

Development of a passive tuned mass damper for ultra-high vacuum beamline optics

Fariha Khan, Jon Kelly, Andy Male, Davide Crivelli

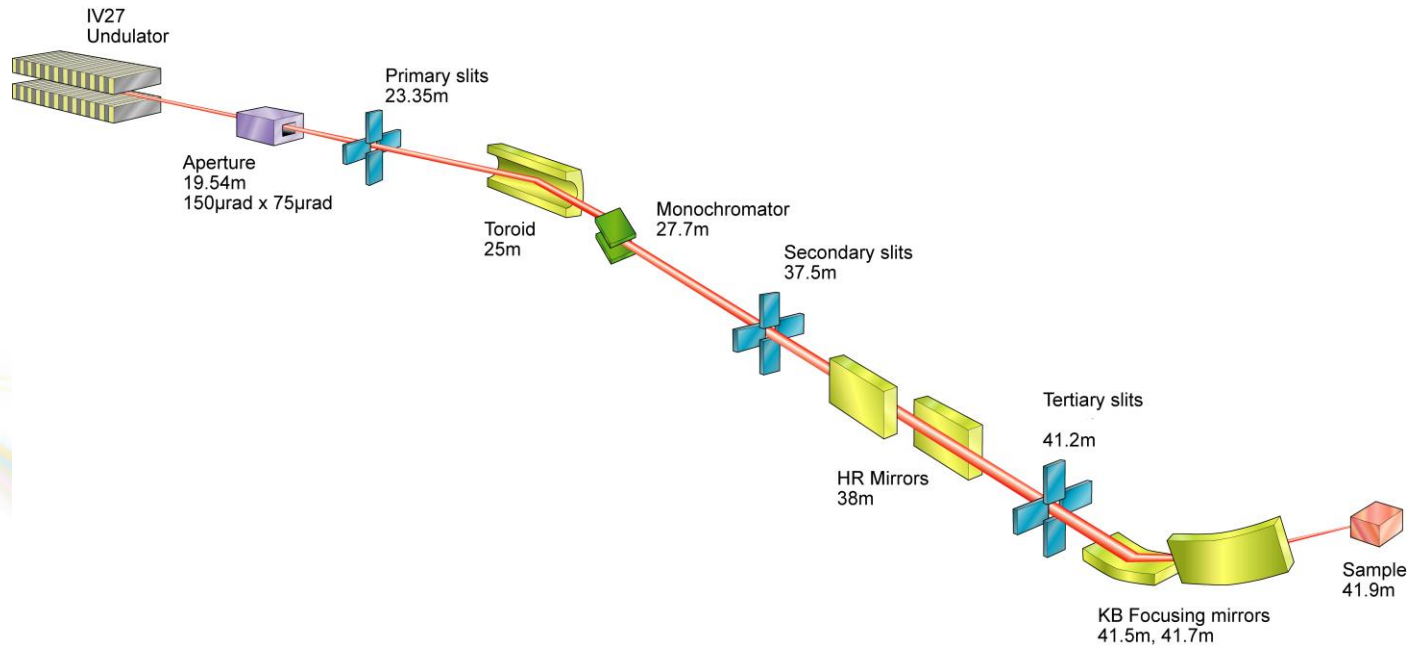
MEDSI Conference 2021

Diamond Light Source Ltd, Didcot, United Kingdom

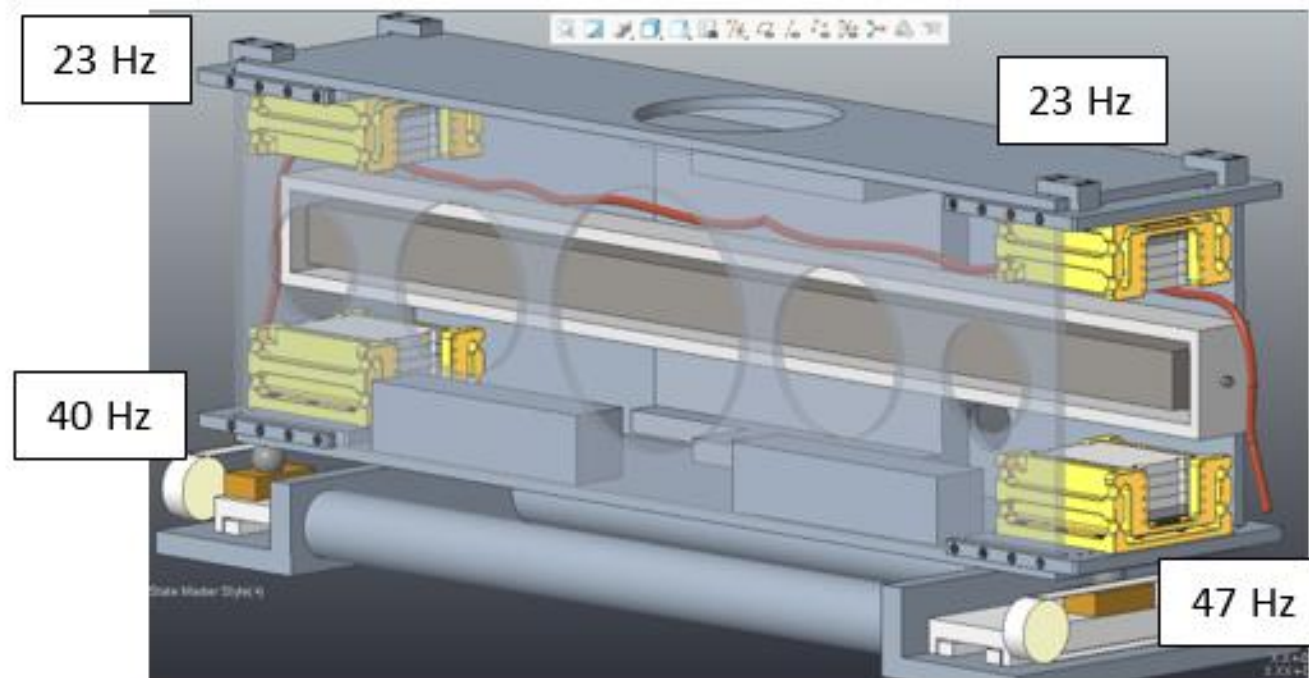
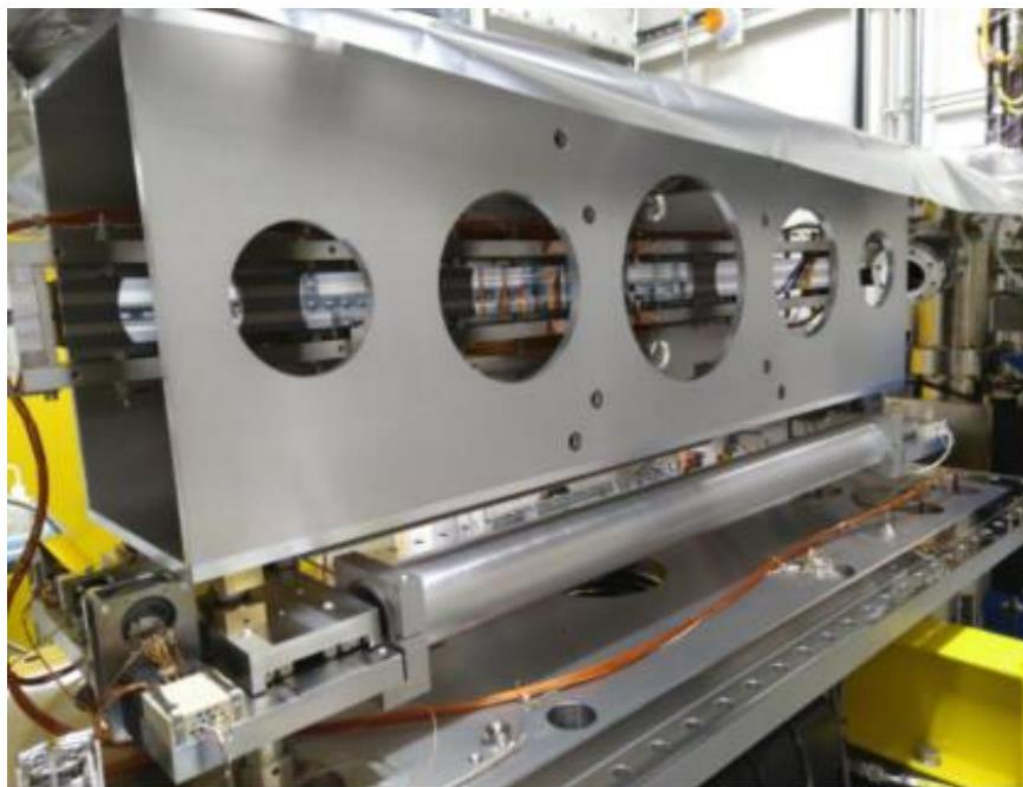


Motivation

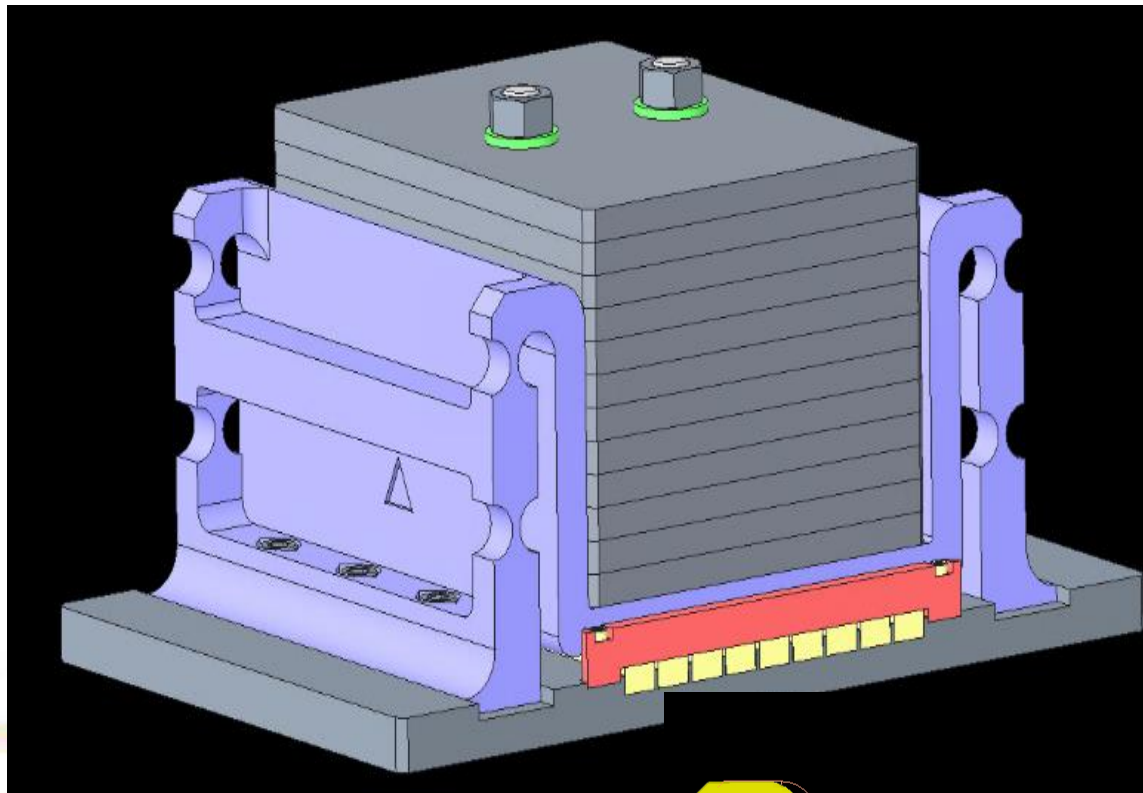
- Diamond-II next generation upgrade
- Precise beam positioning > better imaging at the sample > achieving valuable research!



Horizontally Focussing Mirror (HFM)



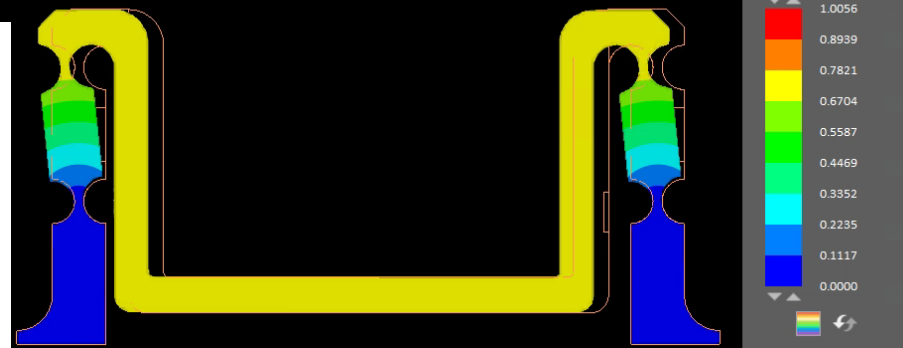
3D Printed TMD



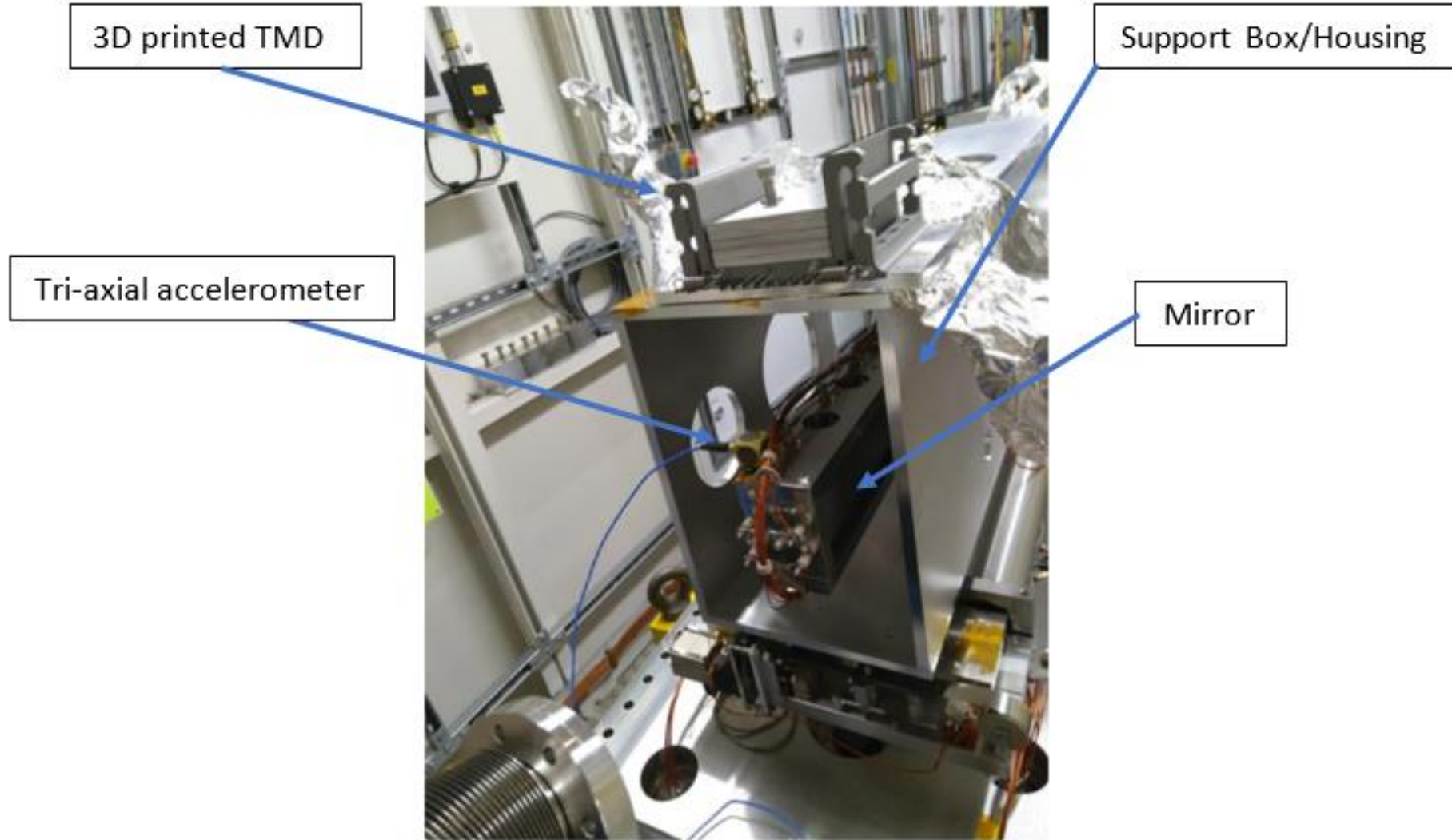
stiffness

mass

damping

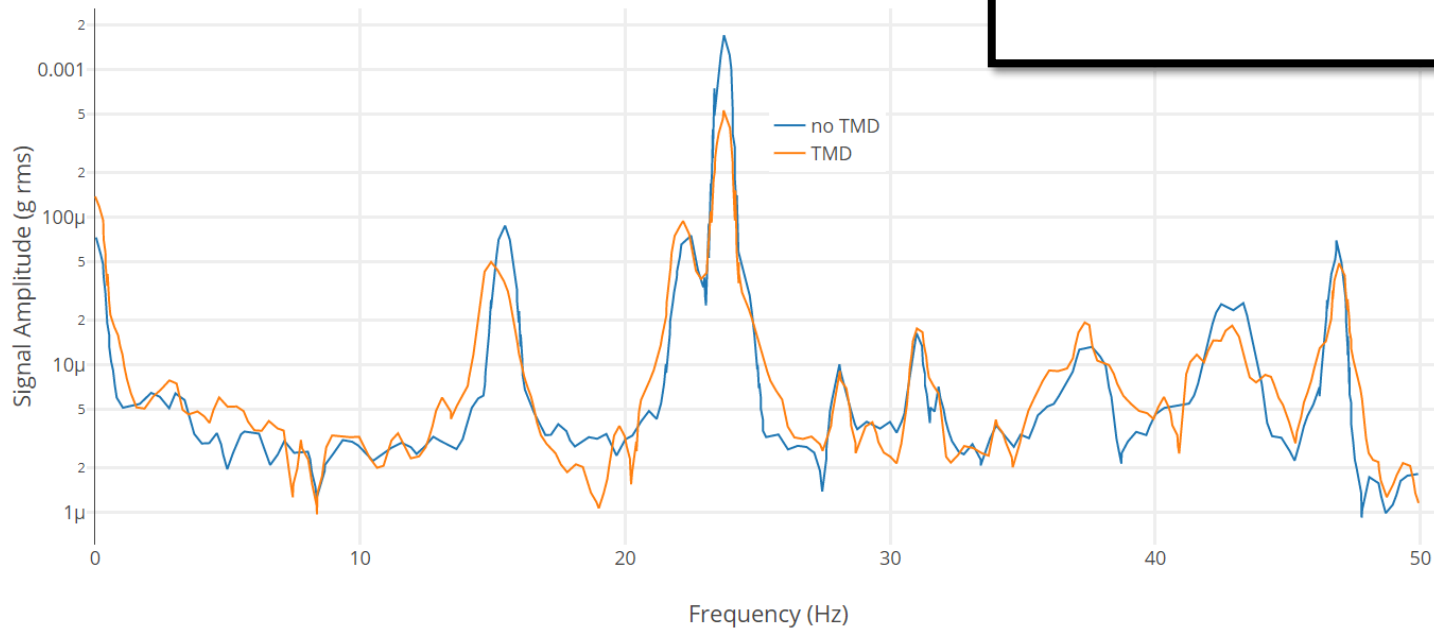


3D Printed TMD

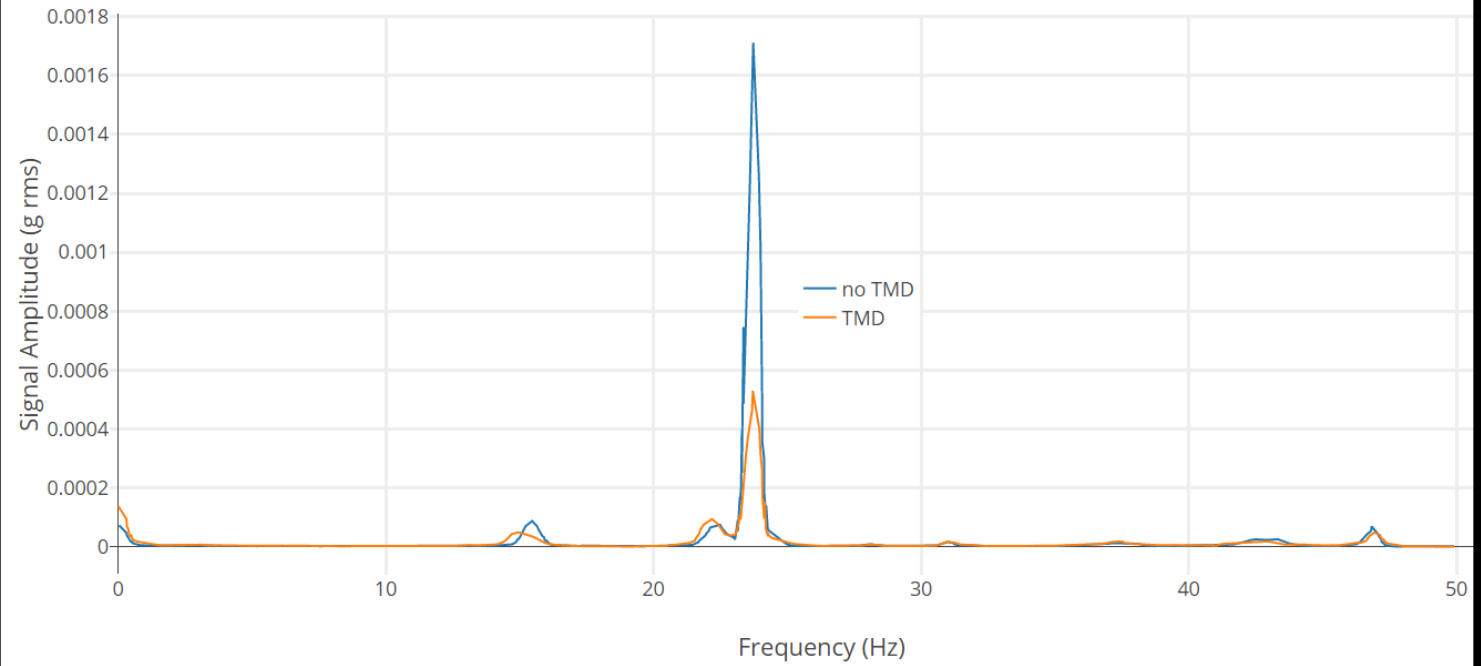


3D Printed TMD

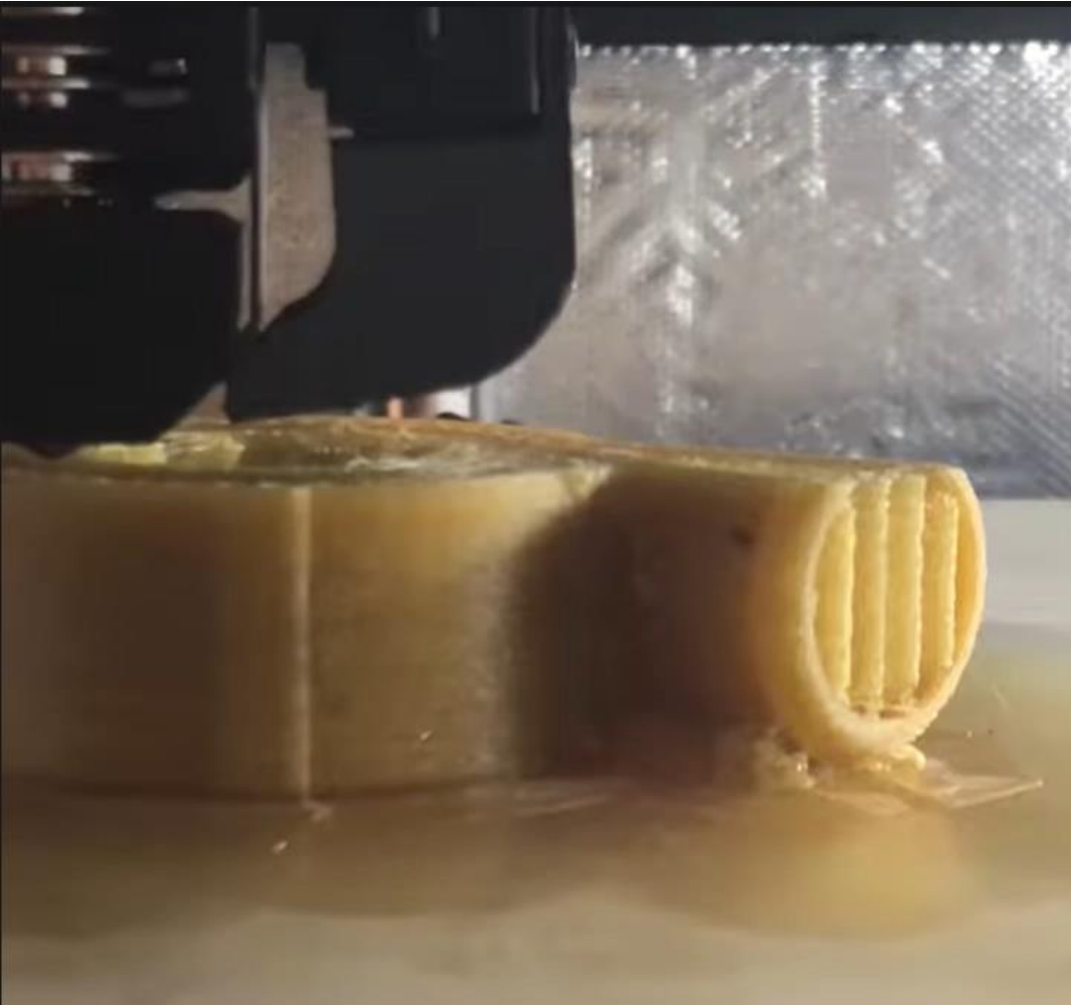
Frequency response of mirror



Frequency response of mirror

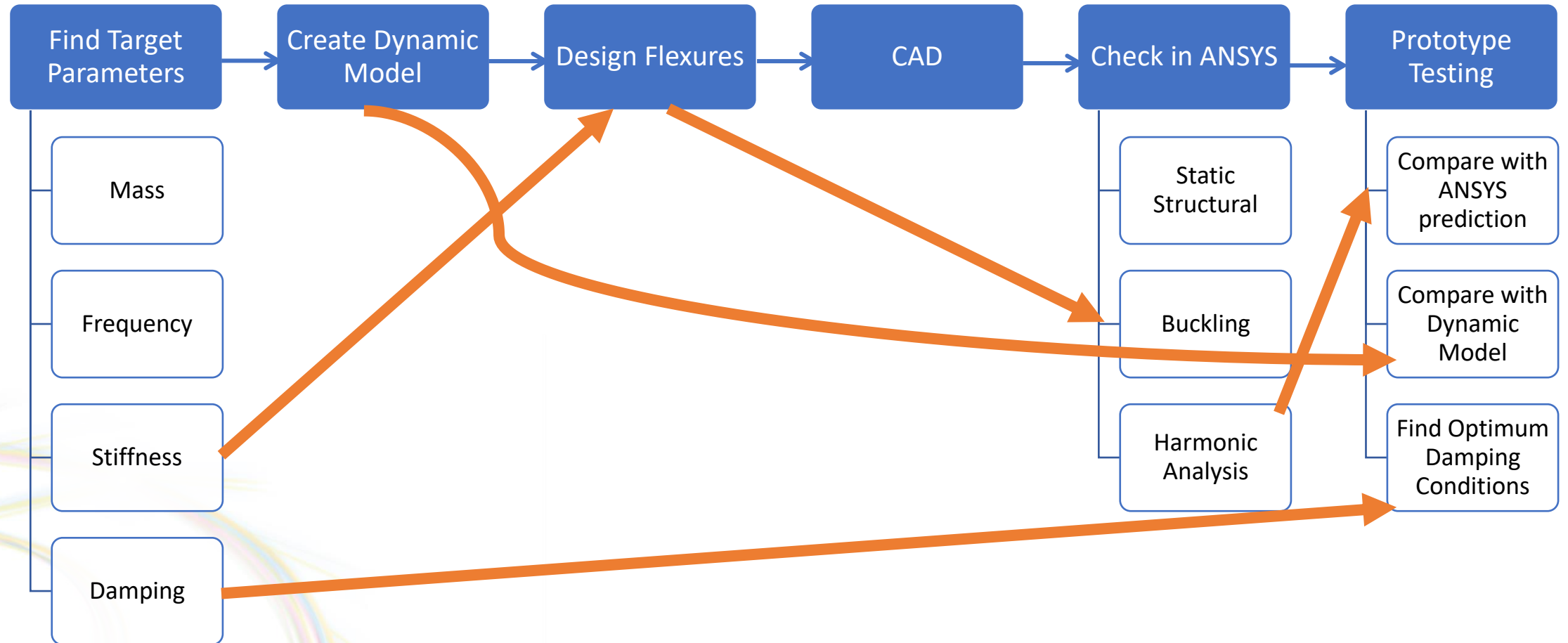


Do we need 3D Printing for this application?

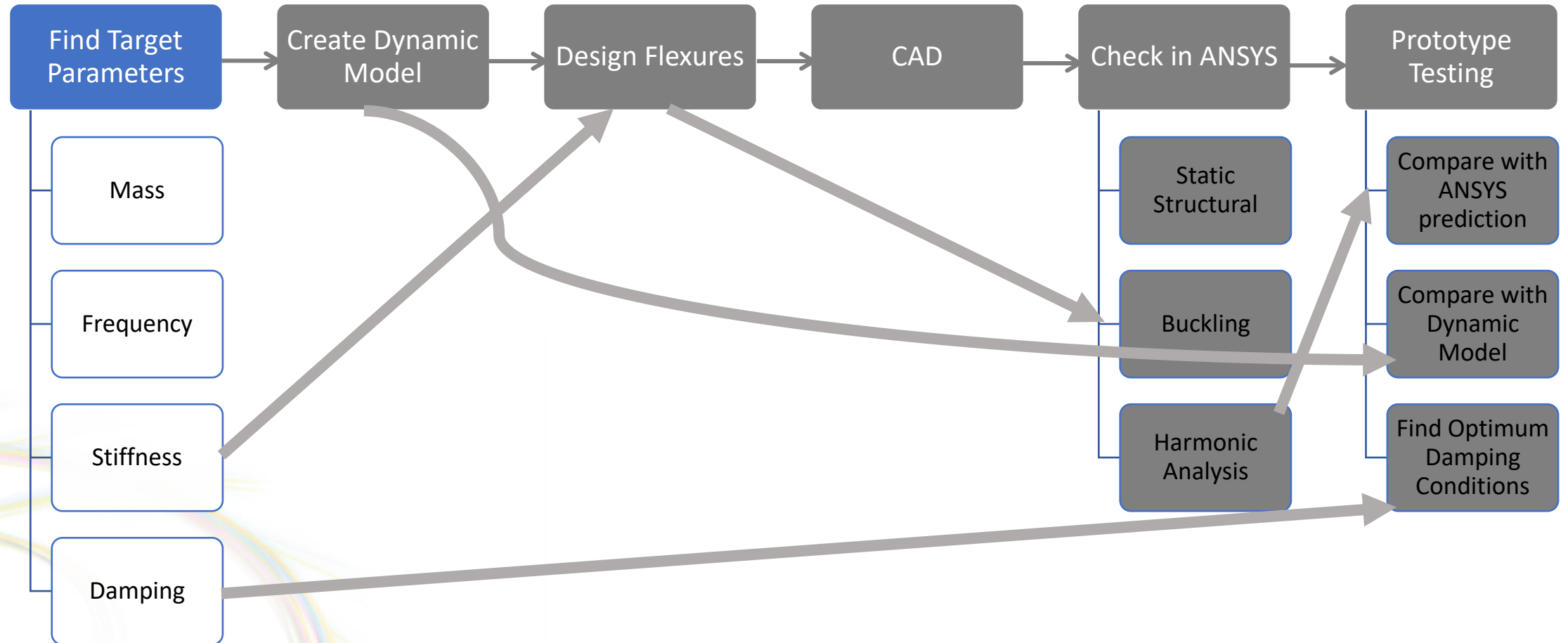


Advantages	Disadvantages
ULTEM is vacuum compatible	Expensive material
Monolithic design	Difficult to print
In-house fabrication	Repeatability and tolerance limitations
	Further investigation into performance (printed part may not fulfil spec)

Design Process

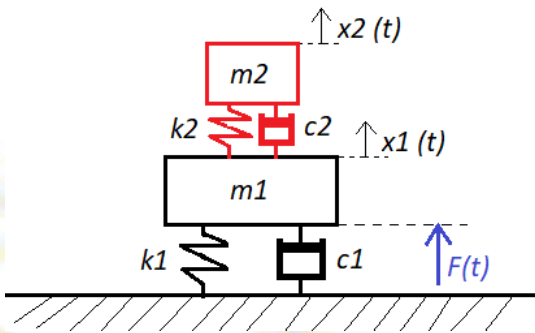


Design Process

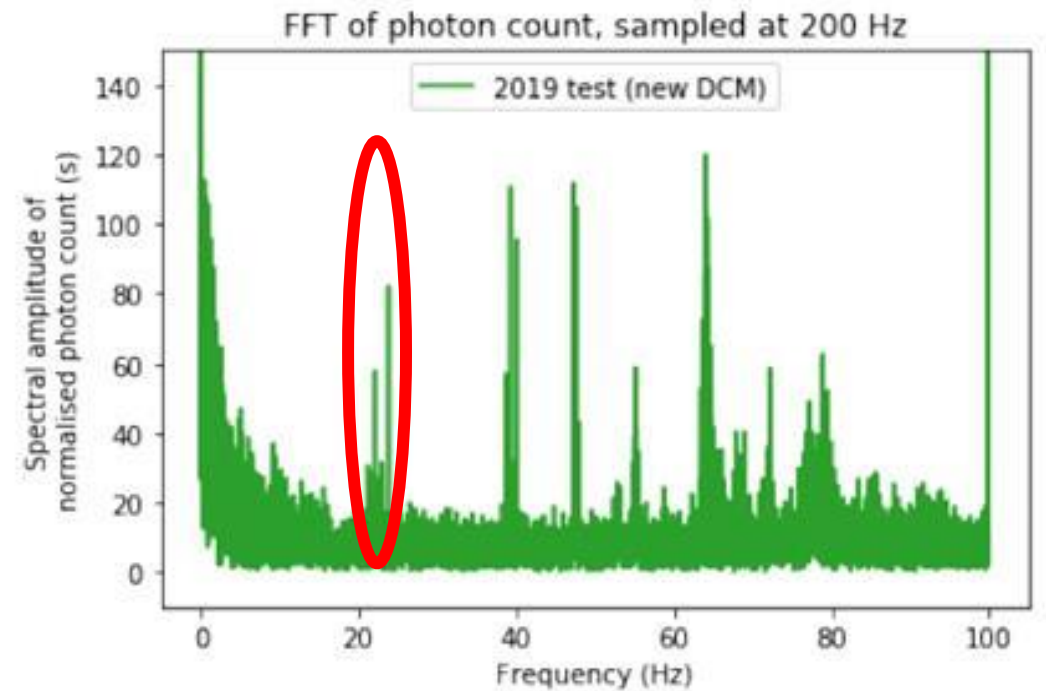


Finding Target Parameters (w/ Case Study)*

1. Choose the mass
2. Find the frequency
3. Calculate the stiffness
4. Choose the required damping



*same process used for 40 Hz and 47 Hz TMDs



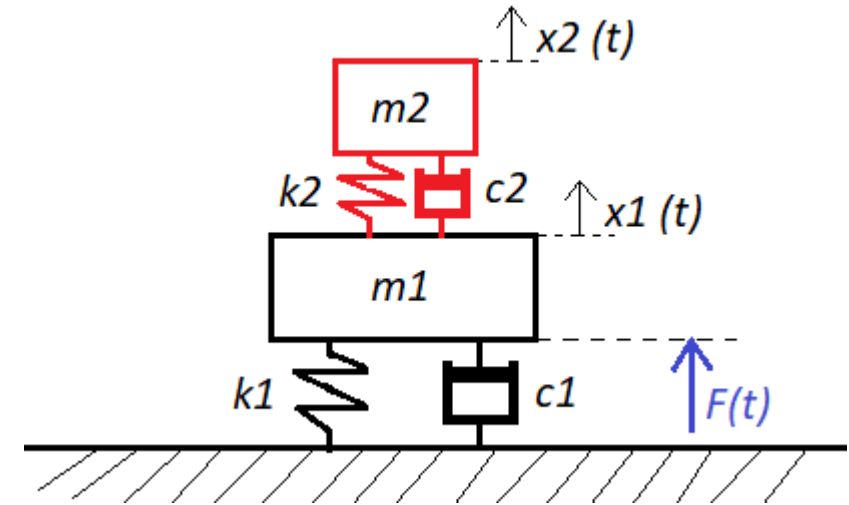
Finding Target Parameters

1. Choose the mass of the TMD

Limit $m_2 = 4\text{kg}$ per TMD

Mass ratio

$$\mu = \frac{m_2}{m_1} = 0.44$$



As a guideline: model the system
and have a target reduction factor

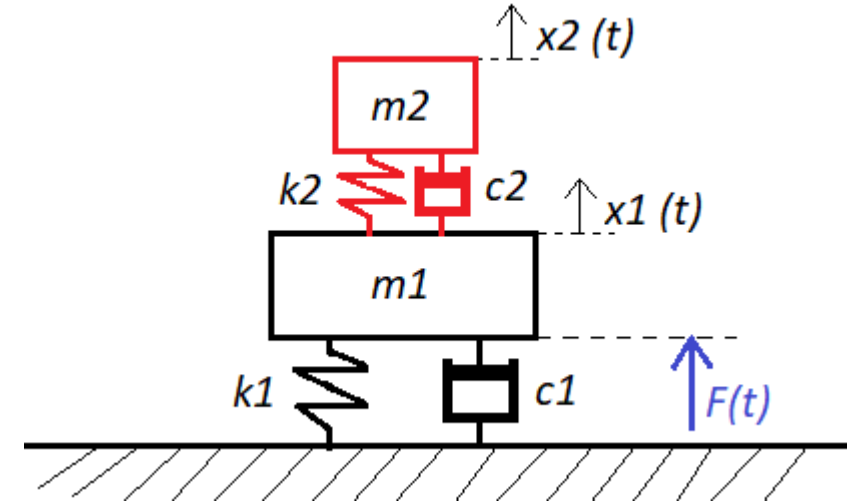
Finding Target Parameters

2. Find the frequency

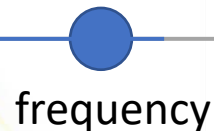
Slightly under the system frequency (remember we're adding mass)

Frequency ratio

$$\frac{f_2}{f_1} = \frac{1}{1+\mu} = 0.69$$



mass



frequency



stiffness



damping

Finding Target Parameters

2. Find the frequency

Slightly under the system frequency (remember we're adding mass)

Frequency ratio

$$\frac{f_2}{f_1} = \frac{1}{1+\mu} = 0.69$$

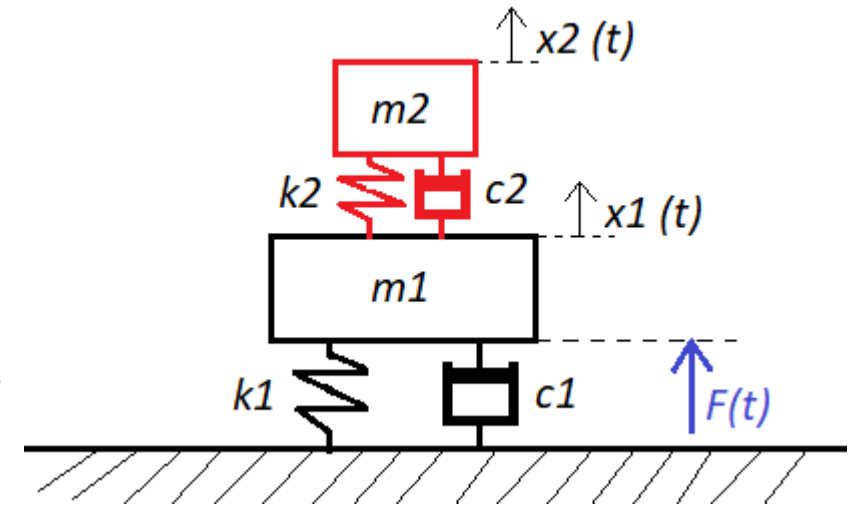
3. Calculate the stiffness

We already have both mass and frequency:

Stiffness

$$k_2 = (2\pi f_2)^2 m_2 = 80403 \text{ N/m}$$

(40202 N/m per TMD)



Finding Target Parameters

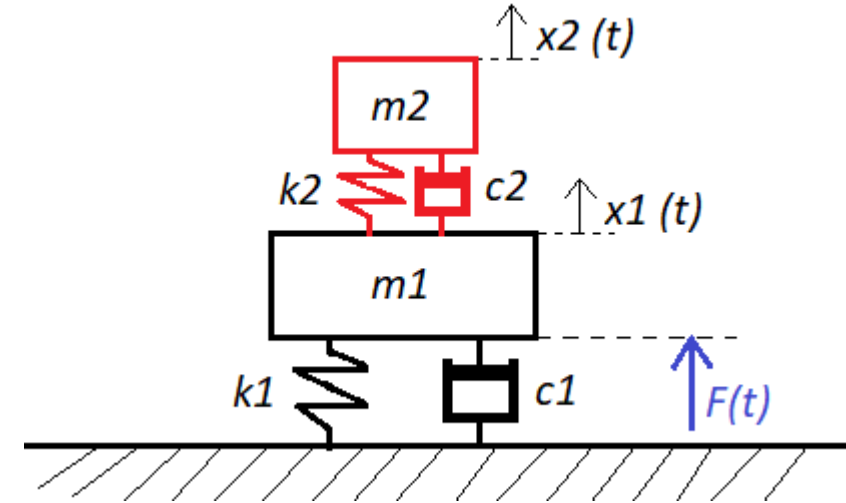
4. Choose the required damping

Optimal (relative) damping:

$$\xi_2 = \sqrt{\frac{3\mu}{8(1+\mu)}} = 0.34$$

Absolute damping:

$$d_2 = 2\xi_2\sqrt{k_2m_2} = 543.6 \text{ Ns/m}$$



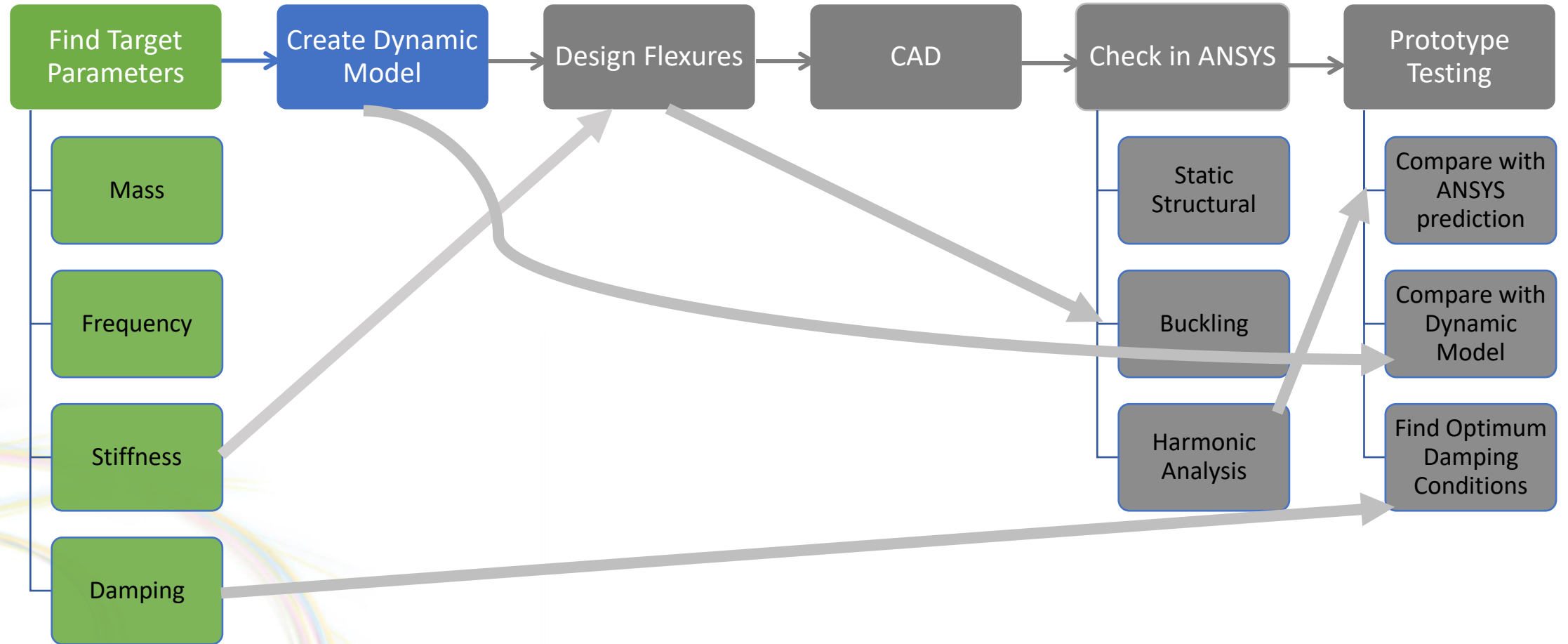
✓ mass

✓ frequency

✓ stiffness

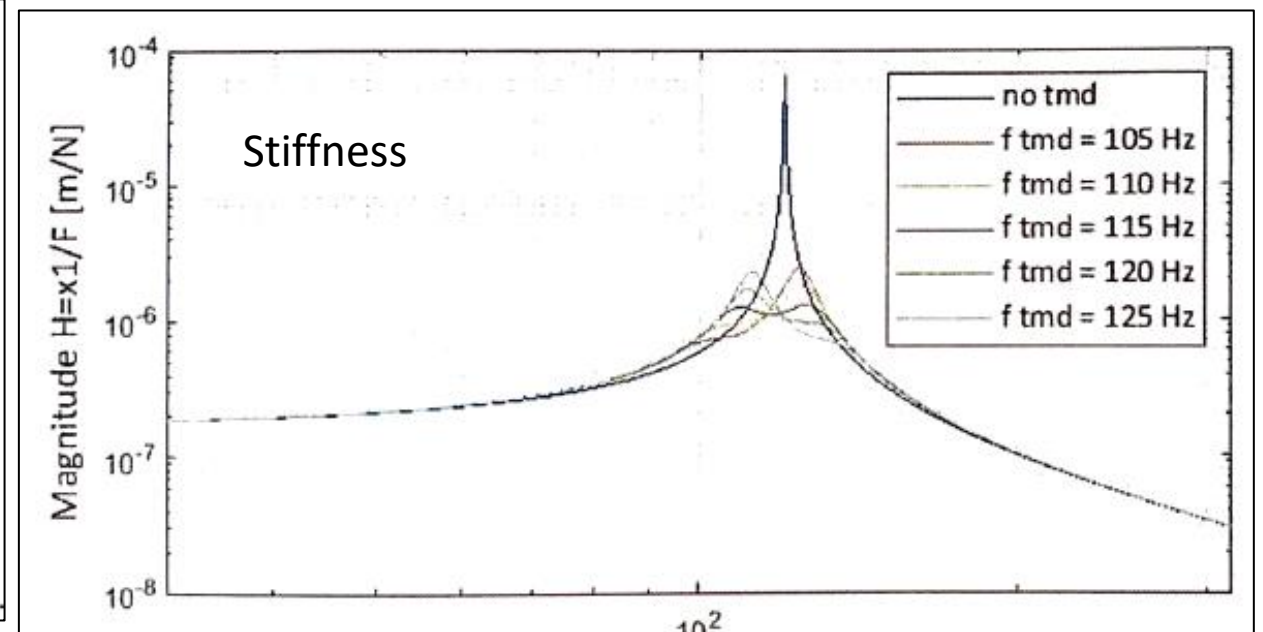
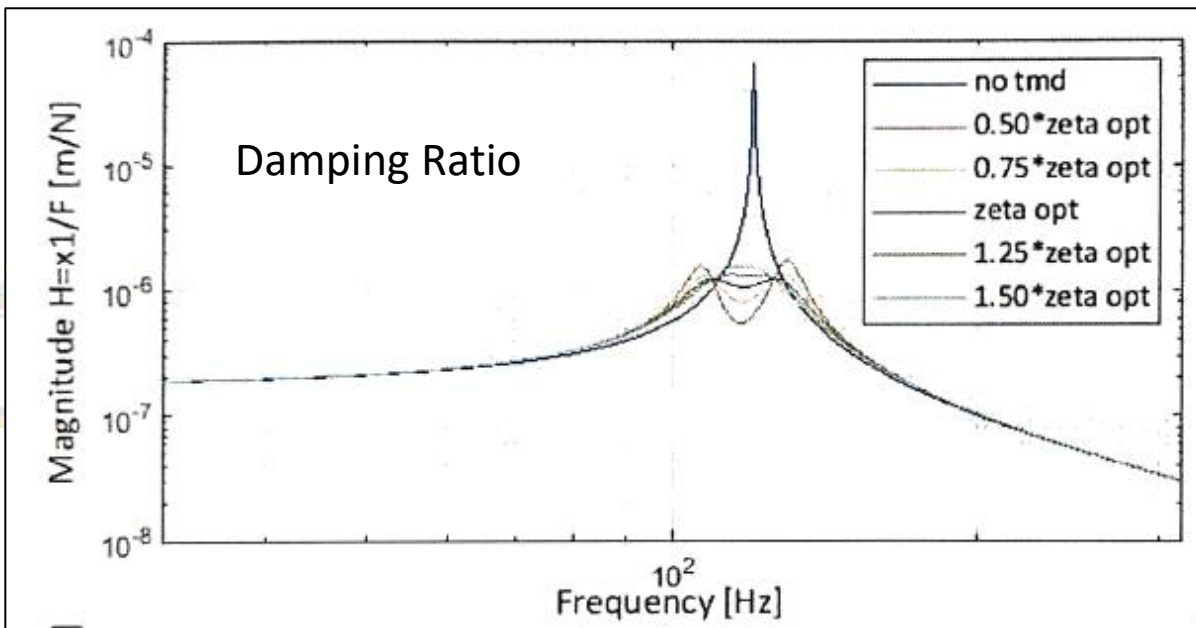
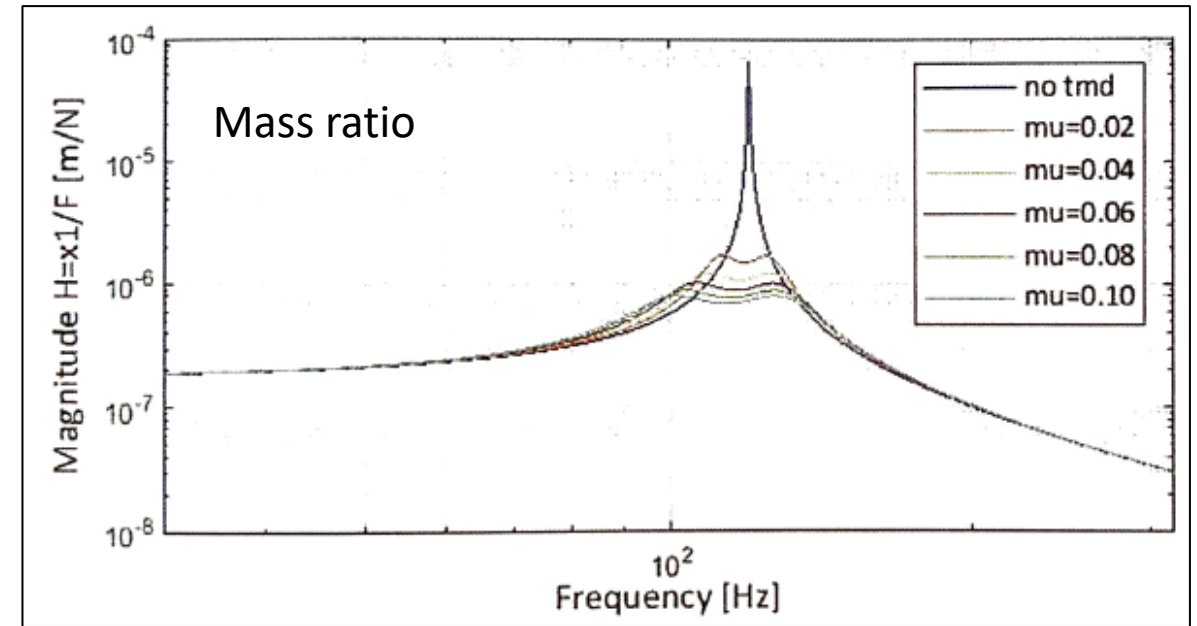
● damping

Design Process

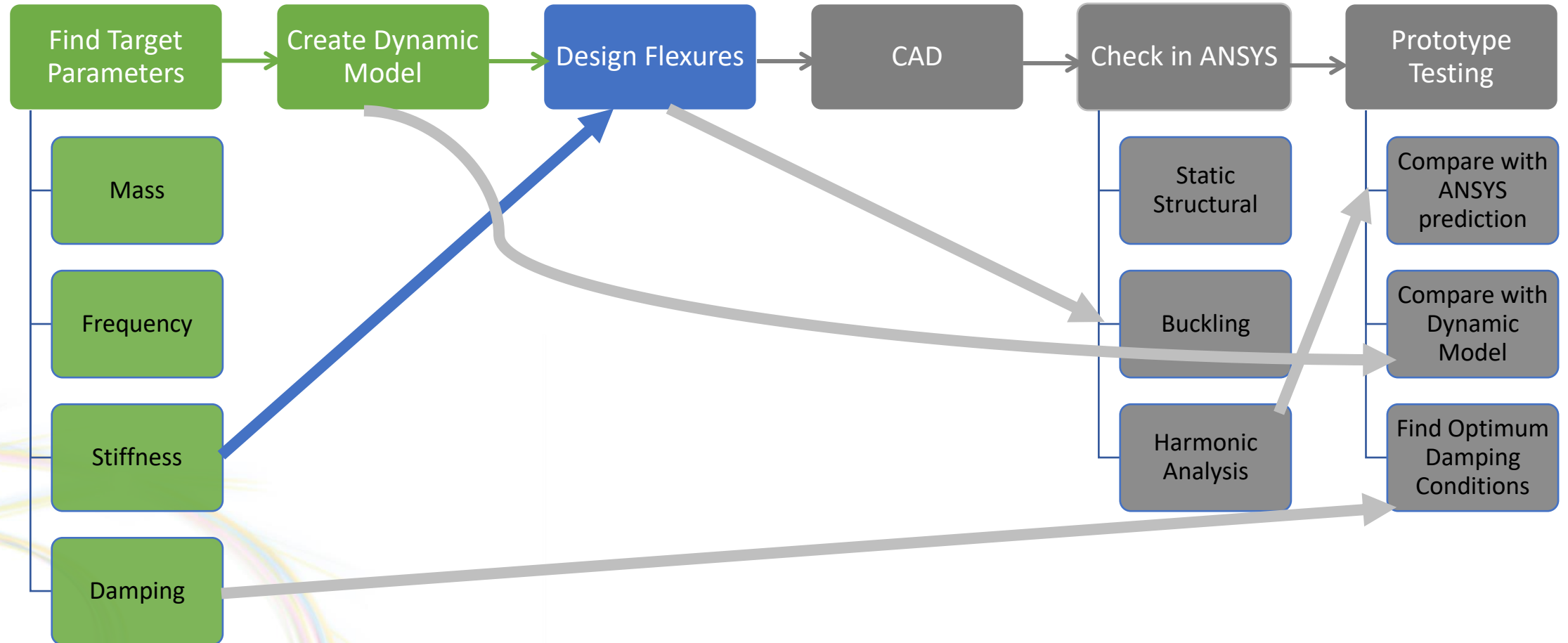


Dynamic Modelling

- Creating double-mass-spring-damper systems in MATLAB / Simscape



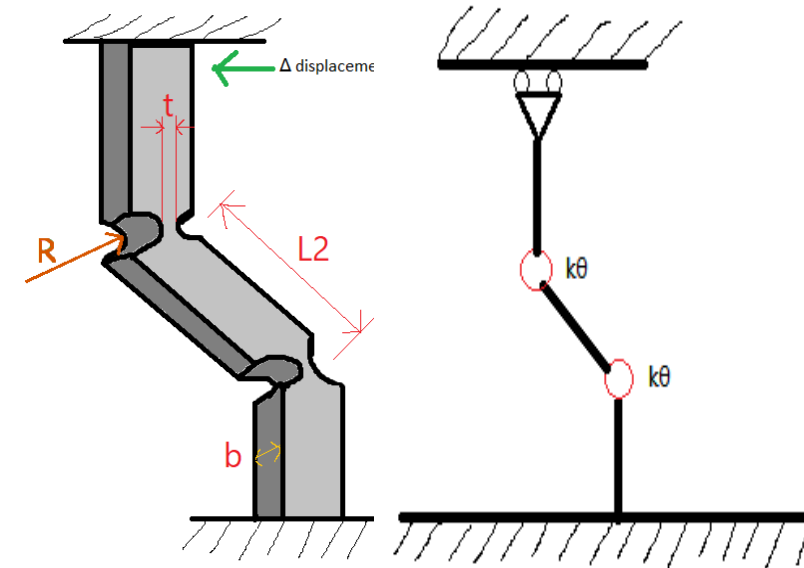
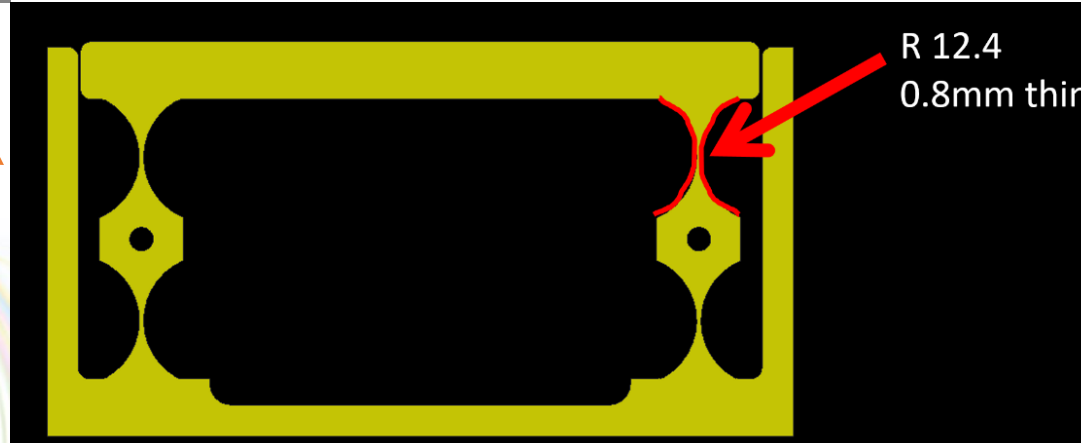
Design Process



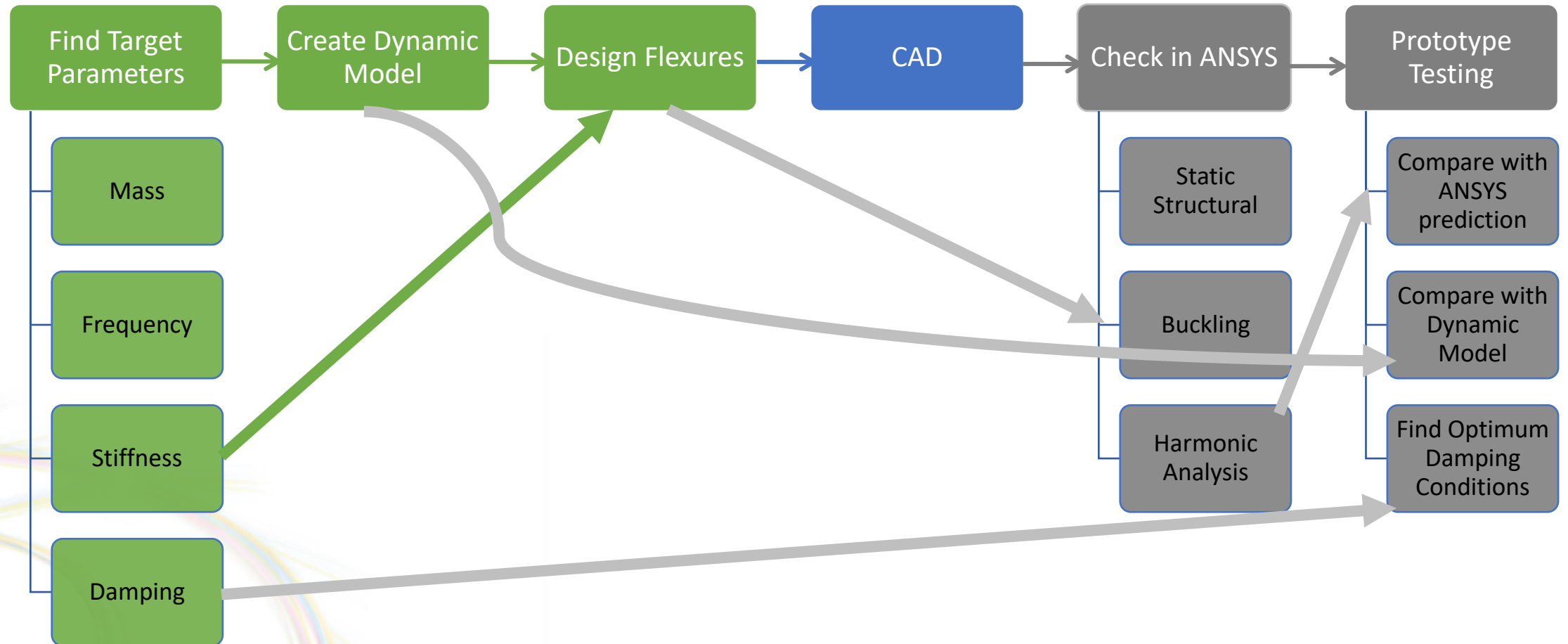
Flexures

$$k_f = \frac{4Ebt^{5/2}}{9\pi L^2 R^{1/2}}$$

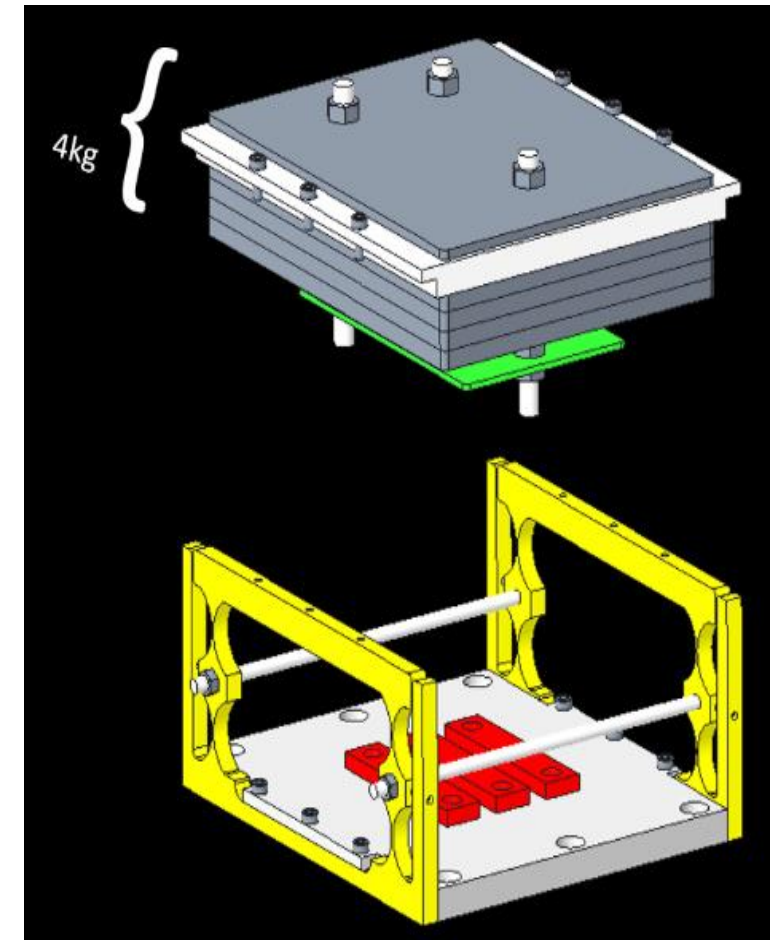
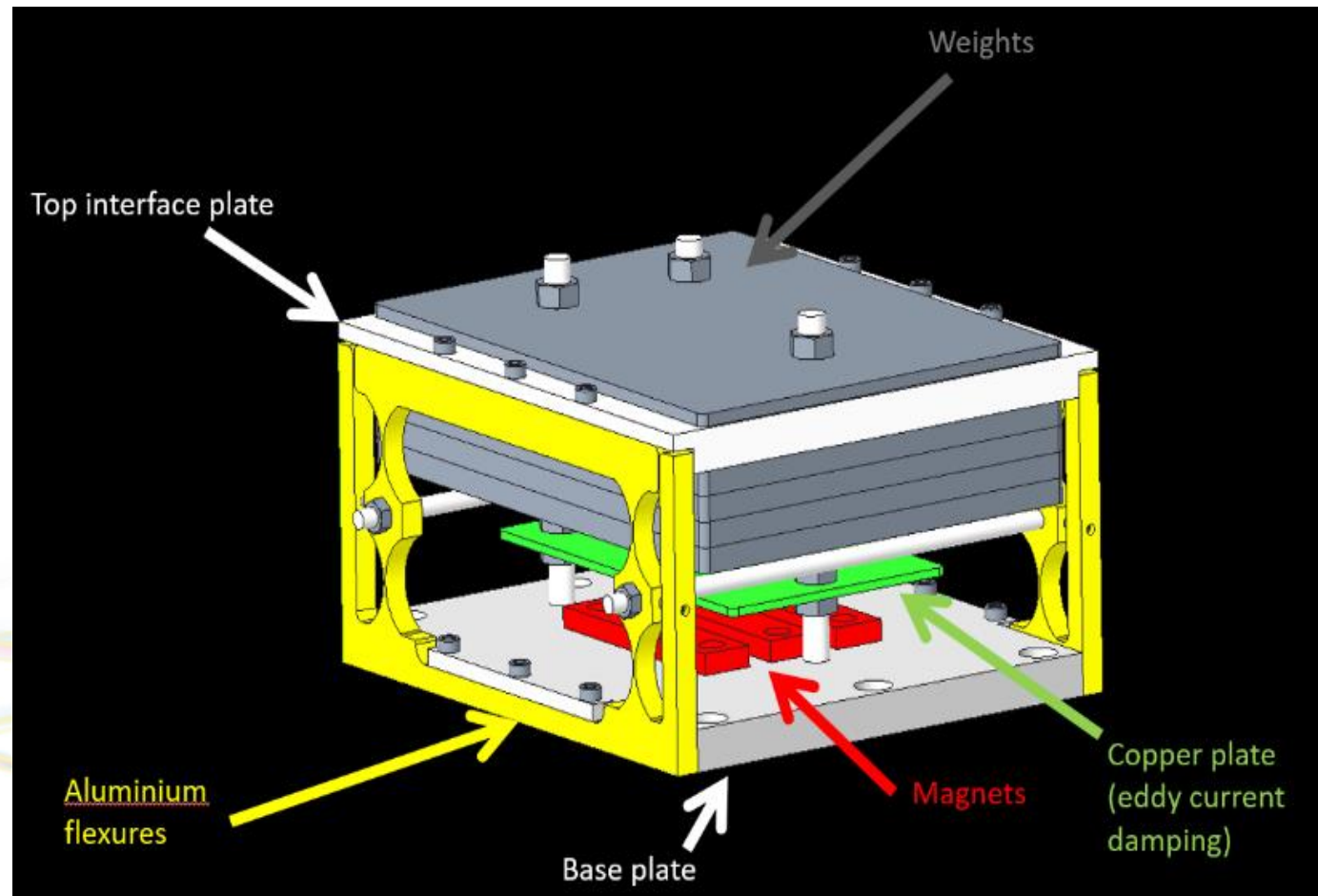
- Derived from first principles
- Relate one double-hinge flexure column to torsional springs



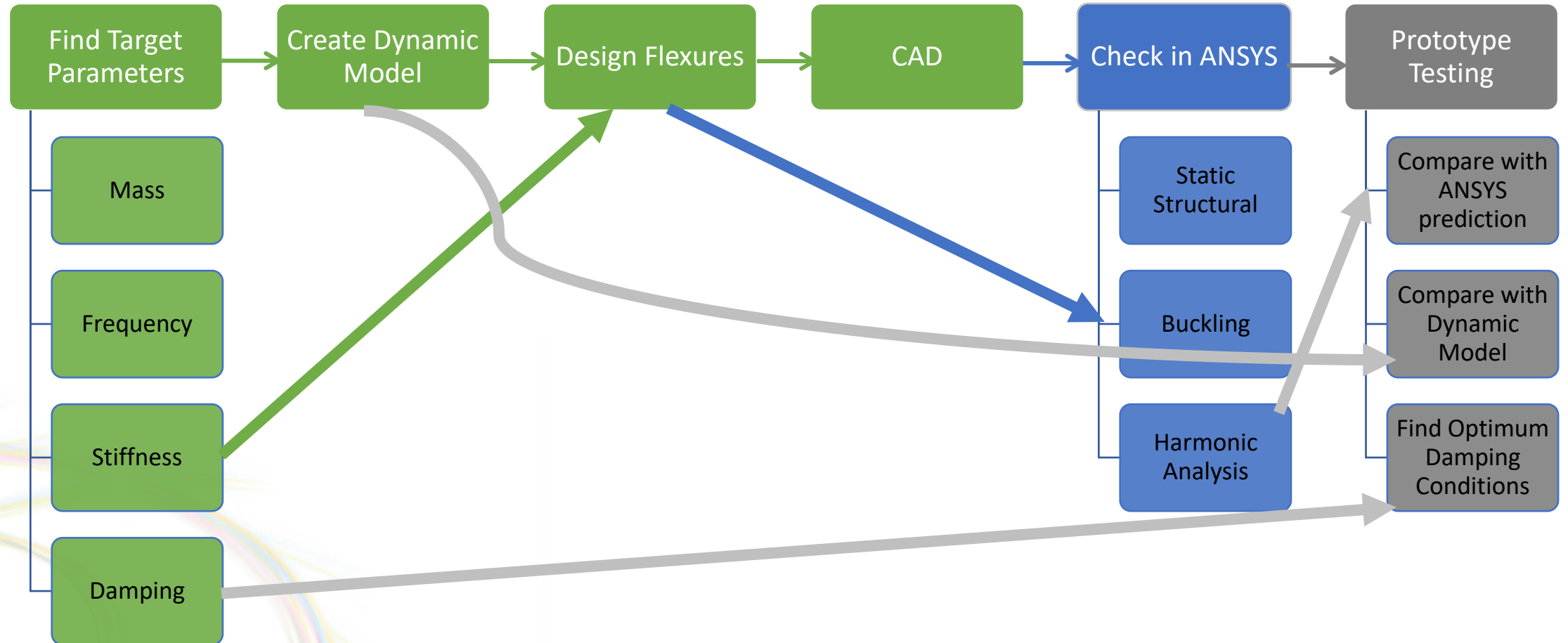
Design Process



Design TMD in CAD

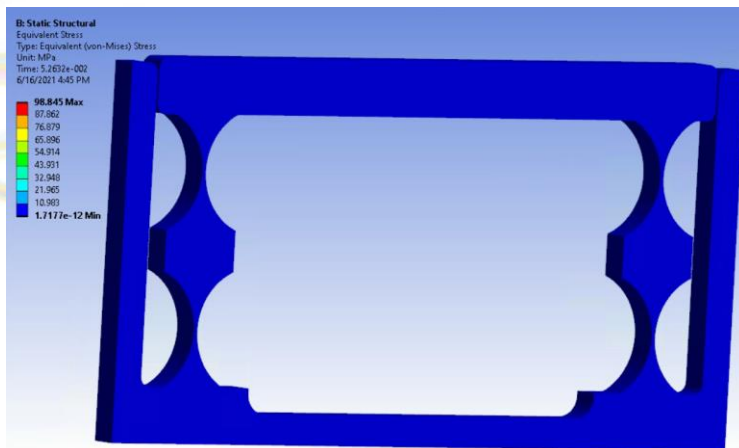
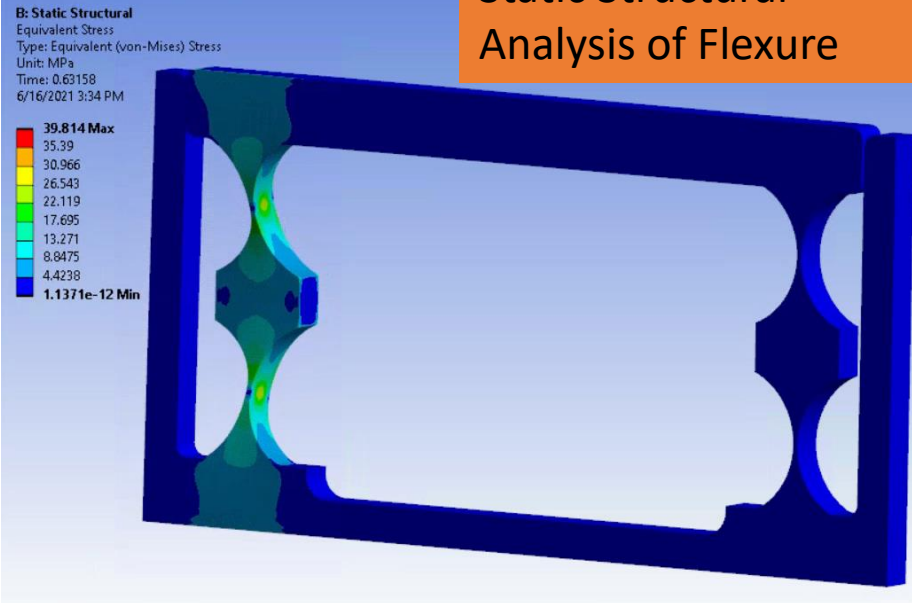


Design Process



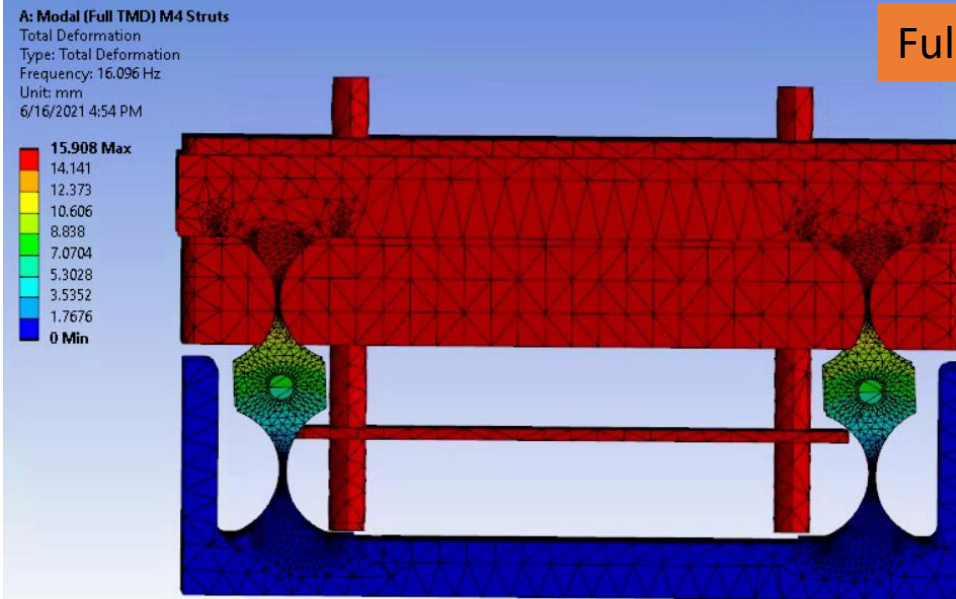
ANSYS Simulation

Static Structural Analysis of Flexure

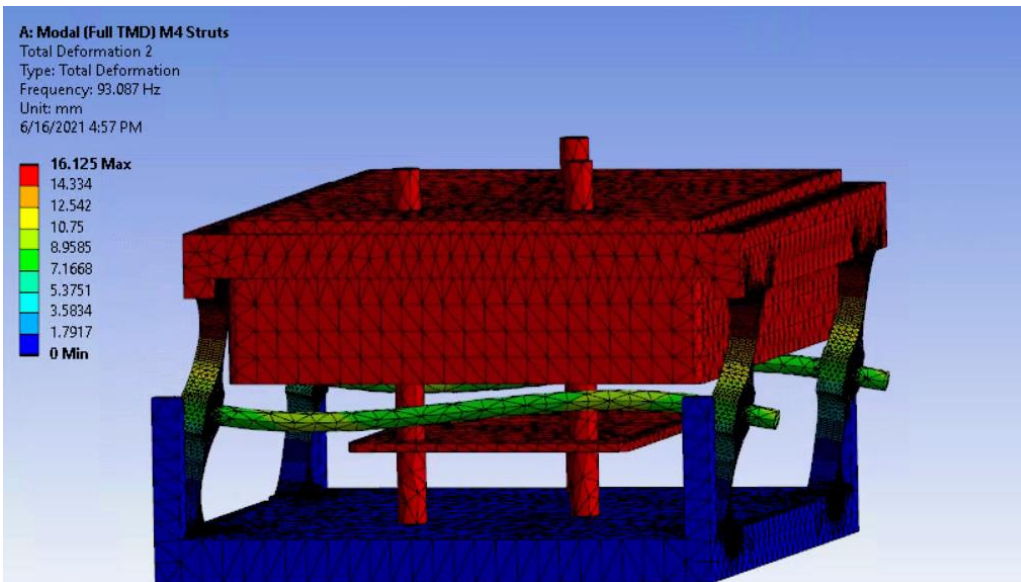


Full Modal Analysis

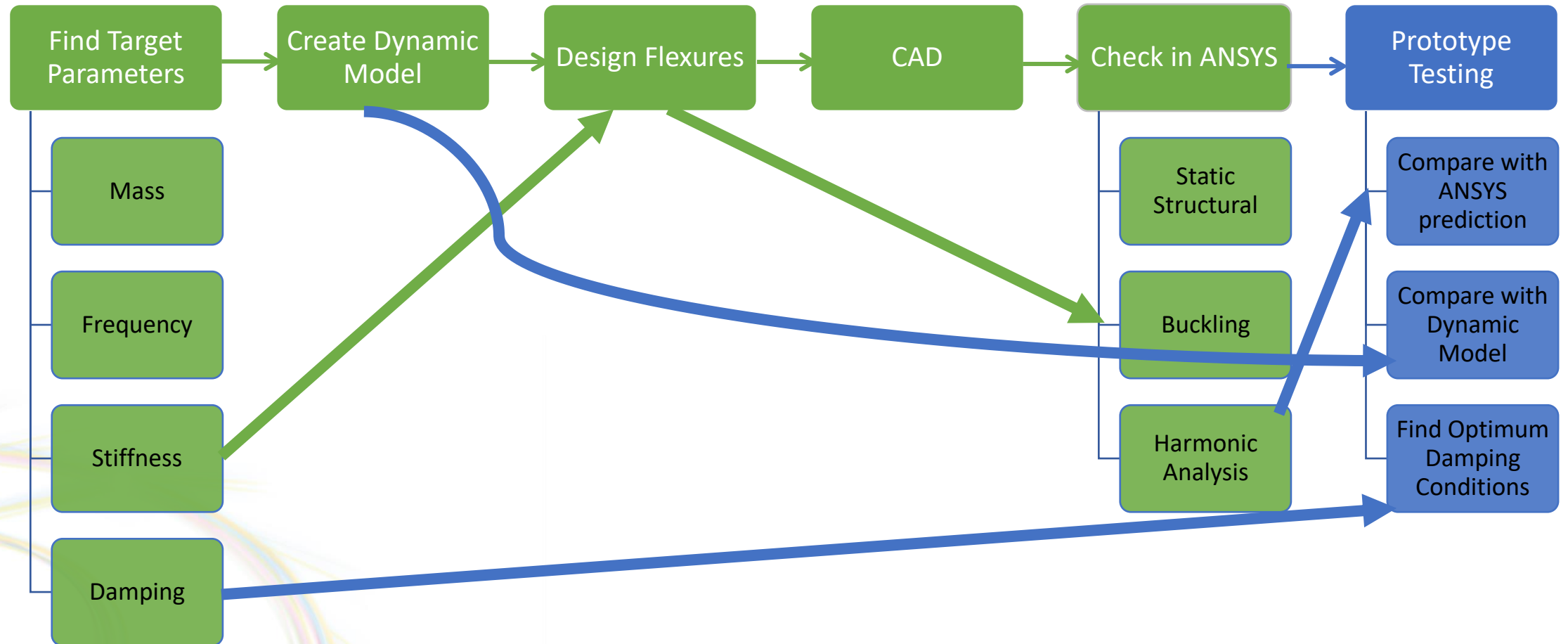
16 Hz Mode



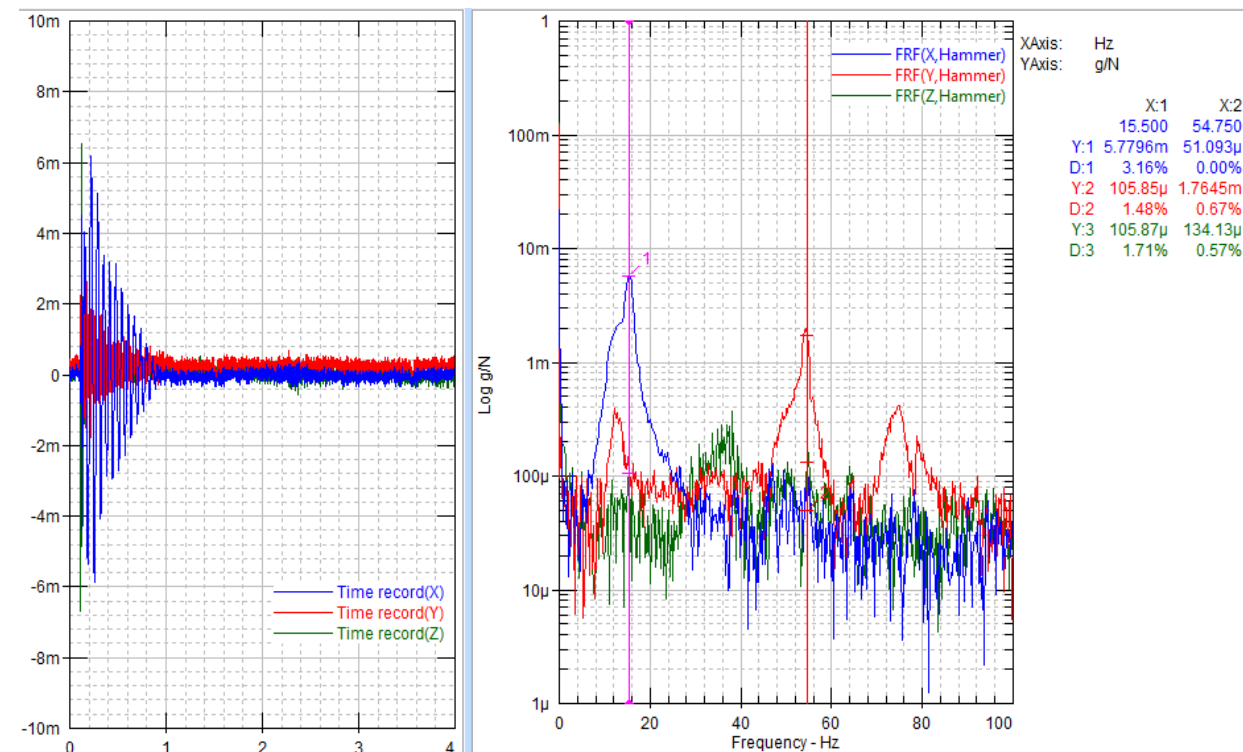
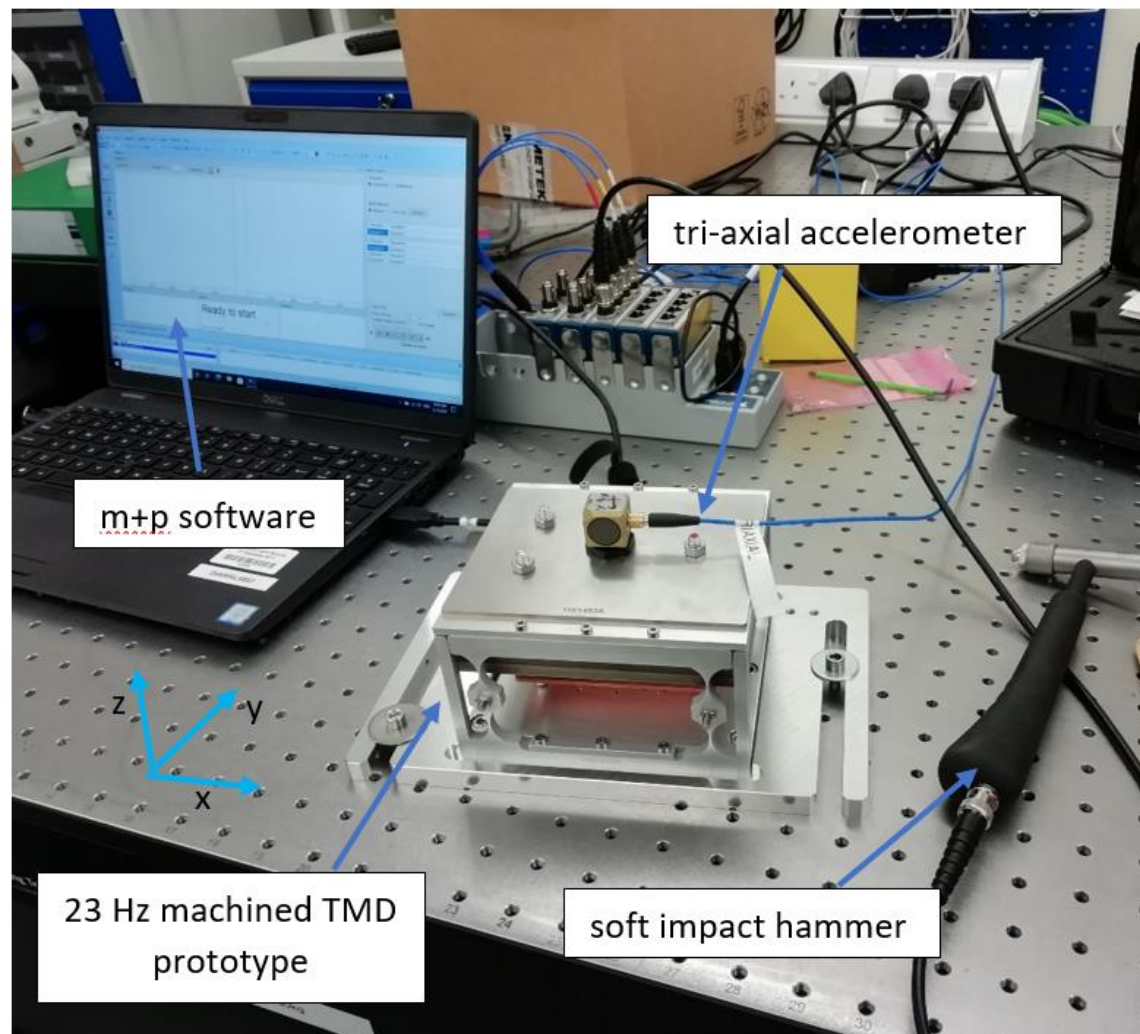
80-90 Hz Mode



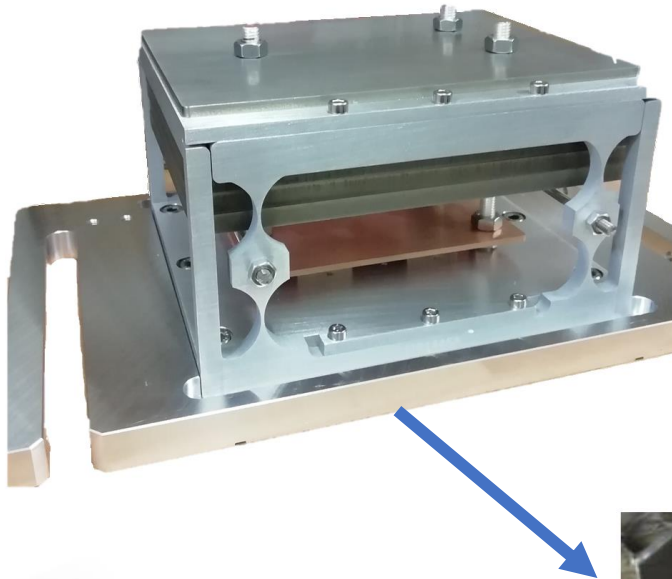
Design Process



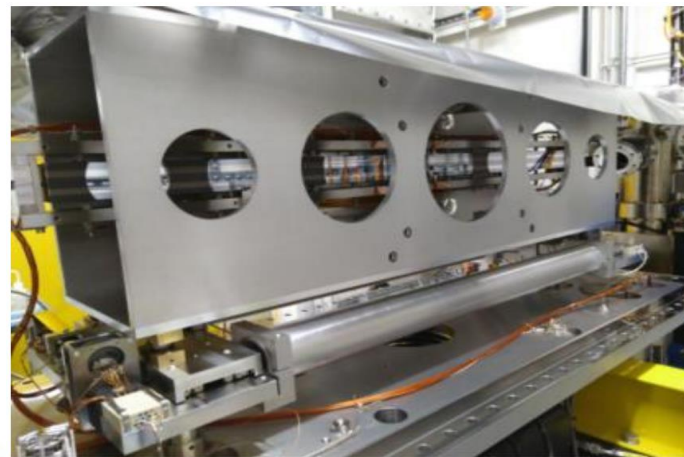
Prototype Testing



Final Comparison + Conclusion



	TARGET	Theory	ANSYS	Prototype
f_2 [Hz]	15.95	16.16	16.268	15.5
k_2 [N/m]	40201.534	40203.8485	41754.94169	36715.2343
m_2 [kg]	4	3.9413	3.9965	3.871
ξ	0.339	-	-	~ 0.0316



- ✓ Modelling
- ✓ Reducing risk on the beamline
- ✓ Extending life of older equipment