

# Experimental Test of a Prototype System for Active Damping of the E-P Instability at the LANL PSR

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# Collaborators

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# **Additional References**

- MOPAS050 Active Damping of the e-p Instability at the LANL PSR - McCrady et. al.
- MOPAS080 A Digital Ring Transverse Feedback Low-Level RF Control System – Polisetti et. al.





# Background

- PSR (Proton Storage Ring) has a well-studied e-p instability. This instability is broadband on the order of 100 MHz in bandwidth!
- The SNS and PSR rings are similar, so a study of PSR instability is important for the upgrade of SNS.
- Test was limited in bandwidth (50-250 MHz) and 7 uC/pulse to stay within the bandwidth of the power amplifiers.
- Deployed two used amplifiers from ENI 1-400 MHz, 100 Watt CW.
- Designed and built 4 LLRF chassis.
- We conducted a proof of principle experiment shows broadband feedback works for e-p instability in a long bunch machine.





#### **Electron Cloud**



# PSR Application and Physics Results







#### **Frequency spectra vs Turn # for two intensities**







### **Grow/Damp with Comb Filter – 7 uC/pulse**

Grow/Damp experiment not possible without comb filter



Damp rate=-0.01442 usecs<sup>-1</sup>

#### Growth rate=0.0213 usec<sup>-1</sup>

R. Macek





- Data below taken during run with one 2-turn comb filter, buncher at 7203 V (part way between thresholds with damper on and off)
- Beam intensity 7.2 μC/pulse, stored for extra 400 μs.







Vertical Difference





Feedback Off

Feedback On

S. Breitzmann







Vertical difference for one turn near end of store





#### **SNS** Instability



### S. Cousineau





# Analog Hardware Design





#### **Block Diagram**



#### pickup

- Delay line is adjustable for differing configurations
- •4 different comb filters for single and dual turn.
- •High impedance pickoff measures signals from the amplifiers





#### **Optical Delay Chassis**



#### **ENI Amplifier Measurement**

- Uses 2 ENI amplifiers 100 Watts 1-400 MHz
- The output of each ENI goes through a High-Z pickoff to measure output signals and to loads.







#### **Comb Filters**

- Uses 2 Miteq Fiber
  transmitters/receivers
- An option to use a single turn or two turn notch spacing is available
- Fine tuning available via ARRA trombones





Long leg tuned to notch spacing accurate to better than 3 psec on average across the band.





#### Notch Depths of Filter #1 and Filter #2

Filter #1

Filter #2



#### Measured VNWA Notch Depths of Filter #1 and Filter #2 in Series









-Signal lines from electrodes

- Main LLRF chassis
- High Z pickoff
- LLRF pre-amplifiers
- Fiber Delay Line

Comb Filters

**Binary Adjustable Delay** 





# **Digital Subsystem Implementation**



 The digital subsystem includes synchronized ADCs, FPGAs, and DACs





## **Analog-to-Digital Converters**

## Two parallel SMT384 ADC Modules

- Quad-channel, 125 MSPS, 14-bit ADC (11.3 ENOB)
- Data interleaving on FPGAs provides a single 500 MSPS, 14bit data stream per channel



\* Figure from Sundance DSP, Inc.





### **Data Interleaving and Storage FPGAs**

## Two parallel SMT 398 FPGA Modules

- Contain Xilinx Virtex-II Pro FPGA
- Store up to 8M 16-bit samples per channel
- Interleave data for further processing



\* Figure from Sundance DSP, Inc.





# **Data Processing FPGA**

## SMT 368 FPGA Module

- Contains Virtex-4 FPGA (500 MHz)
- Stores up to 4M 16-bit samples
- Processes digital data and sends outputs to DAC



Figure from Sundance DSP, Inc.





### **Digital-to-Analog Converters**

### SMT 350 DAC Module

- SMT350 Dual-Channel 500 MSPS, 16-bit DAC
- Accepts data at 125 MSPS and interpolates by 4
- Later upgrade to a true 500 MSPS, 14-bit DAC
- Outputs sent to power amplifiers



\* Figure from Sundance DSP, Inc.





## **Mixed Signal System Realization**



 The offset multipliers and subtraction can be implemented using analog circuits

- + Reduces system complexity
- + May improve accuracy of voltage difference
- Introduces additional distortion from analog components
- Reduces available diagnostic information





## **Mixed Signal System**



- Implementing the offset multipliers and subtraction using analog circuits
  - + Eliminates one of the ADCs and one of the FPGAs modules
  - Reduces available diagnostic information, since individual voltages are no longer available
    Low-Pass
    Filter
    Quad Channel
    SMT 398 with Virtex
    FPGA and 16MB S



ADC 1 Oak Ridge National Laboratory U. S. Department of Energy

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## **Programmable Delay Module**



## Program

Prog

)ela

- Programmable delay module controls the overall system delay: Delay = FIFO length × Clock period
- delay: Delay = FIFO length × Clock period Gain Multiplier
   Implemented using FIFO16 module Output (V<sub>out</sub>)
   Additional fine-tuning of the delay is required Clock





# **Comb Filters**



The comb filters dampen the ring frequency harmonics to save power

- Comb filter output:  $y[n] = x[n] x[n t_n]$
- Comb filter frequency response:  $Y(\omega) = X(\omega)[1 e^{-i\omega t_n}]$
- $-t_n$  is set as a multiple of the ring frequency ( $\approx$  1 µsec)

Implemented using FIFO16 and DSP48 modules





## **FIR Filters**



• The FIR filters compute:

$$y[n] = \sum_{k=0}^{M} b_k x[n-k]$$

- Serve as equalizers that correct for dispersion in analog components
  - Electrodes have non-uniform gain verses frequency
  - Amplifiers have phase dispersion
  - Analog hybrids, low-pass filters, and cables have magnitude and phase dispersion





# **Cable Magnitude Dispersion**

• The cables have magnitude and phase dispersion due to copper and dielectric losses



Characteristics of the measurement cable (in dB) vs. frequency OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



## **Cable Phase Dispersion**

• The cables have magnitude and phase dispersion due to copper and dielectric losses





Phase Response of Ideal cable vs. Actual cable OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



# **Reducing Cable Dispersion**

- Find the frequency (S<sub>21</sub>) characteristics of the cable using a vector network analyzer
- Determine the equalizer characteristics necessary to compensate for magnitude and phase dispersion

$$G(\omega) = \frac{H2(\omega)}{S_{21}(\omega) * e^{i\omega T_d}} \qquad H2(\omega) = \cos^4\left(\frac{\pi\omega}{2\omega_c}\right)$$



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# **Reducing Cable Dispersion**

- Determine the number of taps and tap values for the equalizer
- Run the equalizer in series with the cable to reduce dispersion



Comparison of the time-domain responses of an ideal, actual, and de-embedded cable





# **Future Work**

- Optimize signal levels to stay out of compression
- Optimize signal levels to each hardware component
  - Amplifiers
  - Delay Line
  - Overall system gain
- Optimize growth rate/damp rate for production quality beams.
- Develop mixed signal (analog and digital) transverse feedback system.





# Conclusion

- 15-30% increase in threshold with feedback, depending on beam conditions
- Begin to see instability in the horizontal plane
- We were able to over-damp the beam after optimizing settings, and had to reduce power.
- Production runs show issues with hardware compression and loop gain.
- E-P instability can be damped using wideband feedback.
- Damping varies with real part of signal.
  Dispersion makes us lose about 30% of our power





## **Special Thanks**

to the SNS team who went the extra mile to help pull it all the hardware together



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