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Optimization design of four-point vibration isolation support for spallation neutron source vibration magnet

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Abstract

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CSNS/RCS of the dipole magnets by 25 Hz sinusoidal alternating current (AC) with dc bias field, because the magnet will produce eddy current effect caused by the vibration, this safe and reliable operation of the long-term impact of magnets, so need to CSNS/RCS dipole magnets, support system for dynamic characteristic research and the performance of vibration isolation design. The mechanical model of ac dipole magnet and support system is first established, and ANSYS modal analysis are carried out. On this basis, vibration isolation parameters of the four-point support system are studied.

INTRODUCTION

The pole magnet bracket system is shown in Figure 1. The whole system consists of magnet, bracket and embedded plate. The magnet bracket is composed of upper plate, lower plate, horizontal (x, z) adjustment system, vertical (y) adjustment system and bottom support frame. Because the magnet supported by the support will produce vibration, in order to improve the stiffness and anti vibration performance of the support system, the support adopts the 4-point support scheme with stronger stiffness than the 3-point support scheme.



Fig. 1 Structure of dipolar girder system with the vibration isolator

RESEARCH ON DYNAMIC CHARACTERISTICS OF VIBRATION ISOLATION BRACKET WITH TWO POLE MAGNET

In the two pole magnet bracket system, a variety of schemes can be adopted to connect the magnet and bracket, such as using 3-point, 4-point and 6-point vibration isolators. In order to increase the stability of the magnet, three-point support is generally not considered for vibration isolation connection. Through the modal extraction experiment of the two pole magnet bracket without vibration isolator, it can be shown that the magnet bracket system is not a single degree of freedom. Under the action of vertical vibration force, the bracket has three degrees of freedom, i.e. translation x in the vertical direction and rotation around two orthogonal axes in the horizontal direction θ 1, θ 2. As shown in Figure 2, its dynamic vibration form.



Fig. 4 Dynamic model of magnet support system

In order to increase the stability of the magnet, the connection between the bracket and the magnet is supported by four points. The magnet can be regarded as a single large mass system. There are four elastic damping structures installed between the magnet and the bracket. The elastic damping structure is assumed to be rigid in the horizontal direction. Therefore, the vibration form of the magnet mainly has two axial rotation movements, and the machine rises and falls vertically. The dynamic system is a three degree of freedom system, and the dynamic equation can be expressed as follows:

[m	0	0	∏ x ¯]	$\lceil 2C \rceil$	0	0	[x]	$\lceil 2K \rceil$	0	0]	$\begin{bmatrix} x \end{bmatrix}$	
0	\mathbf{j}_1	0	$\ddot{\theta}_1$	+	0	$2Cl^2$	0	$\dot{\theta}_1$ +	0	$2Kl^2$	0	θ_1	=F(t)
0	0	j ₂	$\left[\ddot{\theta}_{2}\right]$	j	0	0	$2Cl^2$	$\dot{\theta}_2$	0	0	$2Kl^2$	$\left\lfloor \theta_{2} \right\rfloor$	

The equation has two assumptions: all isolators in the same bracket have the same stiffness and damping; The center of mass of the magnet is in the center of the mounting position of the isolator.

1. The modal shapes of the magnet support system before and after vibration isolation are similar, but the dynamic responses of the two conditions are different, especially the vertical response curves

2. Because the vibration isolator is mainly used to isolate the vibration in the vertical direction (Y direction in the figure), the improvement effect on the horizontal direction (x, z direction) of the system is not great, and the dynamic response curve distribution of the magnet in these two directions before and after vibration isolation changes little. The difference is that the response amplitude of the magnet to the exciting force at resonance frequency changes, and the radial stiffness of the system decreases after installing the vibration isolator, which leads to the strong response of the magnet to the low frequency 6Hz in the horizontal direction.

3. After installing the vibration isolator, the vertical vibration response excited by the vibration force of the magnet is very small, there is no resonance peak around the excitation frequency of 25Hz, and the system response spectrum is not in the resonance amplification region, so the vibration isolation system design achieves the expected effect.

DYNAMIC MODAL TEST OF SUPPORT SYSTEM

In order to verify the validity of the parameter design of the support system, the modal extraction test of the magnet support system is carried out. In vibration test, it is an important task to determine the dynamic characteristic parameters of structure. The experimental modal analysis is the most direct way to get the structural dynamic characteristic parameters (natural frequency, damping ratio and vibration mode)

The first step is to establish the measurement system, that is, hanging the specimen, installing the exciter, selecting the force sensor and response sensor, and correcting the system;

The second step is to measure the frequency response data. Once the structure vibrates under a certain exciting force, the time-domain data of the force and response can be measured and converted to the frequency domain to calculate the average estimation of the frequency response function. In some cases, it is not required to calculate the frequency response function, but the time history;

The third step is modal parameter estimation, that is, using the measured frequency response function or time history to estimate modal parameters.

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Fig.7 Modal extraction experiment Table 1 Experimental results of scaffold modal extraction

The figure above shows the average value of long-term monitoring. The vibration isolation efficiency of the bracket is about 60% - 70%. Due to the difference of processing technology and support uncertainty caused by alignment adjustment, the vibration isolation effect of each bracket is slightly different. During most of the operation time of the accelerator, the vibration value of the support system is maintained below 10 microns, and the vibration transmitted by the support to the ground is about 1-2 microns, and there is no vicious behavior of cycle increase. Therefore, it has better protection for the stability of other surrounding equipment.



of dipole magnet support

magnet under rated vibration power

CONCLUSION

The simulation results of the four point support model and the actual experimental modal extraction experiment and vibration response test verify the validity of the model.

The results are as follows: 1. The main degree of freedom of the vibration of the two pole magnet bracket system is the rotation vibration around the x-axis and y-axis, and the chance of vertical vibration is small, so the dynamic model can not be simplified as a single degree of freedom system;

2. The addition of damping can reduce the vibration amplitude of the magnet itself, but it will also increase the shift of the natural frequency to the high frequency, resulting in resonance. Therefore, in the optimization design, we need to consider comprehensively and select the optimized stiffness and damping parameters;

3. In the manufacturing process of the new dipole magnet, the iron core stacking and coil pouring process are improved, which also reduces the vibration of the magnet itself. At the same time, the iron core and coil didn't crack during the baking process, which led to the aggravation of vibration. After adding elastic elements, even in the case of large vibration amplitude, the damage effect of vibration on the equipment will be reduced.

Fig.9 Vibration data of support of bipolar Fig.10 Measurement of long-term vibration