# **VIBRATION EVALUATION FOR DEIONIZED WATER PUMPS IN TPS\***

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#### Abstract

The purpose of this paper is to evaluate the vibration level and spectrum for TPS deionized water pumps. The utility systems started to operate from the beginning of 2014, some of deionized water pumps produced higher vibration and noise level during operation. The possible reason could be inappropriate installation and commission adjustment. In order to figure out the status of these deionized water motors and pumps, the vibration analysis was tested. After vibration measurement, some of the booster (BO) and copper (CU) deionized water pump systems generate higher vibration level and exceed ISO 10816 standards. According to the vibration test results, the unqualified motor system is maintained. Although there is some remain problems for TPS deionized water pump systems, the periodical vibration test is still one important way to preventive maintenance for utility systems. The rotational utility systems could prevent malfunction through regular vibration inspection.

### **INTRODUCTION**

The TPS utility systems started to operate from the beginning of 2014, before TPS commission started. In order to provide accelerator test requirement, the whole utility systems needed to be keep stable operation. The vibration inspection become one method to preventive maintenance [1]. In 2004, ANL [2] studied the mechanical vibration control systems and the specifications for all rotational facilities. In 2007, TLS has also investigated on water induced vibration and vibration propagation by piping system [3]. According to the experience from TLS, the vibration amplitude and spectrum for the TPS utility systems also can be applied the similar criterion.

# TPS LAYOUT OF DEIONIZED WATER SYSTEMS

The main utility system is located in B2 floor of activity center (D building) and the main power station via water/AHU system located in different area. There are several subsystems in utility area, chiller, cooling and deionized water systems, for instance. Because of most of the utility system are rotational machine and needed 24hour operation, the maintenance for whole system require lot of manpower and money. The prevention maintenance therefore could be one way to increase stability of the whole system.

The layout of deionized water systems are shown in Fig. 1. There are two booster (BO), two copper (CU), two

tems from the right to left respectively. Each deionized pumping system pump deionized cooling water directly to the subsystems in the tunnel. The BO deionized water system provide cooling water for magnets and other elements in booster ring. The CU deionized water system provide cooling water for magnets and AL system supply cooling water for vacuum chambers in storage ring. The RF deionized water system supply cooling water to both SR/BR RF system. There are two motors for every subsystem is for redundant operation. In among them, the BO, CU and RF system use horizontal split-coupled end suction pumps type. The AL system use vertical splitcoupled in-line pumps type.

aluminium (AL), and two RF deionized water pump sys-



Figure 1: Layout of TPS deionized water systems.

# TEST POINTS FOR MOTOR AND PUMP VIBRATION MEASUREMENT

The motor energy provide pump to increase water pressure by coupling. The BO, CU and RF system use horizontal split-coupled end suction pumps. The alignment of coupling between motor and pump could affect the stability of the system. Besides, for energy saving, all the motors are variable frequency drive. The variable frequency drive motor also could affect vibration frequency and amplitude. In order to verify the vibration status, the vibration test for each system in 4 different section is specified in Table 1.

Motor	Motor Non-Drive-End (MO)	V-vertical H-horizontal	
	Motor Drive-End (MI)	V-vertical H-horizontal A-axial	
Pump	Pump Drive-end (PI)	V- vertical H- horizontal A-axial	
	Pump Non-Drive End (PO)	V- vertical H- horizontal	

Table 1: Vibration Test Points

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The position of the vibration measurement location was illustrated in Fig. 2. The vertical and horizontal vibration level were tested in non-drive end of motor (MO). The vertical, horizontal and axial vibration level were tested in drive end of motor (MI). On the other hand, the vertical, horizontal and axial vibration level were tested in drive end of pump (PI). And the vertical and horizontal vibration level were tested in non-drive end of pump (PO).



Figure 2: Vibration Test Locations.

# **VIBRATION MEASUREMENT RESULTS**

According to the operation status, the BO, CU and RF pumping systems were tested. Base on the ISO 10816 standards [4], the frequency from 10~1000 Hz and 20~40 Hz velocity vibration level were recorded.

# Booster (BO) Deionized Water System

There are two motor system for redundant operation, which are mark for DIWP-BO-1and DIWP-BO-2 respectively (see Fig. 3). The motor is 215 hp (160 kW) with 380 V-3 phase electrical drive. The maximum rotation speed is 1750 rpm with 1285 GPM (292.0  $\text{m}^3/\text{h}$ ) flow rate. The lift head of motor is 380 ft (115.82 m).



Figure 3: DIWP-BO-1 deionized water systems.

The experimental results are shown in Table 2. According ISO 10816 standards, the vibration velocity below 1.8 mm/s is good. The vibration velocity between 1.8 to 4.5 mm/s is allowable, and between 4.5 to 11.2 mm/s is tolerable. While the vibration velocity is exceeded 11.2 mm/s, the motor/pump system is under not permissible condition.

Vibration level	0-P(mm/s)	RPM(mm/s)					
	10-1000 Hz	20-40 Hz					
DIWP-BO-1							
MO: V	7.7000 0.4724						
MO: H	16.2800 0.9832						
MI: V	1.5500 0.9204						
MI: H	3.1380	80 2.7830					
MI: A	1.6380	1.0110					
PI: V	2.8030	0.9262					
PI: H	6.3050	1.5110					
PI: A	2.1130	0.4881					
PO: V	2.3670	0.7441					
PO: H	4.5330	1.1300					
DIWP-BO-2							
MO: V	5.5690	0.7853					
MO: H	19.3400	1.6570					
MI: V	1.6320	1.3020					
MI: H	2.2370	1.4300					
MI: A	1.3410	0.7757					
PI: V	2.1000	0.9556					
PI: H	4.8740	2.5020					
PI: A	1.8020	0.8599					
PO: V	1.6290	0.6568					
PO: H	3.3710	1.8360					

From the experimental results, some of the vibration amplitude of BO deionized water system were quite high. The vibration amplitude is higher in frequency range between 10 to 1000 Hz. This indicated the part of motor for instance bearing is abrasion. The high frequency vibration not only multi-drive frequency, even higher than 80 Hz and hundreds frequency vibration contribute the total vibration magnitude of BO deionized water system.

## Copper (CU) Deionized Water System

The two motor system for CU deionized water system are marked for DIWP-CU-1and DIWP-CU-2 respectively. The motor is 270 hp (200 kW) with 380 V-3 phase electrical drive. The maximum rotation speed is 1750 rpm with 1670 GPM (379.5  $m^3/h$ )flow rate. The lift head of motor is 380 ft (115.82 m).

The experimental results are shown in Table 3. Some of the vibration amplitude of CU deionized water system were also high. The vibration amplitude is also higher in frequency range between 10 to 1000 Hz. Although the power of CU system is higher than BO system, the total vibration amplitude is lower than BO DIW system. Only some of the DIWP-CU-1 deionized water system needed to be checking.

Vibration level	0-P(mm/s)	RPM(mm/s)	
	10-1000 Hz	20-40 Hz	
DIWP-CU-1			
MO: V	7.8080 0.8369		
MO: H	7.7850	0.7068	
MI: V	1.3660 0.9354		
MI: H	1.2240 0.3404		
MI: A	2.0700	1.7000	
PI: V	2.7490	0.8530	
PI: H	4.5260	2.6850	
PI: A	2.5170	0.2887	
PO: V	2.7170	0.8946	
PO: H	3.3920	2.0970	
DIWP-CU-2			
MO: V	8.3080 0.6793		
MO: H	18.6400	0.2780	
MI: V	1.2800	0.6635	
MI: H	4.1140	1.2800	
MI: A	3.9950	1.2630	
PI: V	1.8690	0.5609	
PI: H	2.9770	1.0120	
PI: A	1.1880 0.2225		
PO: V	1.5900	0.4880	
PO: H	2.3100	2.3100 0.7994	

Table 3:	Vibration	Test for	CU DIW	System
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# RF Deionized Water System

The two motor system for RF deionized water system are marked for DIWP-RF-1and DIWP-RF-2. The size of motor is the same with CU DIW system. The vibration amplitude of RF DIW system is under allowable level. The only thing to do with RF DIW system is remain regular checking. The RF DIW system is under normal operation.

### **MAINTAIN AND REPAIRMENT**

Base on the vibration measurement, the DIWP-BO-1 DIW system generated highest vibration level under normal operation. According ISO 10816 standard, the vibration amplitude is almost reach not permissible. In order to preserve long term operation, utility group request motor supplier to maintain the system.

Figure 4 shows the repair process of motor system. The whole motor is disassembled and replace the new bearing. For alignment requirement, the elastic base was also welding adjust screw block to micro adjustment. After system repair and laser alignment with coupling, the vibration level drop dramatically. For long-term operation, the system still need to be regular checking.



Figure 4: Maintain for DIWP-BO-1 DIW system.

#### **CONCLUSIONS AND DISCUSSIONS**

The evaluation of vibration amplitude and spectrum for TPS deionized water pump system was done. Some of deionized water pumps produced higher vibration and noise level during operation.

The booster (BO) and copper (CU) deionized water systems generate higher vibration amplitude and exceed ISO 10816 standards. The unqualified motor system is maintained.

Although there is some remain problems for TPS deionized water pump systems, the periodical vibration test is still one important way to preventive maintenance for utility systems. The rotational utility systems could prevent malfunction through regular vibration inspection.

#### REFERENCES

- J. P. Den Hartog, *Mechanical Vibrations*, Dover Publications, 1985.
- [2] W Zander, "Mechanical Vibration Controls", sec. 15071, Department of Energy, Argonne National Lab., Argonne, Illinois, 2004.
- [3] Y. H. Liu *et al.*, "Vibration evaluation for utility instruments and water piping system in TLS", *in Proc. APAC'07*, Indore, India, January 2007, paper THPMA093.
- [4] ISO 10816-3:2009, Mechanical vibration Evaluation of machine vibration by measurements on non-rotating parts – Part 3, 2009.