FITTING THE FULLY COUPLED ORM FOR THE FERMILAB BOOSTER*

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Abstract

The orbit response matrix (ORM) method [1] is applied to model the Fermilab Booster with parameters such as the BPM gains and rolls, and parameters in the lattice model, including the gradient errors and magnets rolls. We found that the gradients and rolls of the adjacent combinedfunction magnets were deeply correlated, preventing full determination of the model parameters. Suitable constraints of the parameters were introduced to guarantee an unique, equivalent solution. Simulations show that such solution preserves proper combinations of the adjacent parameters. The result shows that the gradient errors of combined-function magnets are within design limits.

INTRODUCTION

The Fermilab Booster is a fast-cycling synchrotron which accelerates proton beams from 400 MeV to 8 GeV. Its performance is critical for many Fermilab experiments. Among the many efforts to improve the Booster, we were trying to build a realistic lattice model with beam-based measurements, such as the orbit response matrix (ORM) method.

The ORM method, successfully applied to many electron storage rings, is a powerful tool for accelerator lattice modeling. However its application to fast-ramping, proton synchrotrons such as the Fermilab Booster is more difficult because of the reduced orbit stability and precision of orbit measurements. In our study we found another difficulty is the correlation between the model parameters of the adjacent magnets. Suitable constraints have to used to obtain an unique solution.

The Booster has 24 identical periods. Each period has four combined function magnets and two straight sections with a layout of {O FU DU OOO DD FD O}, where OOO stands for the long straight section, O for a half of the short straight section, FU for upstream focusing magnet and DU for upstream defocussing magnet, etc. In each straight section there are one BPM, which measures both horizontal and vertical orbits, one horizontal trim (a steering dipole magnet, or a kicker) and one vertical trim. Note that there is only one BPM in every two magnet elements. The full ORM is 96×96 in dimension.

THE FITTING MODEL AND ALGORITHM

The model ORM is computed with the transfer matrix of the lattice model [2]. Suppose **T** is the one-turn transfer matrix at a trim and **I** is a 4×4 identify matrix, the orbit deviation x_0 and z_0 at the trim's location due to an horizontal kick θ_x of the trim can be found by $(x_0, x'_0, z_0, z'_0)^T =$ $(\mathbf{T} - \mathbf{I})^{-1}(0, -\theta_x, 0, 0)^T$. The ORM elements can then be calculated using the transfer matrices between the trim and BPMs. The same can be done with vertical trims.

The measured ORM needs to be corrected to take into account the imperfections of the measurement systems, e.g. BPMs and trims. The correction parameters include the gains and rolls of BPMs, the gains and rolls of both horizontal and vertical trims, the momentum deviation due to horizontal trims. The additional horizontal orbit changes caused by the momentum deviation are subtracted from the measured orbit to get the correct ORM. The parameters in the lattice model are the gradient errors and rolls of all 96 combined-function magnets. There are a total of 576 fitting parameters.

The difference between the model and measured ORM is characterized by the residual vector \mathbf{r} which is a column vector containing all elements of $(M_{ij}^{\text{act}} - M_{ij}^{\text{model}})/\sigma_{ij}$ and the objective function $\chi^2 = \mathbf{r}^T \mathbf{r}$. The betatron tunes are included by extending the residual vector. The dispersion functions can also be included. The fitting parameters are put in a column vector α . The Levenberg-Marquardt method [4] is used to solve the nonlinear least-square problem of $f(\alpha) = \chi^2$. For each iteration the Jacobian matrix $\mathbf{J} = \frac{\partial \mathbf{r}}{\partial \alpha}$ is computed and the advance of α is found by solving the following equation

$$(\mathbf{J}^T \mathbf{J} + \lambda \mathbf{I}) \Delta \alpha = -\mathbf{J}^T \mathbf{r}$$
(1)

instead of solving $\mathbf{J}\Delta\alpha = -\mathbf{r}$ as suggested in Ref. [1], where **I** is the identity matrix and λ is an adjustable parameter. This approach is more robust. It is also faster because the matrix on the left side of Eq. 1 has a smaller size than **J**. The error bars of the fitting parameters are estimated by computing the covariance matrix $\mathbf{C} = \mathbf{J}^T \mathbf{J}$ and then $\sigma_i = \sqrt{C_{ii}}$ for the *i*'th parameter.

The above fitting scheme is correct in principle but would not work even for simulated noise-free ORM because the Fermilab Booster beam detection system (1 BPM in every 2 magnet elements) is not sufficient for an unique solution. In one simulation, the "measured" ORM is generated by setting the gradient error of one magnet to $\Delta K_1 =$ 0.002 m⁻², or 4% of the nominal quadrupole gradient. The algorithm reduces χ^2 down to zero efficiently but does not converge to the expected solution. The gradients of the

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Figure 1: The correlation coefficients for model parameters of neighboring magnets. (a) The gradient errors. (b) The magnet rolls.

immediate neighboring magnets also pop up and make up part of the contribution to χ^2 . The magnet rolls show similar behavior.

Such observations suggest correlations between model parameters of the adjacent magnets, i.e., changes of these parameters perturb the ORM in similar patterns. The correlation are illustrated in Fig. 1, which shows the correlation coefficients between the columns of the Jacobian matrix.

The gradients of neighboring focusing magnets (FD -FU), the rolls of neighboring upstream magnets (FU-DU) or downstream magnets (DD-FD) have the deepest correlation. The correlation indicates that the ORM fitting problem is deficient and the model parameters cannot be determined individually. The solution is not well-constrained in some directions and tends to have big error bars.

Although the correlation prevents the full determination of the real Booster lattice from the ORM data, it is still desirable to have a definite solution of the fitting problem, which can be obtained by imposing proper constraints. For example, we may require a solution with minimum Euclidean norm. A more efficient way is to limit the drifting along the un-constrained directions by minimizing certain combinations of the correlated parameters. These combinations include: (1) $(\theta(FU, i) + \theta(DU, i))/\sigma_{\theta}$, rolls of upstream magnets; (2) $(\theta(DD, i) + \theta(FD, i))/\sigma_{\theta}$, rolls of downstream magnets; (3) $(\theta(\text{FD}, i) - \theta(\text{FU}, i+1))/\sigma_{\theta}$, rolls of neighboring focusing magnets; (4) $(\Delta K_1(\text{FD}, i) \Delta K_1(\mathrm{FU}, i+1))/\sigma_{K_1}$, quads of neighboring focusing magnets; (5) $(\Delta K_1(FU, i) - \Delta K_1(DU, i)) / \sigma_{K_1}$, quads of upstream magnets; (6) $(\Delta K_1(DD, i) - \Delta K_1(FD, i)) / \sigma_{K_1}$, quads of downstream magnets, where i denotes the period number, $\sigma_{K_1} = 0.00055 \text{ m}^{-2}$ and $\sigma_{\theta} = 5 \text{ mrad are char-}$ acteristic values to scale the parameters.

A comprehensive simulation was used to check the fitting schemes. The parameters were set to random values within a reasonable scope to generate the ORM. The constrained fitting converges to an unique solution and reduces χ^2 from 32 to 0.01. The solution is much less sensitive to random noises. Assuming error sigma of matrix elements of 1.0 m/rad, the average error sigmas of gradients are 0.0042 m^{-2} without constraints and $2.5 \times 10^{-4} \text{ m}^{-2}$ with constraints, while for rolls they are 78.7 mrad and 1.7 mrad, respectively. The constrained directions are faithfully recovered by both methods, as shown in Fig. 2.

Figure 2: Comparisons of the fitting results with ("pair") or without ("none") constraints to the expected solution ("act"). (a) $\Delta K_1(\text{FD}) + \Delta K_1(\text{FU})$, (b) $\theta(\text{FU}) - \theta(\text{DU})$.

APPLICATION TO EXPERIMENTAL DATA

Each ORM element is measured by applying different kick angles and measuring the beam orbits. The slope of orbit – kick angle is obtained by linear fitting and is turned to ORM element according to magnet specifications. The uncertainty levels of the elements are estimated using the residual χ^2 of the linear fittings. The maximum kick angles are 0.58 mrad for horizontal trims and 0.34 mrad for vertical trims, resulting in maximum orbit changes of 8.0 mm and 3.0 mm, respectively. The average error sigma's are 0.33m/rad for M_{xx} , 0.54m/rad for M_{xz} , 0.07m/rad for \mathbf{M}_{zx} and 0.15m/rad for \mathbf{M}_{zz} . The vertical blocks have better precision because the vertical orbit has less cycleto-cycle variations than the horizontal orbit. The betatron tunes are measured by BPM turn-by-turn data. The dispersion functions are also measured. They are both included in the fitting by extending the residual vector. The dispersion terms are $(D_i^{\text{meas}} - D_i^{\text{model}})/(b_{h,i}\sigma_{D,i})$, where $b_{h,i}$ is horizontal BPM gain and $\sigma_{D,i}$ is error sigma for dispersion measurements. The inclusion of dispersion function would de-couple the BPM gains and kicker gains [1].

The Booster model has all up-to-date information, including the experimental settings of the trim quadrupoles and skew quadrupoles. The ORM data are taken at 0.9 ms after injection, corresponding to kinetic energy 0.41 GeV. The constrained fitting is applied, which reduces the normalized χ^2 from 76.0 to 2.5.

The χ^2 contribution of each type of parameters is evaluated by setting all parameters to their fitted values except for that type, which are set to the default. We found that the major contributors are magnet rolls, kick-induced momentum deviation, vertical BPM gains and the gradient errors. The model ORMs and dispersion functions gain good agreements with their measured counterparts through the fitting process. Figures 3 and 4 compare the model result with the measured data before and after the ORM modeling for the dispersion function and the ORM row for one BPM.

The horizontal kicks cause big changes of momentum deviation because of Booster's radial orbit control mechanism, which always tries to fix the horizontal orbit at L20 by introducing momentum changes. Suppose the orbit is indeed fixed at L20, the momentum deviation due to unit kick angle of the *j*'th trim is expected to be



Figure 3: Comparison of dispersion functions before and after the fitting.



Figure 4: Comparing model and measured ORM elements for BPM HS1 before and after fitting. The deviations before fitting are mostly from kick-induced momentum deviation.

 $-M_{xx}(L20, j)/D_x(L20)$. They are compared in Fig. 5.

The correction parameters found by the fitting can be used to calibrate the BPMs or trims. Five special BPMs are found to have large gains and have been fixed. The other BPM gains and trim gains have rms deviations of 5%.

The fitting solution provides a model that is equivalent to the real Booster in the sense of giving the same orbit response properties. Since the ORM is essentially specified by the linear lattice functions, i.e., the beta functions and betatron phase advances, the fitted model should produce the same lattice functions as the real Booster. Such information can be used in machine operations, e.g., to find suitable ratios of trim strengths to create local orbit bumps.

The fitted constrained combinations of the model parameters should approximate the real Booster. The average gradient errors of the focusing magnet in most periods are below $0.0004m^{-2}$, i.e., 0.8% of the nominal values. Such deviations are within the design tolerance [3]. The origin of the errors could be the focusing effects of sextupole components of the magnets. To verify that the sums of neighboring focusing magnets are predictable, we set two trim quads between them to zeros in the model before fitting.



Figure 5: The kick-induced momentum deviation per unit kick angle compared to the orbit response at L20.



Figure 6: The changes of ΔK_1 of adjacent focusing magnets if we turn off two trim quads in the model. The integrated quadrupole components of the two quads are accounted for by body quads in the solution.

The solution reflects the changes as shown in Fig. 6.

We also conducted un-coupled fitting which exclude the off-diagonal blocks of the ORM and all roll parameters. This simpler fitting scheme found the same solution for the related parameters, i.e., the gains, kick-induced momentum deviation and gradient errors because the rolls have only second-order effects on the un-coupled ORM.

CONCLUSION

In this study we measured the fully-coupled orbit response matrix of the Fermi Booster and fit it to the lattice model. The fitting scheme was not able to uniquely determine the lattice parameters because of insufficient information and poor BPM resolution. By imposing constraints on correlations between fitting parameters, we can obtained an unique solution with all correction parameters and an equivalent model to the physical Booster. From the hardware point of view, these constraints are reasonable inputs. The study confirms the gradient errors of the focusing magnets are within design limits.

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