, H₂ and He have saturated vapour pressures higher than 10⁻¹¹ mbar at 20 K.

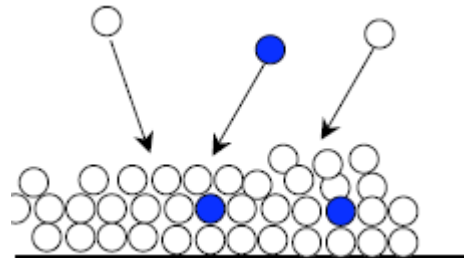
c. The vapour pressure of H₂ at 4.3 K is in the 10⁻⁷ mbar range, at 1.9 K lower than 10⁻¹² mbar.

d. Large quantity of gas can be cryocondensed (limited only by the thermal conductivity of the condensate phase and the thermal flow)



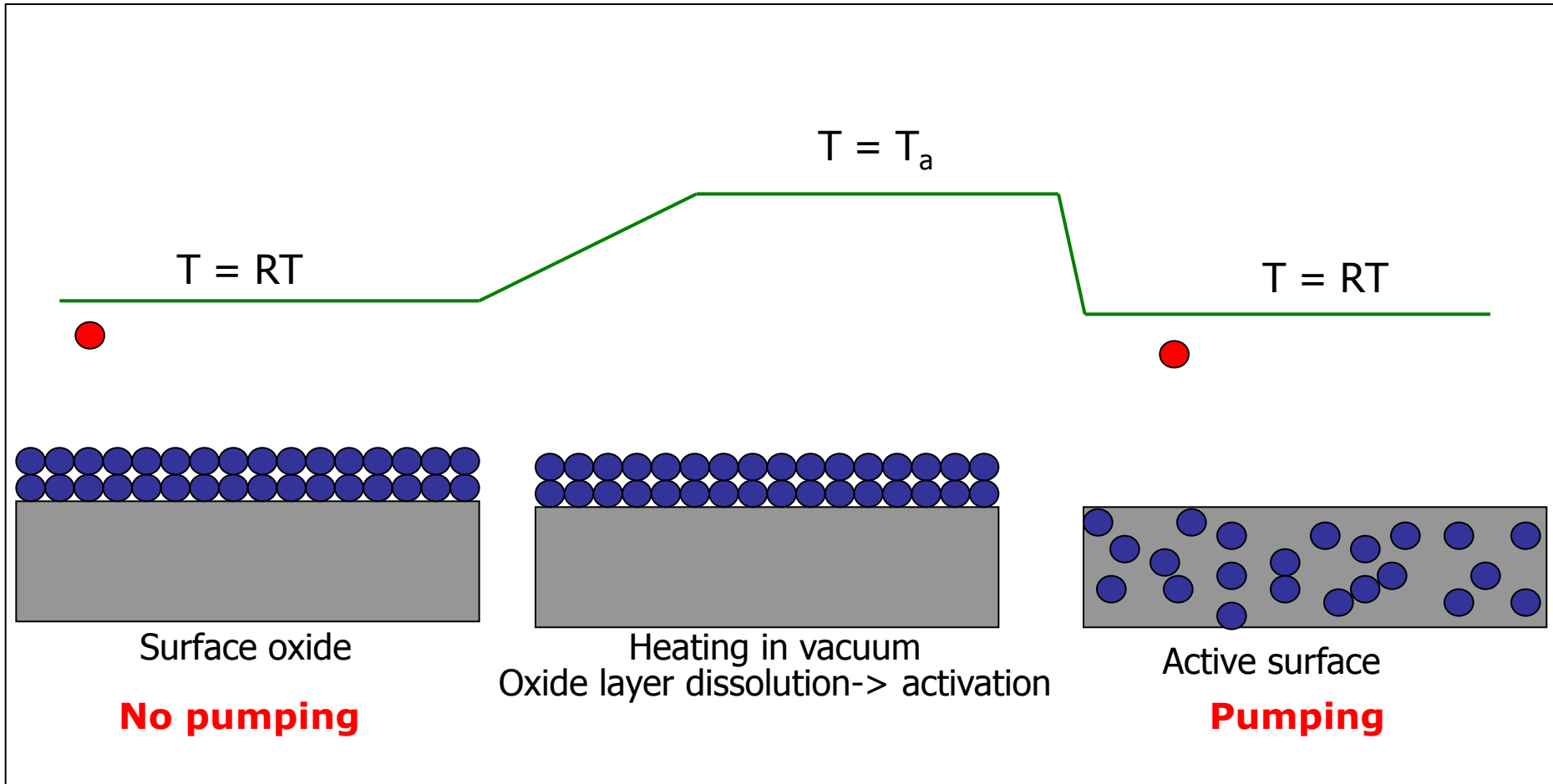
Cryopumping

2. **Cryosorption**: is based on the **attraction between molecules and substrate**. The interaction is much stronger than that between similar molecules:
- a) Gas molecules are pumped at pressures much lower than the saturated vapour pressure providing the adsorbed quantity is lower than one monolayer.
 - a) **Porous materials** are used to increase the specific surface area; for charcoal about 1000 m² per gram are normally achieved.
 - b) The important consequence is that significant quantities of H₂ can be pumped at 20 K and He at 4.3 K.
 - c) Submonolayer quantities of all gases may be effectively cryosorbed at their own boiling temperature; for example at 77 K all gases except He, H₂ and Ne.
3. **Cryotrapping** : low boiling point gas molecules are trapped in the layer of an easily condensable gas. The trapped gas has a saturation vapor pressure by several orders of magnitude lower than in the pure condensate. Examples: Ar trapped in CO₂ at 77 K; H₂ trapped in N₂ at 20 K.



Non-Evaporable Getter (NEG) Pumps

The dissolution of the oxide layer is possible only in metals having very high oxygen solubility limit, namely the elements of the 4th group: Ti, Zr and Hf.



Non-Evaporable Getter Pumps

Gases are categorized into four families based on their interactions with NEG's:

1. **Hydrogen and its isotopes** - sorbed reversibly.
2. **CO, CO₂, O₂, and N₂** - sorbed irreversibly.
3. **H₂O, hydrocarbons** - sorbed in a combination of reversible and irreversible processes.
Hydrocarbons are sorbed very slowly.
4. **Rare gases** - not sorbed at all.

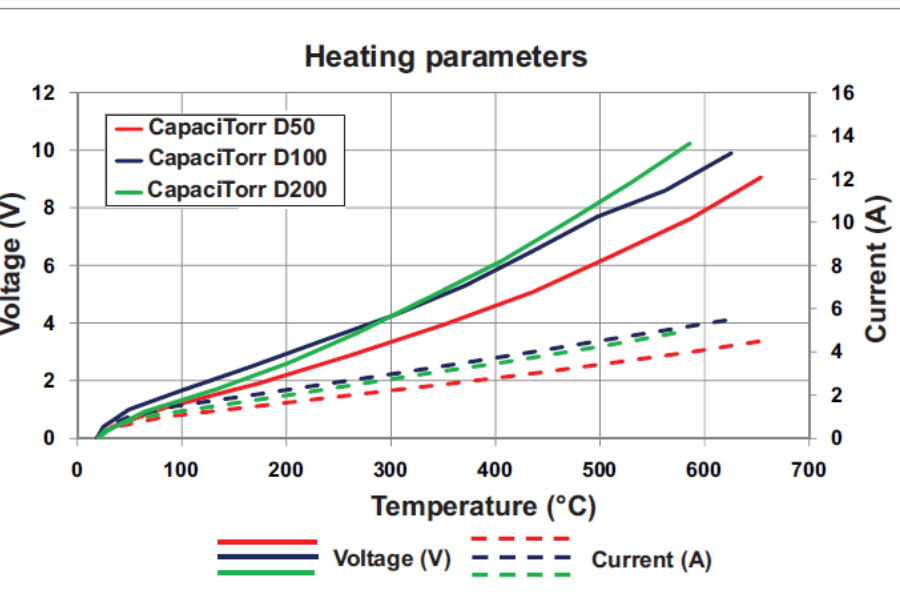
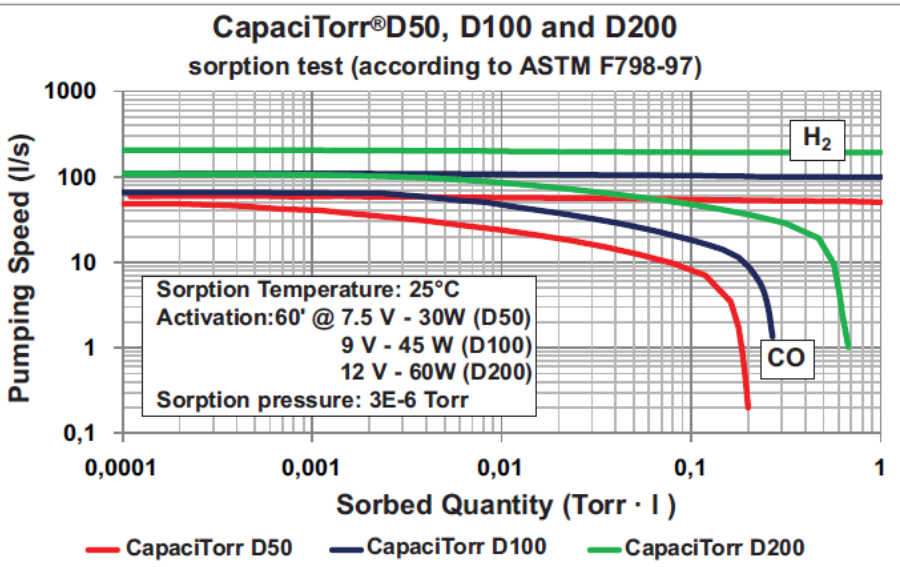
Ion pumps are required in combination with NEG's

A typical alloy produced by **SAES Getter** is St707:

Element	Concentration [wt. %]	Main role in the alloy
Zr	70	<ul style="list-style-type: none">- High O solubility limit.- Chemical reactivity
V	24.6	<ul style="list-style-type: none">- Increases O diffusivity,- Chemical reactivity
Fe	5.4	<ul style="list-style-type: none">- Reduces pyrophoricity

Full pumping speed is obtained after heating at 400°C for 45' or 300°C for 24h

CapaciTorr® , NEXTorr® (SAES Group)

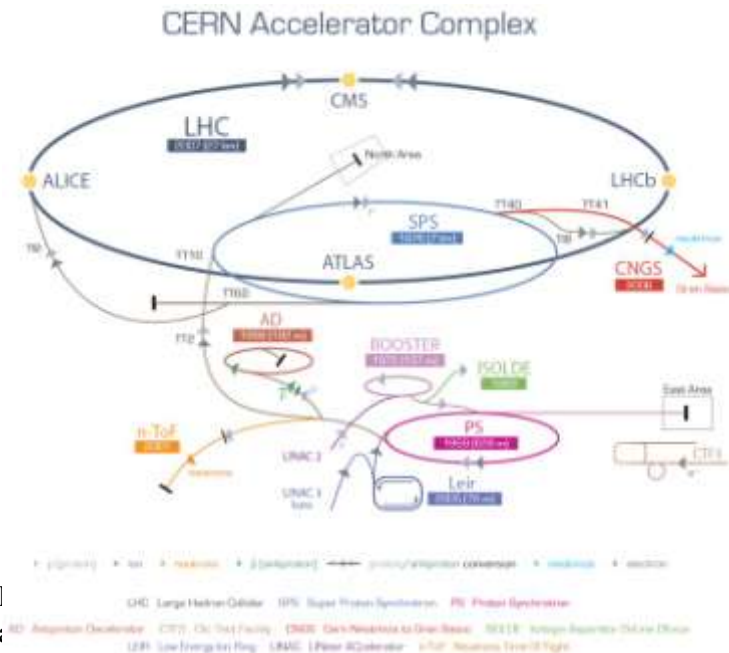


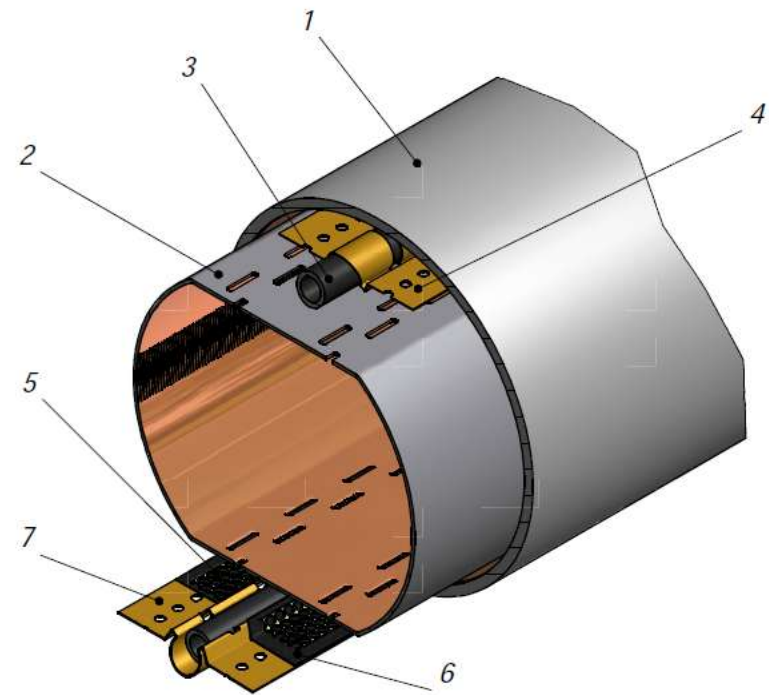
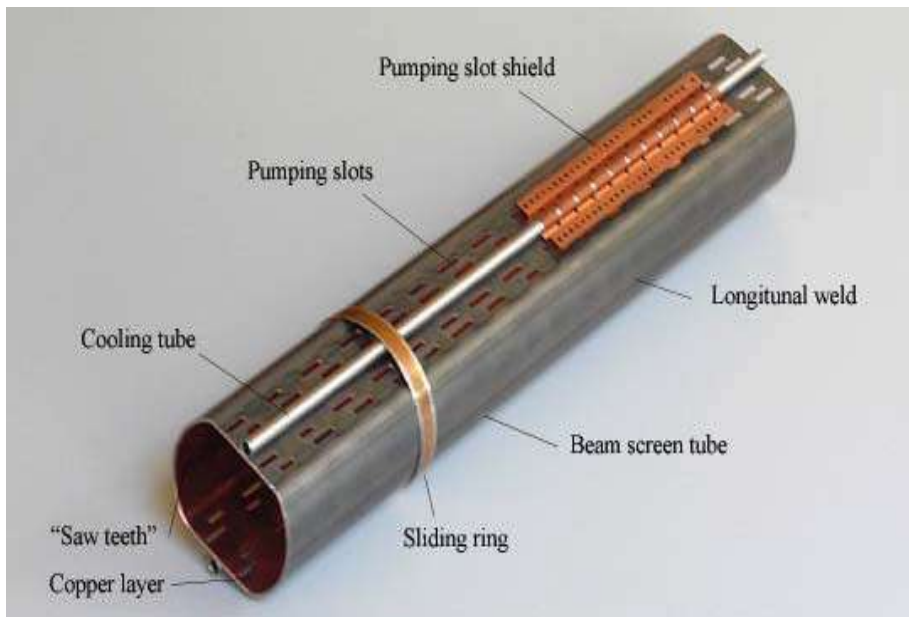


Vacuum, Surfaces & Coatings Group

- **A CERN-wide responsibility for the operation of accelerators and detectors vacuum systems**
 - 128 km of vacuum:
 - 78 km of high/UHV vacuum for beams w/wo NEG coated beam pipes
 - 50 km of high vacuum for insulation
- **A large quantity of gauges, instrumentation, pumps and leak detectors**
 - 2850 ion pumps, 450 turbo molecular pumps and 325 Ti sublimation pumps
 - 2750 pressure gauges, 40 leak detectors and 50 RGAs
 - 1930 roughing valves and 510 gate sector valves

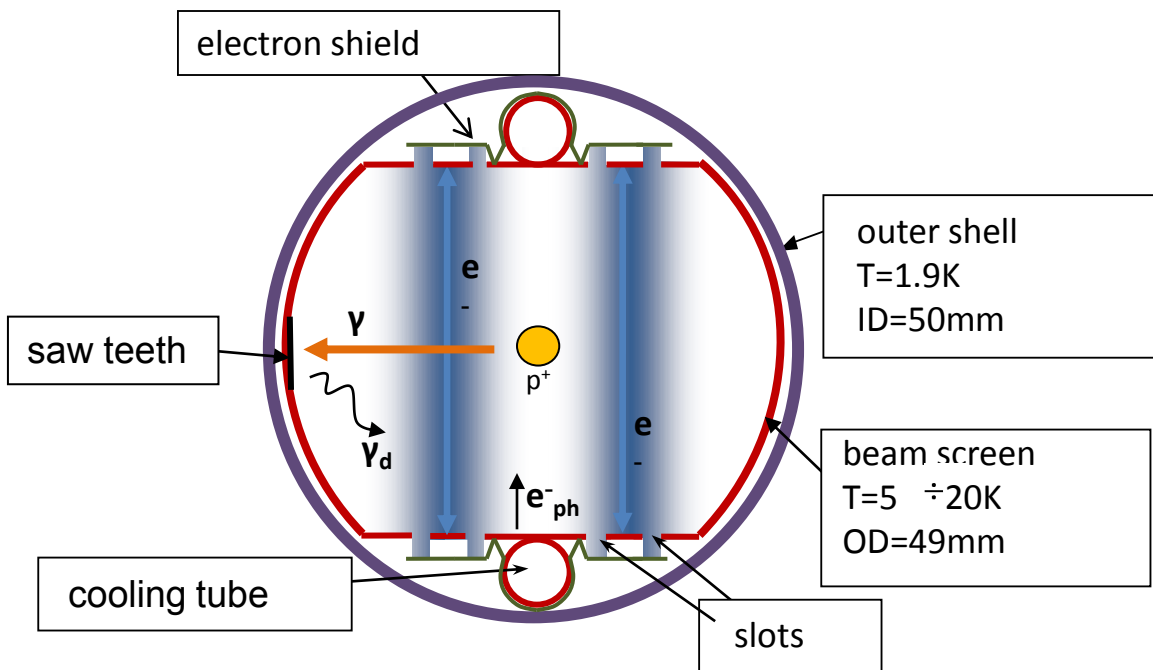
Machine	Type	Year	Energy	Bakeout	Pressure (Pa)	Length	Particles	
Linac, Booster, ISOLDE, PS, n-TOF and AD Complex								
LINAC 2	linac	1978	50 MeV	ion pumps	10^{-7}	2.6 km !	p	
ISOLDE	electrostatic	1992	60 keV	-	10^{-4}	150 m	ions: 700 isotopes and 70 (92) elements	
REX-ISOLDE	linac	2001	3 MeV/u	partly	$10^{-5} - 10^{-10}$	20 m		
LINAC 3	linac	1994	4.2 MeV/u	ion pumps	10^{-7}	30 m	ions	
LEIR	accumulator	1982/2005	72 MeV/u	complete	10^{-10}	78 m	pbar, ions	
PSB	synchrotron	1972	1-1.4 GeV	ion pumps	10^{-7}	157 m	P. ions	
PS	synchrotron	1959	28 GeV	ion pumps	10^{-7}	628 m	P. ions	
AD	decelerator	?	100 MeV	complete	10^{15}	188 m	pbar	
CTF3 complex	linac/ring	2004-09		partly	10^{12}	300 m	e	
PS to SPS TL	Transfer line	1976	26 GeV	-	10^{11}	~1.3 km	P. ions	
SPS Complex								
SPS	synchrotron	1976	450 GeV	Extractions	10^{-7}	7 km	p, ions	
SPS North Area	Transfer line	1976		-	$10^{10} - 10^{12}$	~1.2 km		
SPS West Area	Transfer line	1976		-		~1.4 km		
SPS to LHC T12/8 Line	Transfer line	2004/2006		-		2 x 2.7 km		
CNGS Proton Line	Transfer line	2005		-		~730 m		
LHC Accelerator								
LHC Arcs (Beam x2, Magnets & ORL Insul.)	collider	2007	2 x 7 TeV	complete	$< 10^{-11}$	2 x (2 x 25 km)	p, ions	
LSS RT separated beams						~ 1.4 km		
LSS RT recombination						~ 570 m		
Experimental areas						~ 180 m		
Beam Dump Lines TD62/68	Transfer line	2006	7 TeV	-	10^{15}	2 x 720 m		
						High Vacuum	~20 km	~128 km !
						UHV w/wo NEG	~ 57.5 km	
						Insulation vacuum	~ 50 km	





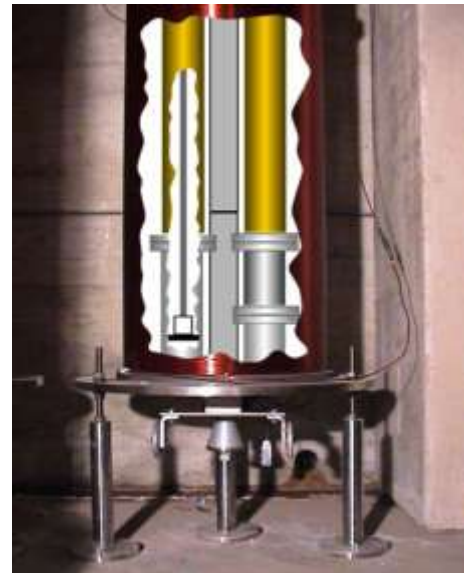
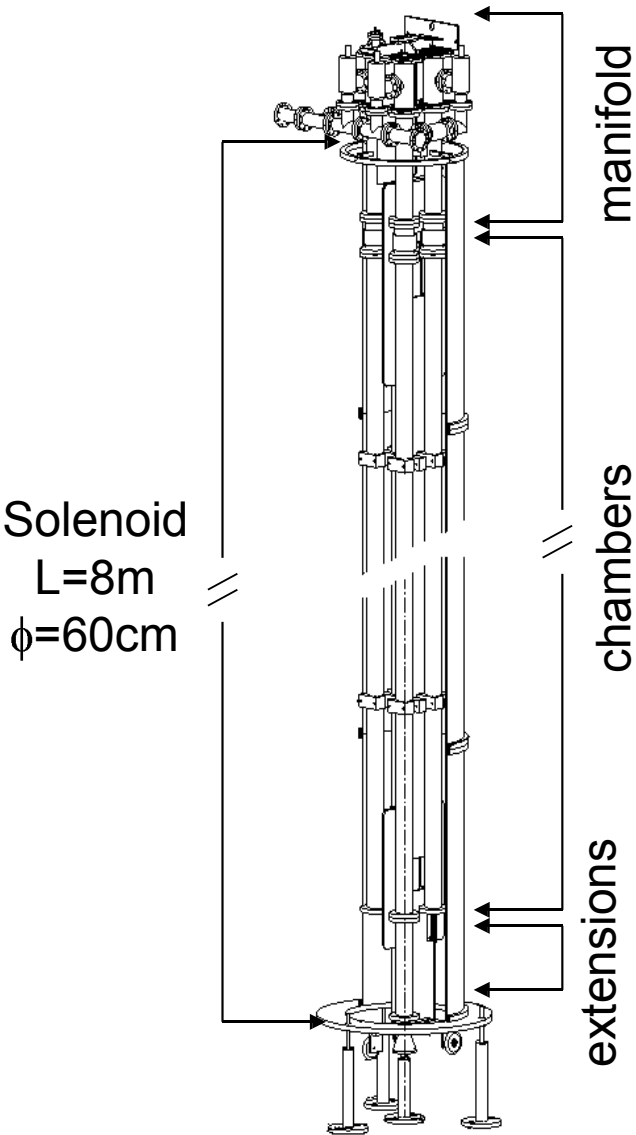
Cold vacuum chamber with cryosorber

1- outer shell, 2 – beam screen, 3 – cooling tube, 4,7 – pumping slot shield, 5 – charcoal fiber, 6 – grid for charcoal fixing



More than 1300 chambers coated with TiZrV NEG for the LHC.

Standard chambers are 7 m long, 80 mm diameter.



CERN's NEG Coating Facility

RHIC @ BNL, Long Island, New York



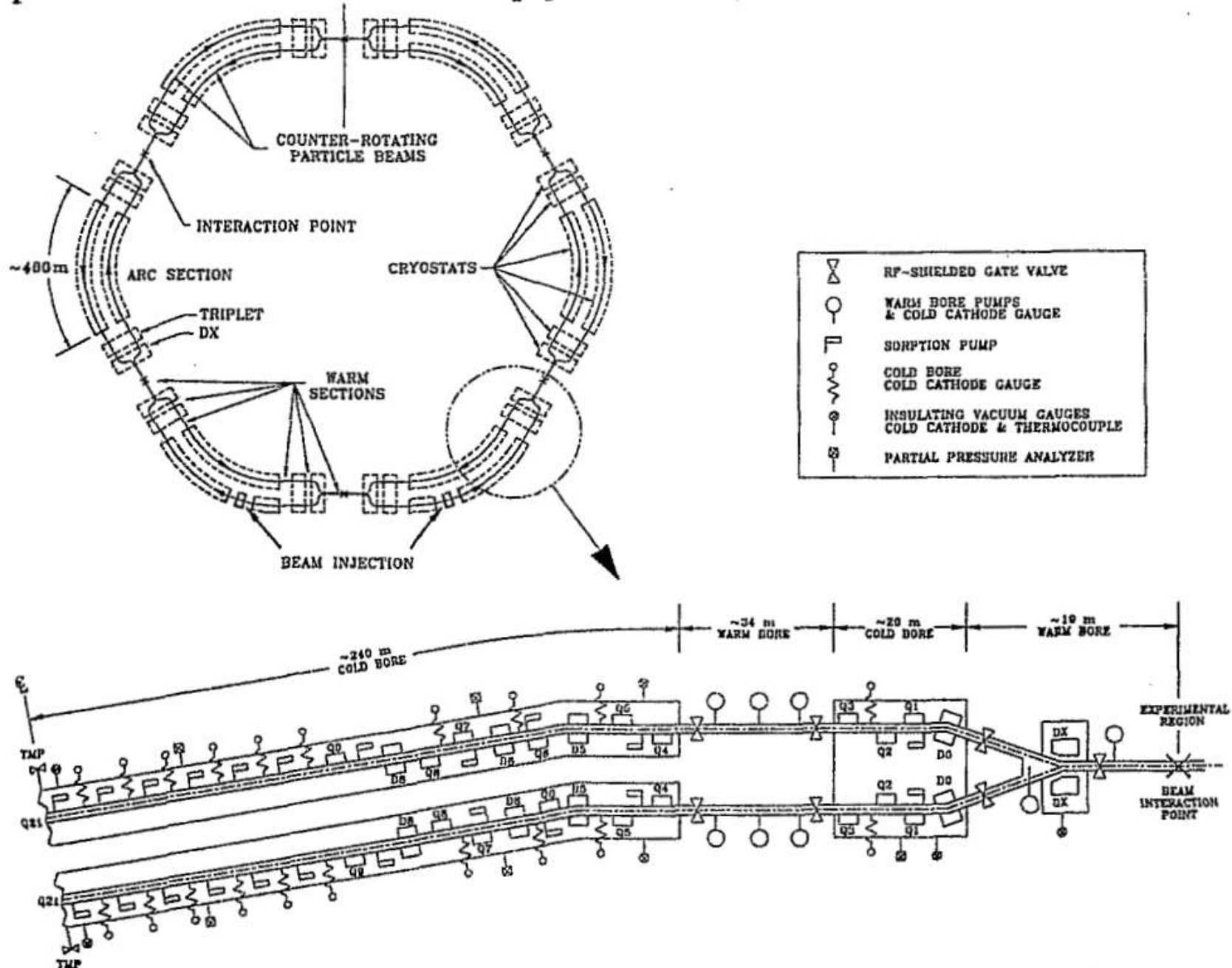


FIGURE 1. Schematic layout of RHIC ring and one-half of sextant showing the three types of warm vacuum regions, the Q3-Q4 insertion, the final DX focusing and the interaction region.

Sorption pumps containing activated charcoal are mounted to the pull through ports of the RF-shielded bellows at every fourth interconnect (B30 m intervals) to pump He and H₂.

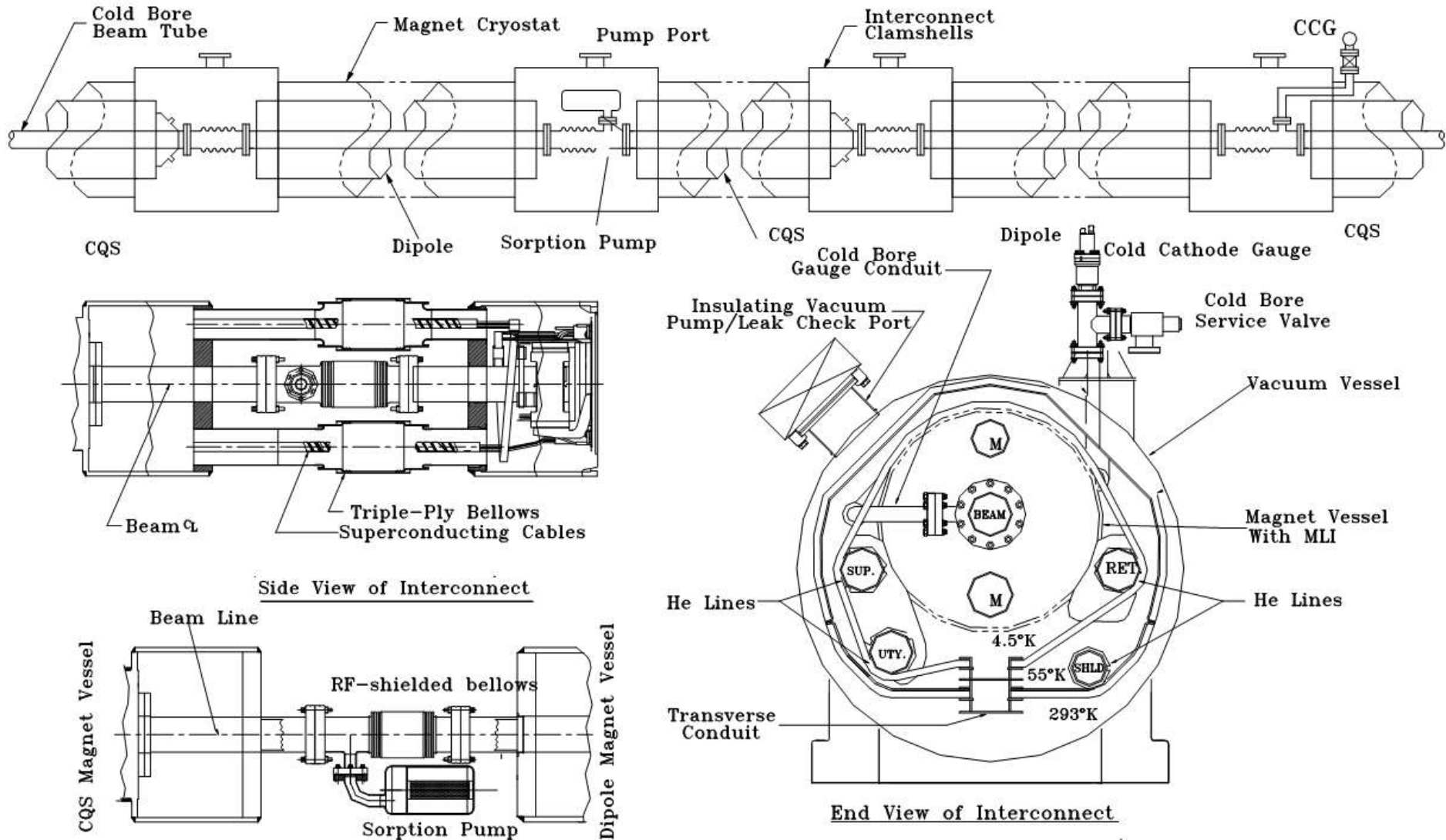


Fig. 2. Vacuum layout of arc sections, and the magnet and beam tube interconnects.

FAIR Vacuum Requirements



Due to ion beam lifetime requirement
(e.g.: U^{28+} in SIS18):

SIS18 (216m): bakeable $p \approx 5 \cdot 10^{-12}$ mbar
ESR (108m): bakeable $p \approx 5 \cdot 10^{-12}$ mbar

SIS100 (1084m): cold arcs $T_{OP} = 7-20K$
bakeable straight section
 $p \approx 5 \cdot 10^{-12}$ mbar

SIS300 (1084m): cold arcs $T_{OP} = 4.2K$
bakeable straight section
 $p \approx 5 \cdot 10^{-12}$ mbar

NESR (223m): $p \approx 5 \cdot 10^{-12}$ mbar (bakeable)

HESR (550m): $p \leq 10^{-10}$ mbar (bakeable)

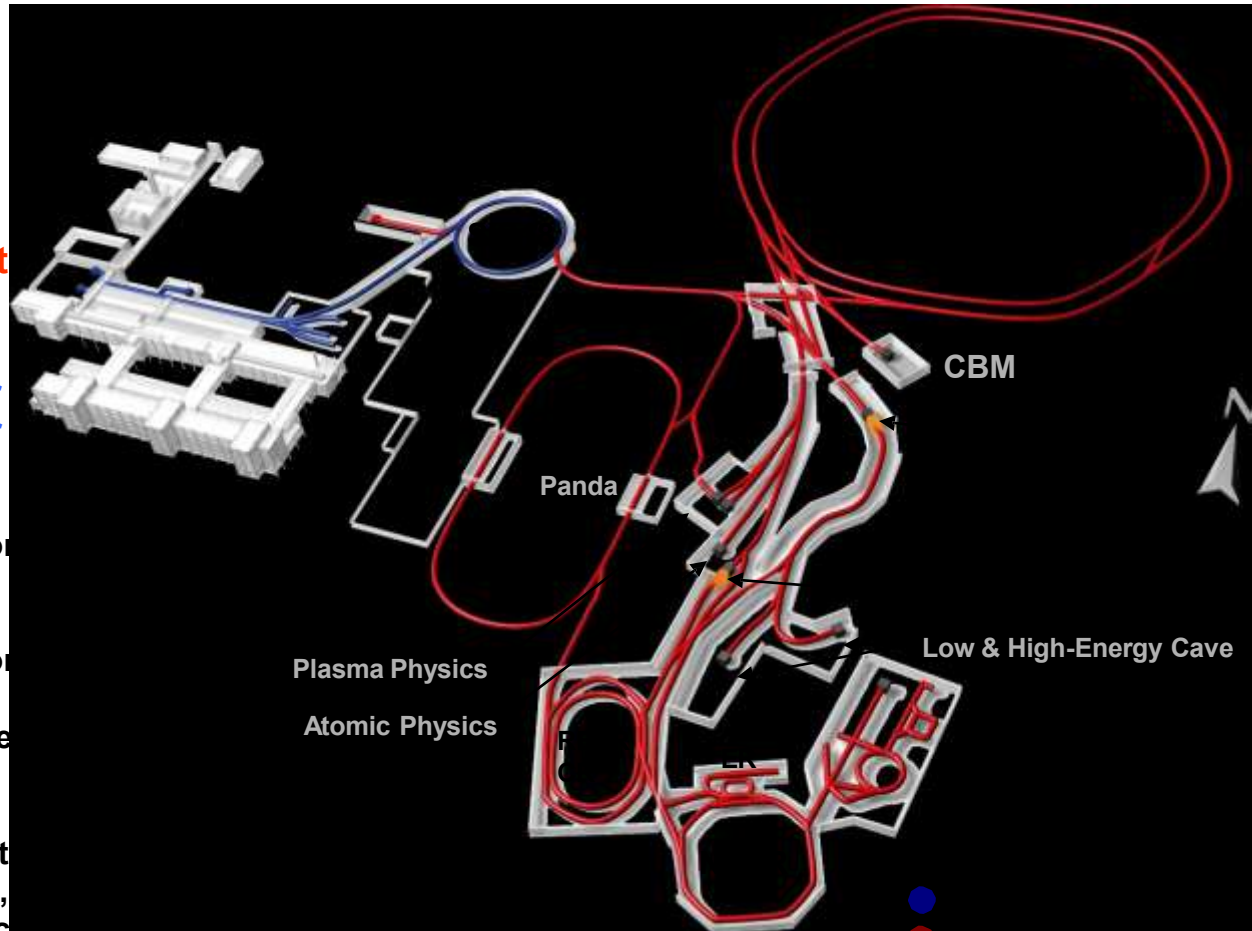
RESR (240m): $p \leq 10^{-10}$ mbar (bakeable)

CR (221m): $p \leq 10^{-9}$ mbar (no bakeout)

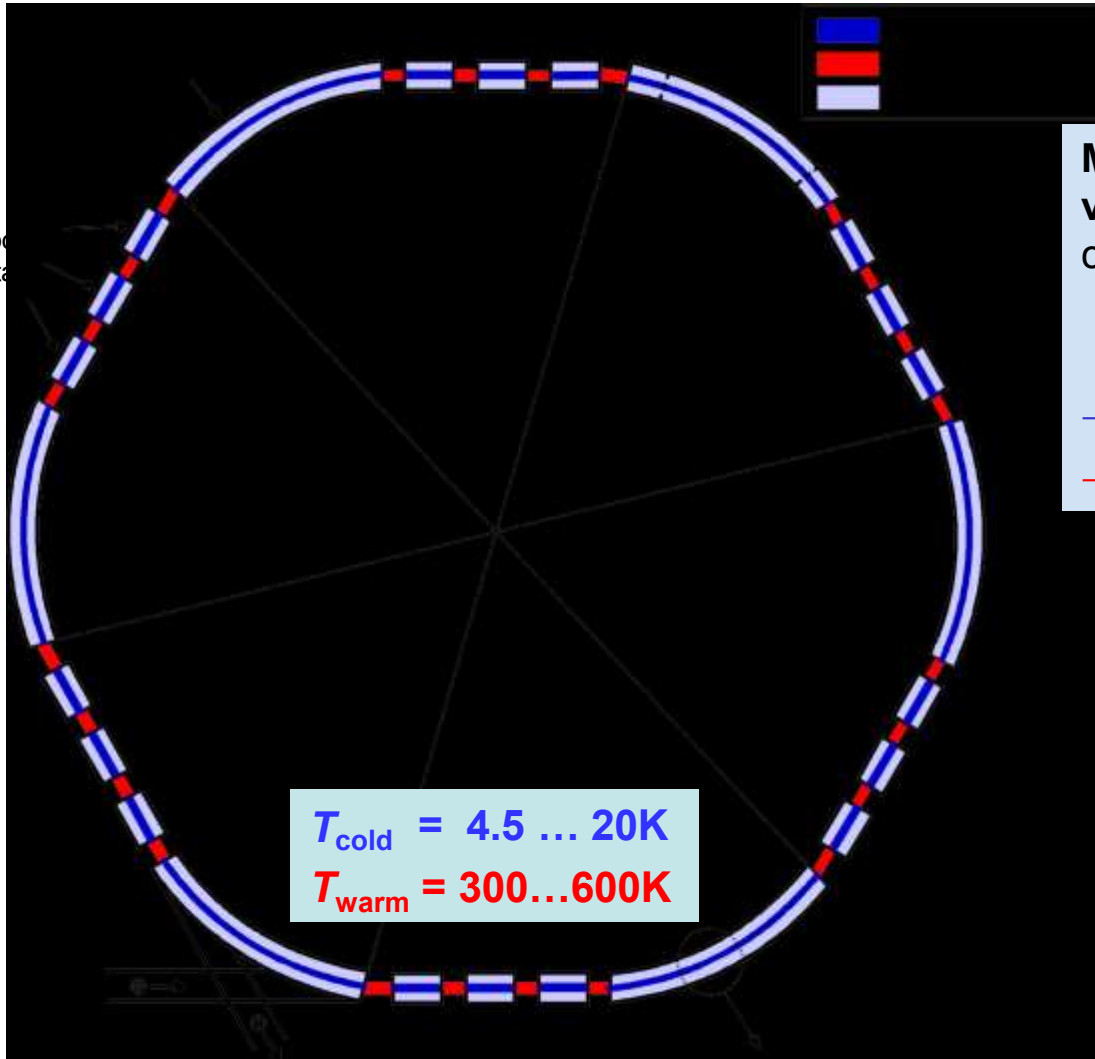
HEBT/Super-FRS: length 2.4 km, 10% cold,
differential pumping sections to rings,
 $p \approx 1 \cdot 10^{-9}$ mbar

P-Linac: $p \approx 1 \cdot 10^{-9}$ mbar

*all pressures: N_2 equivalent



Vacuum Systems of SIS100



Maximum allowed average beam vacuum pressure under dynamic conditions is given by beam life time

$$N_{\text{max}} < 4 \cdot 10^{+12} \text{ m}^{-3} (\text{H}_2)$$

$$\rightarrow p_{\text{cold}} < 5 \cdot 10^{-12} \text{ mbar } (T = 10\text{K})$$

$$\rightarrow p_{\text{warm}} < 1 \cdot 10^{-10} \text{ mbar } (T = 300\text{K})$$

Total length of SIS100: 1083.6 m
(82% cold, 18% warm)
basic structure: hexagonal
six straights and six arcs
25 warm sections (24 x 9.1 m long,
1 x 3.3 m)
25 cold sections (6 long arcs: 5x
135m, 1x 122.6m), 19 short
straight, 18 x 4.3m, 1 x 9.2m)

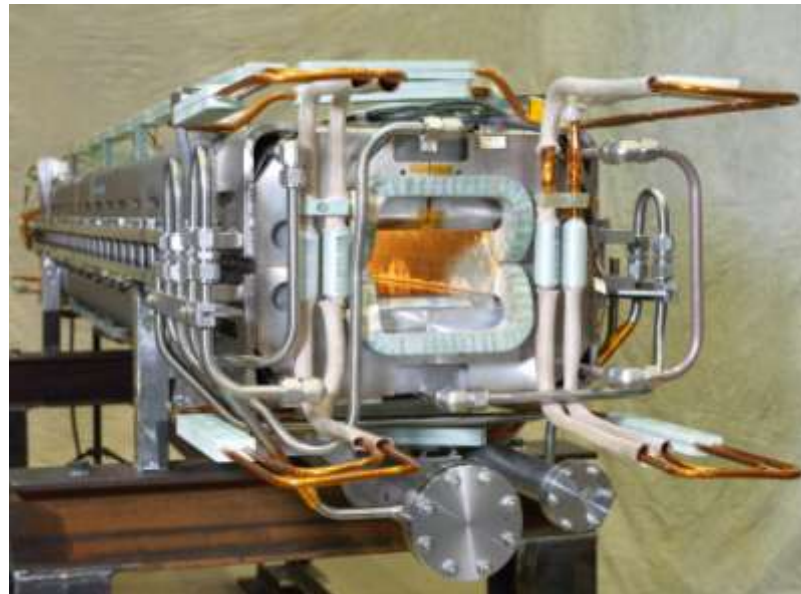
SIS100 Dipole Chamber Design



Length of chamber: 3.35 m
Aperture: 120 x 60mm²
Wall thickness: 0.3mm
Rib thickness: 3.0 mm

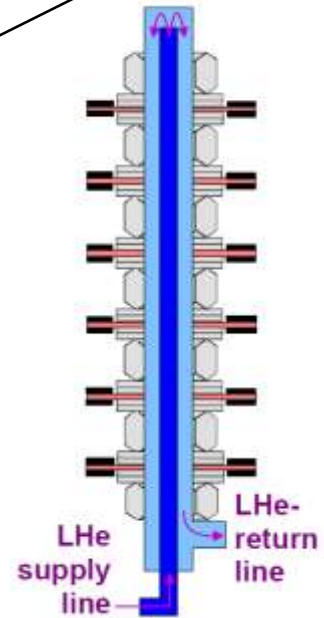
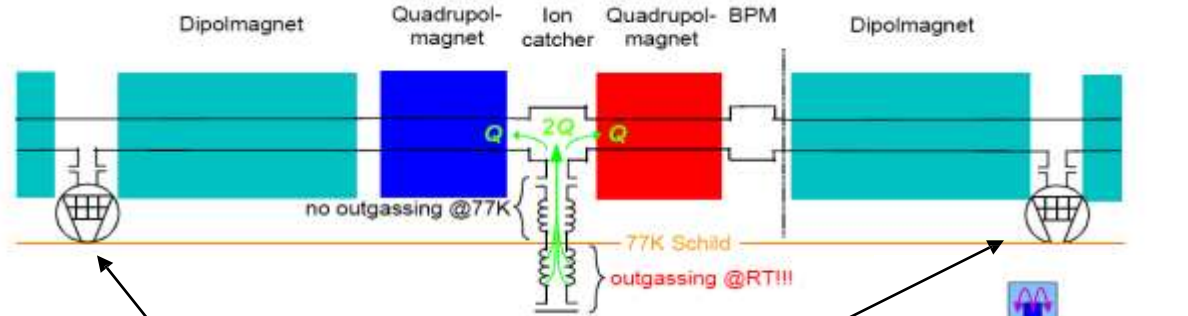
Vacuum physical requirements on the magnet chamber design

- all dipole chambers represent 45% of the total cold surface in the cryogenic arcs
- the inner beam pipe wall will be used as expanded cold surface of an efficient cryopump with practically infinite capacity for nearly all condensable gas species -> wall temperatures as low as possible
- static vacuum pressure inside the chamber 10^{-12} mbar, under dynamic conditions $< 10^{-11}$ mbar
- due to the fast magnet ramping eddy currents heat up the chamber wall to temperatures $> 20\text{K}$



Cryosorption Pumps

- **auxiliary pumps** are used primarily to lower the partial pressures of H₂ and He
- **10 cryosorption pumps per arc** (each 13 m) and **one per short quadrupole doublet in the straight sections**
- **2 different pump layouts**
- cryosorption pump consists of several round cryopanel (i.e. copper disks coated with charcoal of SC2 type made by CHEMVIRON, coating by KIT, Karlsruhe, Germany)
- panels stacked on a central cooling tube cooled down to $T \sim 4.5\text{K}$
- $S_{\text{He}} \sim 1 \text{ l/s cm}^2$ for He and $S_{\text{H}_2} \sim 10 \text{ l/s cm}^2$ for H₂



Layout_1
(to be used in cryogenic arcs)

m_{char}	A_{char}	C_{char}	S_{pump}
$\sim 24 \text{ g}$	$\sim 34000 \text{ m}^2$	$\sim 0.25 \text{ mbar}\cdot\ell$	$\sim 50 \text{ l/s}$

Superconducting accelerator complex **NICA** (**N**uclotron based **I**on **C**ollider **f**Acility)

Fixed target experiments
area (b.205)

Extracted beams from
Nuclotron

KRION-6T
and HILac
(3,5 MeV/u)

SPP and
LU-20
(5 MeV/u)

Cryogenics

Spin Physics
Detector (SPD)

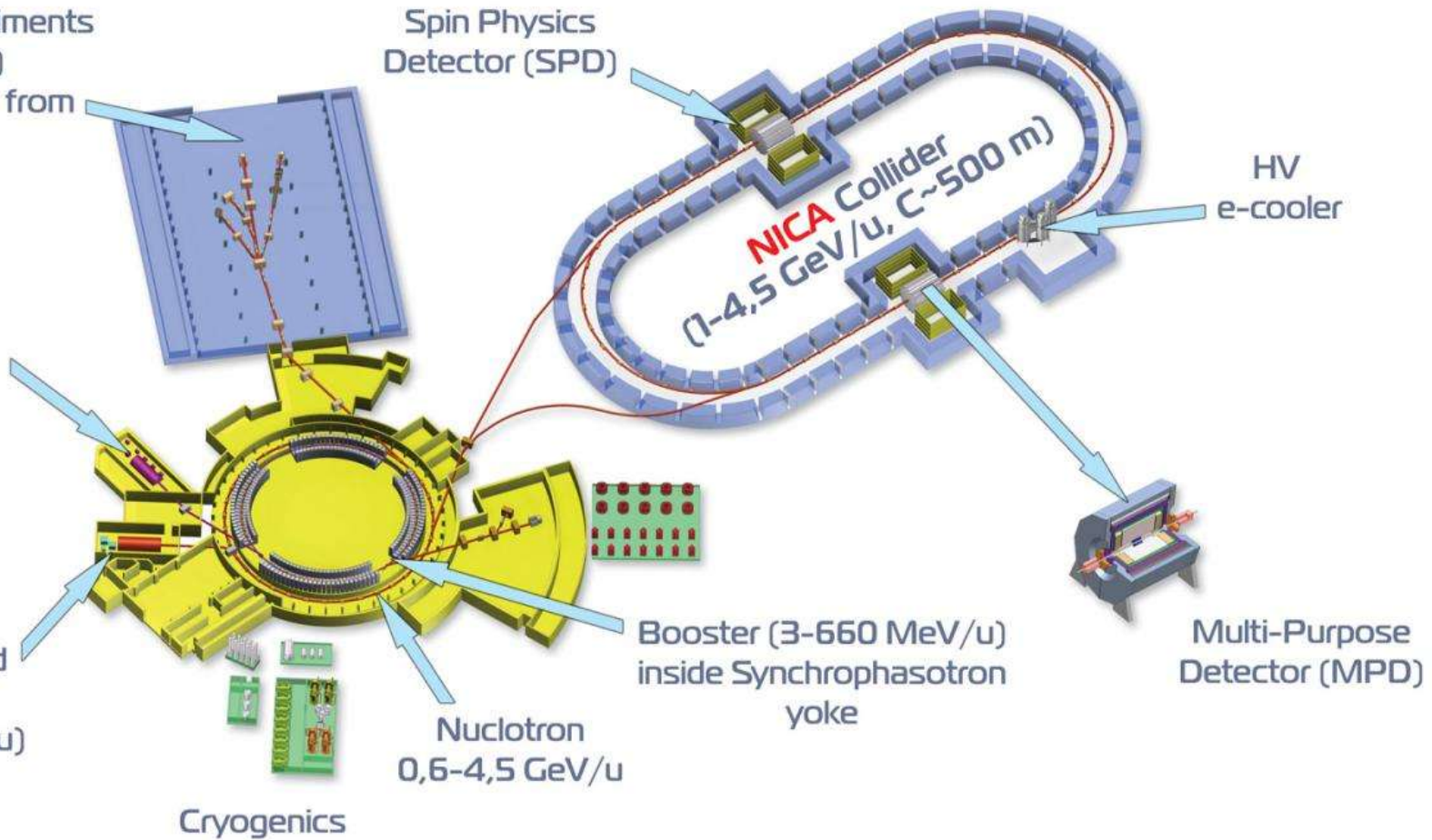
Booster (3-660 MeV/u)
inside Synchrotron
yoke

Nuclotron
0,6-4,5 GeV/u

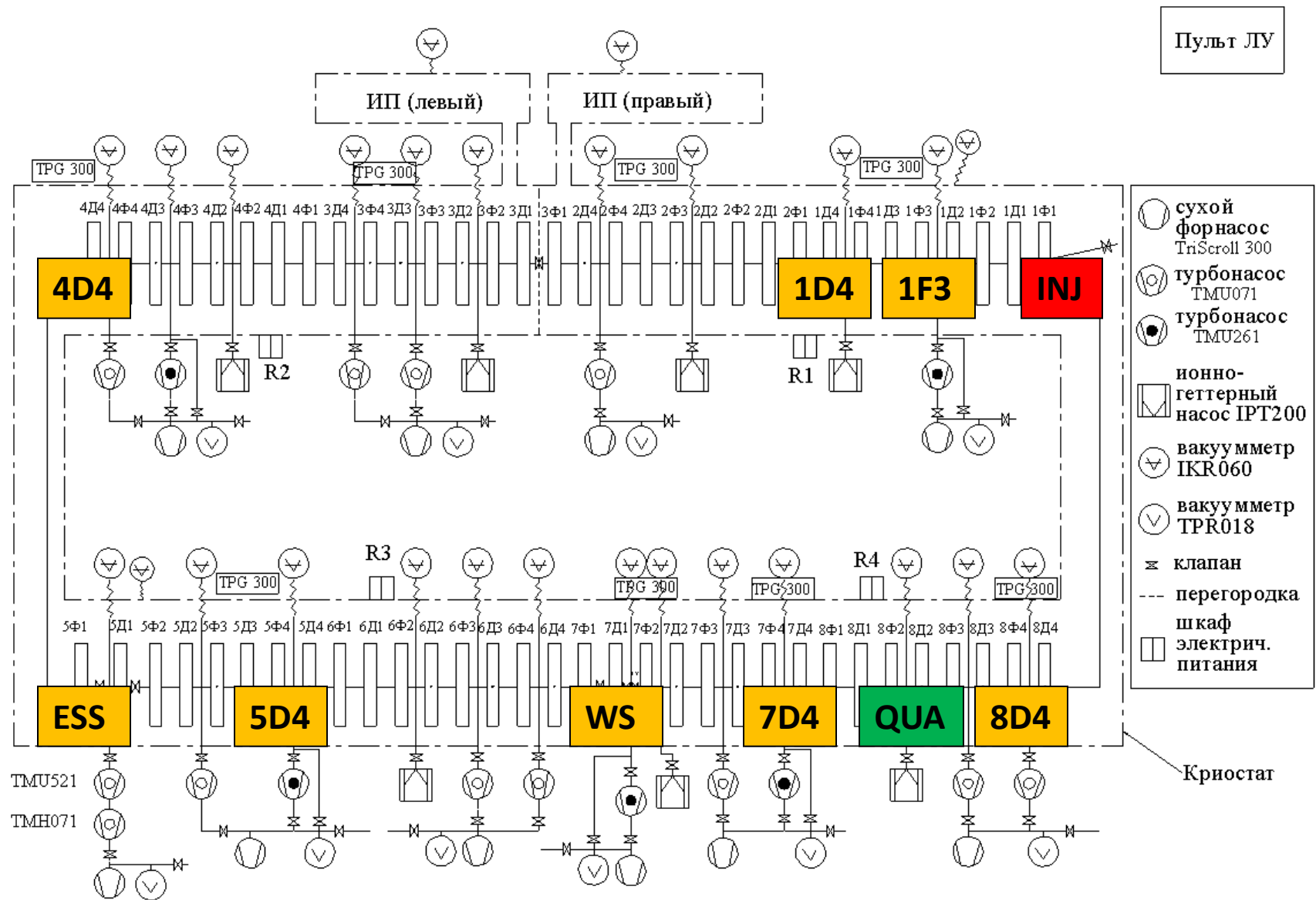
NICA Collider
(1-4,5 GeV/u, C~500 m)

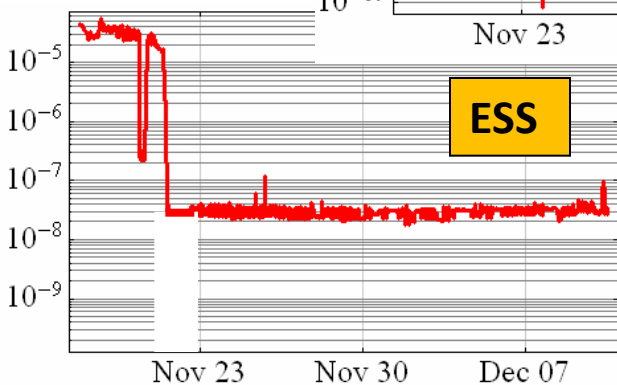
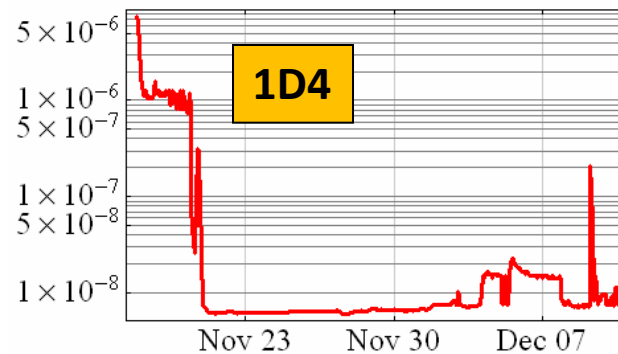
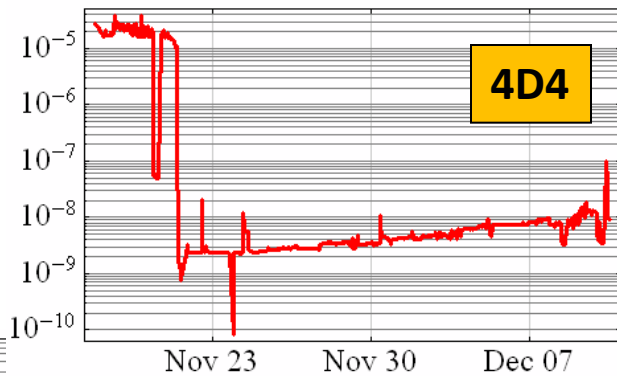
HV
e-cooler

Multi-Purpose
Detector (MPD)

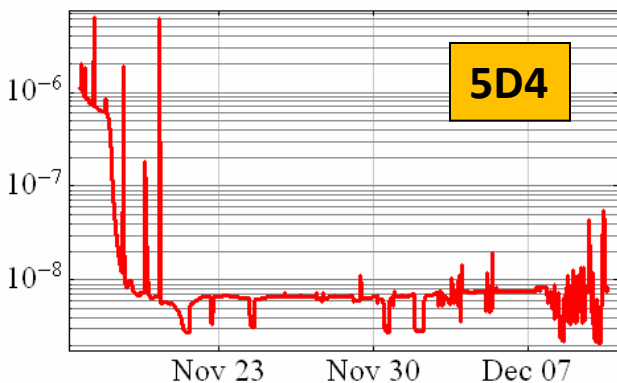
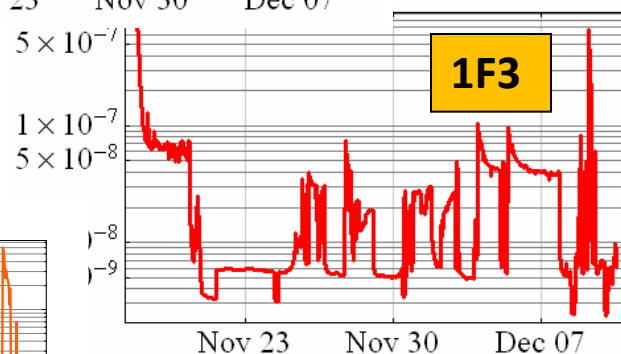
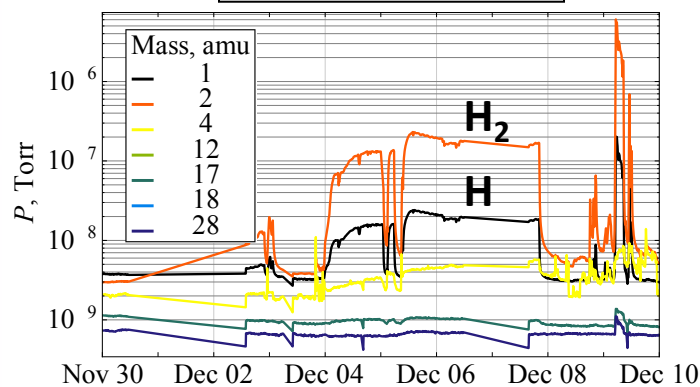


Upgrade of Nuclotron vacuum system

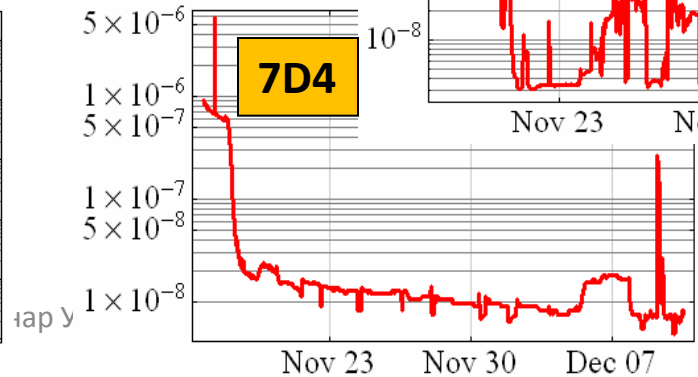
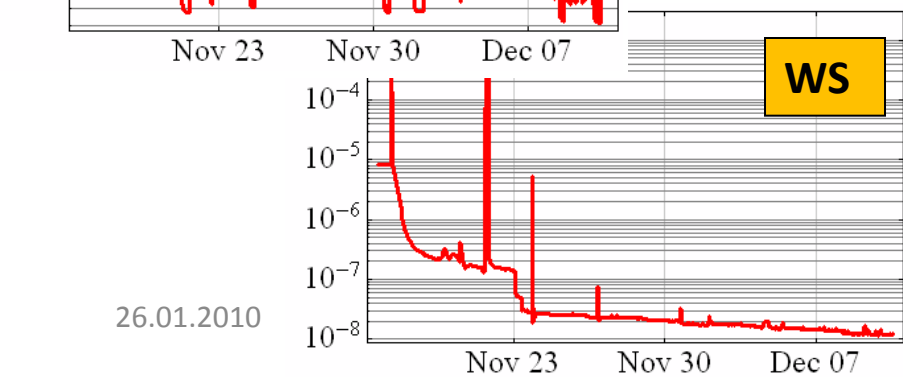
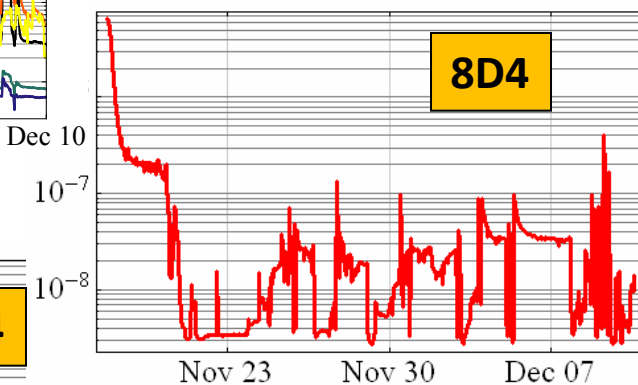




Mass analyzer
QUADERA



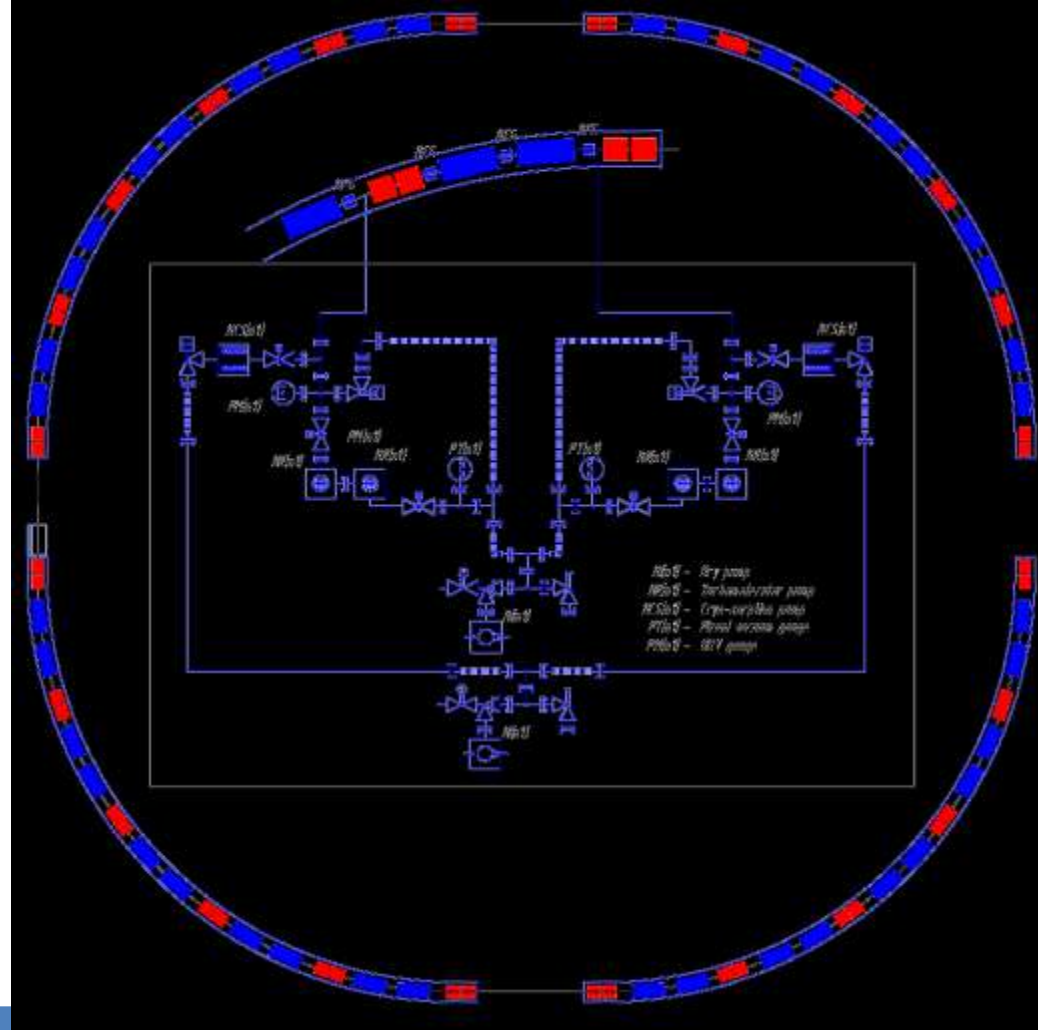
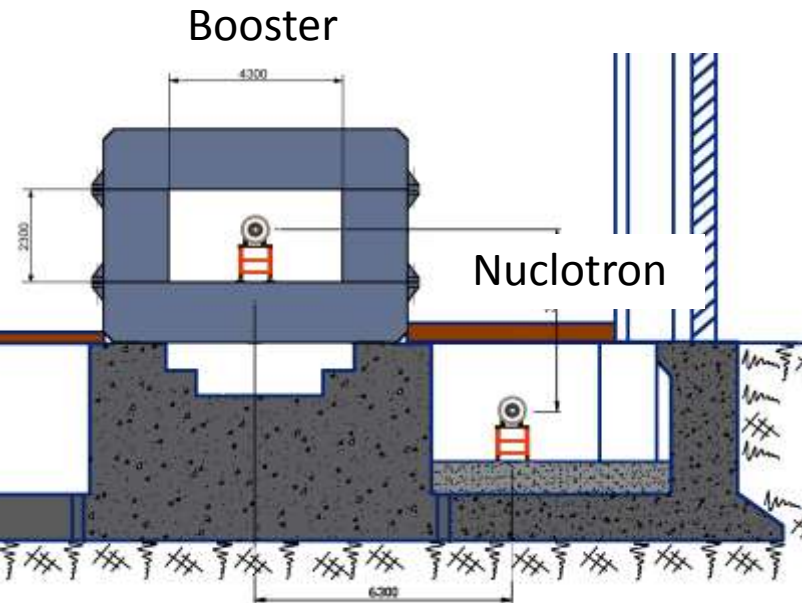
INJECTION



QUADERA

8D2 23

Booster optics structure



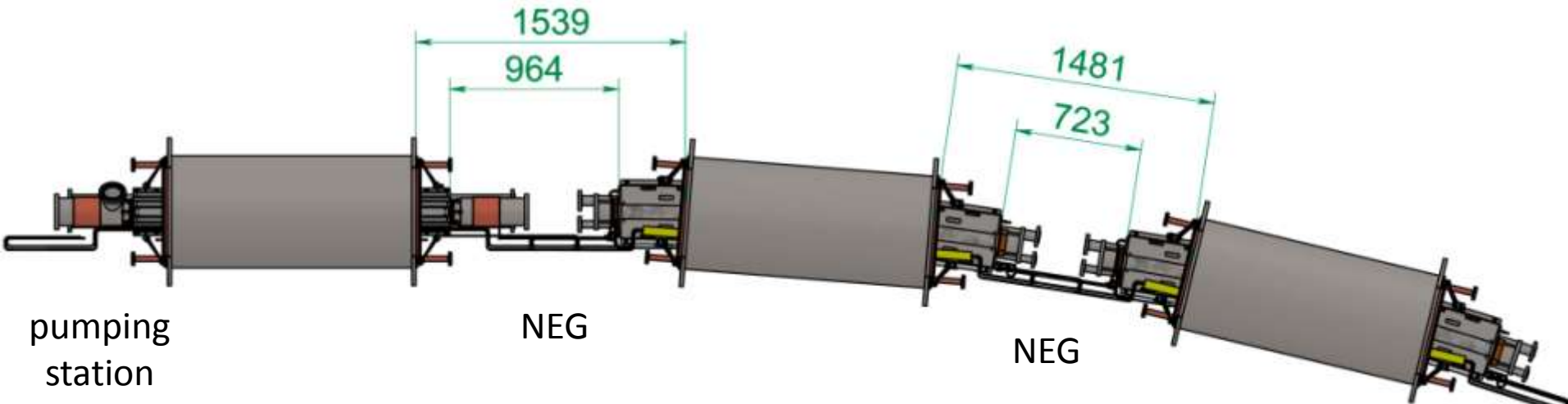
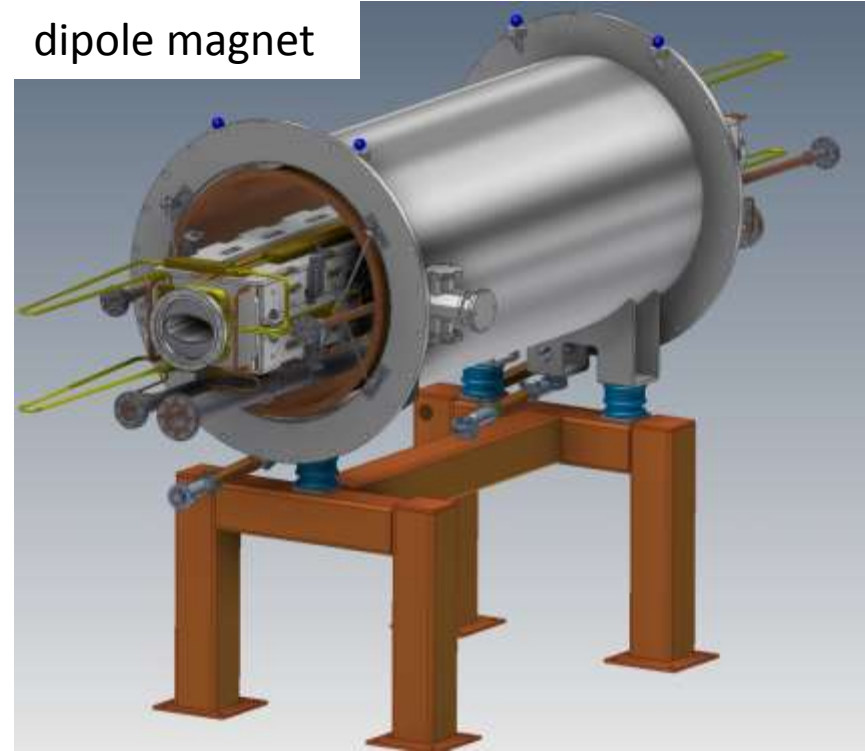
		quantities	cold mass (kg)	beam pipe length (m)
Dipole magnet		40	1000	2,7
Double quadrupole magnet	one corrector	16	365	2,45
	three correctors	8	470	2,45

Booster magnet connection

double quadrupole magnet



dipole magnet



NEG pumps at cryogenic temperature

NEG still have good pumping speed for H₂ close to liquid nitrogen temperature

3444 Bofflito *et al.*: Gettering in cryogenic applications

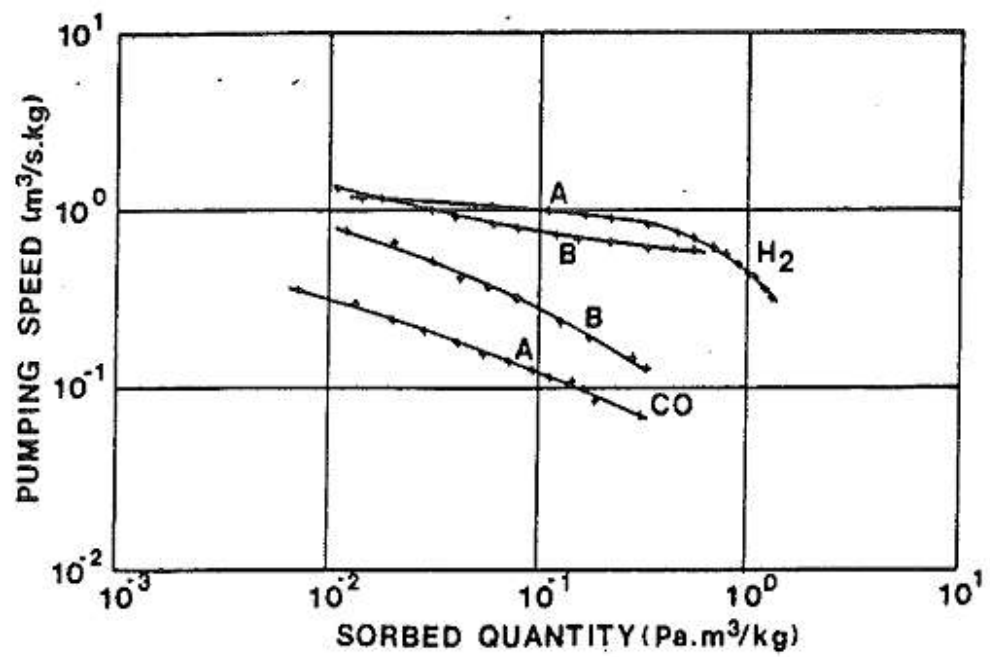
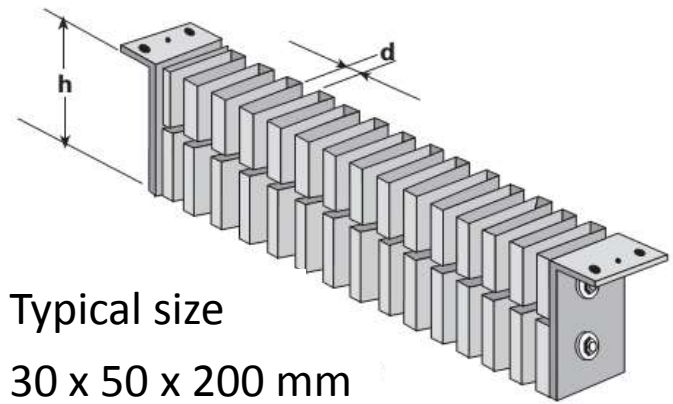


FIG. 3. H₂ and CO sorption characteristics for the Zr-V-Fe getter alloy at (A) room and (B) LN₂ temperature, after activation at 400 °C for 30 min.

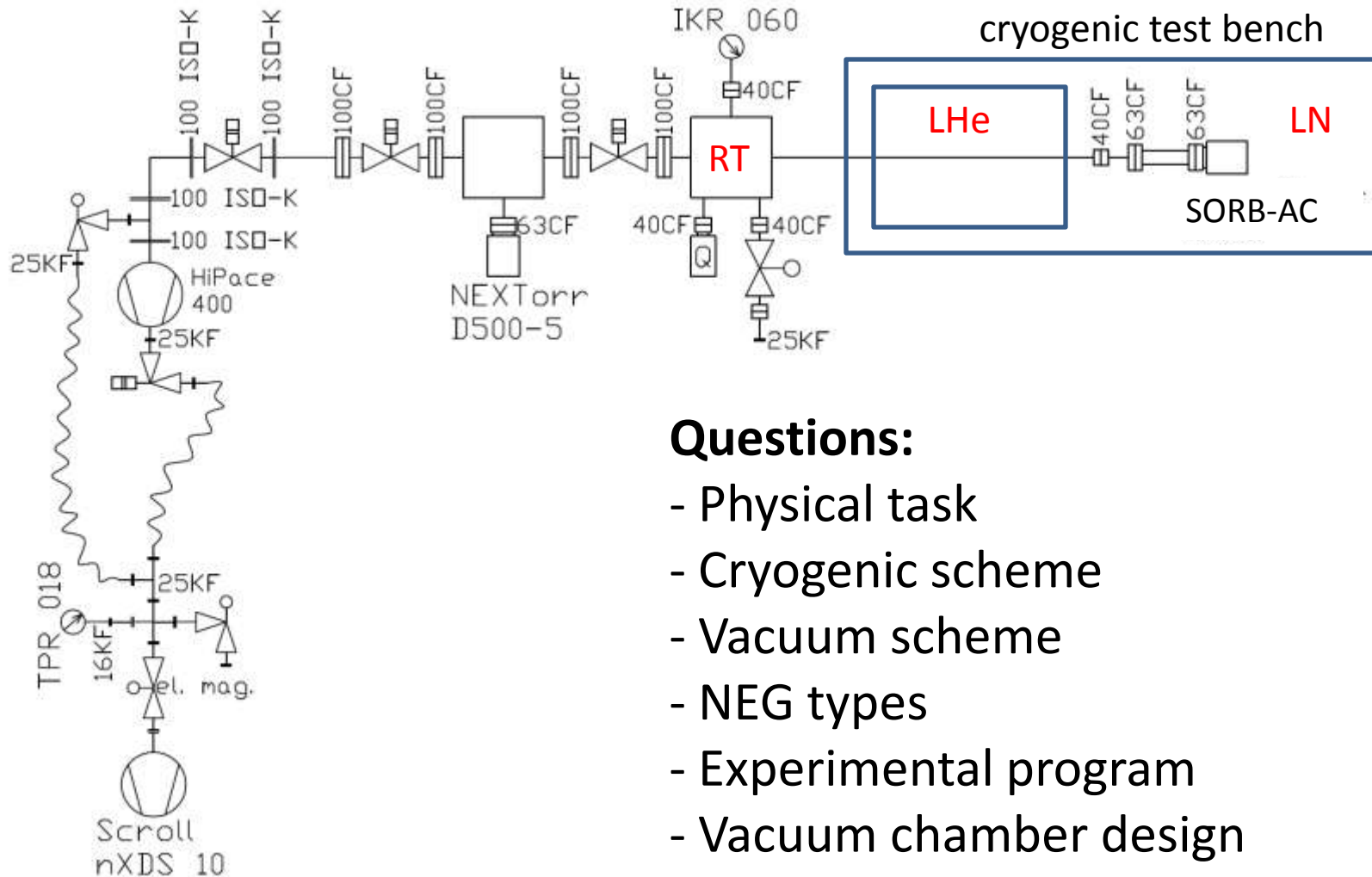
SORB-AC® Getter
Wafer Modules and Panels



Typical size
30 x 50 x 200 mm

Vacuum scheme for NEG test under cryogenic temperatures

in collaboration with SAES Group



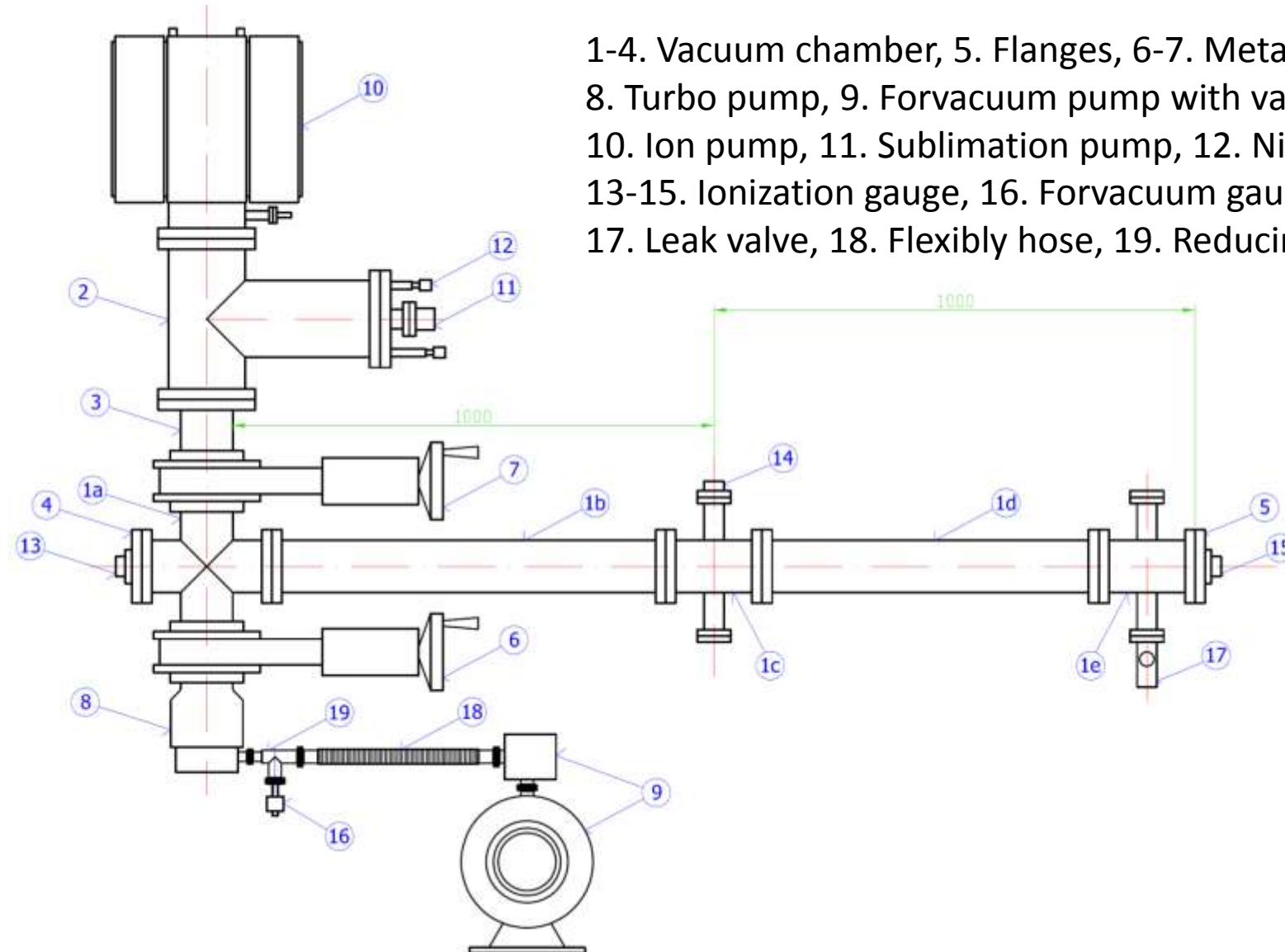
Questions:

- Physical task
- Cryogenic scheme
- Vacuum scheme
- NEG types
- Experimental program
- Vacuum chamber design

Warm test bench at JINR

in collaboration with Vakuum Praha (Czech Republic)
and ФГУП СКБ ИРЭ РАН (г.Фрязино, МО)

1-4. Vacuum chamber, 5. Flanges, 6-7. Metal valve, 8. Turbo pump, 9. Forvacuum pump with valve, 10. Ion pump, 11. Sublimation pump, 12. Nitrogen trap, 13-15. Ionization gauge, 16. Forvacuum gauge, 17. Leak valve, 18. Flexibly hose, 19. Reducing T-piece



Backing of Test Bench at JINR

After baking during 30 hours with 280°C
vacuum was reached value about **10^{-11} Torr !**

