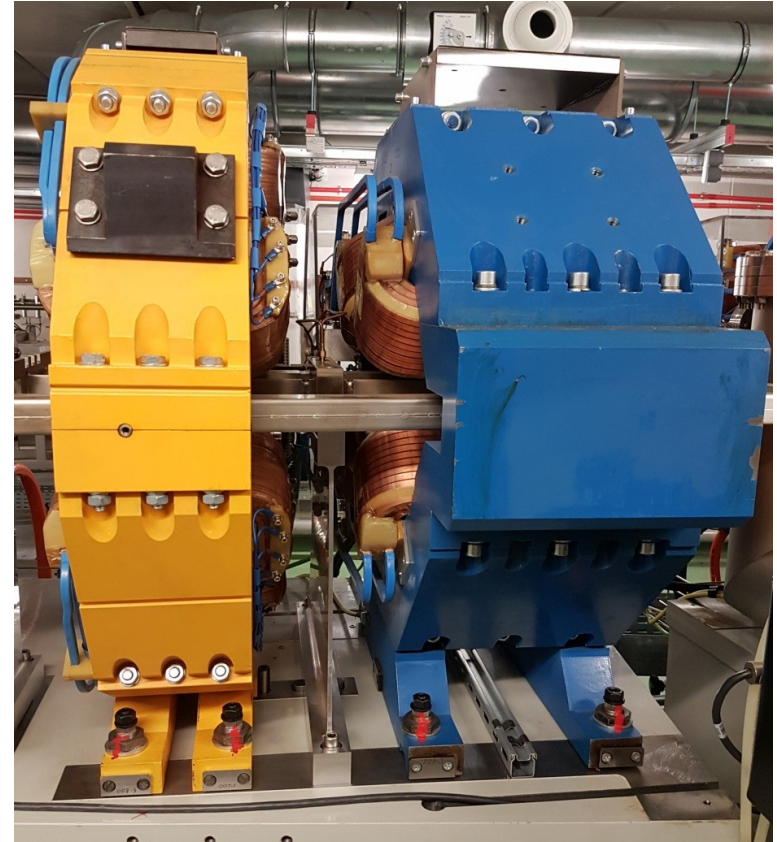


# Fast **B**eam **B**ased **A**lignment Using AC Corrector Excitations\*\*

Z.Martí, A. Franchi,  
E.Morales, G.Benedetti,  
U.Iriso, A.Olmos, J.Moldes



\*paper: <https://link.aps.org/doi/10.1103/PhysRevAccelBeams.23.012802>

\*\* Python & Matlab implementations: <https://gitlab.com/fbba/zeus@cells.es>

BBA

FBBA

ALBA set up

Results

*It is needed to:*

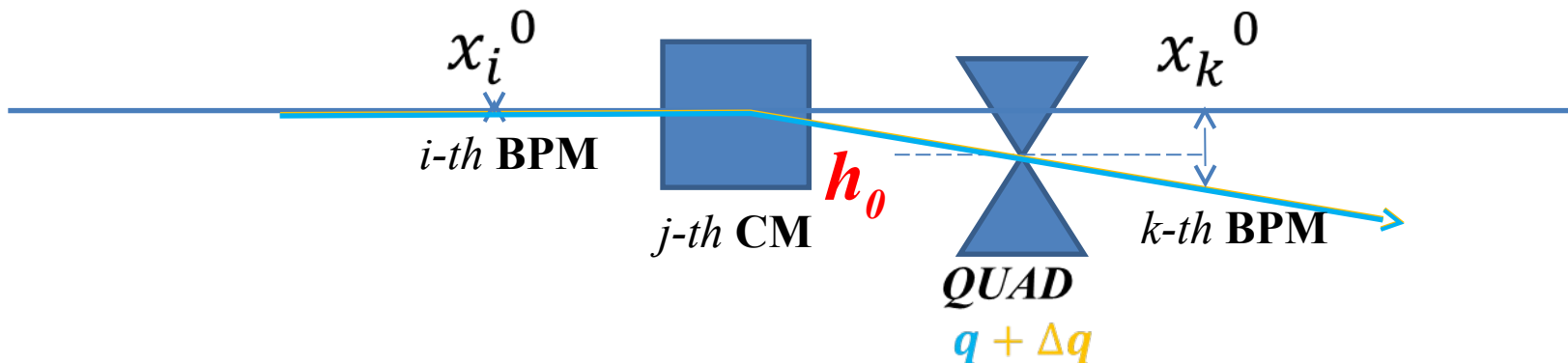
- Minimize **multipole feed down** effect, minimizes the corrector strength needed:
  - **Optic** & coupling errors due to Sextupoles.
  - **Orbit** errors due to Quadrupoles.
- Bring the machine closer to the **model** in-between BPMs.

## Misalignments come from:

- Real: mechanical
- Apparent: electronic

## Several measurement methods:

- **Beam2quad**: Quad scan: **Fast** but **Model dependent**.
- **BPM2quad**: Quad&CM scan: **Slow** but **Model independent**.
- There is a systematic error (orbit angle):



Instead of scanning sequentially in DC the CM, it uses the FOFB hardware:

- 10kHz **Fast Acquisition Archiver**
- AC CM excitation (quads **could** also be AC)

The FBBA measurable quantities are the same as for the normal **bpm2quad** BBA, but:

- The **two planes** are done at the same time ( $h_0$  and  $v_0$ )
- **Optics coupling** is taken into account -> **skew** magnets can also be aligned
- BPM gain and **coupling**, CM calibration and **tilt** are also considered

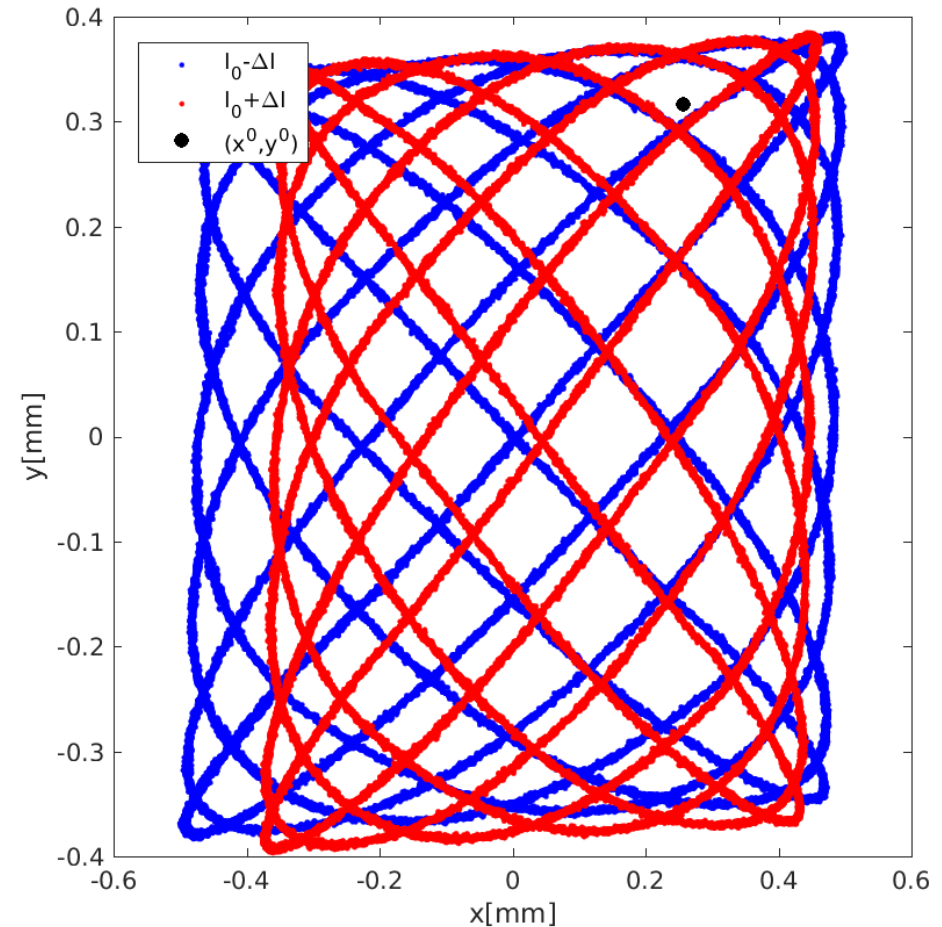
## QUAD FBBA-DC BPM data example:

The method is valid for:

- *DC quad*
- *AC quad (additional factor 2 faster)*

And also:

- *Normal quad*
- *Skew quad (sextupole yoke)*



The method is a **factor 2 faster** if two different **frequencies** are used in each plane.

$$h_j(t_n) = \hat{h}_j \cos(2\pi f_h t_n + \psi_h)$$

$$v_j(t_n) = \hat{v}_j \cos(2\pi f_v t_n + \psi_v)$$

The offset is obtained combining the **Fourier components** of each BPM signal.

$$h_j(t_n) = \Re \left\{ \left( \hat{h}_j e^{i\psi_h} \right) e^{i2\pi f_h t_n} \right\} = \frac{1}{2} \left( \langle h_j | f_h \rangle e^{i2\pi f_h t_n} + c.c. \right) ,$$

$$v_j(t_n) = \Re \left\{ \left( \hat{v}_j e^{i\psi_v} \right) e^{i2\pi f_v t_n} \right\} = \frac{1}{2} \left( \langle v_j | f_v \rangle e^{i2\pi f_v t_n} + c.c. \right) .$$

In the linear regime, the BPM readings as a function of CMs change with **coupling** are:

$$\begin{cases} x_k(t) - x_k^0 = R_{kj}^{xx} (h_j(t) - h_0) + R_{kp}^{xy} (v_p(t) - v_0) \\ y_n(t) - y_n^0 = R_{np}^{yy} (v_p(t) - v_0) + R_{nj}^{yx} (h_j(t) - h_0) \end{cases}$$

**DC quad:**

$$R_{kj}^{xx}, R_{kp}^{xy}, R_{np}^{yy} \text{ and } R_{nj}^{yx}$$

have 2 values: **two sets** of data are acquired.

**AC quad:**

$$R_{kj}^{xx}, R_{kp}^{xy}, R_{np}^{yy} \text{ and } R_{nj}^{yx}$$

vary with time: only **one set** of data.



Both for quads and skews the **solution** is:

$$\begin{cases} x_l^0 = \Re \{ \langle x_l | 0 \rangle \} + \mathcal{S} \{ \langle x_l | f_h \rangle \} \mathcal{M}_h + \mathcal{S} \{ \langle x_l | f_v \rangle \} \mathcal{M}_v \\ y_l^0 = \Re \{ \langle y_l | 0 \rangle \} + \mathcal{S} \{ \langle y_l | f_v \rangle \} \mathcal{M}_v + \mathcal{S} \{ \langle y_l | f_h \rangle \} \mathcal{M}_h \end{cases}$$

Where the **observable** ( $h_0$  and  $v_0$  are not) **relative corrector offsets**

are:

$$\begin{cases} \mathcal{M}_h = \frac{h_{0j}}{\hat{h}_j} = -\frac{\mathcal{D}_x \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_y}{\mathcal{D}_{xh} \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_{yh}} = \frac{\mathcal{Y}_{hk}}{\mathcal{X}_{hk}} \\ \mathcal{M}_v = \frac{v_{0j}}{\hat{v}_j} = -\frac{\mathcal{D}_{xh} \mathcal{D}_y - \mathcal{D}_x \mathcal{D}_{yh}}{\mathcal{D}_{xh} \mathcal{D}_{yv} - \mathcal{D}_{xv} \mathcal{D}_{yh}} = \frac{\mathcal{Y}_{vk}}{\mathcal{X}_{vk}} \end{cases}$$

BPM gain and coupling, CM calibration and tilt are taken into account.

**DC** Quad/skew (1&2 measurements)

$$\left\{ \begin{array}{l} \mathcal{D}_x = \Re \{ \langle x_{k2} | 0 \rangle \} - \Re \{ \langle x_{k1} | 0 \rangle \} \\ \mathcal{D}_y = \Re \{ \langle y_{k2} | 0 \rangle \} - \Re \{ \langle y_{k1} | 0 \rangle \} \\ \mathcal{D}_{xh} = \mathcal{S} \{ \langle x_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle x_{k1} | f_h \rangle \} \\ \mathcal{D}_{yv} = \mathcal{S} \{ \langle y_{k2} | f_v \rangle \} - \mathcal{S} \{ \langle y_{k1} | f_v \rangle \} \\ \mathcal{D}_{xv} = \mathcal{S} \{ \langle x_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle x_{k1} | f_h \rangle \} \\ \mathcal{D}_{yh} = \mathcal{S} \{ \langle y_{k2} | f_h \rangle \} - \mathcal{S} \{ \langle y_{k1} | f_h \rangle \} \end{array} \right.$$

**AC** Quad (at  $f_s$ : 1 measurement)

$$\left\{ \begin{array}{l} \mathcal{D}_x = \mathcal{S} \{ \langle x_k | f_s \rangle \} \\ \mathcal{D}_y = \mathcal{S} \{ \langle y_k | f_s \rangle \} \\ \mathcal{D}_{xh} = \mathcal{S} \{ \langle x_k | f_h + f_s \rangle \} + \mathcal{S} \{ \langle x_k | f_h - f_s \rangle \} \\ \mathcal{D}_{yv} = \mathcal{S} \{ \langle y_k | f_v + f_s \rangle \} + \mathcal{S} \{ \langle y_k | f_v - f_s \rangle \} \\ \mathcal{D}_{xv} = \mathcal{S} \{ \langle x_k | f_v + f_s \rangle \} + \mathcal{S} \{ \langle x_k | f_v - f_s \rangle \} \\ \mathcal{D}_{yh} = \mathcal{S} \{ \langle y_k | f_h + f_s \rangle \} + \mathcal{S} \{ \langle y_k | f_h - f_s \rangle \} \end{array} \right.$$

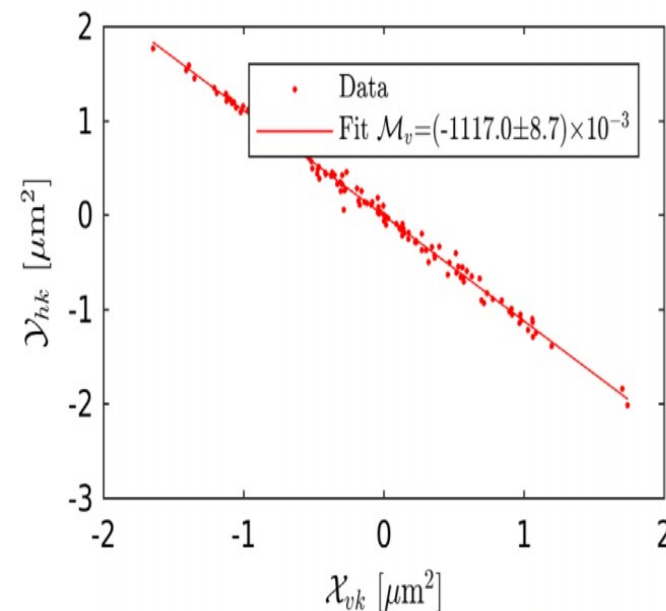
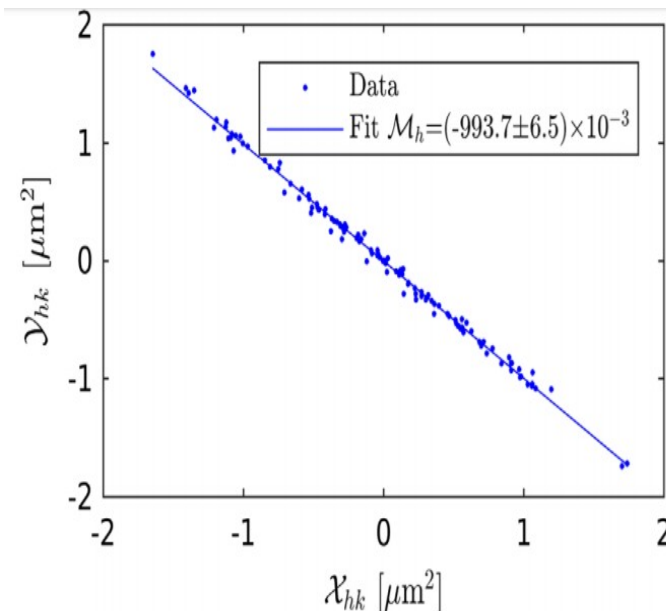
**Example:** a 90° rotation ( $x \Rightarrow y$  &  $y \Rightarrow -x$ ) changes  $\mathcal{D}_x \Rightarrow \mathcal{D}_y$ ,  $\mathcal{D}_y \Rightarrow -\mathcal{D}_x$ ,  $\mathcal{D}_{xh} \Rightarrow \mathcal{D}_{yh}$ ,  $\mathcal{D}_{yh} \Rightarrow -\mathcal{D}_{xh}$ ,  $\mathcal{D}_{xv} \Rightarrow \mathcal{D}_{yv}$  and  $\mathcal{D}_{yv} \Rightarrow -\mathcal{D}_{xv}$  leaves  $M_h$  and  $M_v$  unchanged: **Any linear coupling** is automatically taken into account.

The **signed amplitude** of a signal  $x$  at a frequency  $f_z$  is defined as:

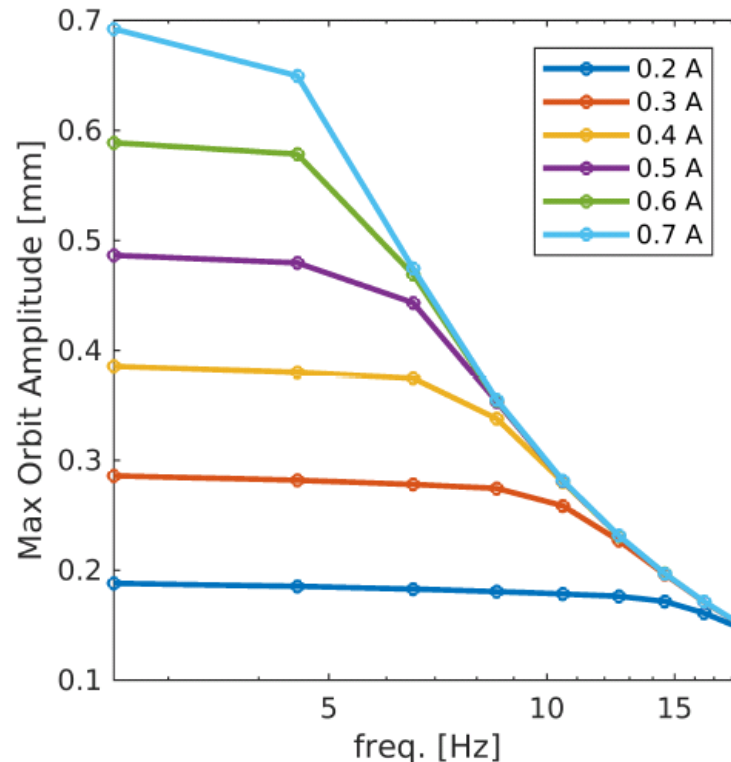
$$\mathcal{S} \{ \langle x | f_z \rangle \} = |\langle x | f_z \rangle| \operatorname{sgn} \left\{ \cos(\psi_x^{(z)} - \psi_z) \right\}$$

**Relative corrector offset fit:**  $\frac{h_{0j}}{\hat{h}_j}$

For every BPM, a point in the  $x_{hk}$  and  $y_{hk}$  plane is calculated. Then, the fit result is used to calculate the offsets of a single BPM- $l$ :  $x_l^0$  and  $y_l^0$ .



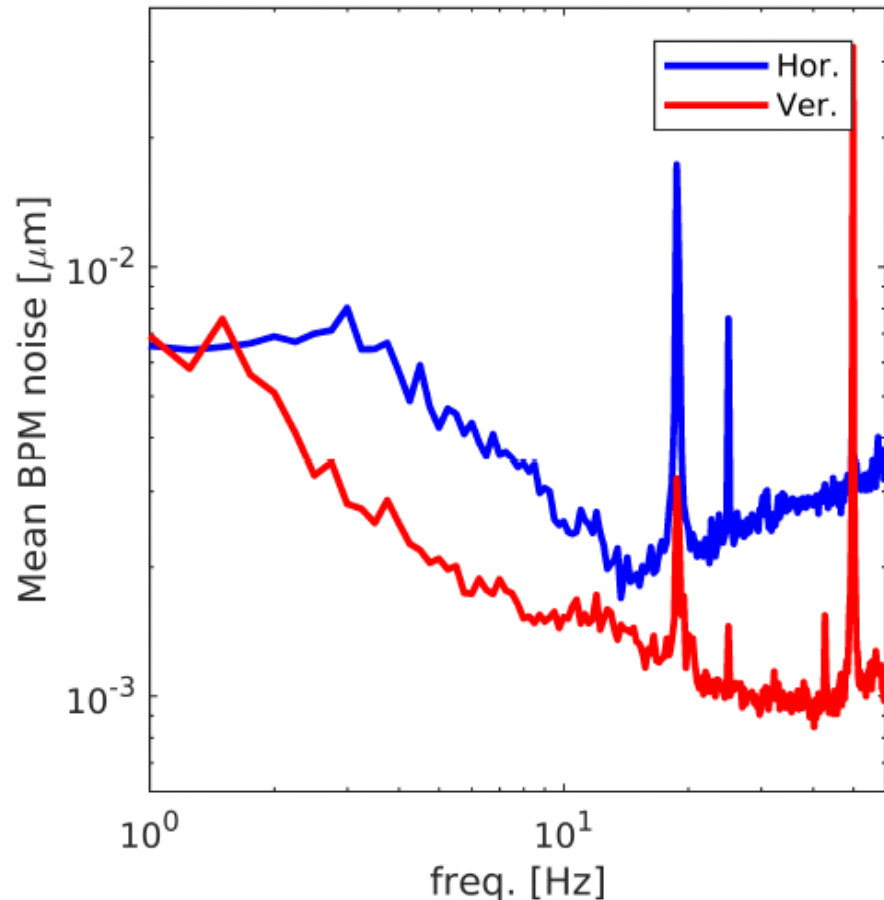
**Frequency choice:** The CM waveforms have a limited effective kick as a function of the frequency:



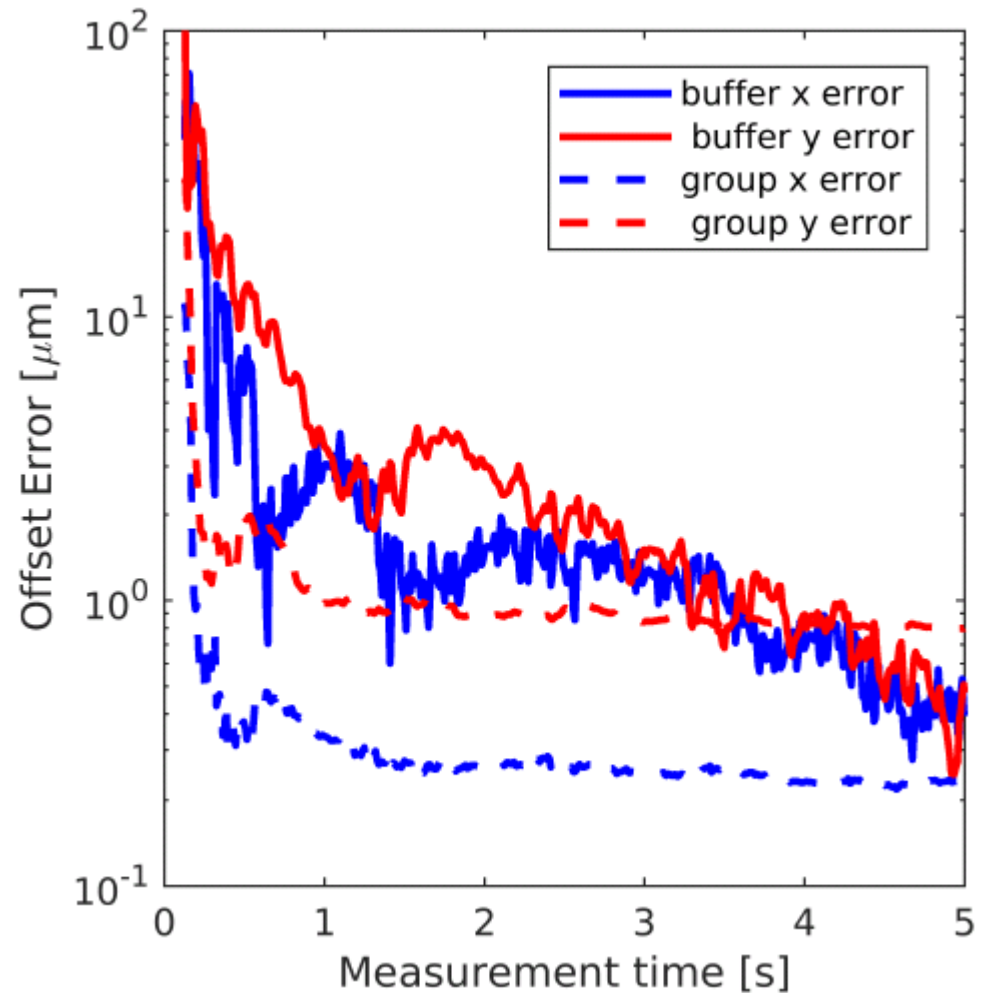
A minimum of **0.5 A** is needed to properly measure large offsets.

Also, we study the BPM noise as a function of the frequency. It gets better the higher the frequency, in the 0 Hz-18 Hz range:

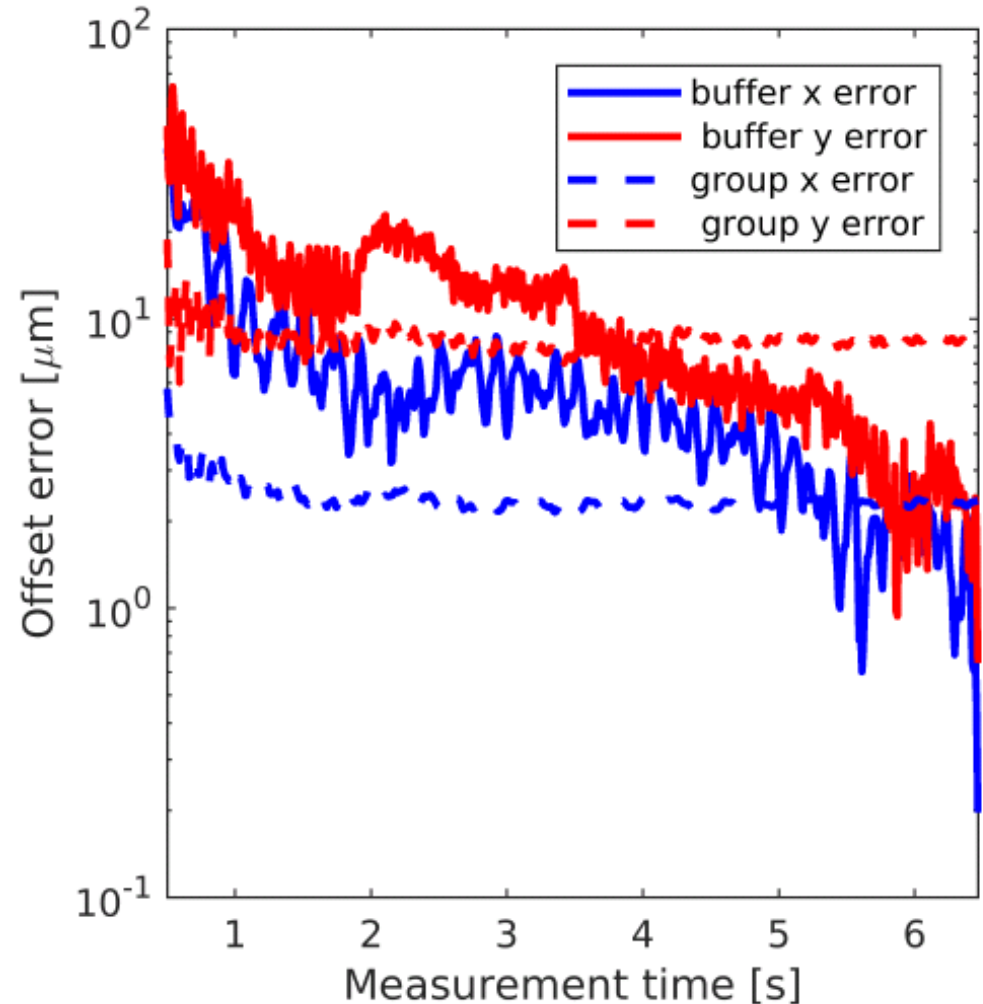
We decided to use **6 Hz** and **7 Hz** for the vertical and horizontal plane respectively (0.5mm).



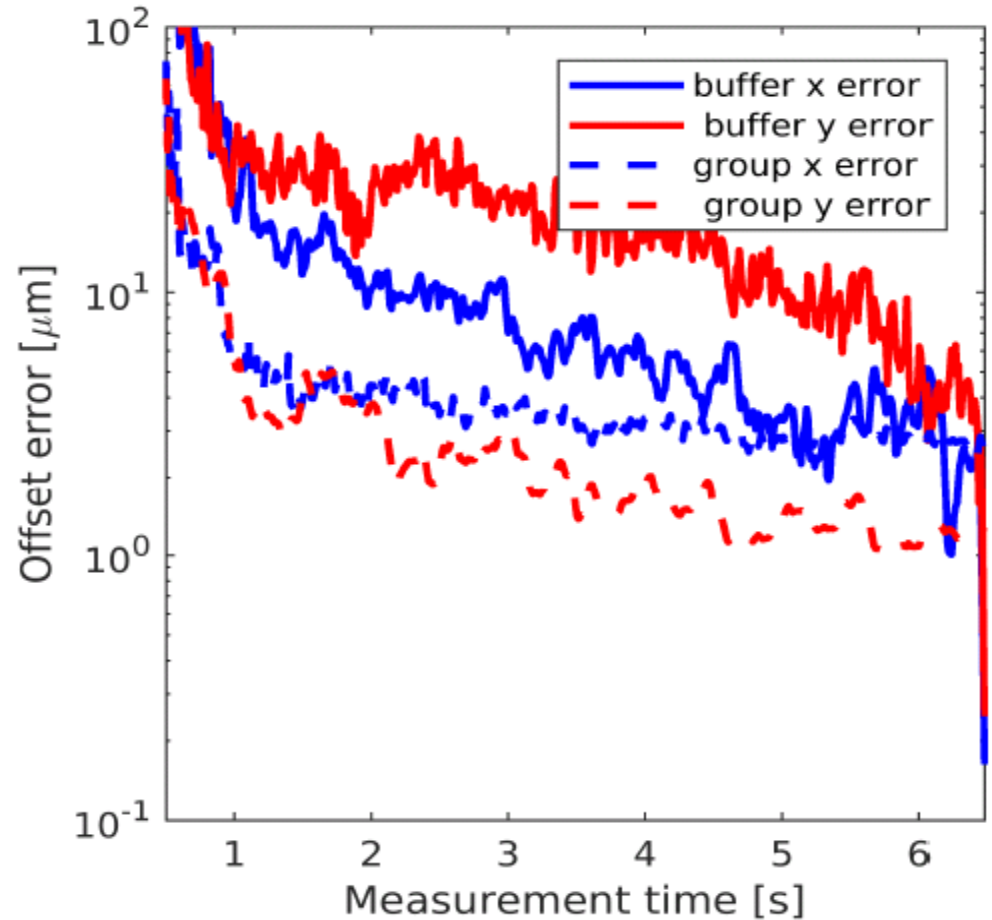
For a DC quad change of 2.5A, the **acquisition time** is optimized:  
1.5 seconds (3 s/meas.)



For a DC skew change of 2.5A, the acquisition time is optimized: 6 sec (12s/meas)



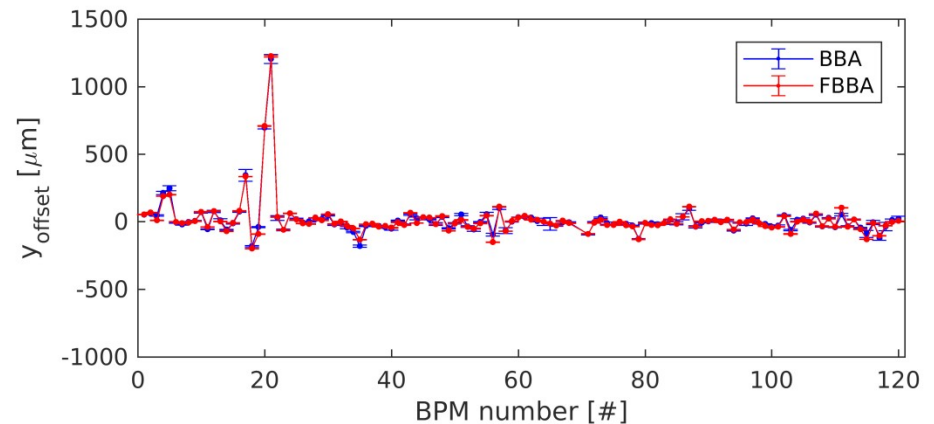
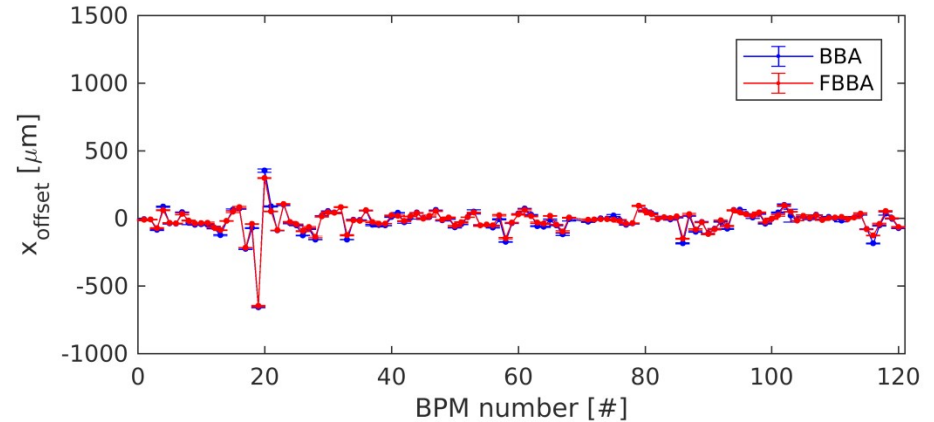
For an AC skew change of 2.5A at 1.6Hz, the acquisition time is optimized: 6 sec (6s/meas)





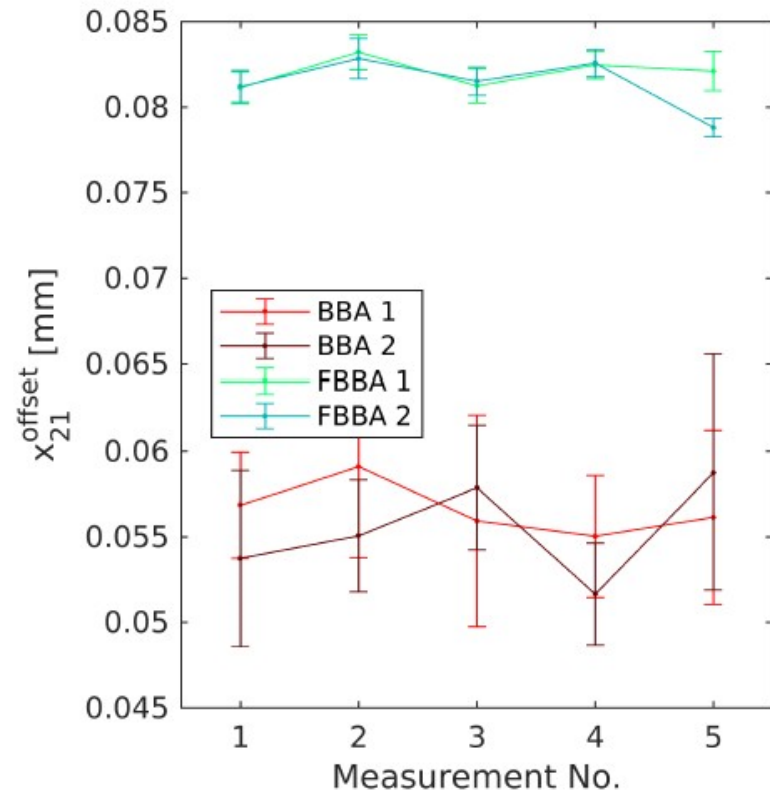
## BBA vs FBBA:

- The presented FBBA is **~30 times faster** (10 min vs 5h) than the standard BBA.
- The level of precision is similar: **1 $\mu\text{m}$** .
- There is a  **$\pm 10\mu\text{m}$**  unexplained difference.



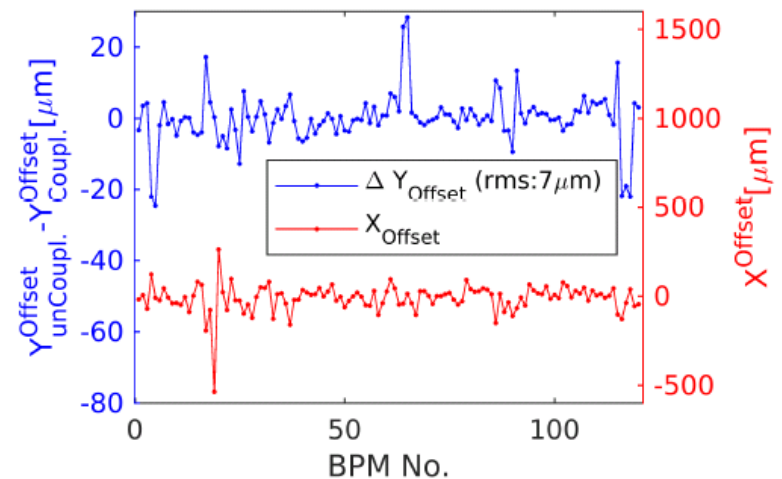
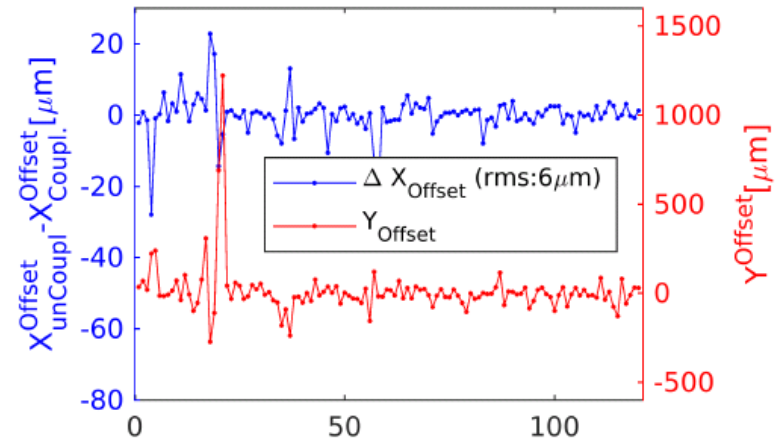
For some BPMs, there are some **systematic** discrepancies effects **not** related to **quad hysteresis**...

The measurements were performed with (1) and without (2) quad hysteresis cycles before the measurement.



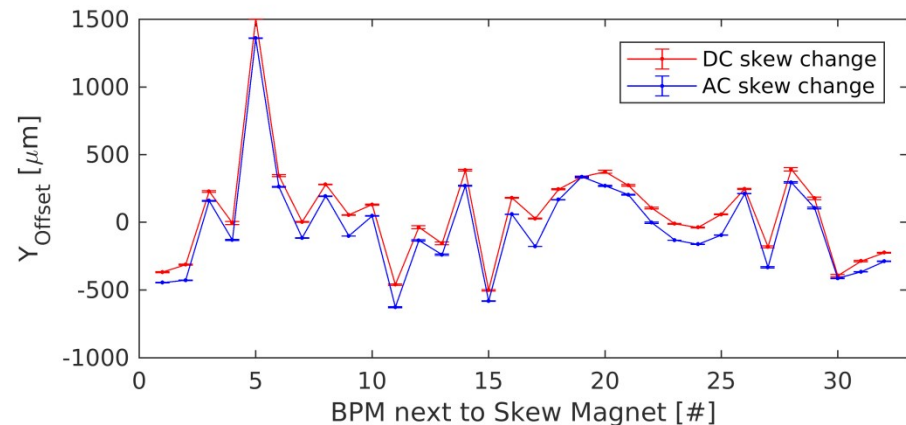
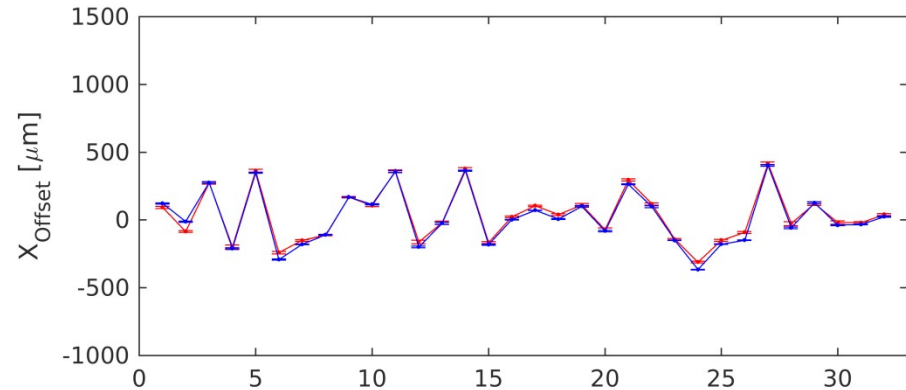
Regarding to **coupling** effects, they are of similar order.

It seems **not very relevant** except in the case of large coupling or for **skew quads**...

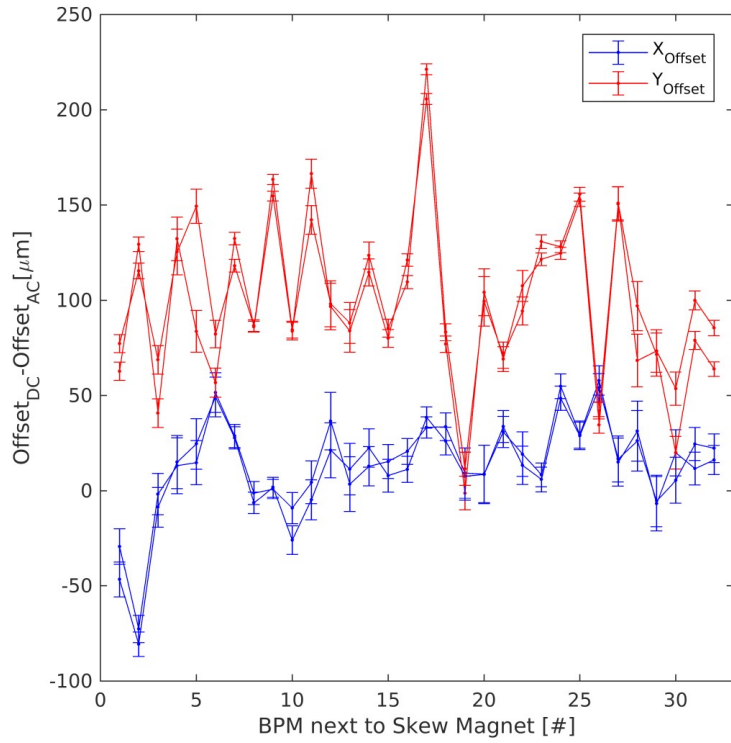


AC and DC magnet excitation give quite consistent results.

The AC is about 2 times faster, but there is a **systematic difference (unexplained)** of around  $100\mu\text{m}$ .



We have performed **random realistic simulations** of FBBA at ALBA on skew quadrupoles and this effect is **not expected**.



	Horizontal	Vertical
Model rms quadrupole offset	150 $\mu\text{m}$	150 $\mu\text{m}$
Mean difference between offsets:		
(Normal quad.) BBA vs model	15 $\mu\text{m}$	12 $\mu\text{m}$
(Normal quad.) dc FBBA vs model	16 $\mu\text{m}$	12 $\mu\text{m}$
(Normal quad.) ac FBBA vs model	16 $\mu\text{m}$	13 $\mu\text{m}$
(Skew quad.) dc FBBA vs model	19 $\mu\text{m}$	9 $\mu\text{m}$
(Skew quad.) ac FBBA vs model	19 $\mu\text{m}$	6 $\mu\text{m}$
(Normal quad.) dc FBBA vs BBA	4 $\mu\text{m}$	2 $\mu\text{m}$
(Normal quad.) ac FBBA vs BBA	4 $\mu\text{m}$	3 $\mu\text{m}$
(Normal quad.) ac FBBA vs dc FBBA	0 $\mu\text{m}$	3 $\mu\text{m}$
(Skew quad.) ac FBBA vs dc FBBA	0 $\mu\text{m}$	5 $\mu\text{m}$

- Using the FOFB hardware, we have developed a method to perform quadrupole BBA which is **30times faster** than standard BBA and achieves even better **precision** (not sure about accuracy).
- The FBBA allows to perform simultaneous analysis of both planes, and accounts for any level of optics **coupling, BPM roll and CM tilt**.
- This novel approach allows also a **skew** quadrupole BBA (**sextupole** yoke).
- Some small **differences** between AC and DC modes remain **unexplained** ( $\sim 30\mu\text{m}$  for the quads case, and  $\sim 100\mu\text{m}$  for the skews case).