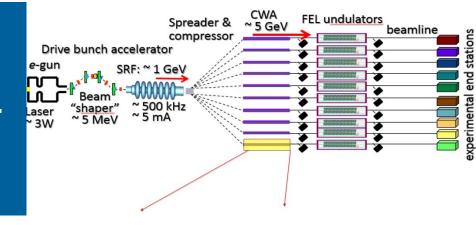
A-STAR DEVICE



DETERMINATION OF MAXIMUM REPETITION RATE OF A CORRUGATED-WAVEGUIDE-BASED WAKEFIELD ACCELERATOR (A-STAR)



KAMLESH SUTHAR MECHANICAL ENGINEER - APS

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U.S. DEPARTMENT OF ENERGY Argonne National Laboratory is a U.S. Department of Energy laboratory managed by UChicago Argonne, LLC July 29, 2021 MEDSI 2020

OUTLINE

- Introduction to A-STAR device
 - What is a wakefield accelerator?
 - Power deposition and repetition rate
 - Specifics of physical design
 - CWA modules
 - · Corrugated waveguide
 - Transition section
- Multiphysics FEA
 - FEA Formulation
 - Results
- Fabrication Challenges in designing A-STAR
- Existing state and future challenges.



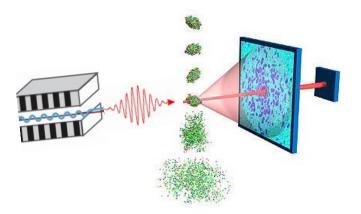


APPLICATION - FEL

Enables diffraction imaging of aperiodic biological molecules

Optimal x-rays^{*)}

- Photon energy 8–13 keV
- Pulse duration: a few fs or less
- Pulse rep. rate 50 kHz



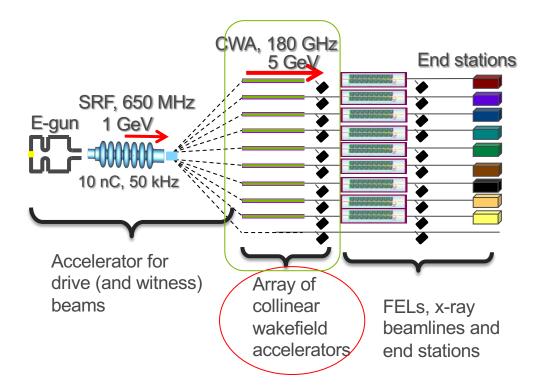
A protein exposed to an ultra-short X-ray pulse. Images show the molecule before, at and after interaction (see also Neutze, R. Wouts, D. van der Spoel, E. Weckert, and J. Hajdu, "Potential for biomolecular imaging with femtosecond X-ray pulses," Nature 406 (2000) 752).



A CONCEPT OF A- STAR DEVICE

High repetition rate operation is essential goal

- Multiple FELs maximize facility productivity.
- Each FEL uses its own accelerator.
- Single SRF gun and single SRF linac drive 10 collinear wakefield accelerators.
- Collinear wakefield accelerators increase witness beam energy from 1 GeV up to 5 GeV.
- Repetition rate up to 20 kHz per FEL minimizes data collection time.



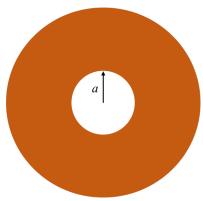


WAVEGUIDE WITH CORRUGATIONS

Repetition rate and wakefield

Theoretical models^{*)} predict the wakefield's dependence on inner radius a: **Drive Bunch** & Witness Bunch 0.3nC **10nC** ~800MeV 1GeV 1 200MeV 5GeV а RF power produced in 50 cm long corrugated waveguide: TM01 expected power is ~1kW.

Inner radius largely defines loss and kick factors due to wakefield



Value chosen: *a* =1mm

a: inner radius of cylinder.
d: depth of corrugations.
t: corrugation "tooth"
width.
v: gap width between
teeth.



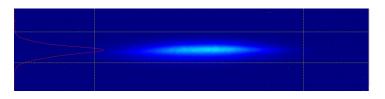


*) K. Bane and G. Stupakov, Nucl. Instrum. Meth. Phys. Res., Sect. A 677, 67 (2012).

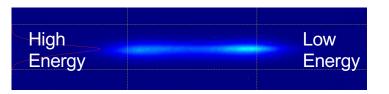
EXPERIMENTAL RESULTS

Evidence of 180GHz acceleration

Spectrometer Measurements Tube with smooth wall

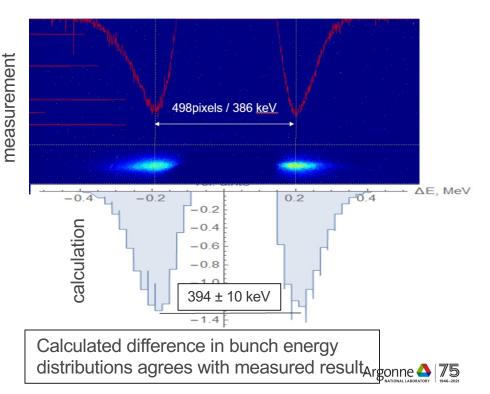


Corrugated Waveguide



Impact of the wakefield on slice medium energy

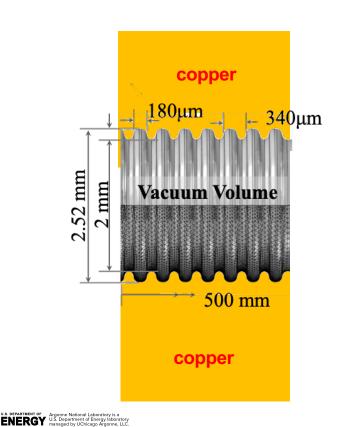
The measurement for the tube with smooth wall is subtracted from the corrugated waveguide measurement to show the effect of the corrugations.





CORRUGATED RF DESIGN OPTIMIZATION

Corrugation Geometry



RF Calculation

RF Simulation (CST)

Wakefield Simulation (ECHO)

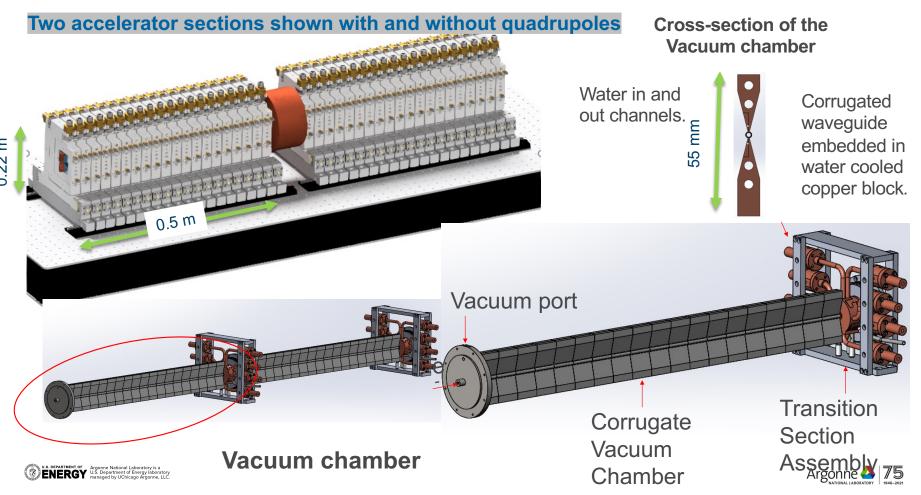
RF power produced in 50 cm long corrugated waveguide:

- TM01 expected power is ~<u>1kW.</u>
- TE11 expected power is $\sim 1 \text{mW}/\mu \text{m}^2$.
- TM11 dipole mode power is weaker than TE11.



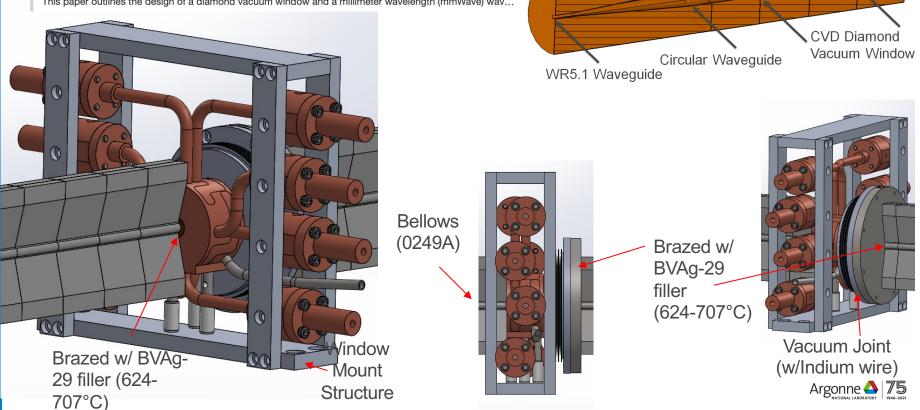
7

CWA MODULE



TRANSITION SECTION

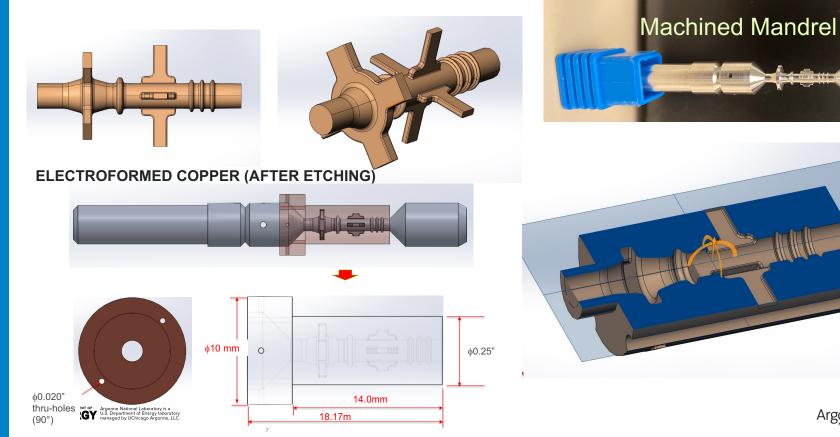
[TUPB06] Design of Miniature Waveguides and Diamond Window Assembly for RF Extraction and V... This paper outlines the design of a diamond vacuum window and a millimeter wavelength (mmWave) wav...



Double Window Section

Waveguide Transition (Rectangular to Circular)

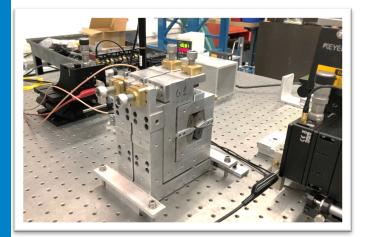
TRANSITION SECTION



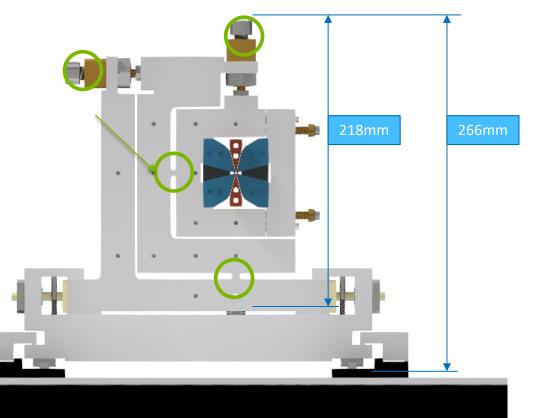
Argonne 合 75

QUADRUPOLE WIGGLER

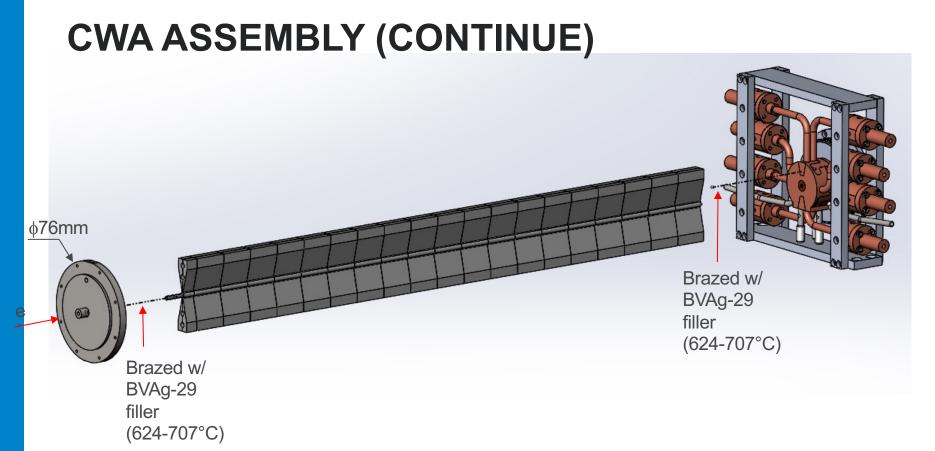
Requirement: quad-to-quad misalignment tolerance ≤ 1 µm



Two prototype quadrupoles on the bench for magnetic measurements. Bore radius: 1.5 mm; Gradient: 0.95 T/mm.



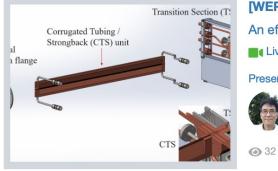




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PUBLICATION – MEDSI2020



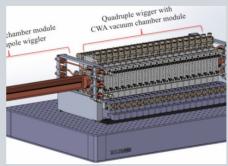
[WEPB04] Design and Fabrication Challenges of Transition Section for the CWA Module An effort to build Argonne's Sub-THz AcceleRator (A-STAR) for a future multiuser x-ray free-electron laser ... Live presentation starts on 07/28/2021

Presenters



Soonhong Lee Principal Mechanical ... Argonne National La...

 $\bigcirc 0$



[WEPB05] Mechanical Design of a Compact Collinear Wakefield Accelerator

The Argonne National Laboratory is developing a compact collinear wakefield accelerator (CWA) based on... Live presentation starts on 07/28/2021

Presenters



Soonhong Lee Principal Mechanical ... Argonne National La...

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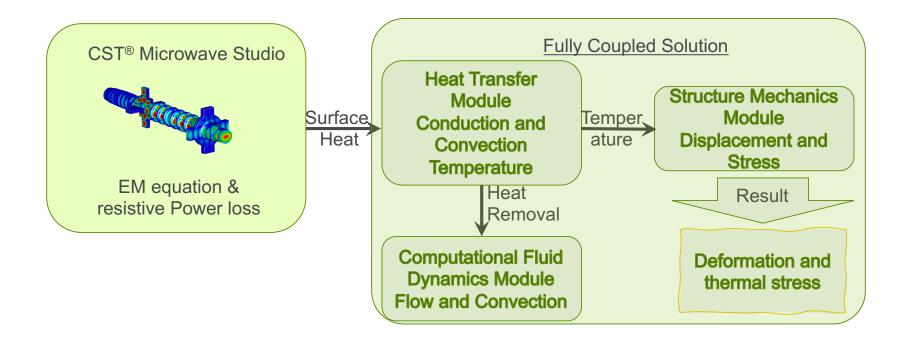
MULTIPHYSICS FEA



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MULTIPHYSICS FORMULATION



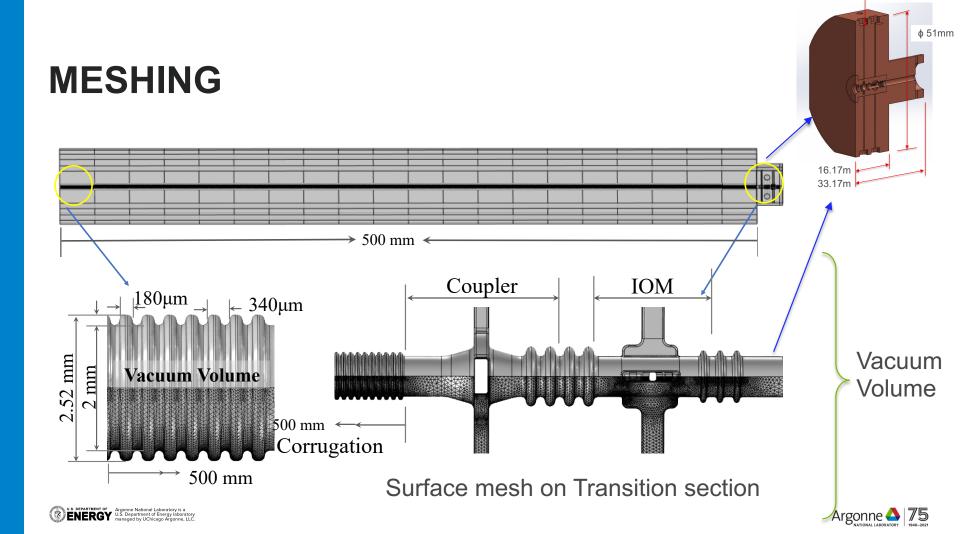




COMPUTATIONAL MODEL Boundary Conditions \rightarrow Heat Deposition Water Channels Water in Line of **Bellow Support** Fixed Support Water out **Roller Support** ← symmetry







PARAMETERS

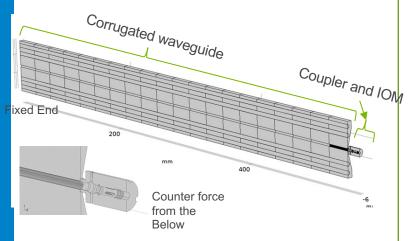
Rep rate vs heat load

Parameters	Rep. Rate (kHz)	Heat Load (W)
1	10	590
2	20	1181
3	30	1771
4	40	2362





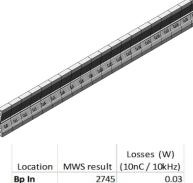
HEAT LOAD -10KHZ



- Bunch charge: 10 nC (180GHz Modified Bane function)
- Repetition rate: 50 kHz
- Copper reduced conductivity: 2.3e7
 S/m
- Total power in Cu: 21.81W (after ~4ns)
- Bunch loss factor: 46.76W

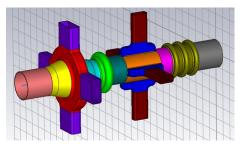


Corrugated Waveguide



		Losses (VV)	
Location	MWS result	(10nC / 10kHz)	
Bp In	2745	0.03	
Bp Out	1.11E+05	1.11	
Cu 1	3.94E+05	3.94	
Cu 2	9.90E+05	9.90	
Cu 3	1.48E+06	14.80	
Cu 4	1.91E+06	19.06	
Cu 5	2.24E+06	22.40	
Cu 6	2.54E+06	25.45	
Cu 7	2.77E+06	27.71	
Cu 8	2.99E+06	29.90	
Cu 9	3.14E+06	31.40	
Cu 10	3.30E+06	33.00	
Cu 11	3.40E+06	34.00	
Cu 12	3.52E+06	35.20	
Cu 13	3.58E+06	35.80	
Cu 14	3.67E+06	36.70	
Cu 15	3.70E+06	37.00	
Cu 16	3.77E+06	37.70	
Cu 17	3.79E+06	37.88	
Cu 18	3.84E+06	38.44	
Cu 19	3.85E+06	38.49	
Cu 20	3.96E+06	39.57	
Total	58947445	589.47	

Transition Section



Part Name	Color	Power [W]	Area [mm^2]	[W/cm^2]
Cyl_WG_In		156mW	12.56	1.24
Taper_In		267mW	10.20	2.62
TM01_Cavity		16.93W	32.35	52.3
TM01_WR_Out		2.39W	31.45	7.60
Taper_Out		284mW	10.20	2.78
TM01_Convolution		366mW	12.40	2.95
TM01_IOM_Spacer		130mW	7.23	1.80
IOM_Cylinder_Wall		209mW	11.54	1.81
IOM_Step		138mW	20.56	0.67
IOM_WR_Out		47mW	25.01	0.19
IOM_Notch_Spacer		97mW	5.93	1.64
IOM_Notch_Filter		651mW	22.48	2.90
Cyl_WG_Out		143mW	12.56	1.14

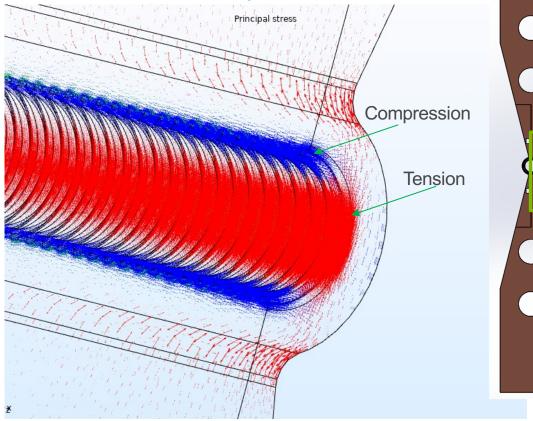
TM01_Cavity has high Q ringing at 110GHz. Simulation results are extrapolated to estimate total power loss. Argonne 75

THERMAL STRESS

Thermal Stress and Strain

CTE: $\alpha = 17.7 \times 10^{-6} \ m/m/C^{o}$ Volume average temperature rise: $T = 5.5^{\circ}$ C Length: L = 0.5mThermal Strain : $\frac{\varepsilon_T}{L} = \alpha T$ Thermal Strain : $\Delta L = 48.675 \mu m$ Thermal Stress: $\sigma_T = \varepsilon_T E$ Mod. Of elasticity: E = 110GPa $\sigma_T = \frac{48.675 \mu m \cdot 110 GPa}{0.5m}$

Average stress : $\sigma_T = 10.7 MPa$



Principal Stress

Principal Stress in Tension

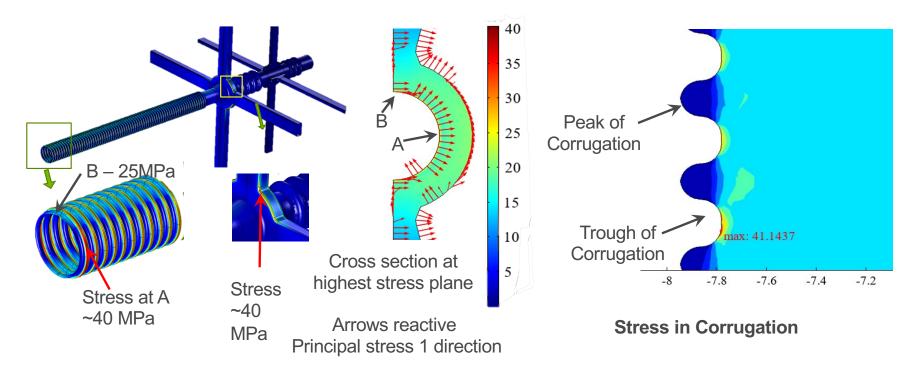




Principal Stress in compression



SURFACE STRESS

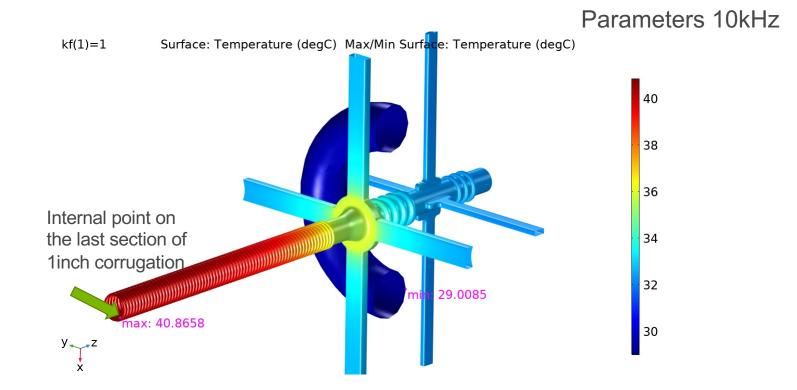


Von Mises Stress Profile





TEMPERATURE PROFILE FOR CASE # 1 (HEAT LOAD 590W)

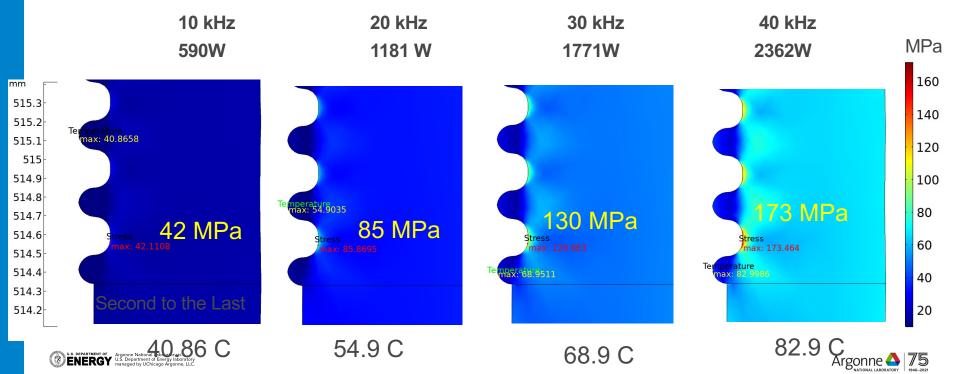


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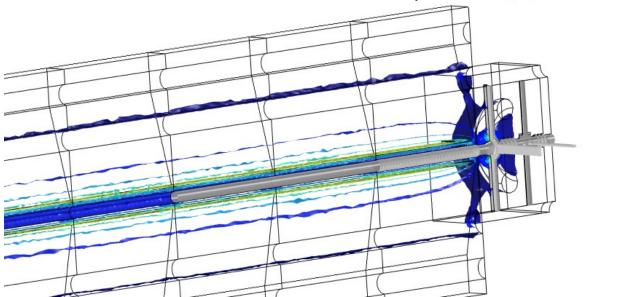
STRESS PROFILE WITH MAXIMUM TEMPERATURE MARKED ON THE THINNEST SECTION OF THE CORRUGATION

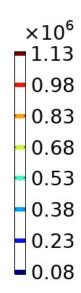
Last few Corrugation Sections



ISOSURFACE OF TEMPERATURE AND HEAT FLUX

kf(1)=1 Isosurface: Conductive heat flux magnitude (W/m²) Surface: Temperature (K)

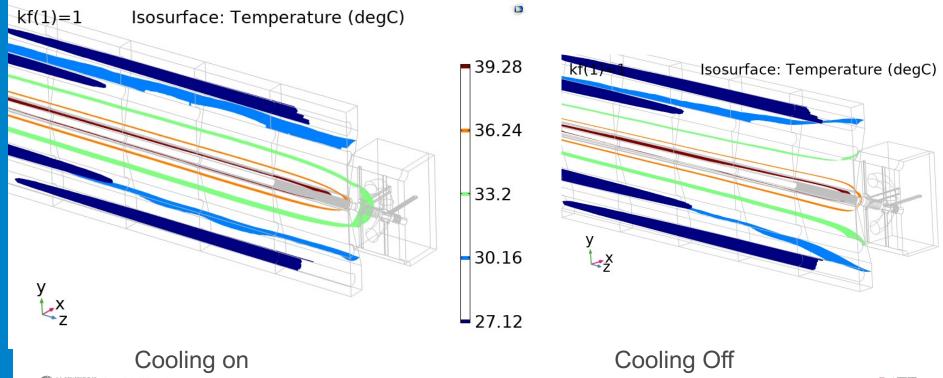


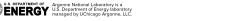






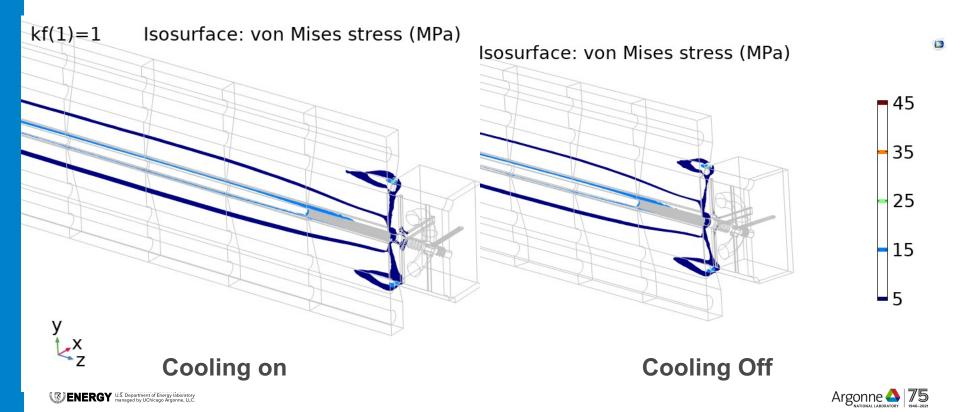
TEMPERATURE COMPARISON



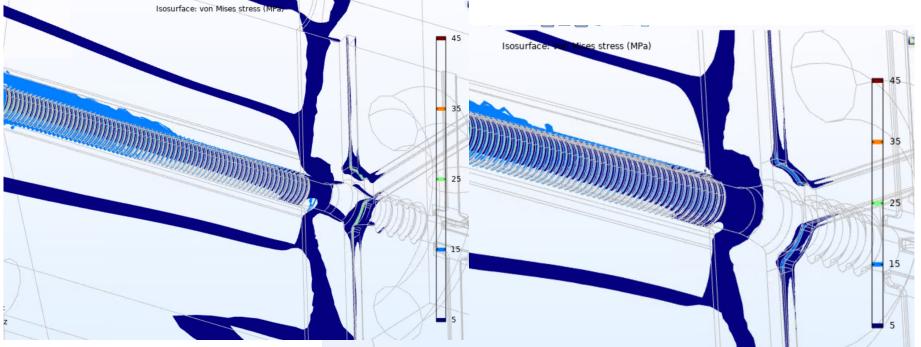


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STRESS COMPARISON



STRESS COMPARISON



Cooling on



Cooling Off



CONCLUDING SLIDE

- The accelerator design is primarily controlled by thermal stress at the trough region
- Thermal load is linearly increasing along the length.
- The maximum temperature doesn't occur at the extreme end rather it is occurring 5-10 mm away from the end towards the upstream
- Therefore, the trough area near this end of the corrugation showed higher stress
- In order to reduce the thermal stress and equalize the heat distribution we decided not to cool transition section, which has improved the thermal stress by expansion.
- We were able to optimize the rep-rate to 15 kHz level as compared to an excessive cooling design which showed 11 kHz of heat load as maximum possible limit.





FABRICATION



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PROTOTYPING BY ELECTROFORMING

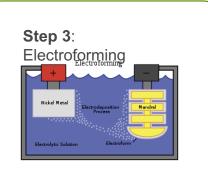
Step 1: Mandrel Design



The mandrel is the base machined component, typically made from Aluminum 6061T which defines the internal geometry of an electroform.



Electroforms can be manufactured to less than a 0.5mm diameter with a wall thickness of less than 0.008mm.



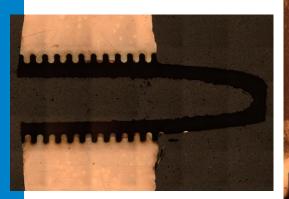


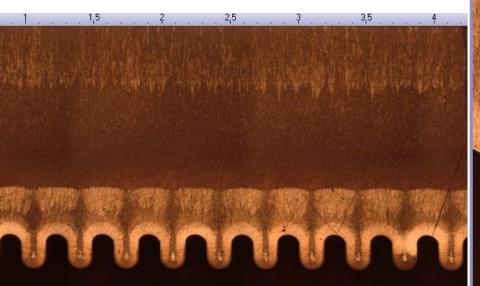
Step 4: Removing the Mandrel





AFTER IMPROVED DESIGN



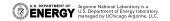


[TUPC01] Study of Copper Micro Structure Produced by Electroforming for the 180 GHz Frequency ... Fabrication of the corrugated structure that generates a field gradient 100 m^-1 at 180 GHz is challenging...



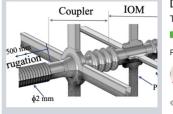
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A-STAR DEVICE GROUP PUBLICATION



[TUPB06] Design of Miniature Waveguides and Diamond Window Assembly for RF Extraction and V... This paper outlines the design of a diamond vacuum window and a millimeter wavelength (mmWave) wav... Live presentation starts on 07/27/2021 Presenters Alexander Zholents Kamlesh Suthar Principal Mechanical ... Scientist Argonne National La... ANL Enter







Live presentation starts on 07/27/2021

Presenters

Porous or sparse grain boundaries can decreat increase electrical resistivity and cause variation

(Left) Electroformed cooper remains uniform a

(Center) When fully annealed, the microstructs

grow to roughly 8 µm in diameter with void coa

(Right) A typical microstructure of oxygen-free large grains, variations in crystallographic orier (linear bands within grains).

I grains at the apex of each corrugation single crystal follow the seed layer contour

lization preferentially oriented away from (2)

st amorphous, and the highest hardness region crystallization characteristics as region (4)

s character

inct interface between dark and light regis change (noted as region (4) in panel at left).





ENERGY Argonne National Laboratory U.S. Department of Energy & managed by UChicago Argo



Enter

Gary Navrotski **Research Engineer** Argonne National La...

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Thank you



We thank our colleagues, W. Jansma, A. Nassiri, B. Popovic, and J. Xu for useful discussions.

This material is based upon work supported by Laboratory Directed Research and Development (LDRD) funding from Argonne National Laboratory, provided by the Director, Office of Science, of the U.S. Department of Energy under Contract No. DE-AC02-06CH11357.