

Design and FEA of an Innovative Rotating SiC Filter for High-Energy X-ray Beam

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T. Connolley

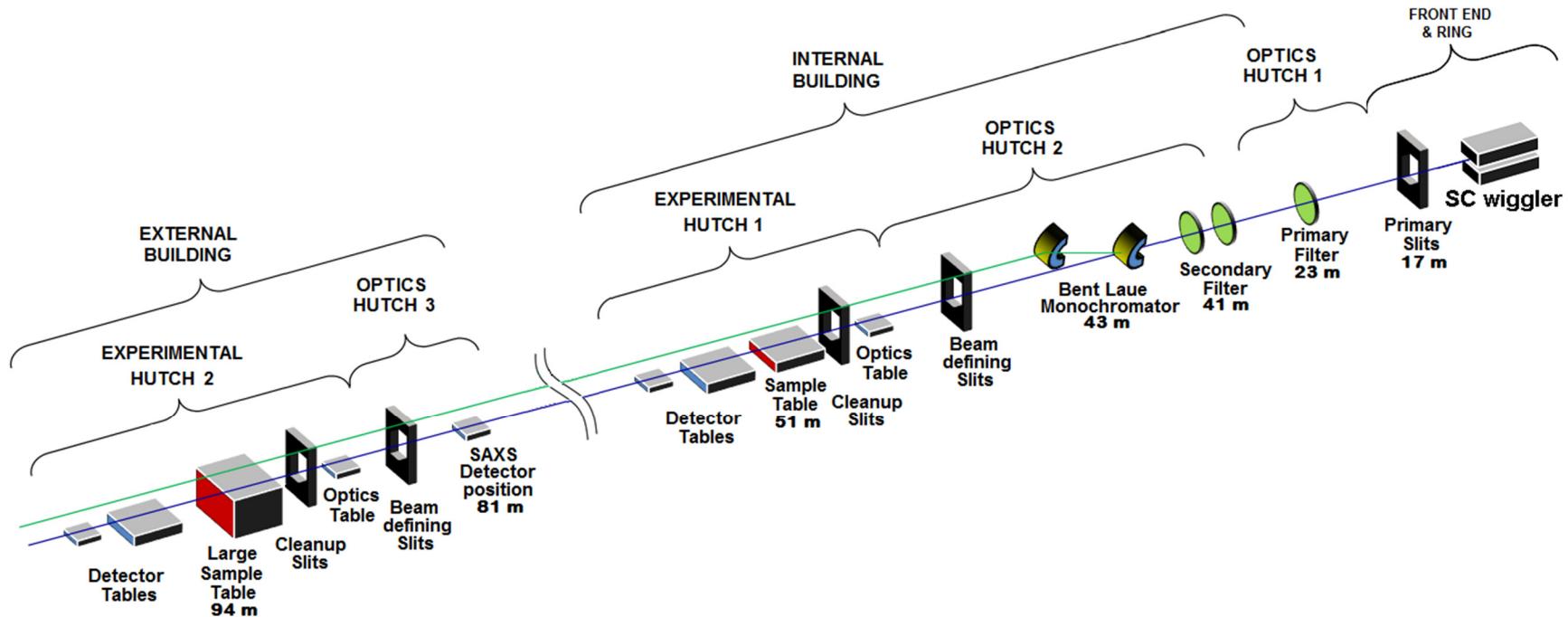
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G. E. Howell

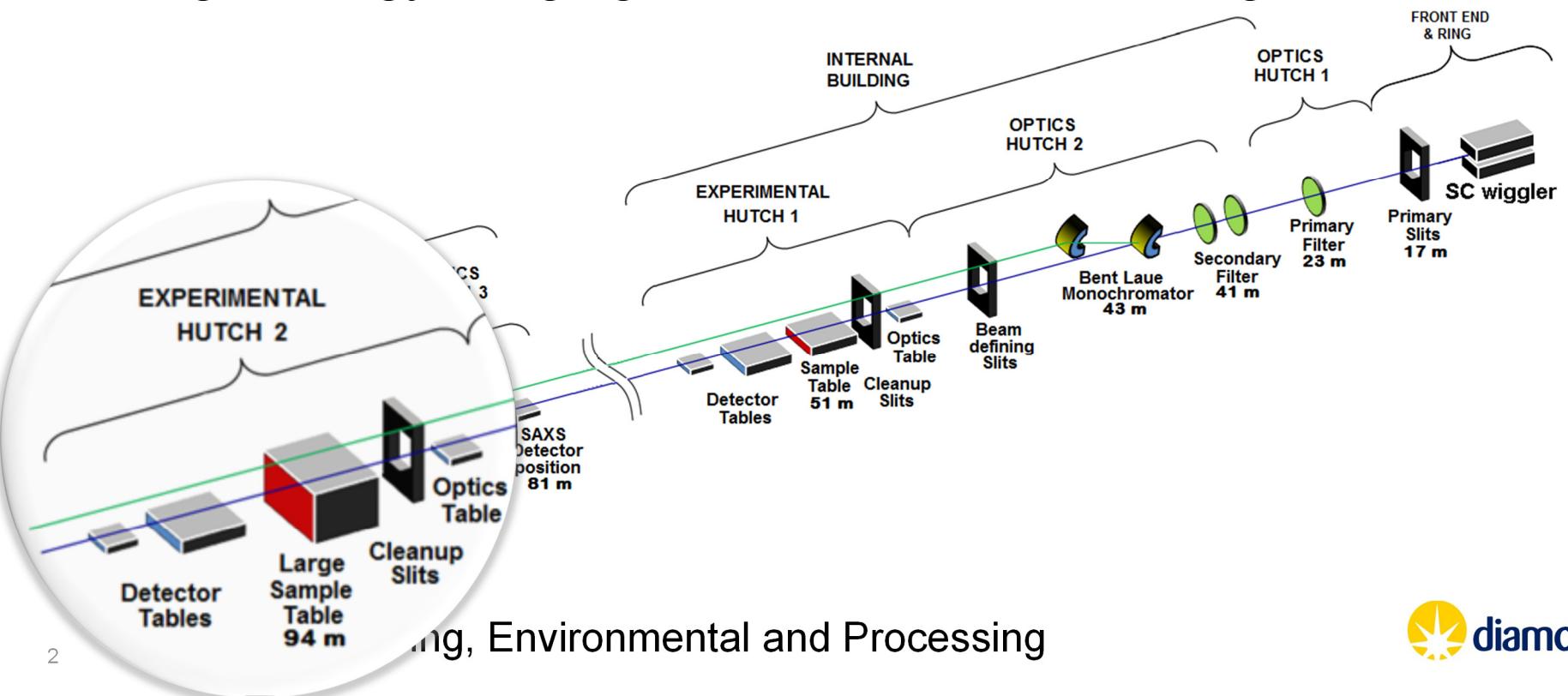
I12 JEEP*

A high energy imaging, diffraction and scattering beamline



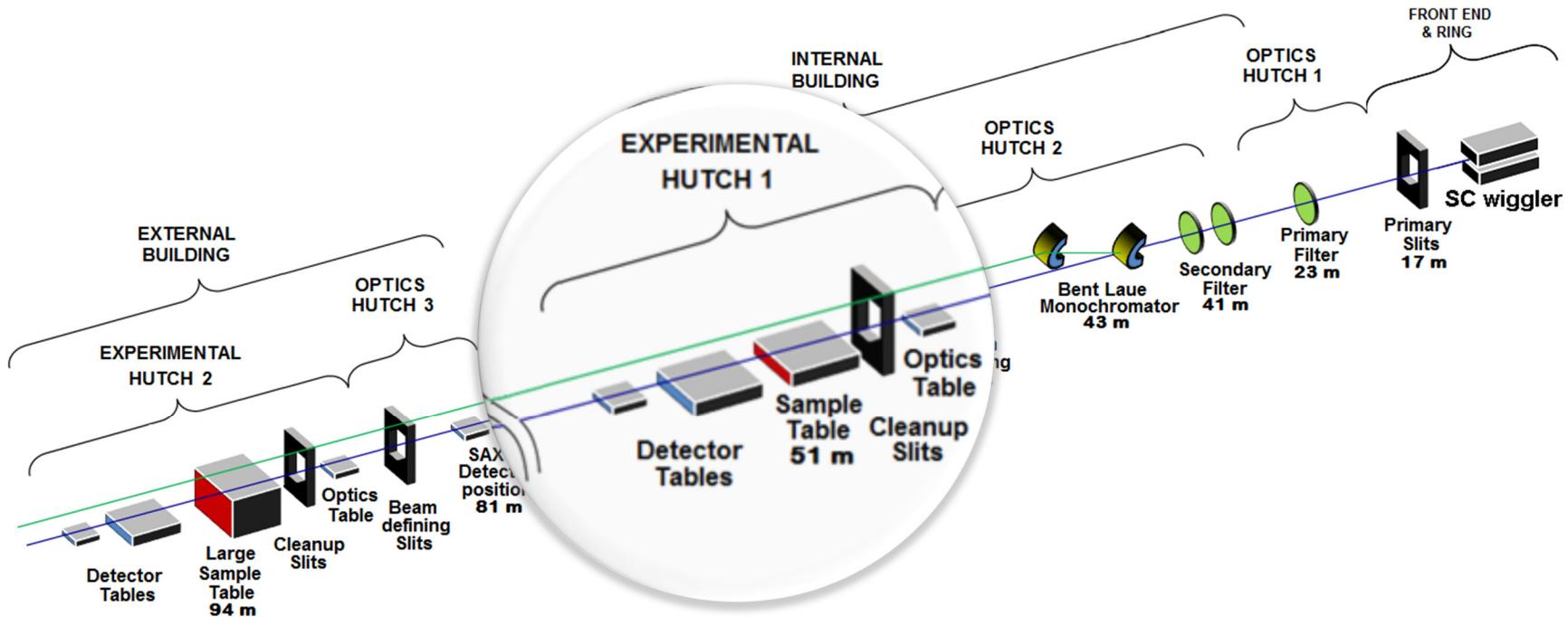
I12 JEEP*

A high energy imaging, diffraction and scattering beamline



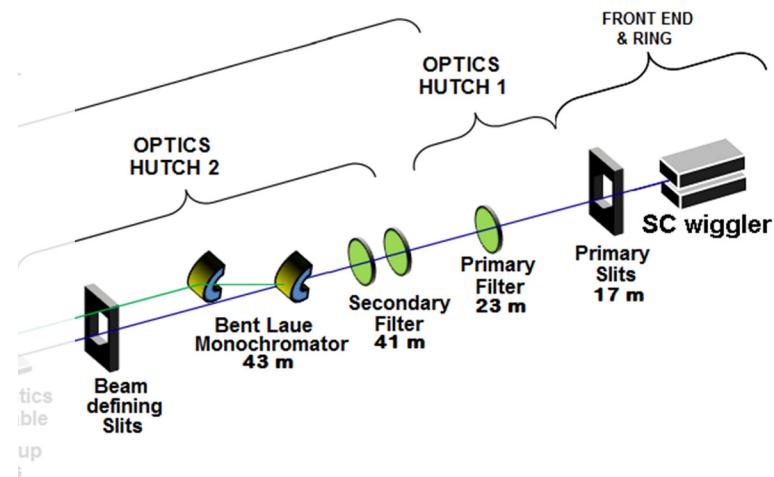
I12 JEEP*

A high energy imaging, diffraction and scattering beamline

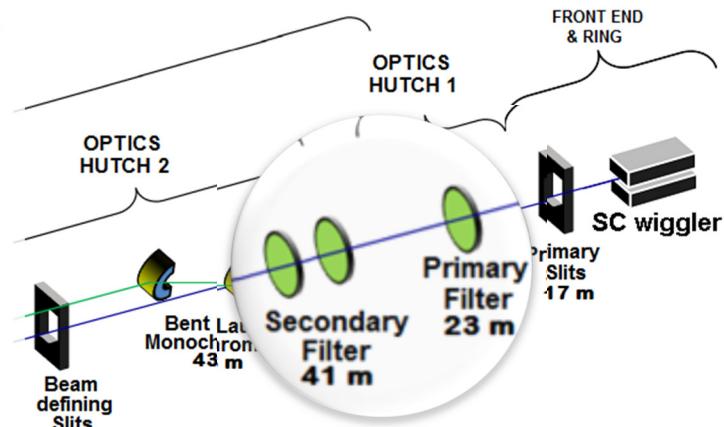
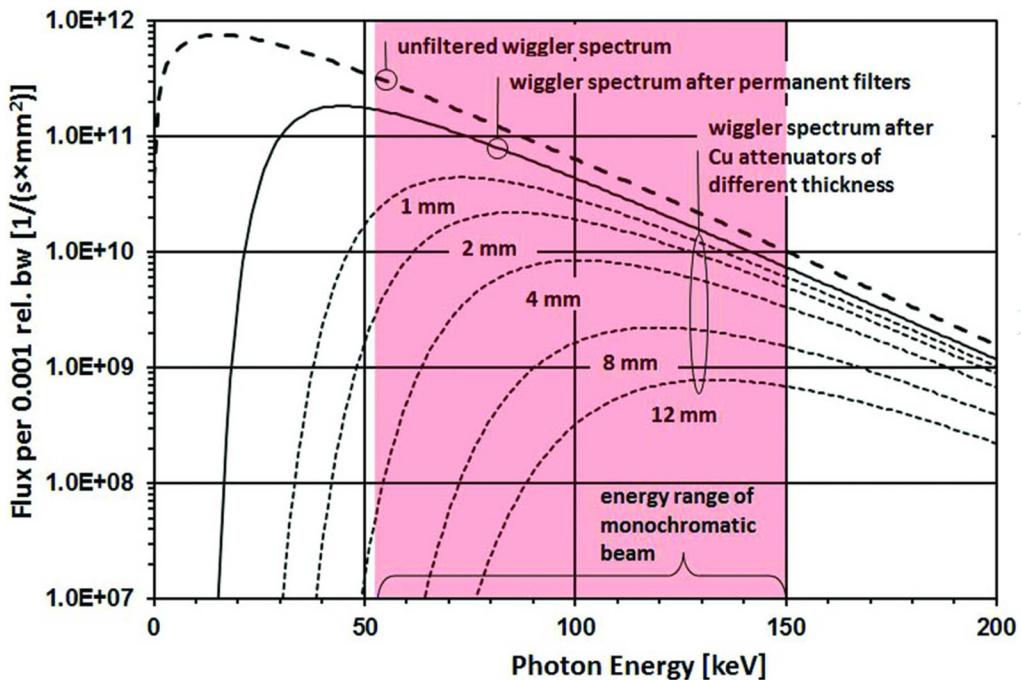


ID, Front End and Optics

Source	Super-conducting wiggler 4.2 T, 48mm periodicity, 22 periods
Monochromator	Cryo-cooled double crystal bent Laue
Primary filter	CVD diamond
Secondary filter	SiC disk
Energy range	50-150 keV

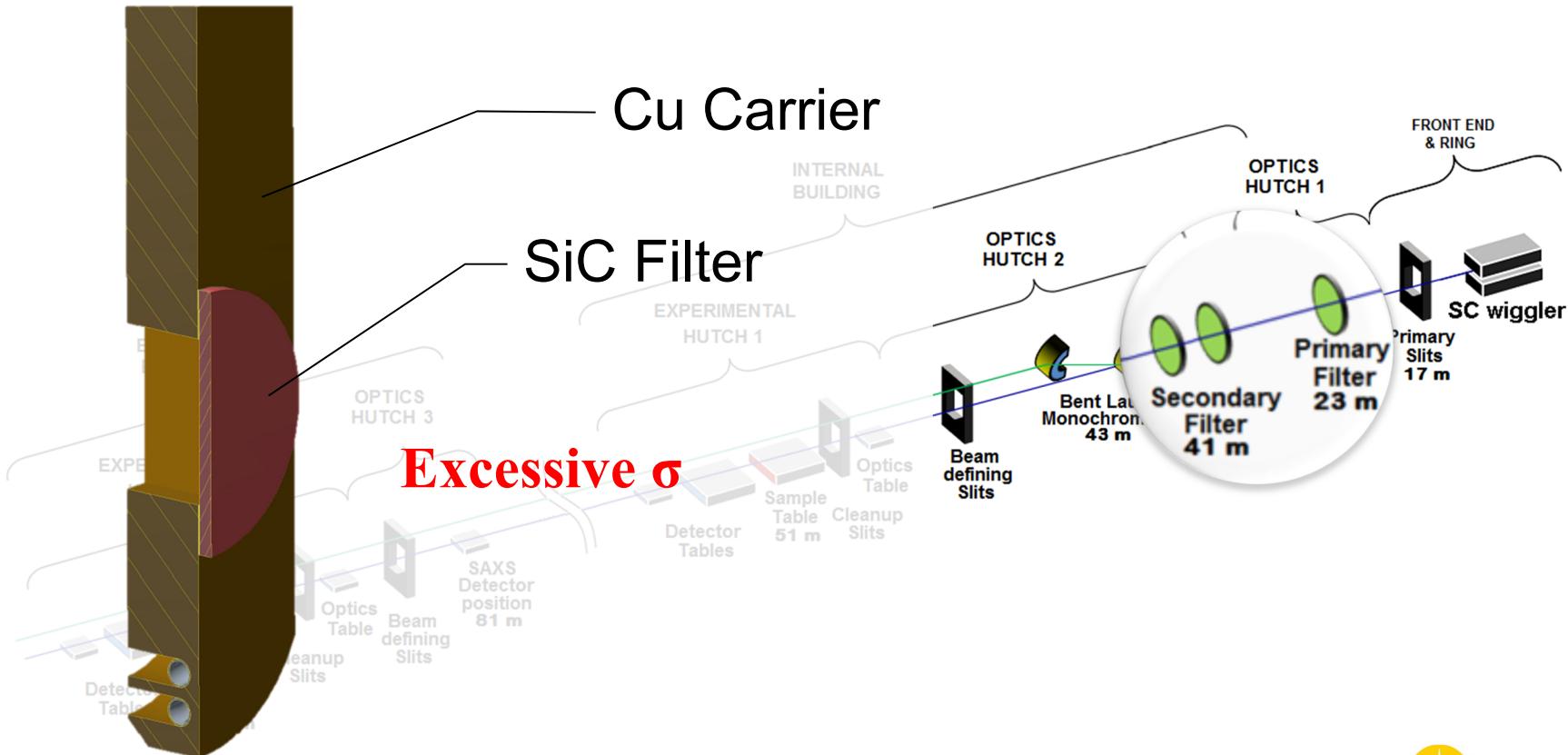


Heat Load Management

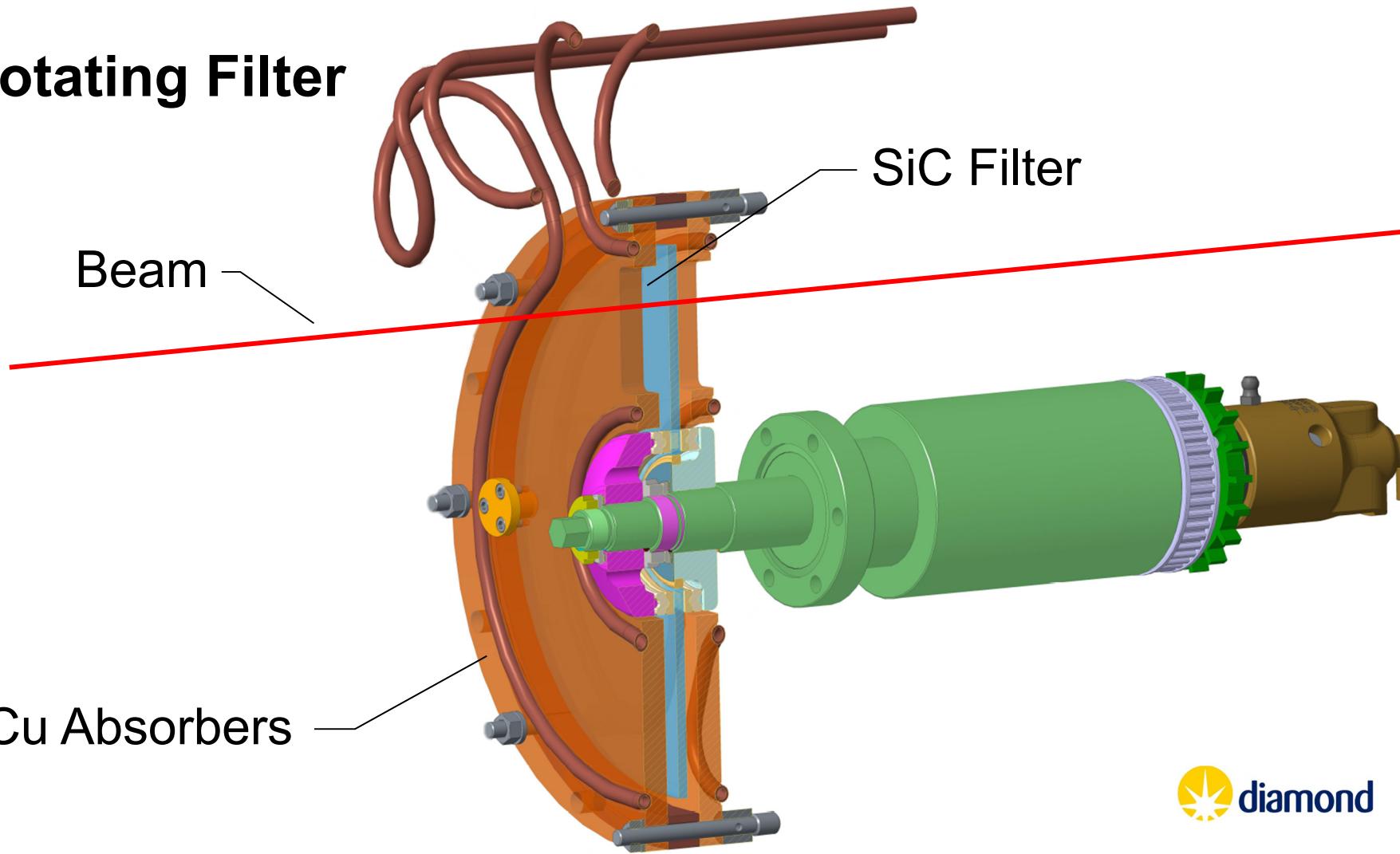


9 kW @ 500 mA after front-end
6.2 kW after primary filter
2.6 kW after secondary filter

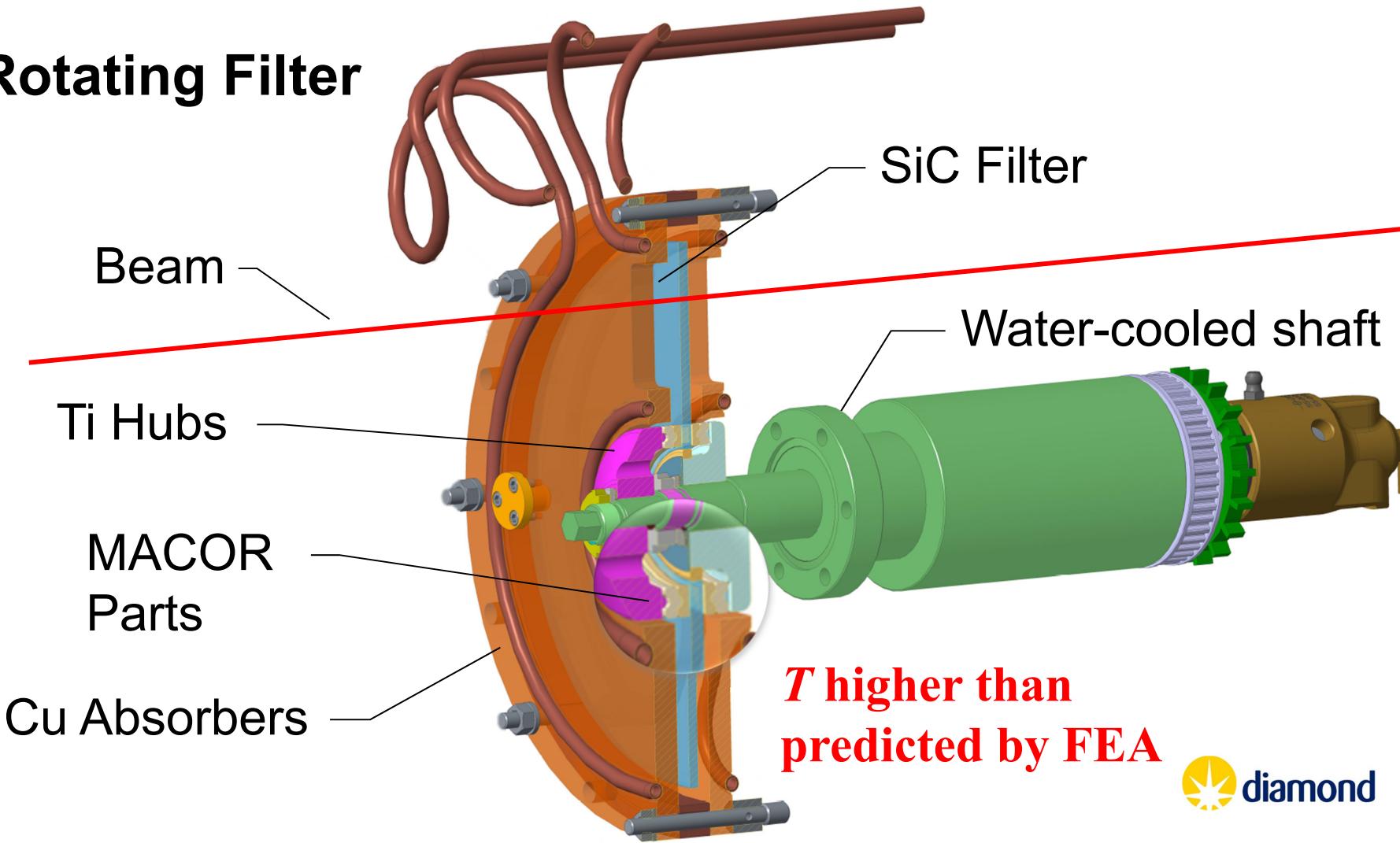
Secondary Static Filter



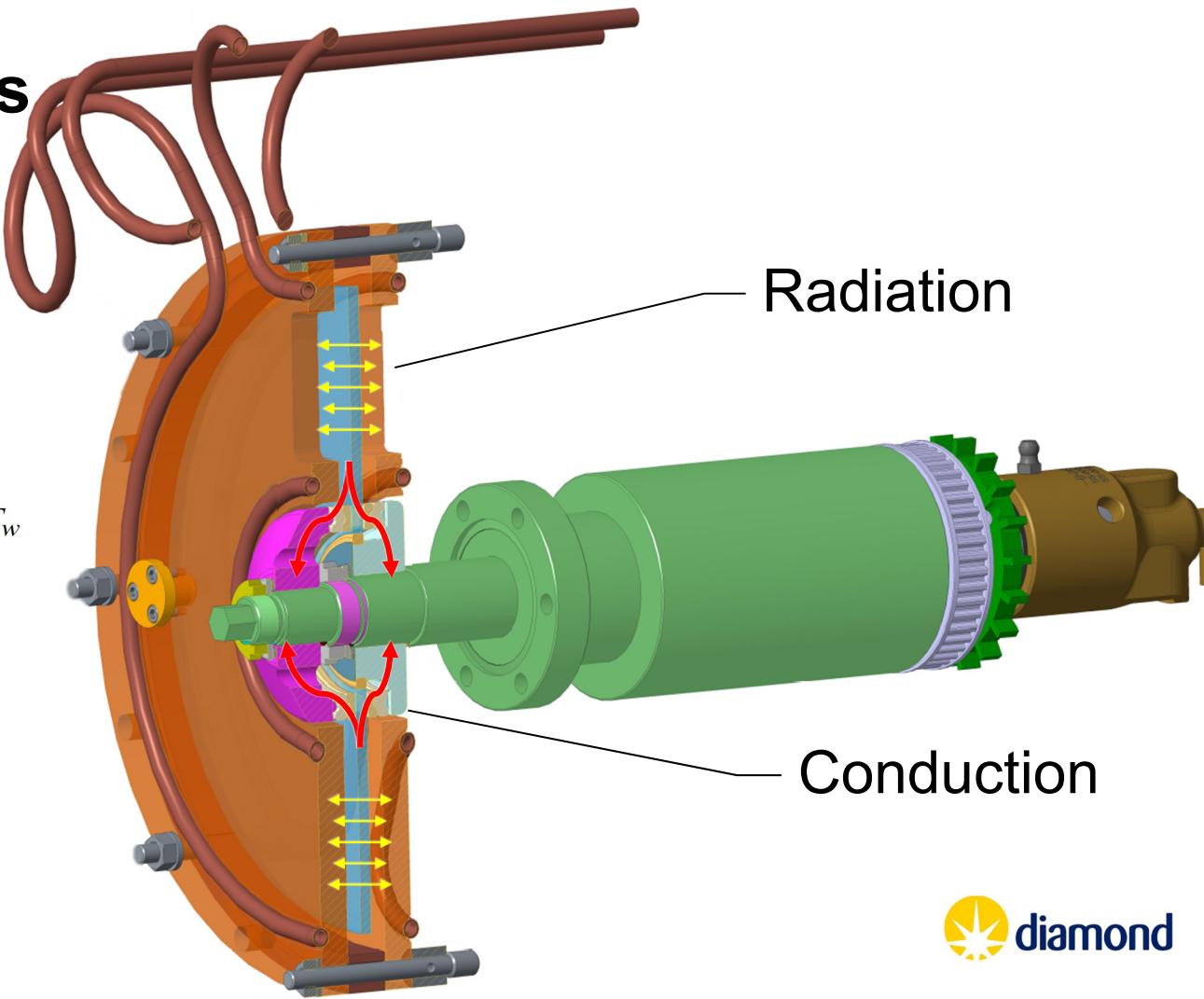
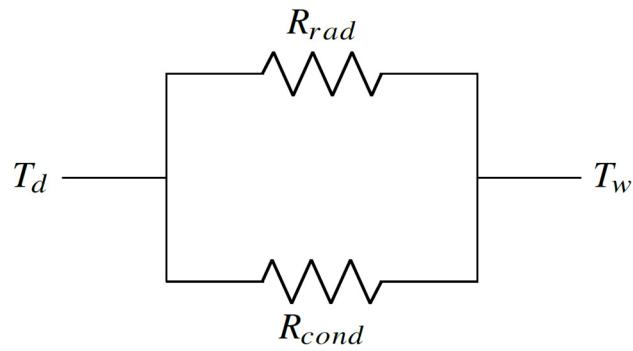
Rotating Filter



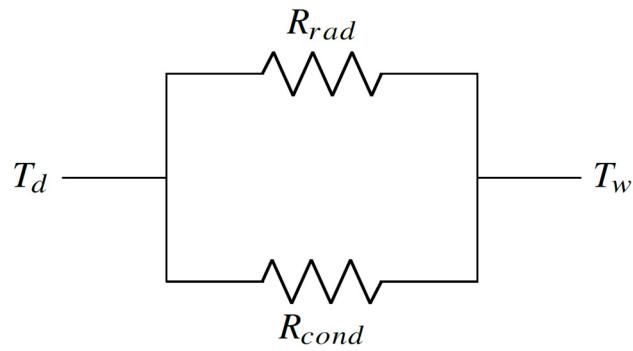
Rotating Filter



Failure Analysis



Circuit Analogy



Boundary conditions

Heat load, convection
(h coefficient, T_w ...)

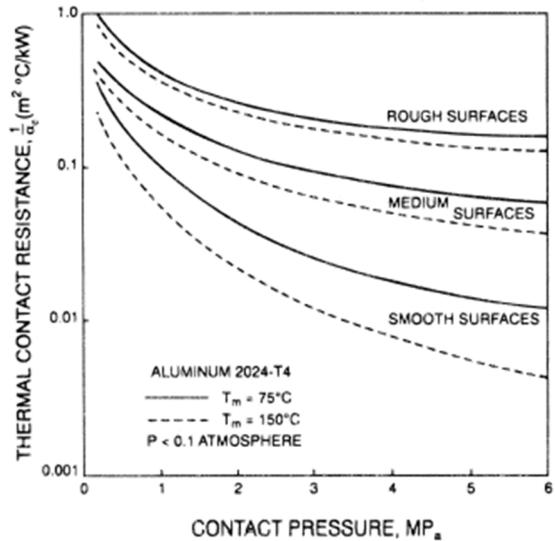
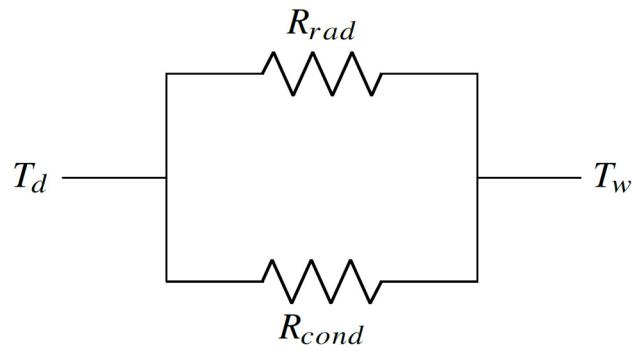
Radiation

Emissivity ε , geometry
and view factor

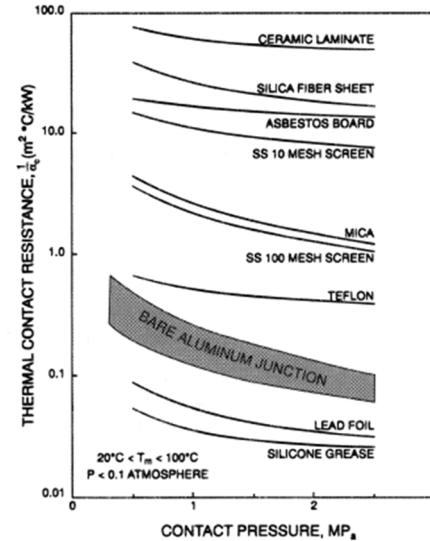
Conduction

Materials (conductivity)
and geometry; contacts

Circuit Analogy

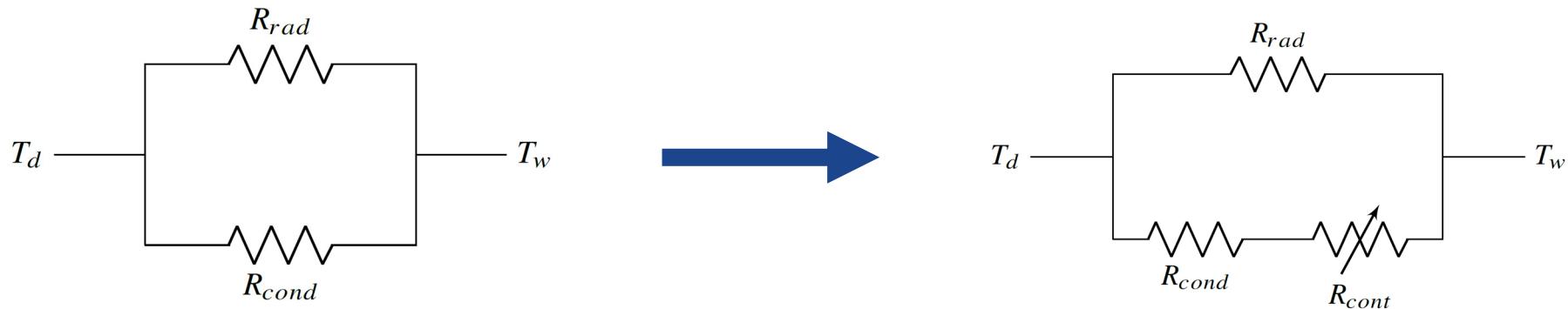


Conduction



Materials (conductivity) and geometry; contacts

Estimating the Thermal Contact Resistance

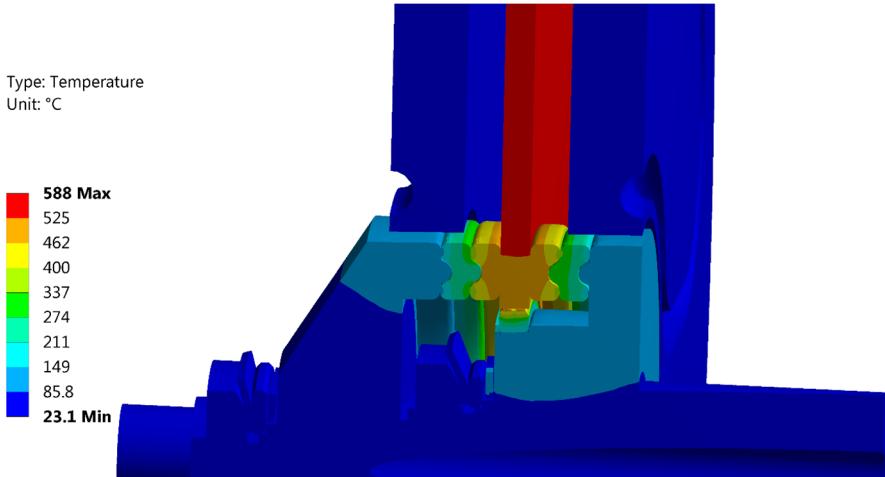


$T_d \approx 780^\circ\text{C}$, measured with a LAND SoloNet SN21 Infra-red pyrometer looking at the SiC disc through a viewport

Effect of TCR

$\text{TCR} \approx 0^*$
60% of Q to the shaft

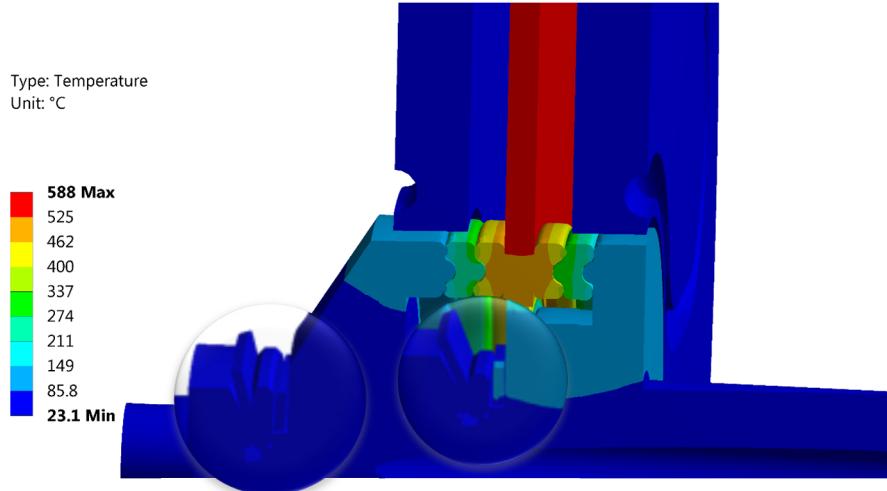
Type: Temperature
Unit: °C



$$^*TCC = K_{xx} 10^3 / ASM_{diag}$$

Effect of TCR

$\text{TCR} \approx 0^*$
60% of Q to the shaft

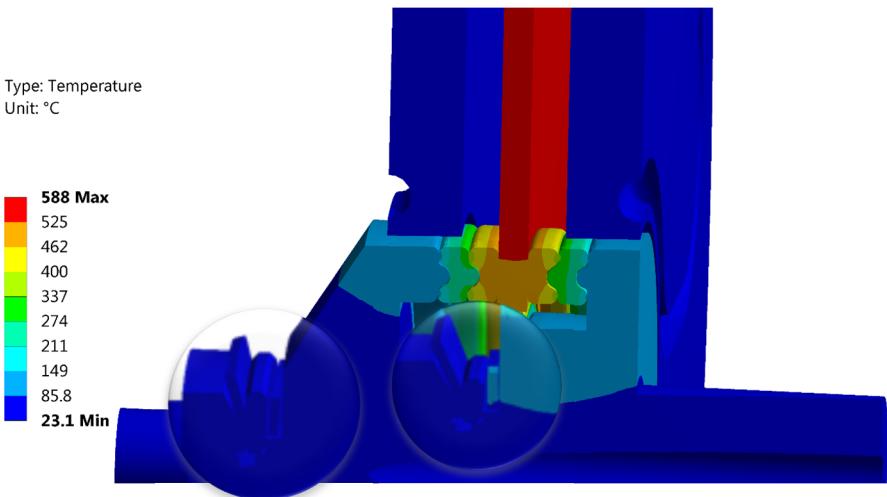


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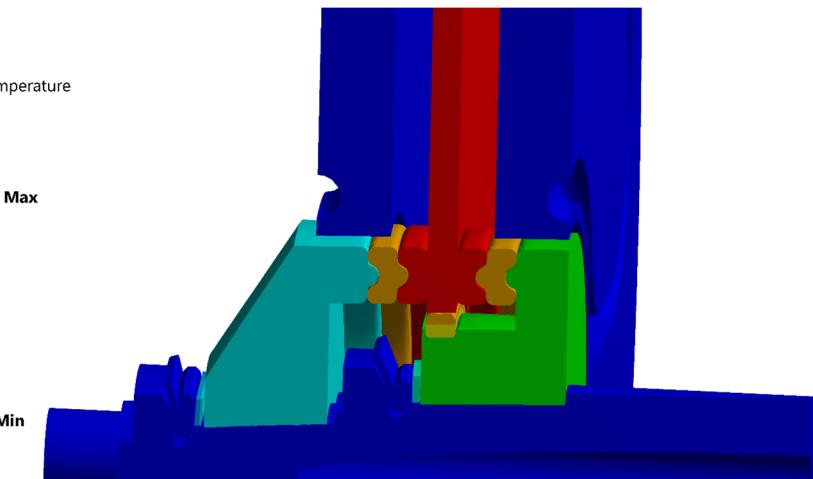
Type: Temperature
Unit: °C



$$\text{TCR} = 5 \frac{m^2 \cdot ^\circ\text{C}}{kW}$$

11% of Q to the shaft

Type: Temperature
Unit: °C

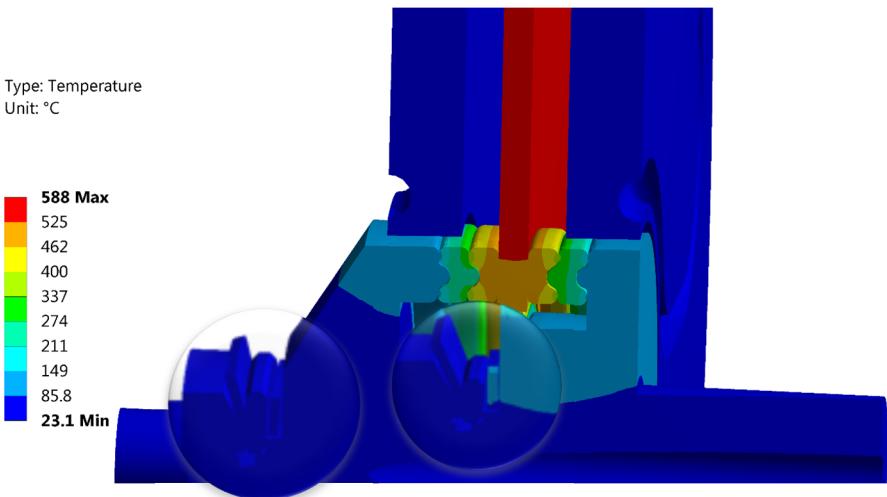


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Type: Temperature
Unit: °C

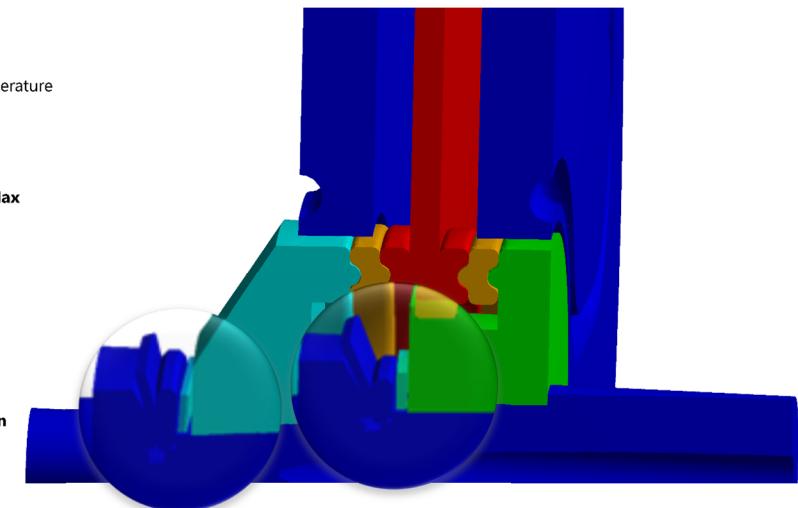


$$TCR = 5 \frac{m^2 \cdot ^\circ C}{kW}$$

11% of Q to the shaft

High TCR for metal parts!

Type: Temperature
Unit: °C

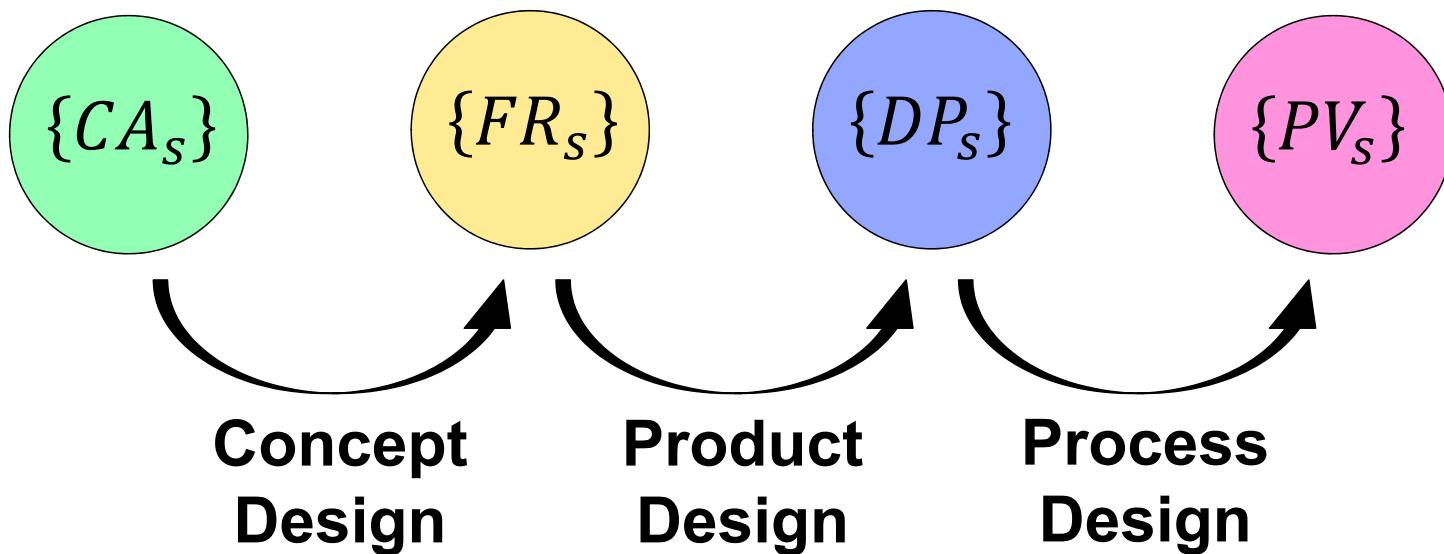


* $TCC = K_{xx} 10^3 / ASM_{diag}$

Axiomatic Design

Four design domains

Customer $\{CA_s\}$, Functional $\{FR_s\}$, Physical $\{DP_s\}$, Process $\{PV_s\}$; The relationship between them is modelled with matrices.



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Independence Axiom

Functional Requirements should be independent:

$$\begin{cases} FR_1 \\ FR_2 \end{cases} = \begin{bmatrix} a_{1,1} & a_{1,2} \\ a_{2,1} & a_{2,2} \end{bmatrix} \begin{cases} DP_1 \\ DP_2 \end{cases}$$

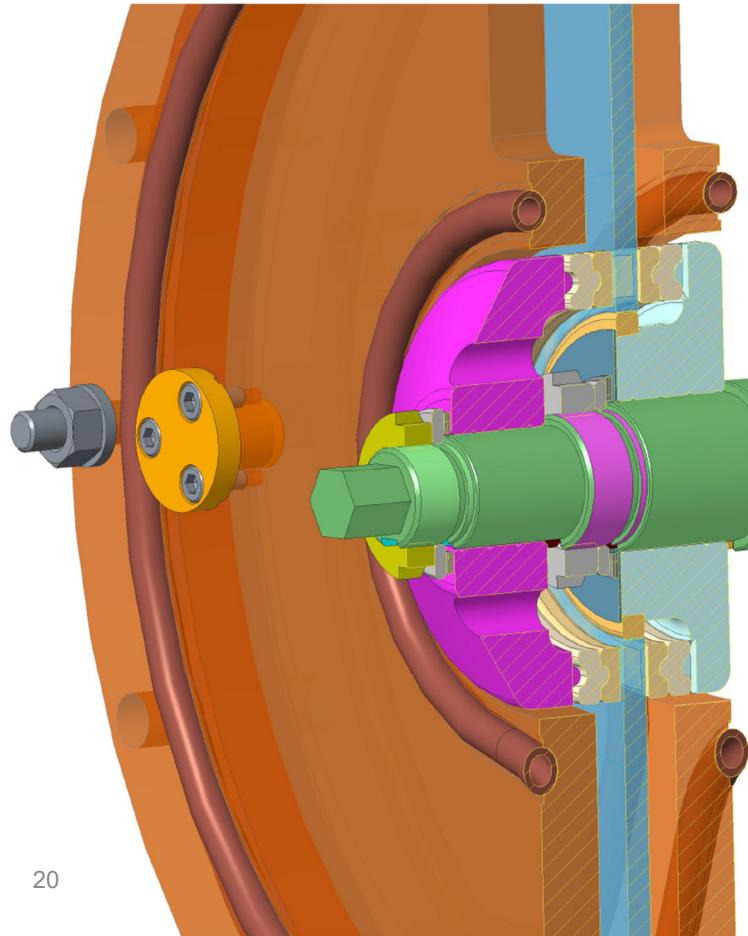
The matrix $[A]$ should be diagonal.

Information Axiom

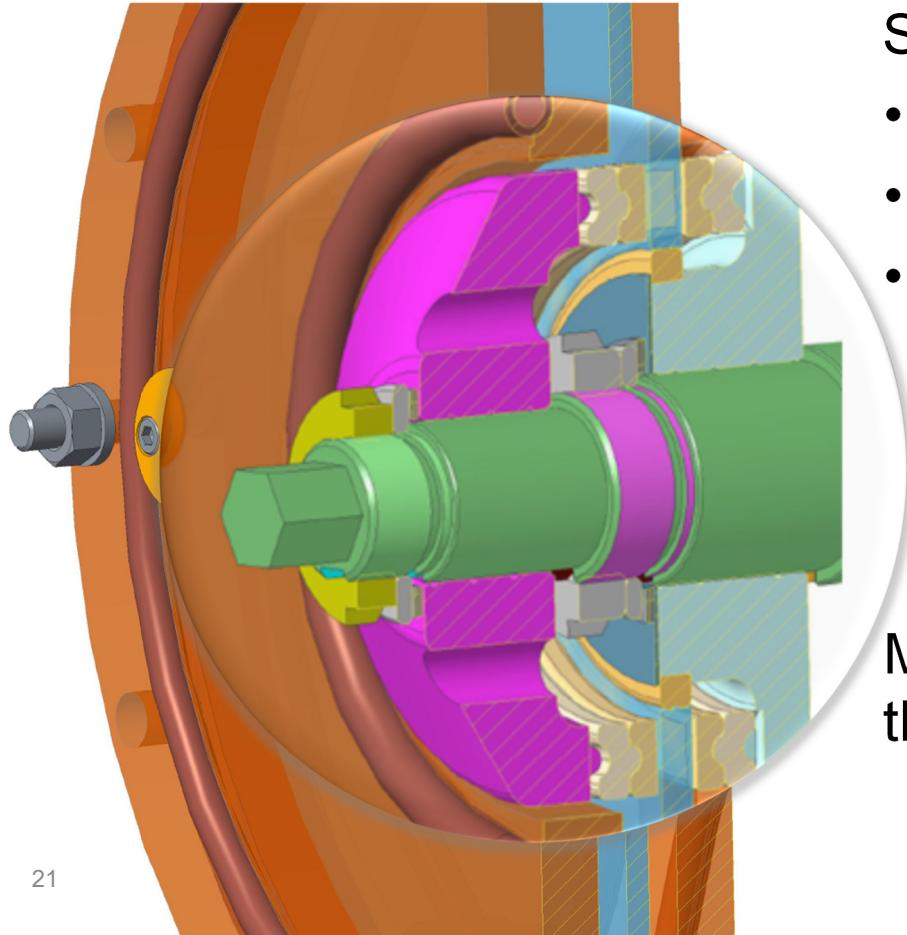
Information content should be minimised:

$$I = \log_2 \frac{1}{P} = -\log_2 P$$

Axiomatic Design



Axiomatic Design



Subassembly with hubs and shaft:

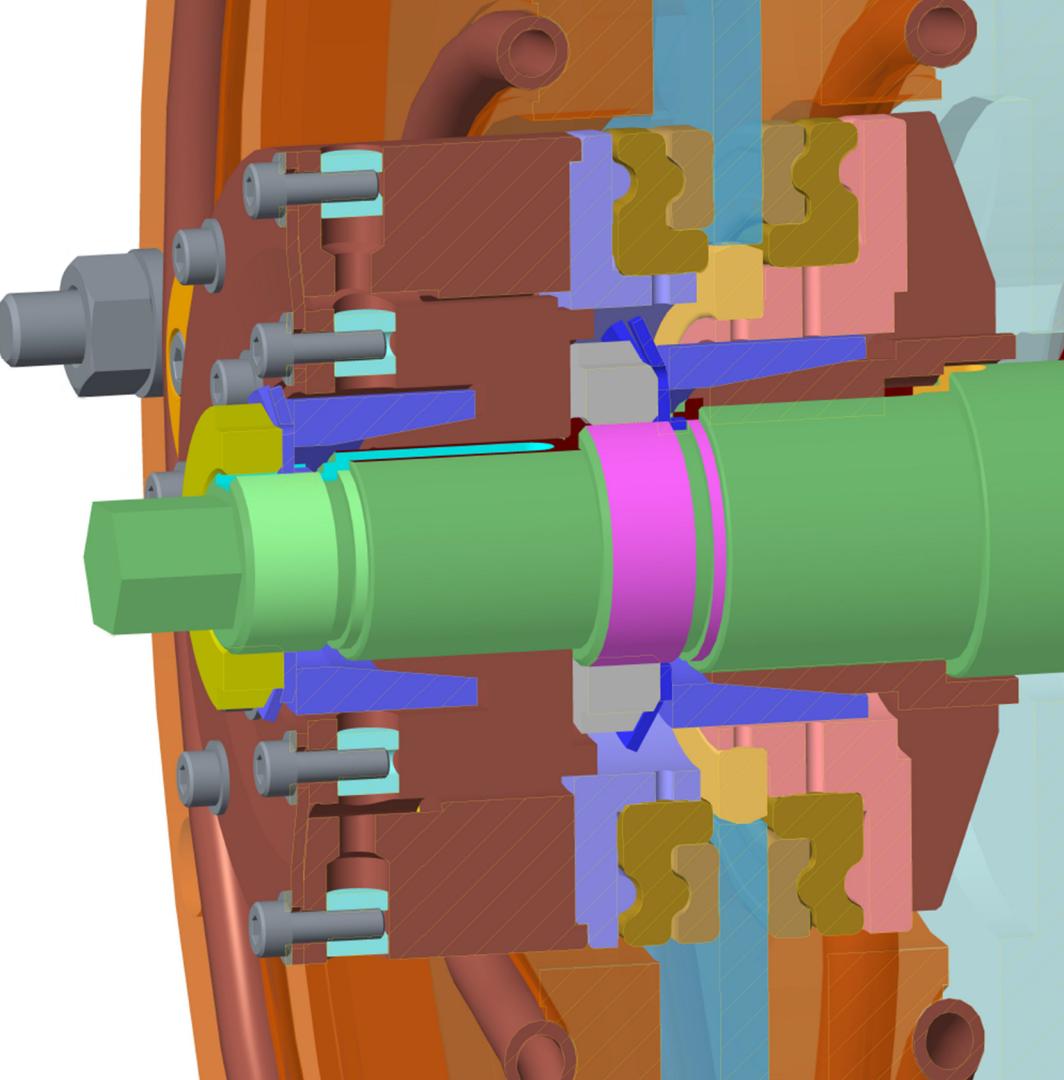
- Can assemble $\{FR_1\}$
- Transfers heat $\{FR_2\}$
- Contact pressure $x \{DP_1\}$

$$\begin{cases} FR_1 \\ FR_2 \end{cases} = \begin{bmatrix} a_{1,1} & 0 \\ a_{2,1} & 0 \end{bmatrix} \begin{cases} x \\ 0 \end{cases}$$

Coupled design

Moreover, x depends on ΔT ;
thermal runaway (positive feedback)

Final Design



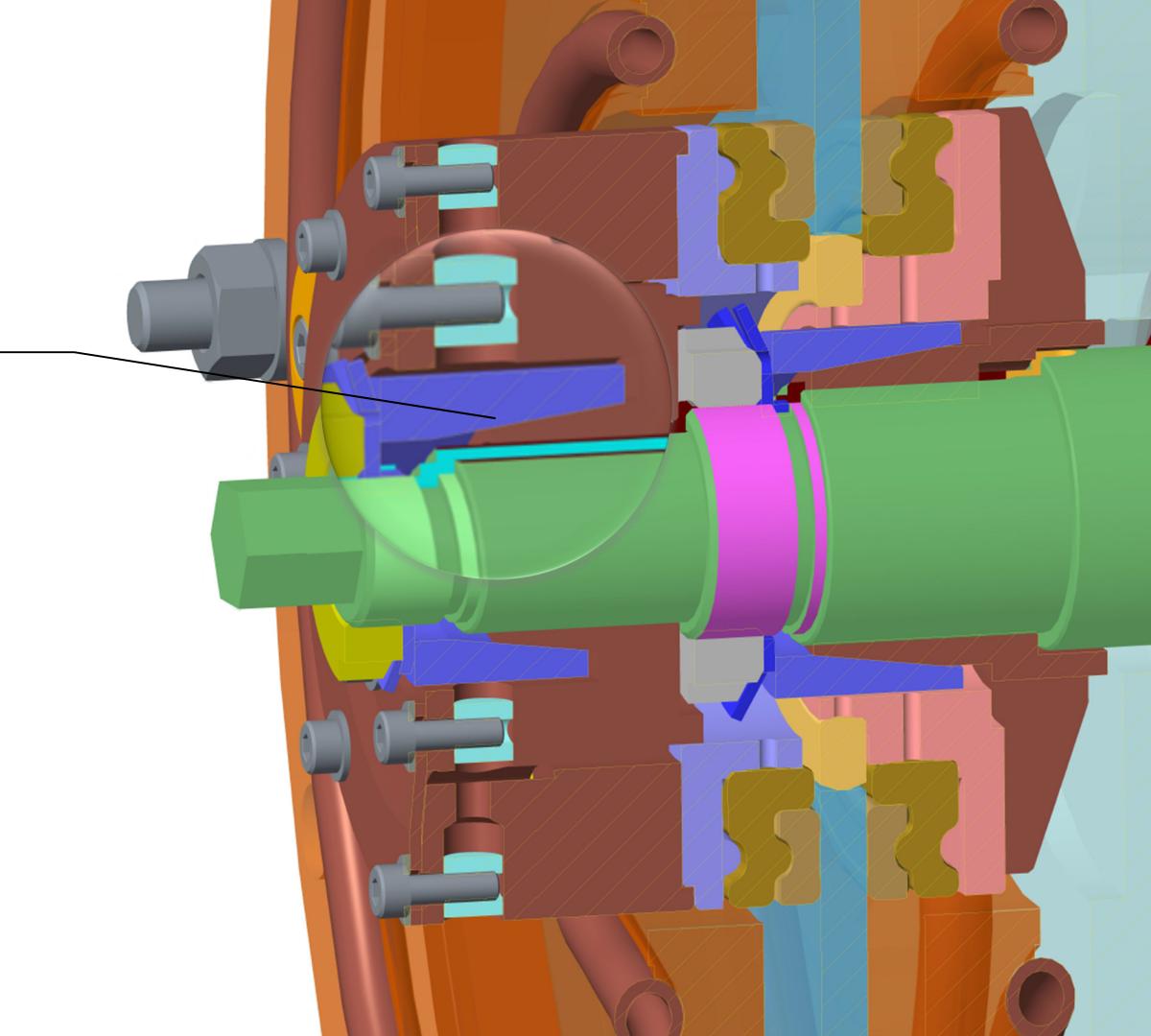
Final Design

Wedges

$$\begin{Bmatrix} FR_1 \\ FR_2 \end{Bmatrix} = \begin{bmatrix} a_{1,1} & 0 \\ 0 & a_{2,2} \end{bmatrix} \begin{Bmatrix} x \\ y \end{Bmatrix}$$

Uncoupled design

Also, y depends on ΔT ;
(negative feedback)



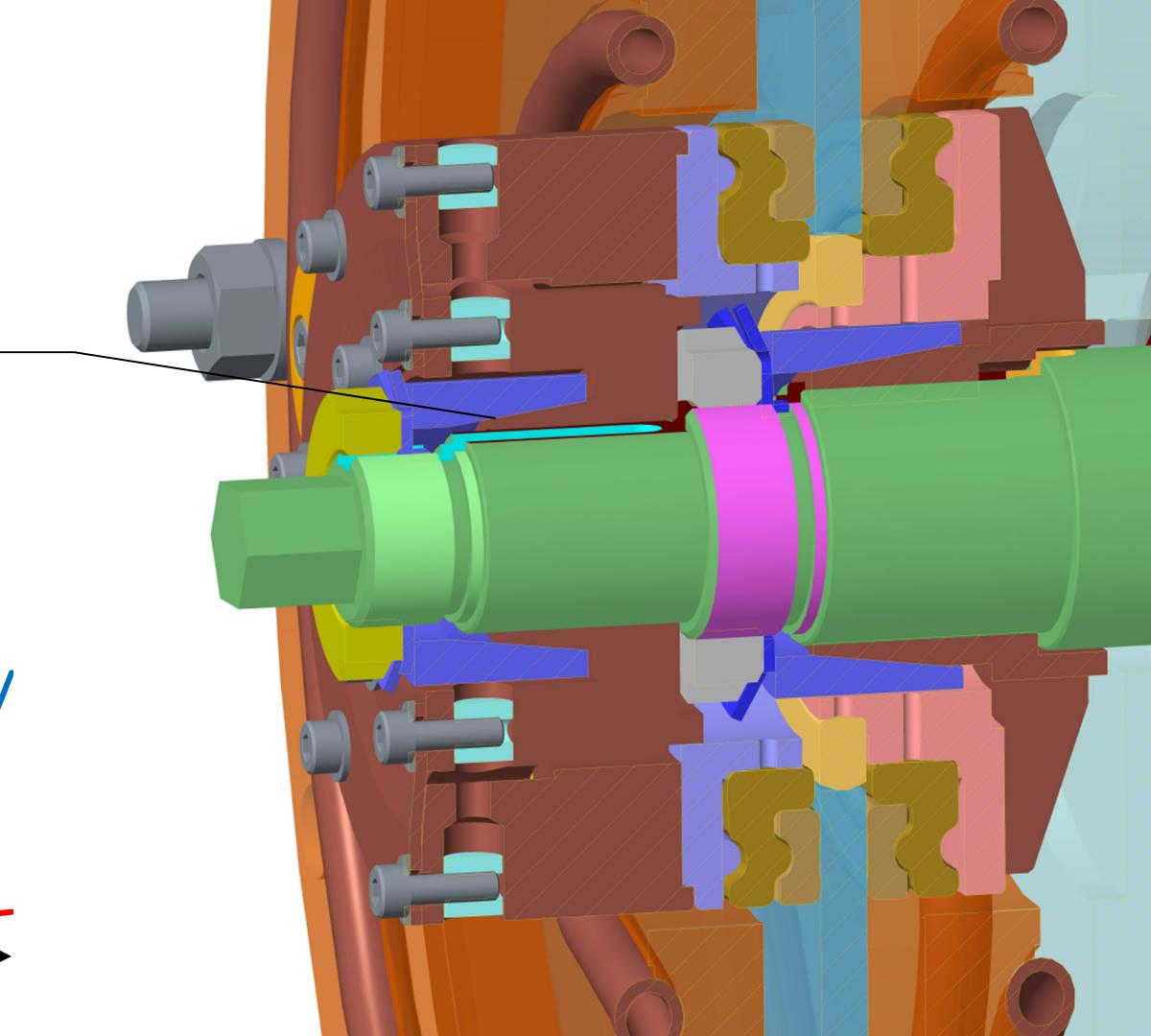
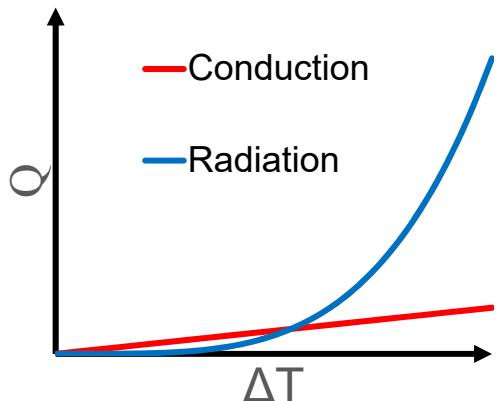
Final Design

Wedges

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Uncoupled design

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Final Design

Wedges

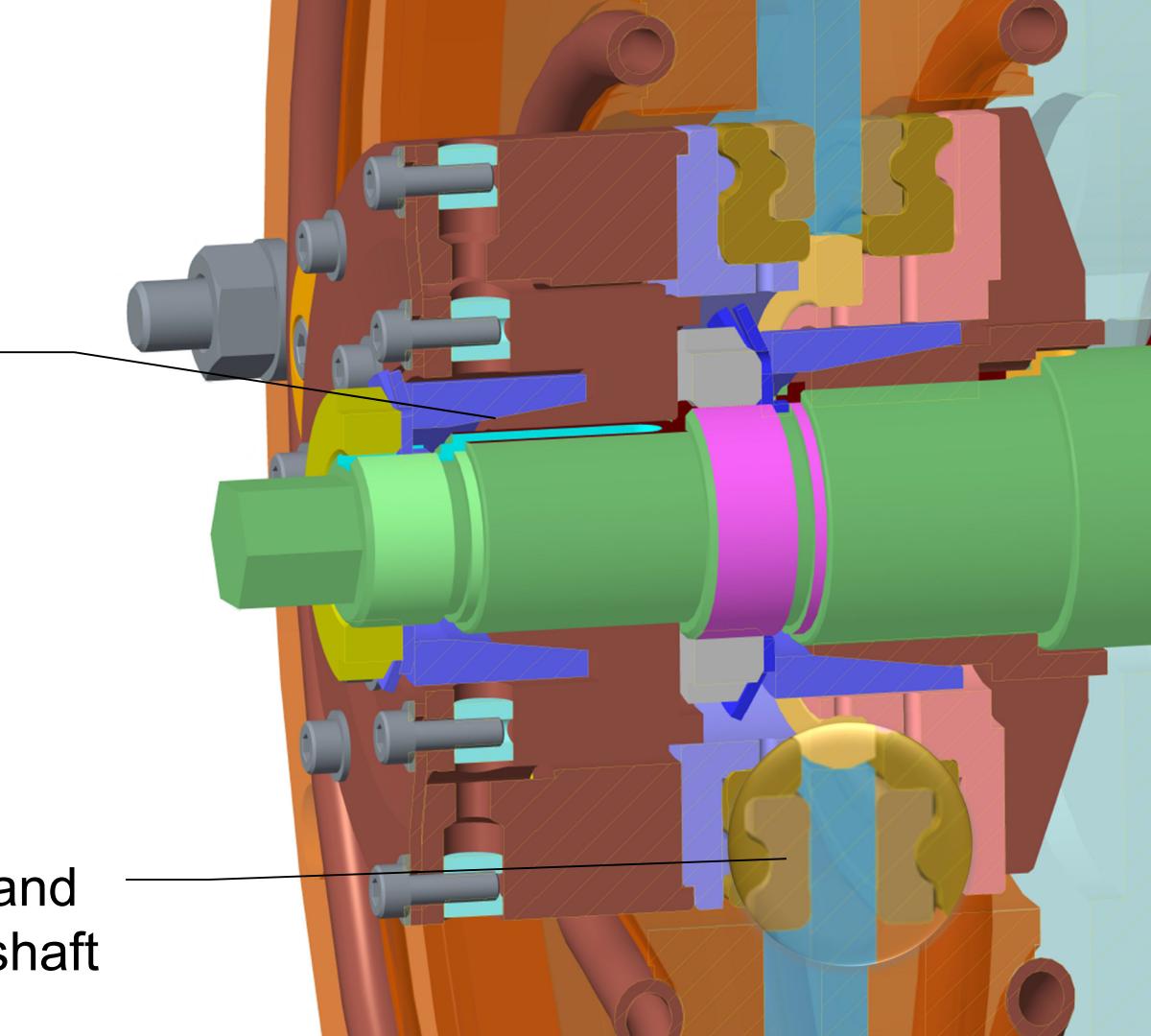
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Grooves

to reduce contact area and
heat transferred to the shaft



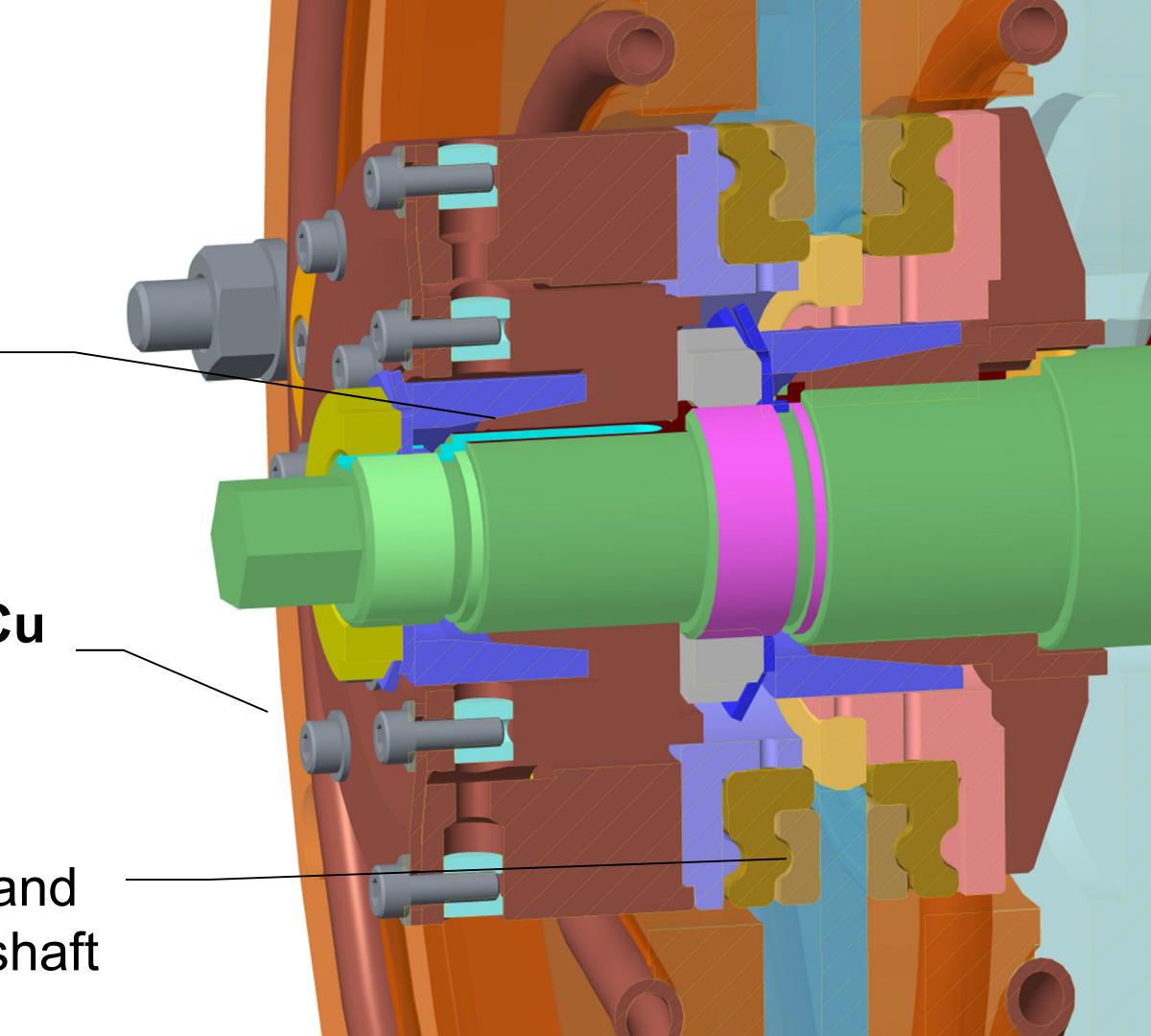
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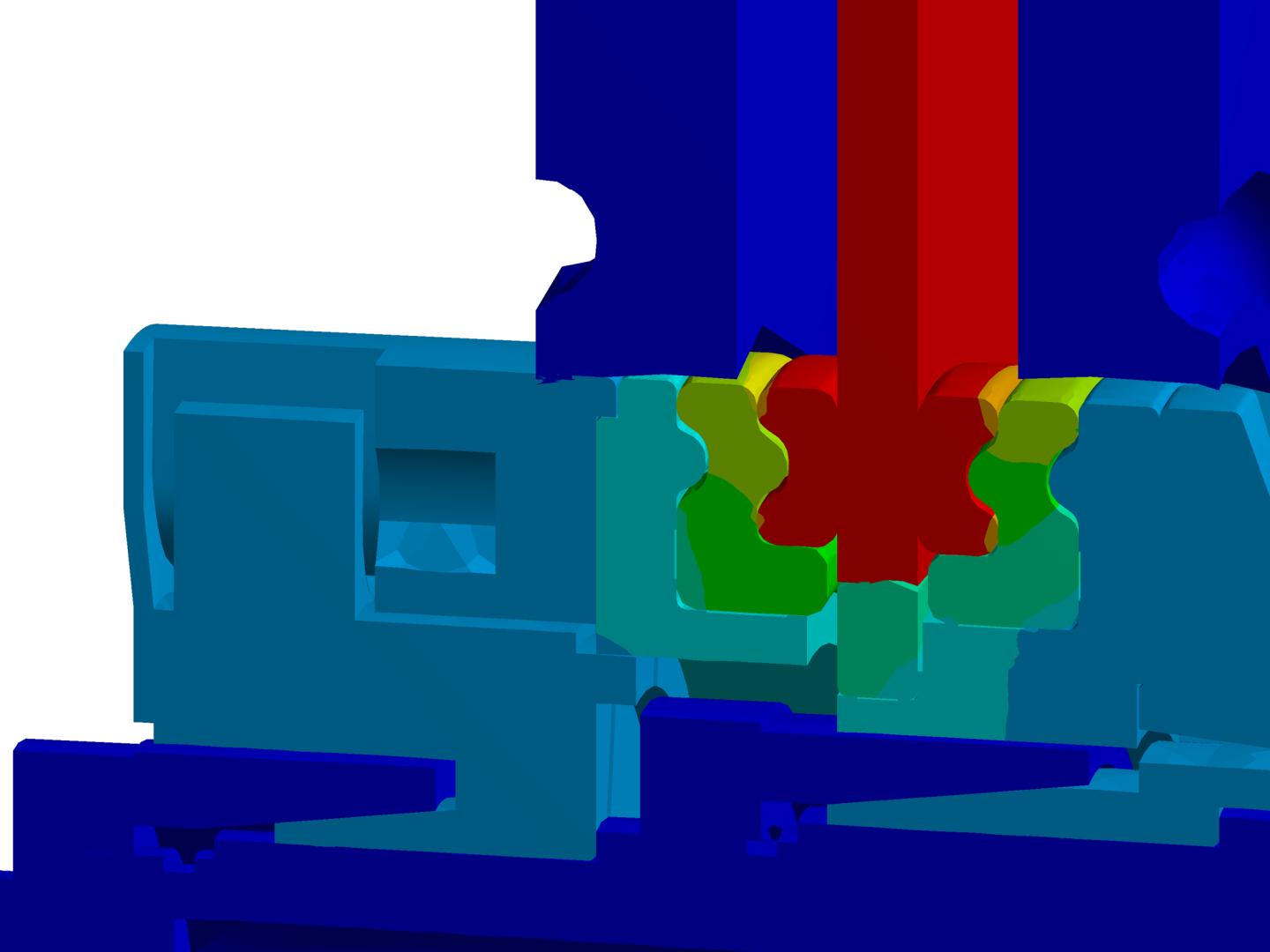
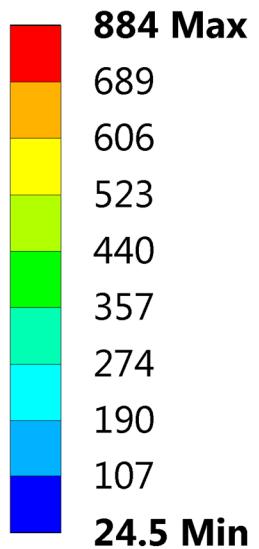


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Simulation

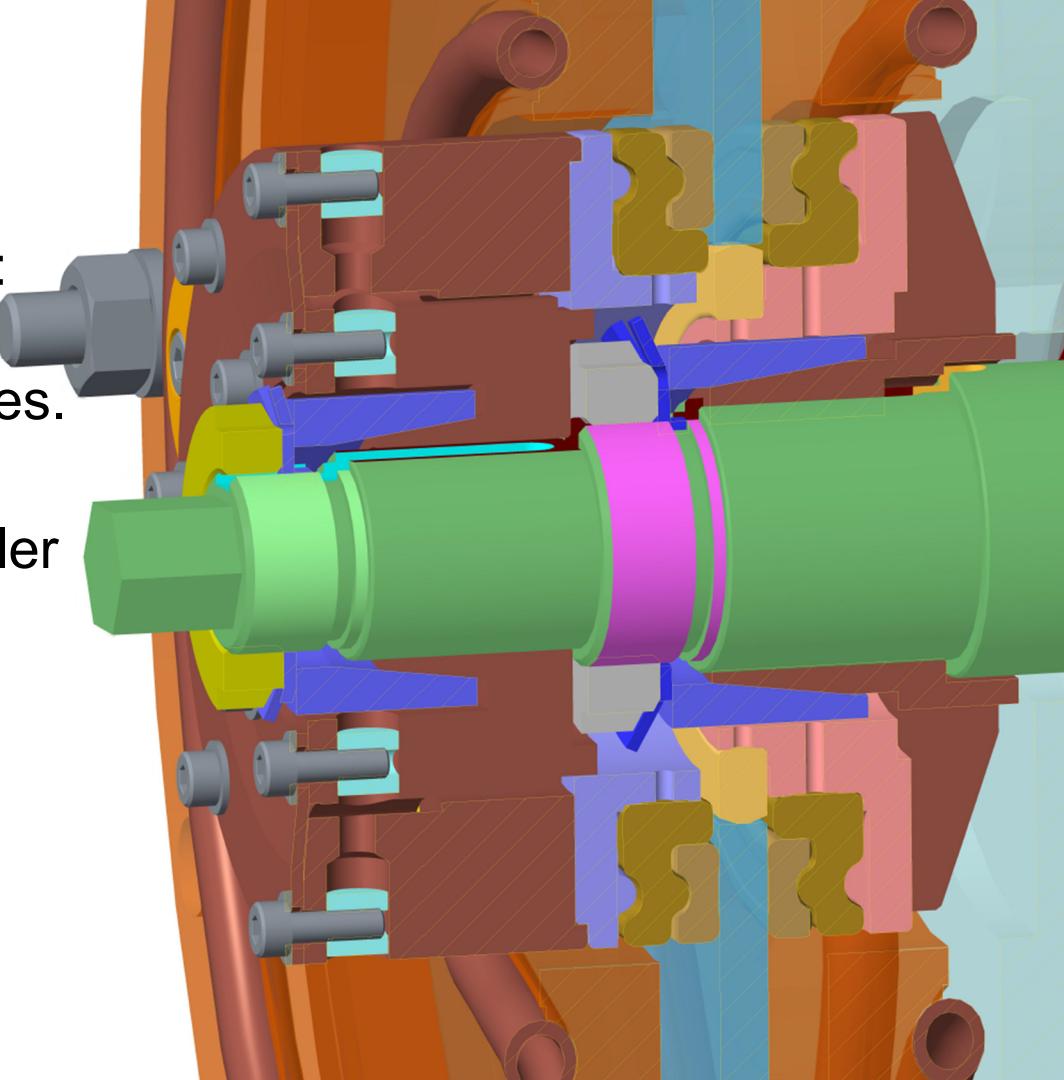
Type: Temperature
Unit: °C



Conclusion

Design *Reliable and robust:* operational since Sep'16 with no issues.

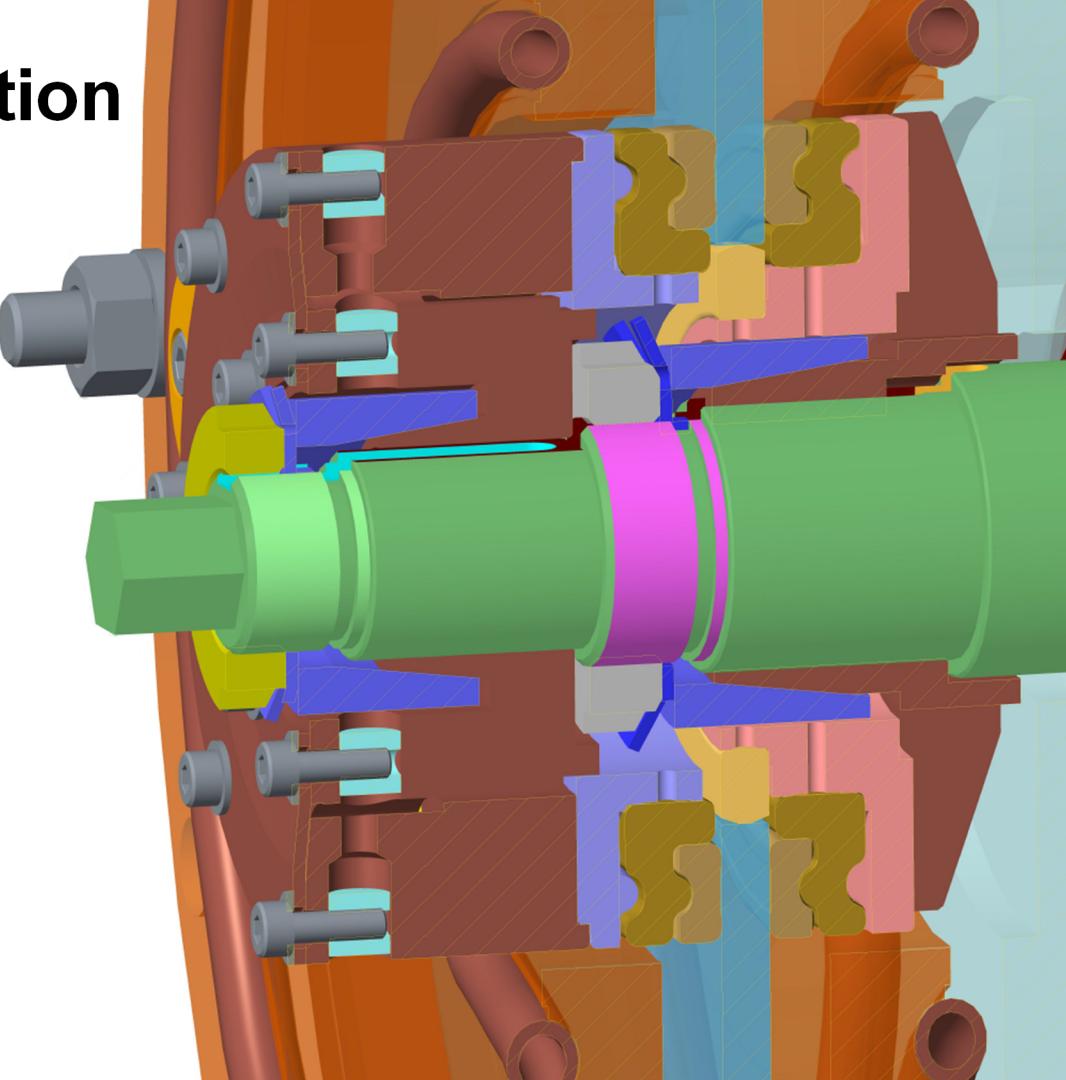
FEA *Conservative, the measured T is smaller than the simulated one. Accurate, the error is <10%*



Thanks for your attention

... and thanks to
George, Michael, Steve,
and Thomas

Any questions?



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