

# FEM Simulations for a High Heat Load Mirror

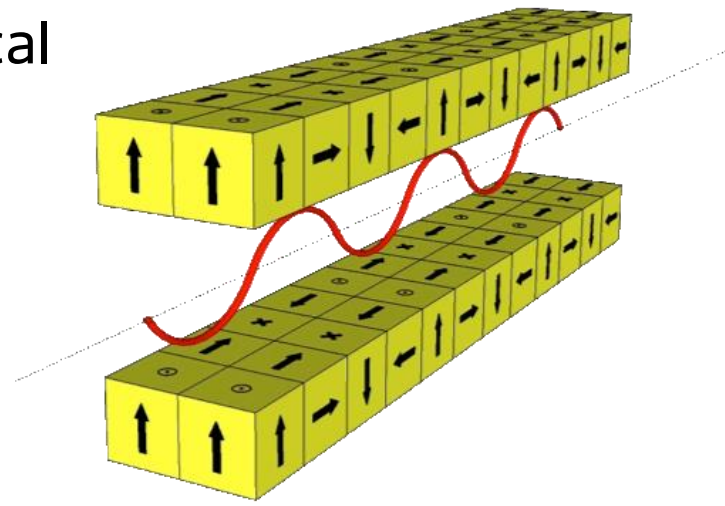
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## Heat Load

### Variable heat loads with APPLE II undulator

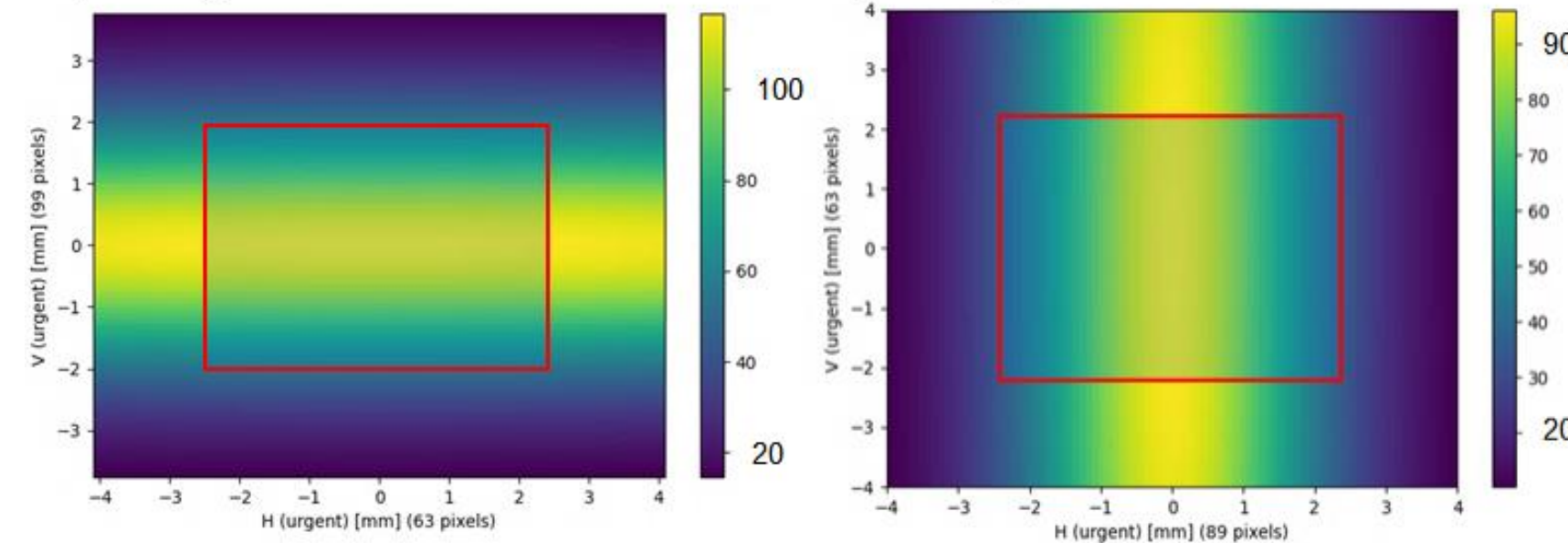
APPLE II allows to use the polarization modes linear and circular and all their permutations:

- Highest power for linear horizontal polarization => 2.1 kW.
- High power density for linear vertical polarization => 1.5 kW.
- Lower power for circular polarization => 300 W
- Main power contribution by photons between 8-40 keV => attenuation length



Schematic of APPLE II undulator magnetic arrays

a) Integrated Power: 3902 W b) Integrated Power: 3211 W



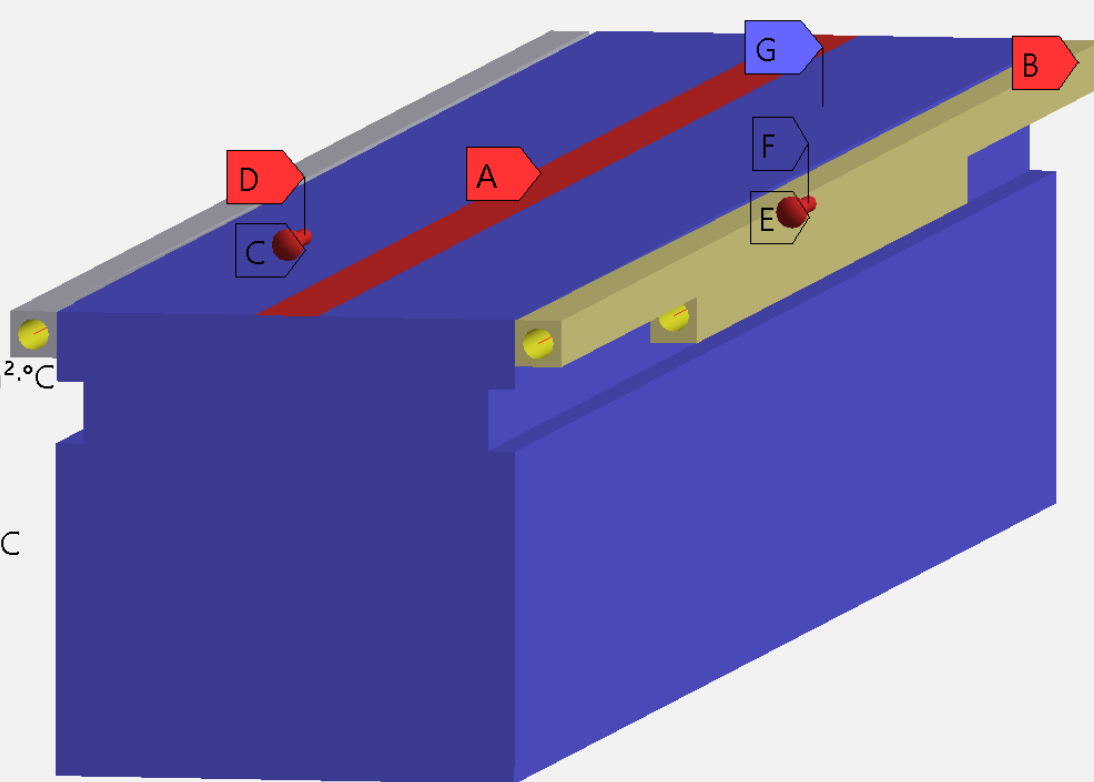
Power density [W/mm<sup>2</sup>] distributions of a) linear horizontal and b) linear vertical polarization. Mirror footprint is shown in red.

## Comparison of Notched and Double Bracket Design

### Steady State Thermal setup.

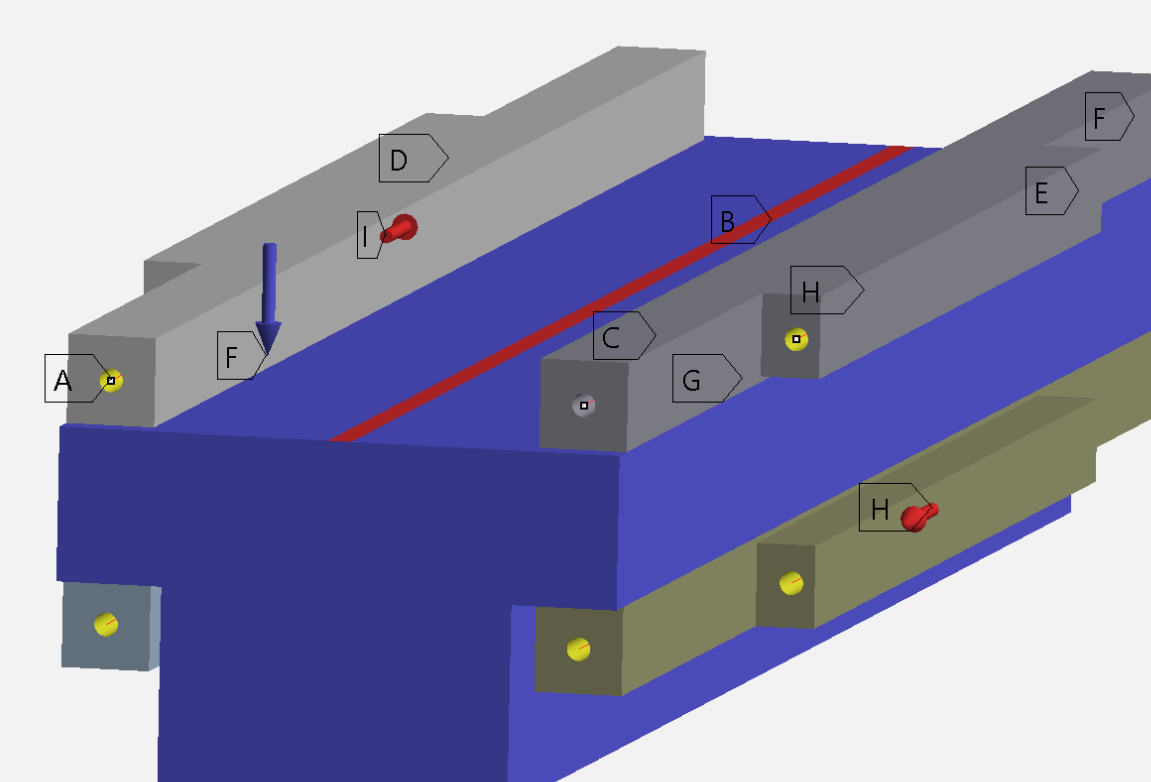
C: Steady-State Thermal  
Steady-State Thermal  
Time: 1, s  
20.10.2023 18:06

- A Imported Heat Flux
- B Temperature: 20, °C
- C Conv\_Vert: 22, °C, 20803 W/m<sup>2</sup>\*°C
- D Kanaele\_Vert
- E MF\_Vert: 8,3333e-002 kg/s
- F Conv\_Hor: 22, °C, 662, W/m<sup>2</sup>\*°C
- G Kanaele\_Hor
- H MF\_Hor: 3,32e-003 kg/s
- I Radiation: 22, °C, 1,



E: LinVert Thermal  
Steady-State Thermal  
Time: 1, s  
Items: 10 of 15 indicated  
20.10.2023 19:00

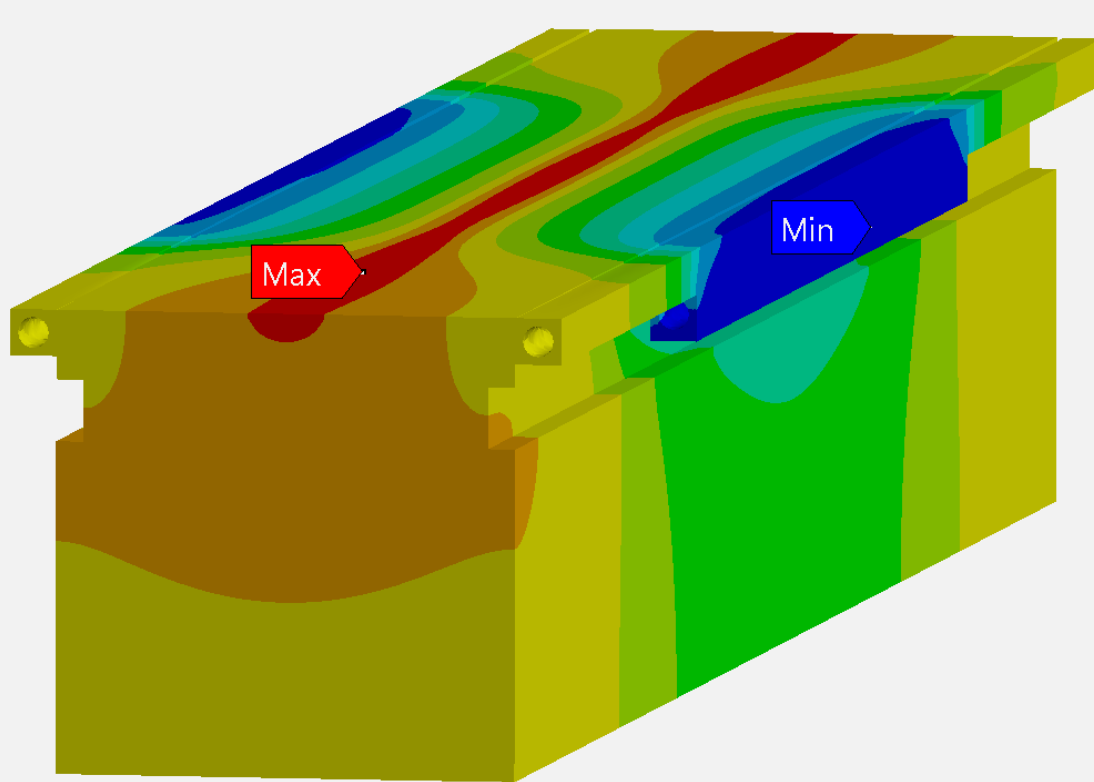
- A Temperature: 16, °C
- B Imported Heat Flux
- C Coupling 2: Temperature (TEMP)
- D Coupling 2: Temperature (TEMP)
- E Coupling 3: Temperature (TEMP)
- F Coupling 4: Temperature (TEMP)
- G Convection\_Long: 22, °C, 660, W/m<sup>2</sup>\*°C
- H WaterBeam\_Long
- I Convection\_Short: 22, °C, 27000 W/m<sup>2</sup>\*°C
- J WaterBeam\_Short



### Steady State Thermal result.

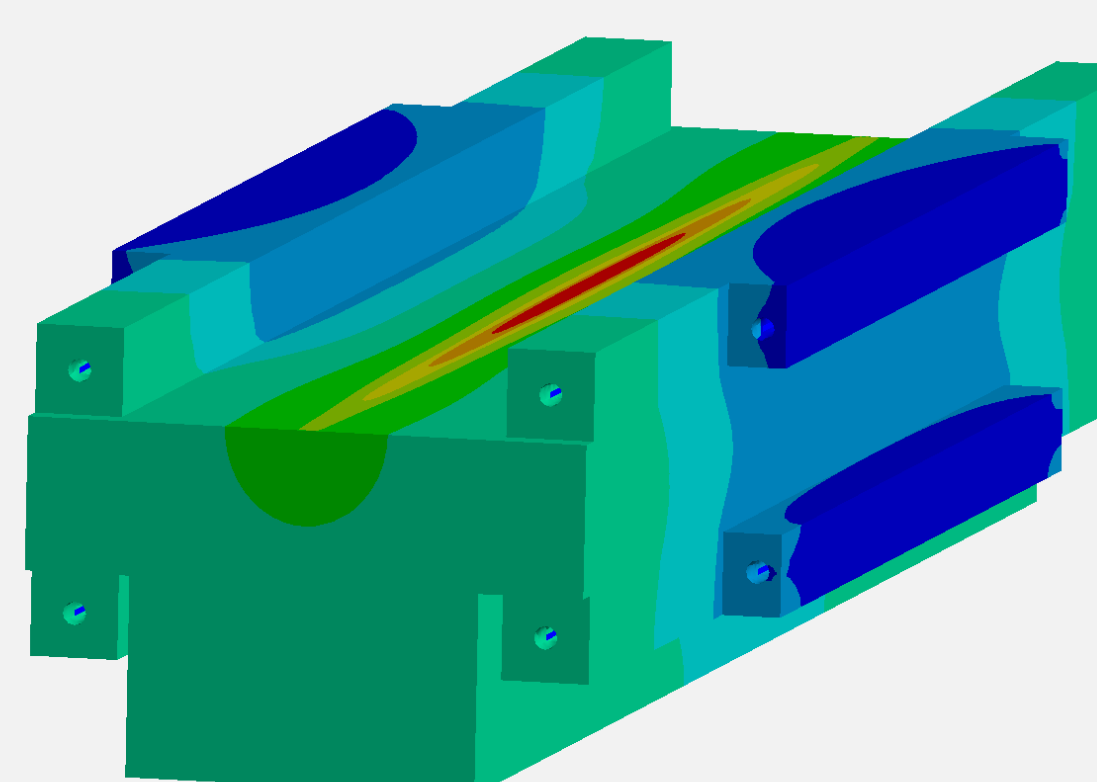
C: Steady-State Thermal  
Temperature  
Type: Temperature  
Unit: °C  
Time: 1 s  
20.10.2023 18:05

- 170,75 Max
- 155,12
- 139,5
- 123,87
- 108,24
- 92,609
- 76,981
- 61,352
- 45,723
- 30,094 Min

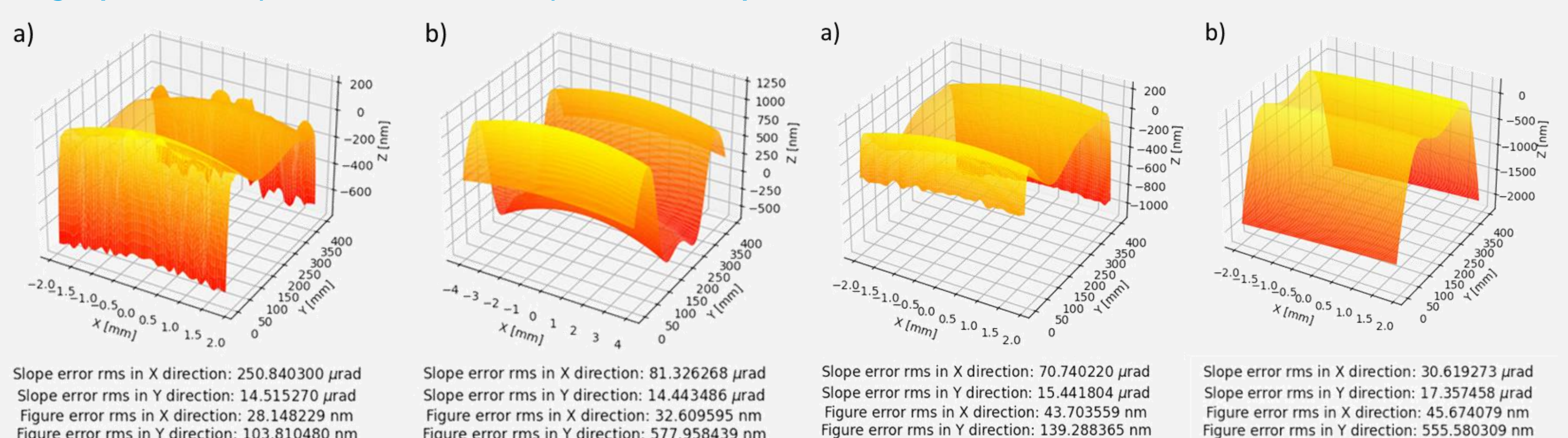


E: LinVert Thermal  
Temp - Water  
Type: Temperature  
Unit: °C  
Time: 1 s  
20.10.2023 19:07

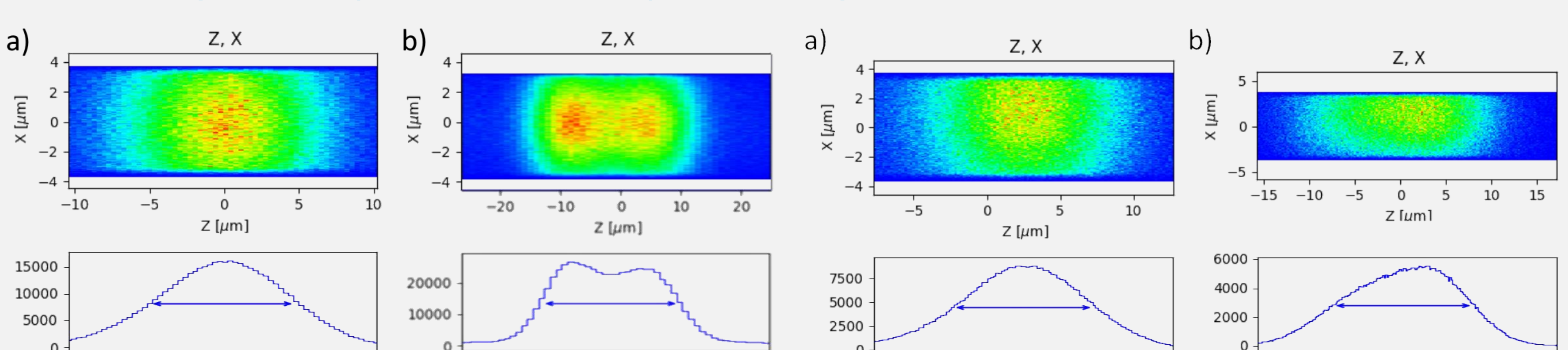
- 80,13 Max
- 73,005
- 65,879
- 58,754
- 51,628
- 44,502
- 37,377
- 30,251
- 23,126
- 16 Min



### Height profiles for a) linear horizontal and b) linear vertical polarization.



### Beamline focus profiles for a) linear horizontal and b) linear vertical polarization.



## Conclusions

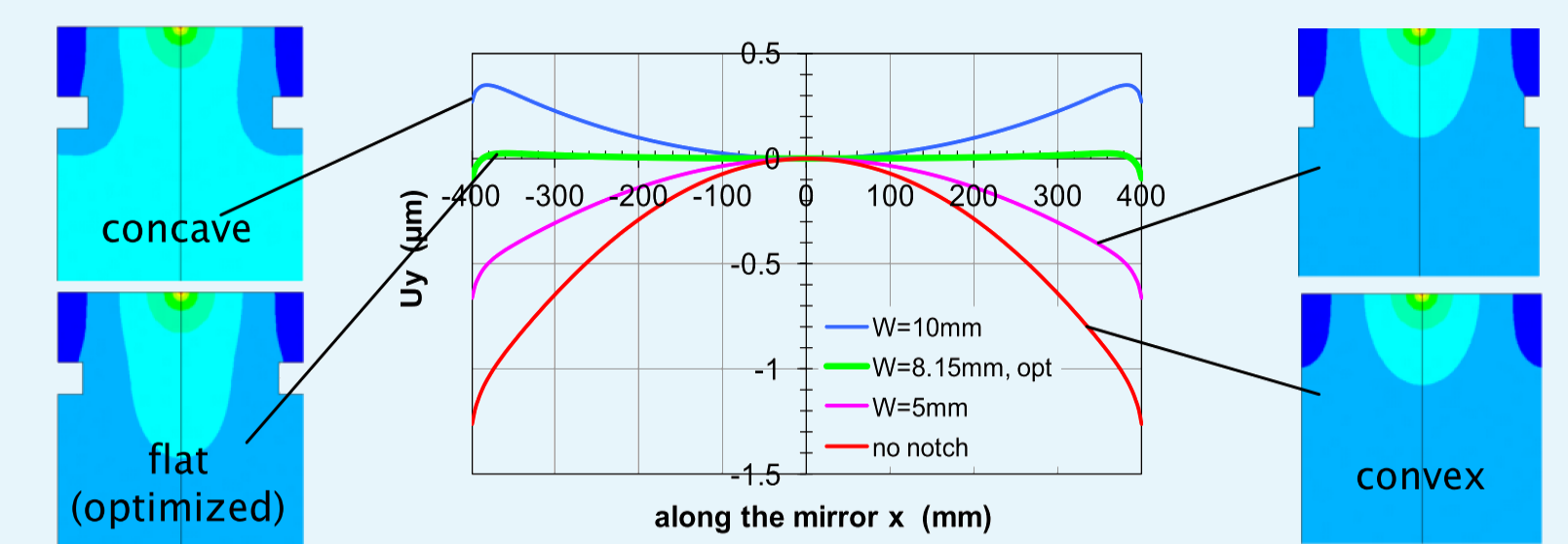
- Notched design works best with linear horizontal polarization.
- Second cooling loop allows use of linear vertical polarization.
- Double bracket design results in lower temperatures which also improves the linear vertical profile.

## What lies ahead

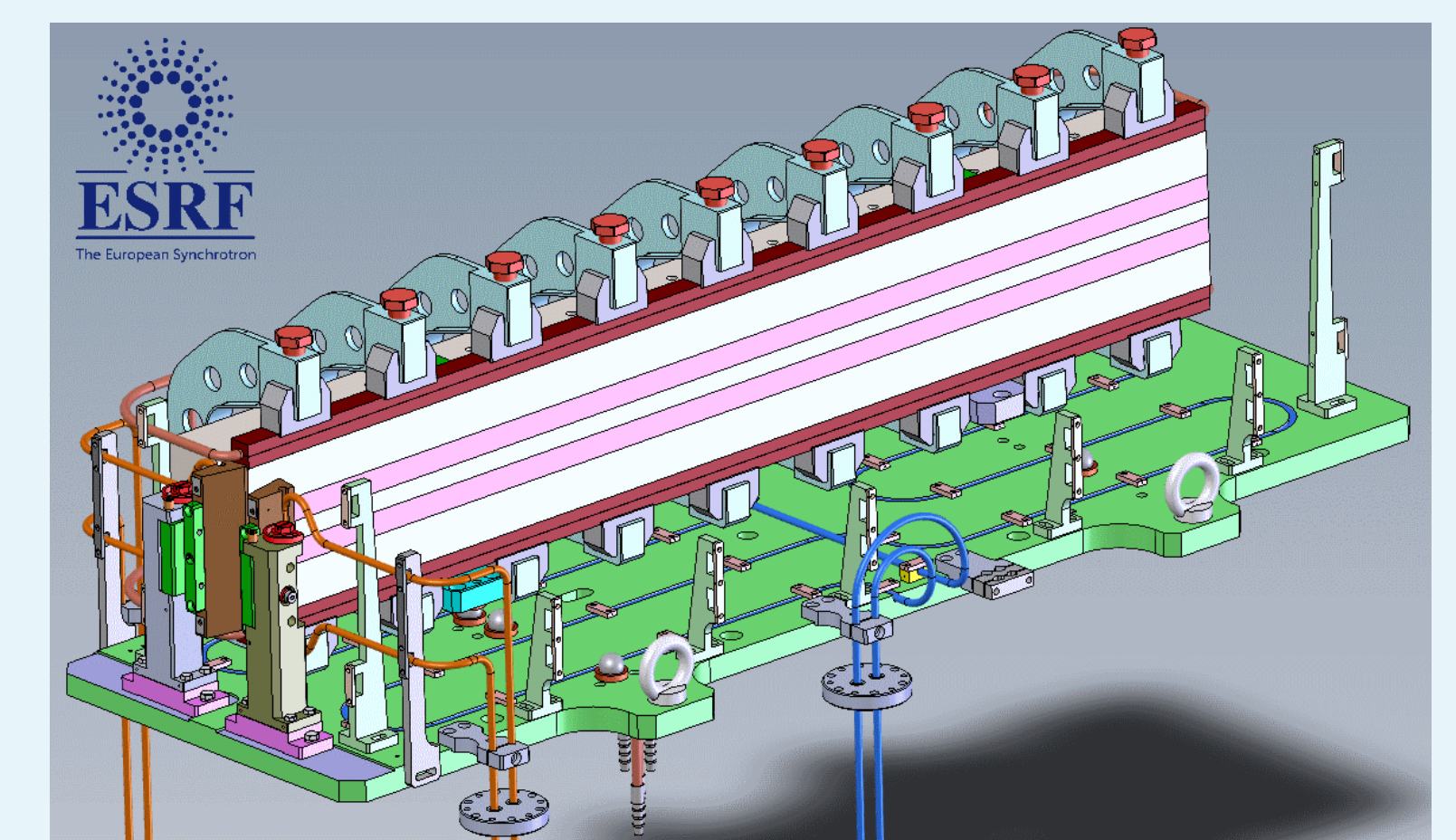
- Influence of clamping pressure on thermal conductance between copper and silicon
- Mirror support structure
- Specs of water chiller
- Chin guard performance -> additional Frontside effects?

## ESRF-Design

The notched mirror design [1-2] is used for some white beam mirrors at ESRF [2-3]. Depth of notch changes resulting surface profile along centerline.

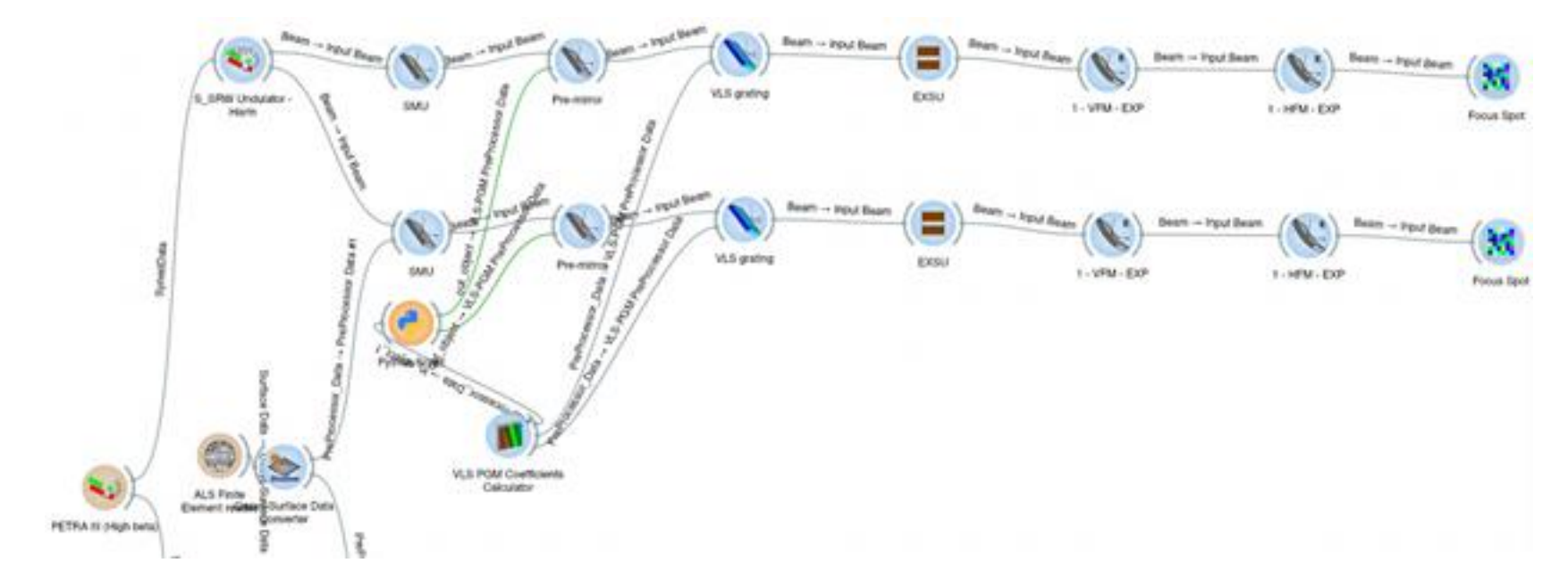


Influence of notch depth



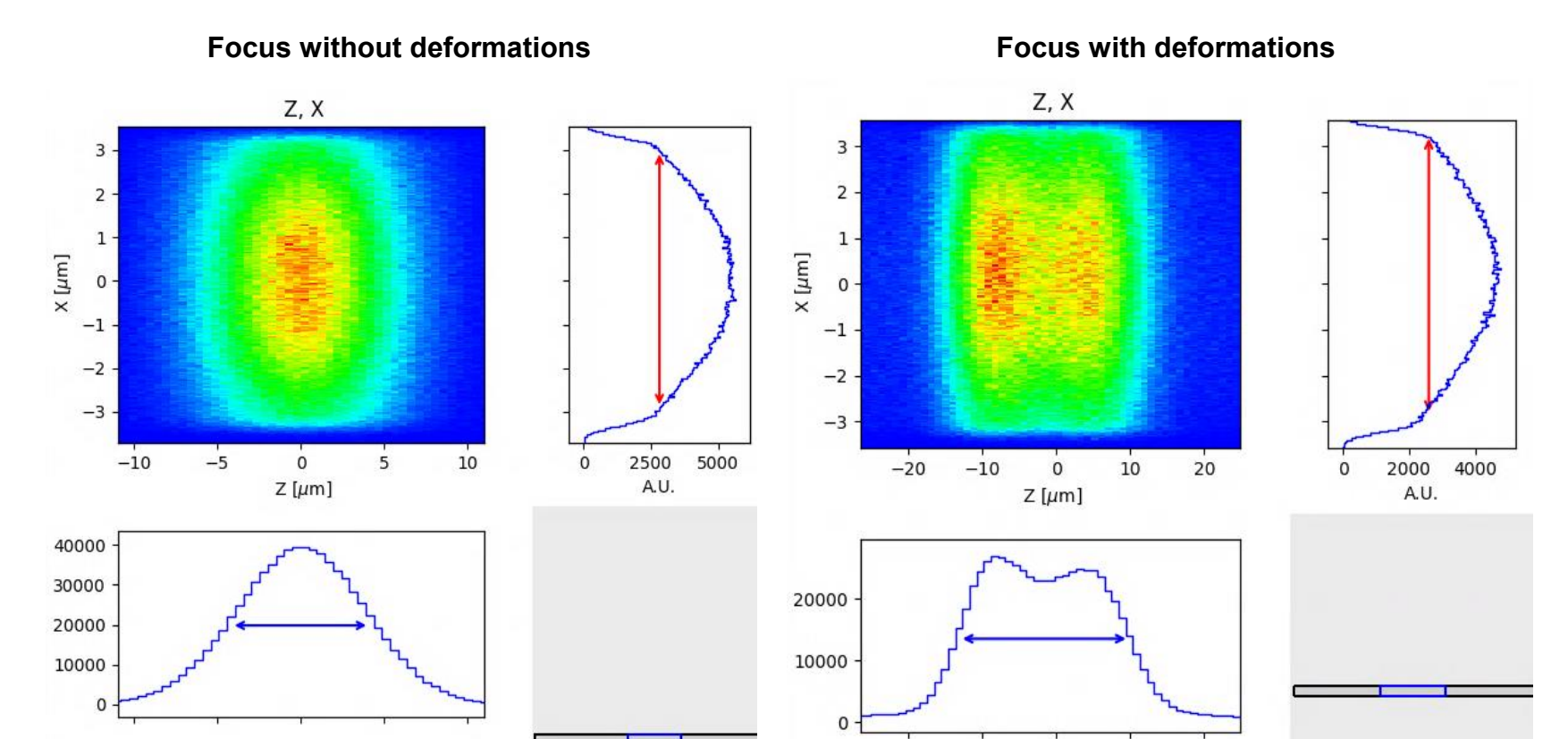
ESRF mirror design.

## OASYS - Shadow



OASYS [4] setup for parallel evaluation of P04-focus.

The results from ANSYS Static Structural were forwarded to the raytracing program Shadow to evaluate the difference of the focus profiles for a beamline without and with deformations on the first mirror.



Notched mirror with linear vertical polarization.

## References

1. Ali M. Khounsary, "Thermal management of next-generation contact-cooled synchrotron x-ray mirrors", Proc. SPIE 3773, X-Ray Optics Design, Performance, and Applications, (16 November 1999); <https://doi.org/10.1117/12.370114>
2. L Zhang et al, "Thermal distortion minimization by geometry optimization for water-cooled white beam mirror or multilayer optics", J. Phys.: Conf. Ser. 425 052029 (2013); <https://doi.org/10.1088/1742-6596/425/5/052029>
3. R Baker et al, "New generation mirror systems for the ESRF upgrade beamlines", J. Phys.: Conf. Ser. 425 052015 (2013); <https://doi.org/10.1088/1742-6596/425/5/052015>
4. Luca Rebuffi, Manuel Sanchez del Rio, "Interoperability and complementarity of simulation tools for beamline design in the OASYS environment," Proc. SPIE 10388, Advances in Computational Methods for X-Ray Optics IV, 1038808 (23 August 2017); <https://doi.org/10.1117/12.2274232>

