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Abstract

The development of innovative model-based design high bandwidth mechatronic systems with stringent performance specifications has become ubiquitous at LNLS-Sirius beamlines. To achieve such unprecedented specifications, closed loop control architecture must be implemented in a fast, flexible and reliable platform such as NI's CompactRIO (cRIO) controller that combines FPGA and real-time capabilities. The design phase and life-cycle management of such mechatronics systems heavily depends on high quality experimental data either to enable rapid prototyping, or even to implement continuous improvement process during operation. This work aims to present and compare different techniques to stimulus signal generation approaching Schröder phasing and Tukey windowing for better crest factor, signal-to-noise ratio, minimum mechatronic stress, and plant identification. Also shows the LabVIEW implementation that requires specific signal synchronization and processing on the main application containing a hardware-based control architecture, increasing system diagnostic and maintenance ability. Finally, experimental results from the High-Dynamic Double-Crystal Monochromator (HD-DCM-Lite) of QUATI (quick absorption spectroscopy) and SAPUCAIA (small-angle scattering) beamlines and from the High-Dynamic Cryogenic Sample Stage (HD-CSS) from SAPOTI (multi-analytical X-ray technique) of CARNAÚBA beamline are also presented in this paper.

Stimulus generation

Multi-sine signals are broadly applied to system identification [5] due to their periodic and flexible structure, as shown by the equation below:

$$x(t) = \sum_{k=1}^N A_k \cos(\omega_k t + \varphi_k)$$

Different approaches exist to define phase for each frequency component. Resulting properties in time and frequency domain such as crest factor (ratio between peak and effective values) and bandpass spectrum were compared for different methods.

Table 1: Crest factor comparison for different multi-sine phasing methods

Phase method	Crest factor
Random	3.5 – 5.5
Linear difference	1.9
Linear phase	64.56
Schröder phasing	1.66

Schröder phasing is defined by the following quadratic relation and offers the best crest factor and a near perfectly distributed bandpass spectrum

$$\varphi_k = -\frac{k(k-1)\pi}{N_k}$$

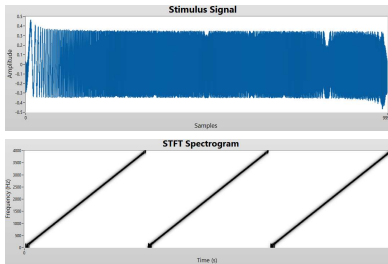


Figure 1: Time signal (single-period) and spectrogram (3 periods) of multi-sine signal with period of 1 second, Schröder phasing and maximum frequency of 4 kHz.

Tukey windowing helps smoothing abrupt start and end of excitation signals, providing a less demanding operation for the tested system and preserving its integrity during prototyping and offline commissioning.

$$\text{Tukey window: } w(t) = \begin{cases} \frac{1}{2} \left\{ 1 + \cos\left(\frac{2\pi}{r} \left[x - \frac{r}{2}\right]\right) \right\}, & 0 \leq t < \frac{r}{2} \\ 1, & \frac{r}{2} \leq t < 1 - \frac{r}{2} \\ \frac{1}{2} \left\{ 1 + \cos\left(\frac{2\pi}{r} \left[x - 1 + \frac{r}{2}\right]\right) \right\}, & 1 - \frac{r}{2} \leq t \leq 1 \end{cases}$$

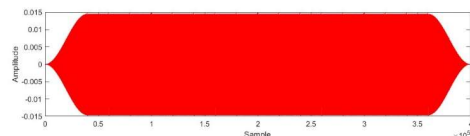


Figure 2: Multi-period signal with Tukey windowing.

Architecture

Generation of multi-sine excitation signals and system response acquisition are performed by the same cRIO unit used to control the system during the offline commissioning.

The new architecture multiplexes the control effort and feedback signal from the pre-existing controller embedded on FPGA, connecting them to the stimulus generator and system response logger, both implemented on the cRIO Real-Time CPU, saving FPGA resources.

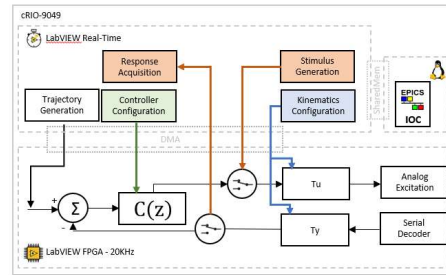


Figure 3: System identification modules on cRIO.

A Matlab routine calculates FFT for each period (1 second) of excitation and output signals, from which system frequency responses are calculated and averaged together to improve signal-to-noise ratio (SNR).

Low-level implementation

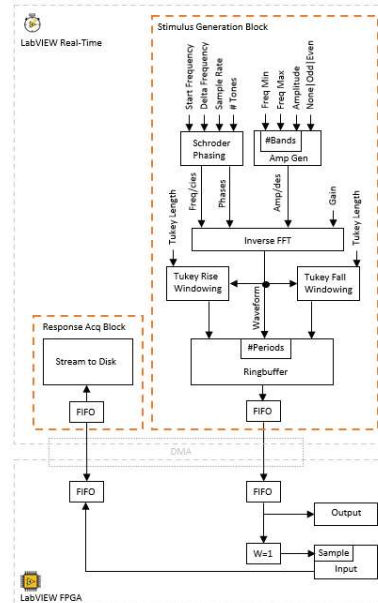


Figure 4: Block diagram of LabVIEW implementation for stimulus generation and system response acquisition.

System identification results

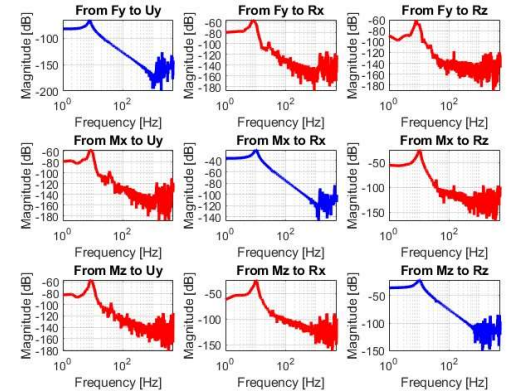


Figure 5: Experimental frequency responses (1 Hz-10 kHz) for short-stroke stage of HD-DCM-Lite using Schröder multi-sine.

Conclusion

The proposed approach for system identification was successfully embedded in a cRIO platform alongside the pre-existing control architecture and infrastructure, providing a flexible and convenient tool for model-based controller design and diagnostics of precision mechatronic systems, such as the new generation of monochromators and samples stages for LNLS beamlines. Different multi-sine excitation signals were compared and the Schröder method was chosen due to its properties both in time and frequency domain. Tukey windowing and multi-periods were adopted to deal with limitations of physical systems under test, such as electro-mechanical restrictions and noise. Frequency response data with up to 10 kHz (resolution of 1 Hz) of a high-dynamic monochromator was obtained, matching simulated results from mechanical modelling. Also, the controller was designed for that experimental plant, and the in-position error (RMS) for all degrees of freedom matched the project expectations.

Acknowledgement

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