



Frascati – 13 September 2022

# MGB<sub>2</sub> CONDUCTORS FOR FUTURE DETECTOR MAGNETS

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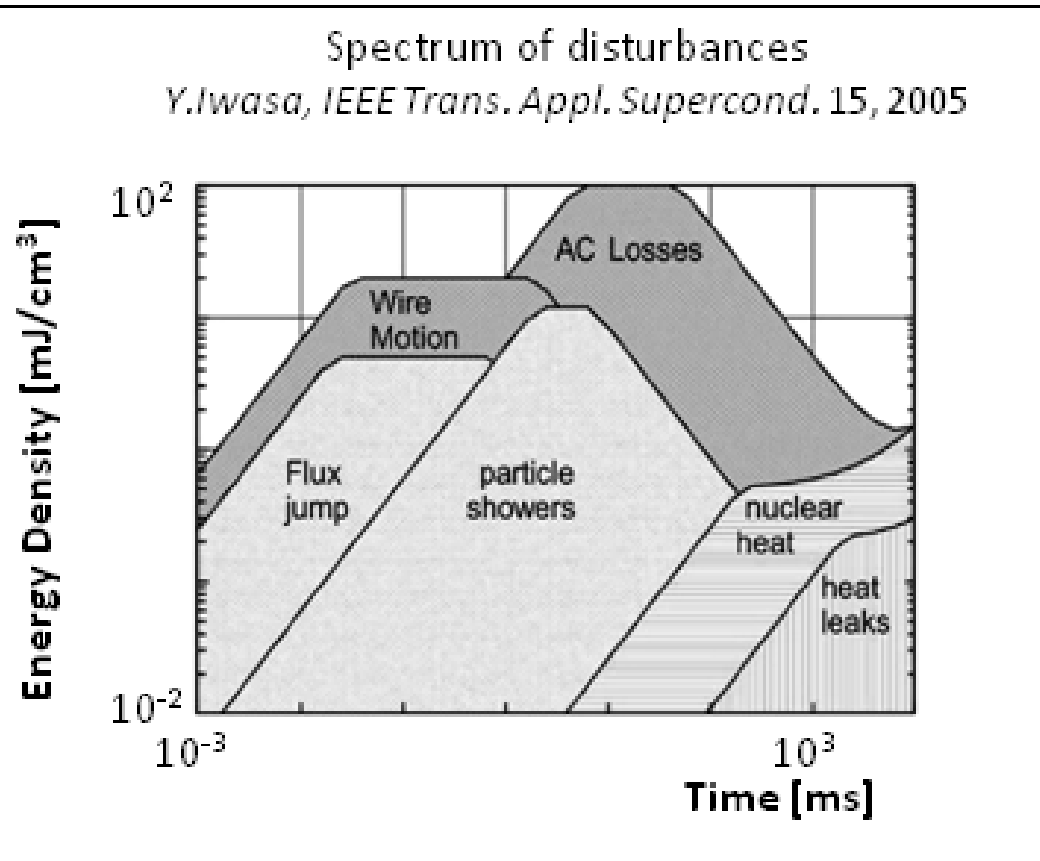
## SUPERCONDUCTING MAGNETS FOR PARTICLE DETECTORS

Main characteristics:

- Large volume
- Moderate magnetic field (0.5 to 4 T)
- Transparency to particles is often required
- Generally solenoidal or toroidal shape

An important feature of superconducting magnets is **stability**

Stability is related to the release of energy that a magnet can withstand without quenching



$$\nabla(k_{cond}\nabla T) + \rho_{cond}J^2 + g - h = c_{cond} \frac{\partial T}{\partial t}$$

↑  
Joule  
dissipation

disturbances

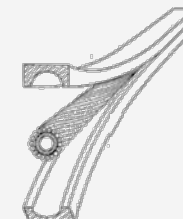
↑  
cooling  
power

## Cryogenic stability

$$\nabla(k_{cond}\nabla T) + \rho_{cond}J^2 + g - h = c_{cond}\frac{\partial T}{\partial t} \quad \longrightarrow \quad \rho_{cond}J^2 + g \leq h$$

- reduce  $\rho_{cond}$ : low resistivity normal metal matrix (in parallel with superconductors)
- reduce  $J$ : increase conductor cross section
- Increase  $h$ :
  - magnets in liquid Helium pool
  - forced flow magnets

OMEGA magnet (CERN)





## Adiabatic stability

The heat generation terms ( $\rho_{cond}J^2$  e  $g$ ) integrated over time duration must be limited to a maximum permissible level

$$\Delta e_{max} = \int_{T_{op}}^{T_{max}} c_{cond} dT$$

$\Delta e_{max}$  is the energy density margin

$T_{max}$  is the temperature at which the superconductor undergoes the transition to the normal state (it depends on  $B$  and  $J$ )

$T_{max} - T_{op}$  is the temperature margin. Typical value for NbTi is between 2 K and 3 K



## Thin solenoids

Thin solenoids are based on adiabatic stability (indirect cooling)

Aluminum: Low density, high radiation length, low resistivity at 4.2 K (RRR>2000)

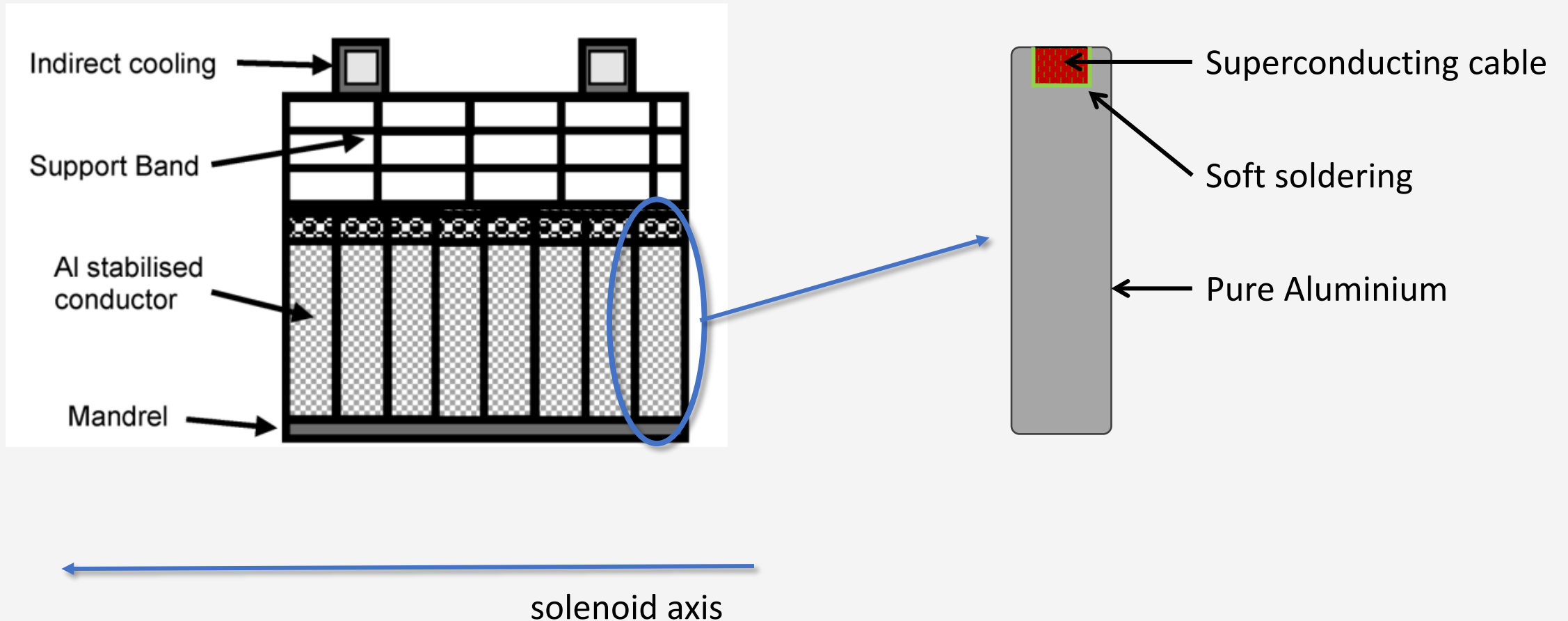
Pure Aluminum in parallel to the superconducting composite:

- increases the conductor thermal capacity per unit length
- limits the dissipation in case of local transition to the normal state
- limits the magnet weight
- allows positioning calorimeters outside the magnet.

The first detector solenoid based on aluminum stabilized conductor was CELLO (DESY) in 1978



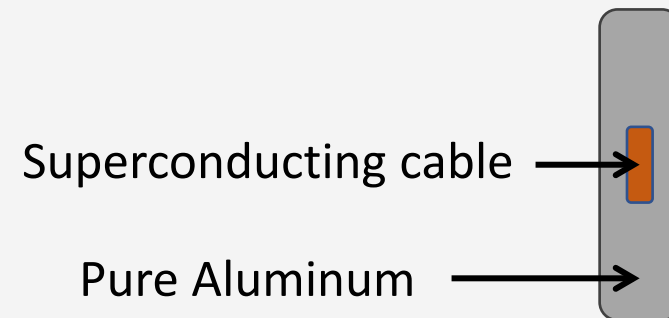
## Sketch of the CELLO magnet



## Thin solenoids

Later, Aluminum stabilized conductors have been manufactured by co-extrusion in such a way that the superconducting cable is embedded in pure aluminum matrix

The co-extrusion technology was applied for the first time in the CDF magnet (FERMILAB) in 1984

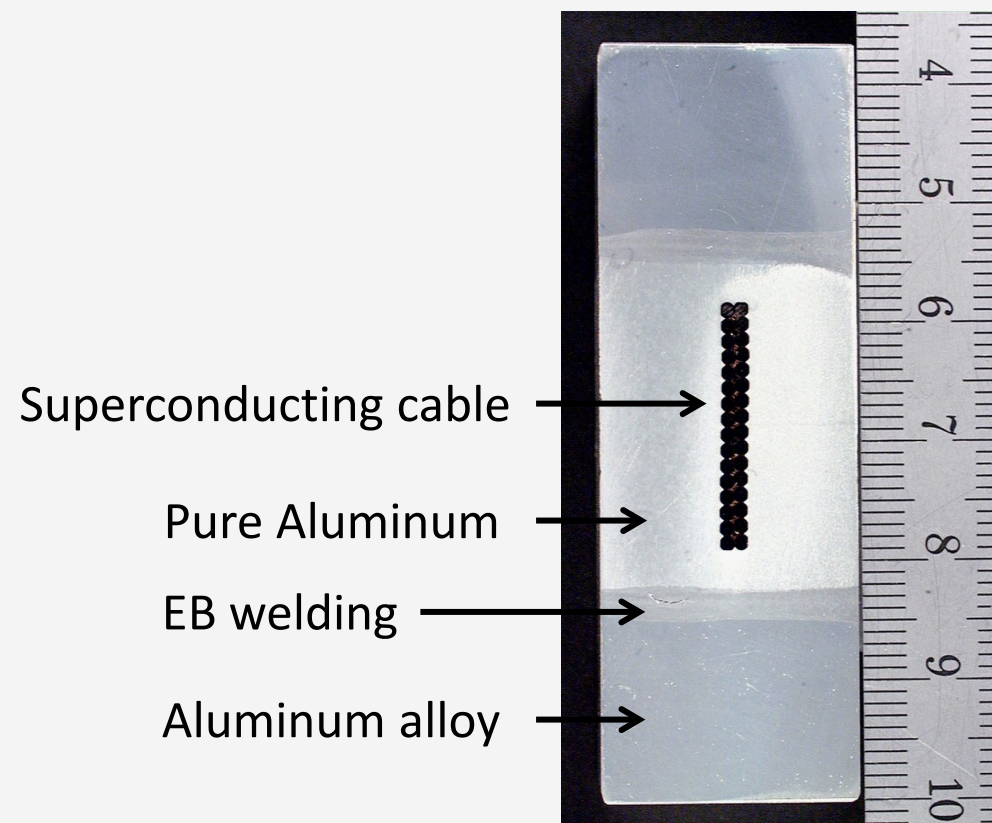




## Thin solenoids

### CMS conductor

Aluminum stabilized cable reinforced with EBW Aluminum alloy



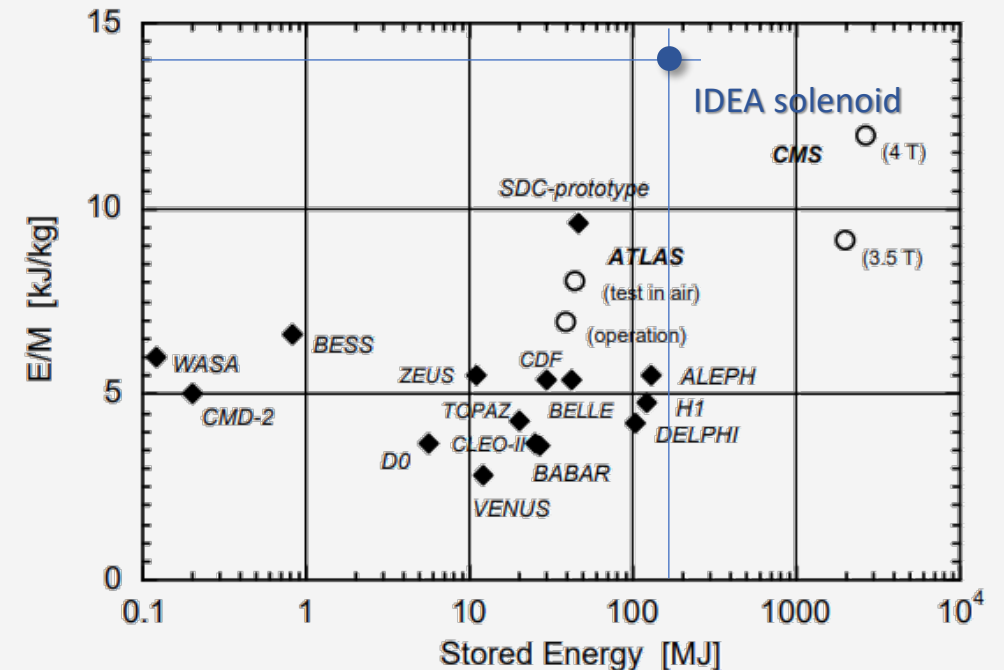
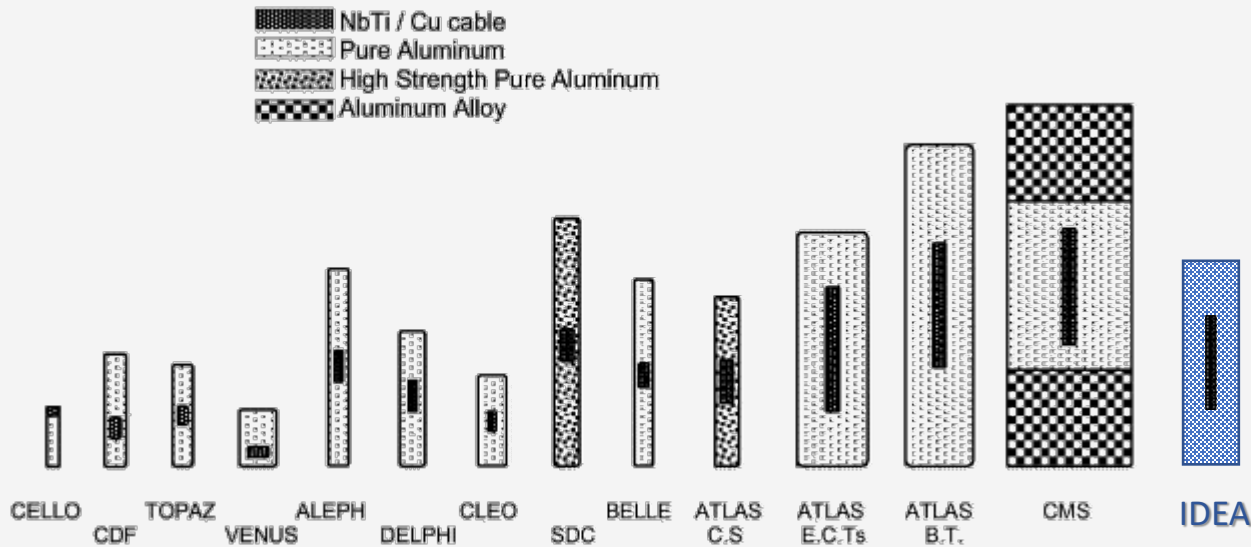


## Thin solenoids

In some detector magnet, pure Aluminum is replaced by high strength, low resistivity Aluminum-Nickel alloys.

**ATLAS central solenoid** [A.Yamamoto et al. NIM A 584, 2008, 53–74]

# Thin solenoids evolution



A.Yamamoto and Y.Makida, *Nuclear Instruments and Methods in Physics Research A* 494 (2002)

IDEA data from N.Deelen <https://indico.cern.ch/event/1162992/contributions/4945512/>  
presented @ Superconducting magnet Workshop, Sept. 12th 2022



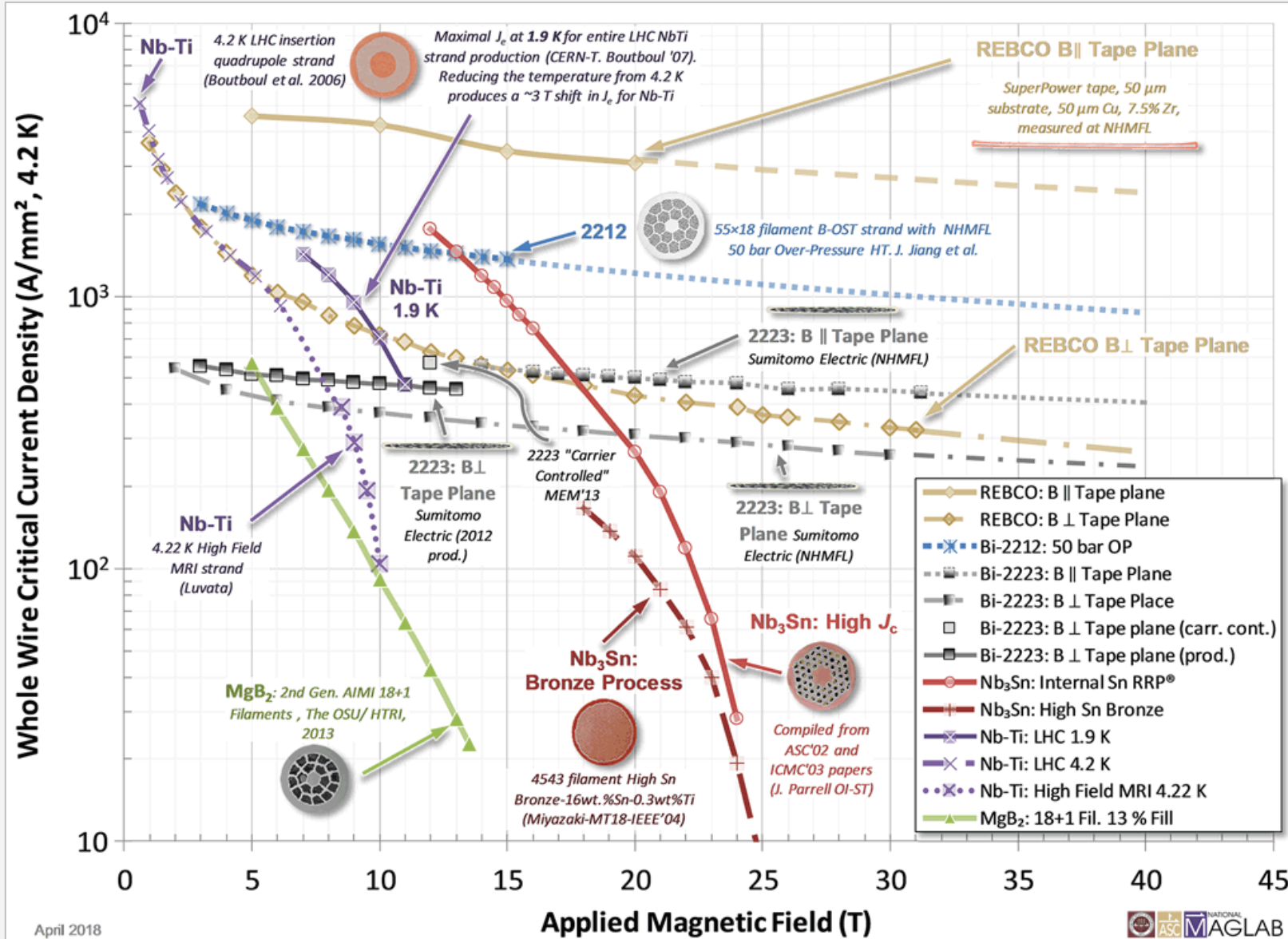
At present, only NbTi alloy is used for detector magnets.

NbTi is ductile, relatively cheap and robust ( $J_C$  is not affected by mechanical stress).

However, fabrication of aluminum stabilized conductors is an industrial process performed by very few firms.



Would it make sense to use other superconductors ?



## Technical superconductors

REBCO (tape)  $T_c = 92 K$

BiSCCO 2223 (tape – Ag matrix)  $T_c = 108 K$

BiSCCO 2212 (Ag matrix)  $T_c = 96 K$

Nb<sub>3</sub>Sn  $T_c = 18 K$

MgB<sub>2</sub>  $T_c = 38 K$



**MgB<sub>2</sub>** is more expensive than NbTi but much cheaper respect to REBCO and BiSCCO

It is produced by reacting the precursors (Mg and B) powders at about 700°C for few minutes

**In situ:** wires are prepared by powder-in-tube method using the precursors. MgB<sub>2</sub> is then obtained inside the wire by suitable heat treatment

**Ex situ:** wires are prepared by powder-in-tube method directly using MgB<sub>2</sub> powders



MgB<sub>2</sub> has low reversibility field  $B_{irr}$  (if  $B \geq B_{irr}$  then  $J_c = 0$ )  
(@  $B_{irr}$  superconductivity is hold, but no current can flow)

Pure MgB<sub>2</sub>:  $B_{irr} \approx 12 T$

Doping increases  $B_{irr}$

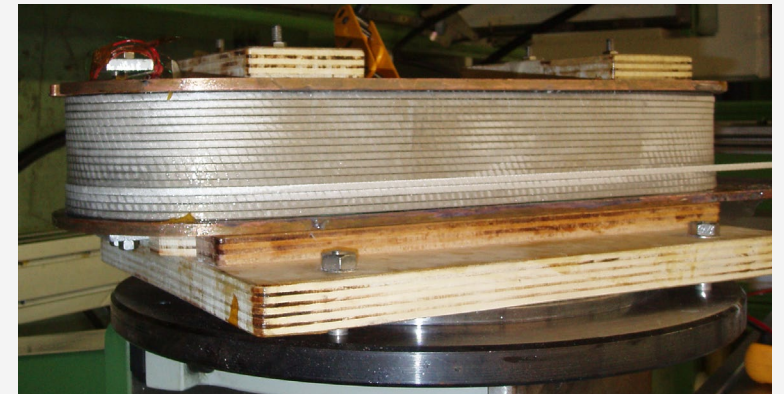
But detector magnets must not generate high magnetic field

Generally  $B < 4 T$



Like all technical superconductors except NbTi, **MgB<sub>2</sub> is brittle**:  
for a given MgB<sub>2</sub> composite conductor, a critical bending radius does exist (order of 4 cm for a 0.65 mm thick tape).

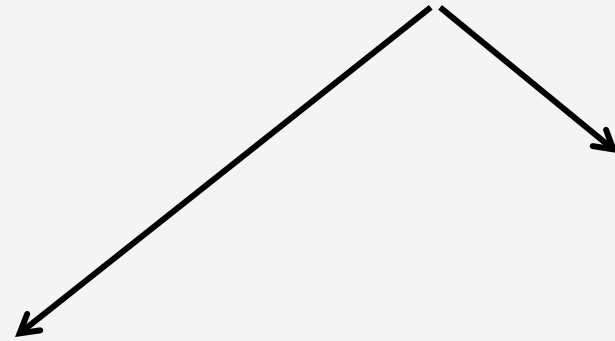
Not an issue for large magnets!



Winding of a racetrack coil  
with ex-situ MgB<sub>2</sub> tape



MgB<sub>2</sub> would allow operating the magnet at  $T > 10 K$  ( $T_c = 38 K$ )



More efficient cryogenics

Higher COP

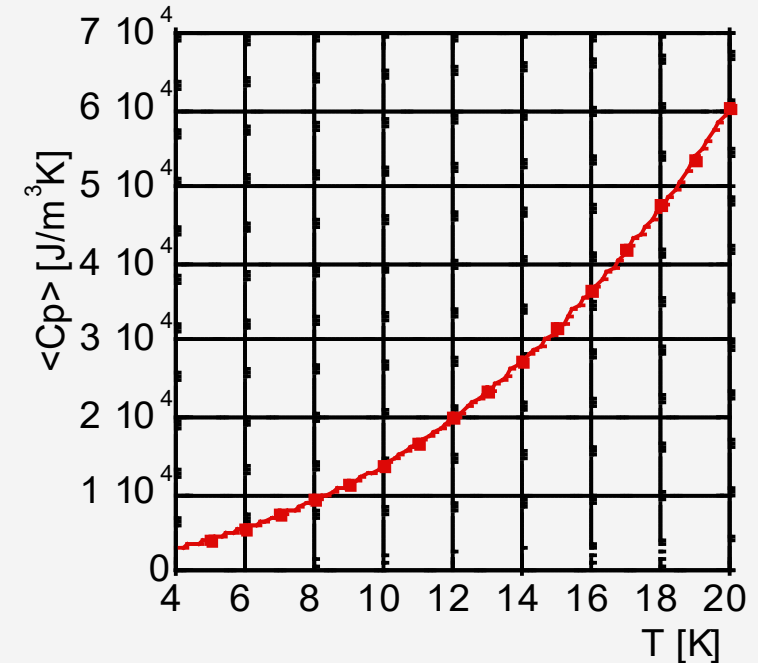
Better conduction cooling

$$\frac{K_{Al6061}@12 K}{K_{Al6061}@4.2 K} \approx 3$$

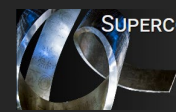
Higher energy density margin

$$\Delta e_{max} = \int_{T_{op}}^{T_{max}} c_{cond} dT$$

$$c_{cond} \propto \left( \frac{T}{\theta_D} \right)^3$$



Aluminum matrix is not necessary for stabilization.  
It can be necessary/useful for quench protection.



First proposals about MgB<sub>2</sub> conductors coupled with Aluminum were related to space applications due to low weight requirement

P. Spillantini

Superconducting magnets and mission strategies for protection from ionizing radiation in interplanetary manned missions and interplanetary habitats

Acta Astronautica, 68 (9–10), 2011, 1430-1439

R. Battiston, W. J. Burger, V. Calvelli, V. I. Datskov, S. Farinon, and R. Musenich

Superconducting Magnets for Astroparticle Shielding in Interplanetary Manned Missions

IEEE Trans. on Appl. Supercond., 23 (3), 2013, 4101604



## EU FP7 project to study superconducting shields to protect astronauts from space radiation

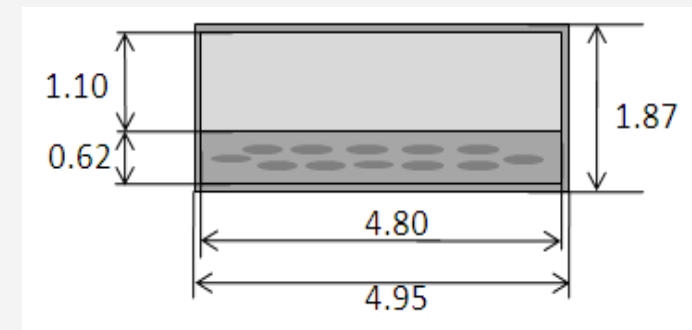
Conductor: Titanium clad MgB<sub>2</sub> tape + Aluminum strip

Ti/MgB<sub>2</sub> ratio 2.7/1.

75 μm thick insulation.

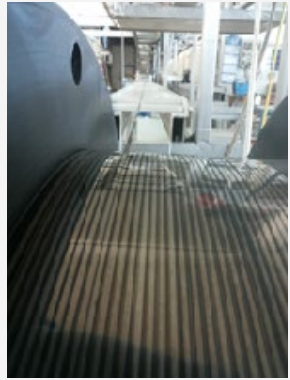
Total conductor cross section: 9.25 mm<sup>2</sup>.

Average mass density : 3000 kg/m<sup>3</sup>.





## Development of SR2S conductor prototype



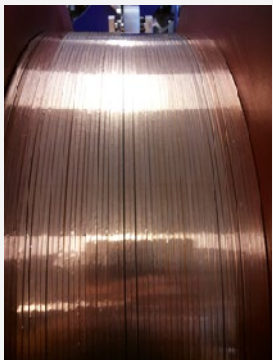
360 m Ti-MgB<sub>2</sub>



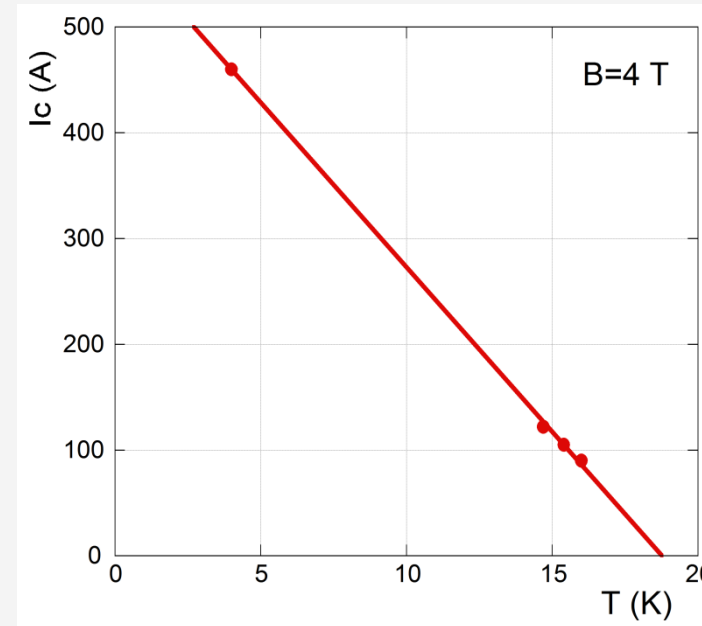
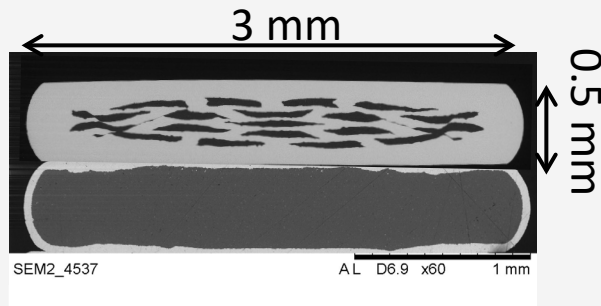
Ti-MgB<sub>2</sub> tape during copper plating



copper plated Ti-MgB<sub>2</sub> tape

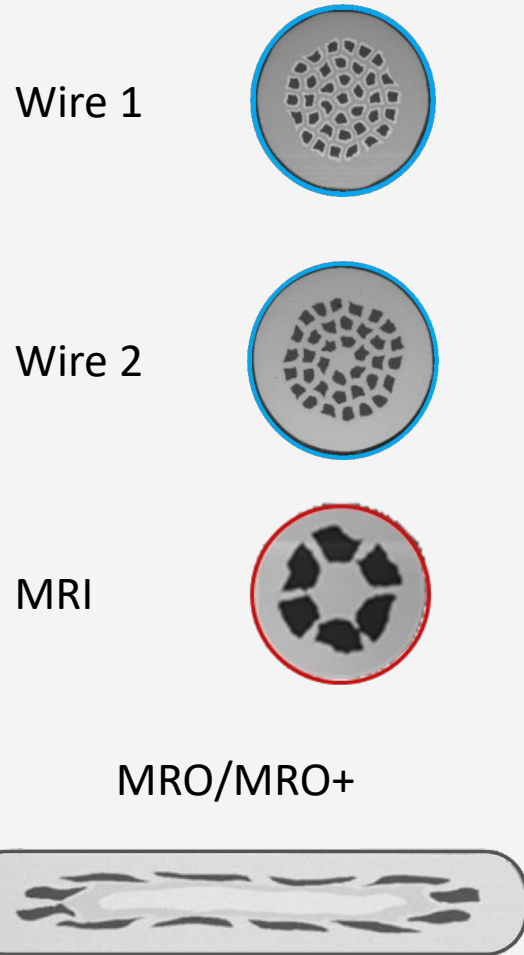


Cu-Ti-MgB<sub>2</sub> tape

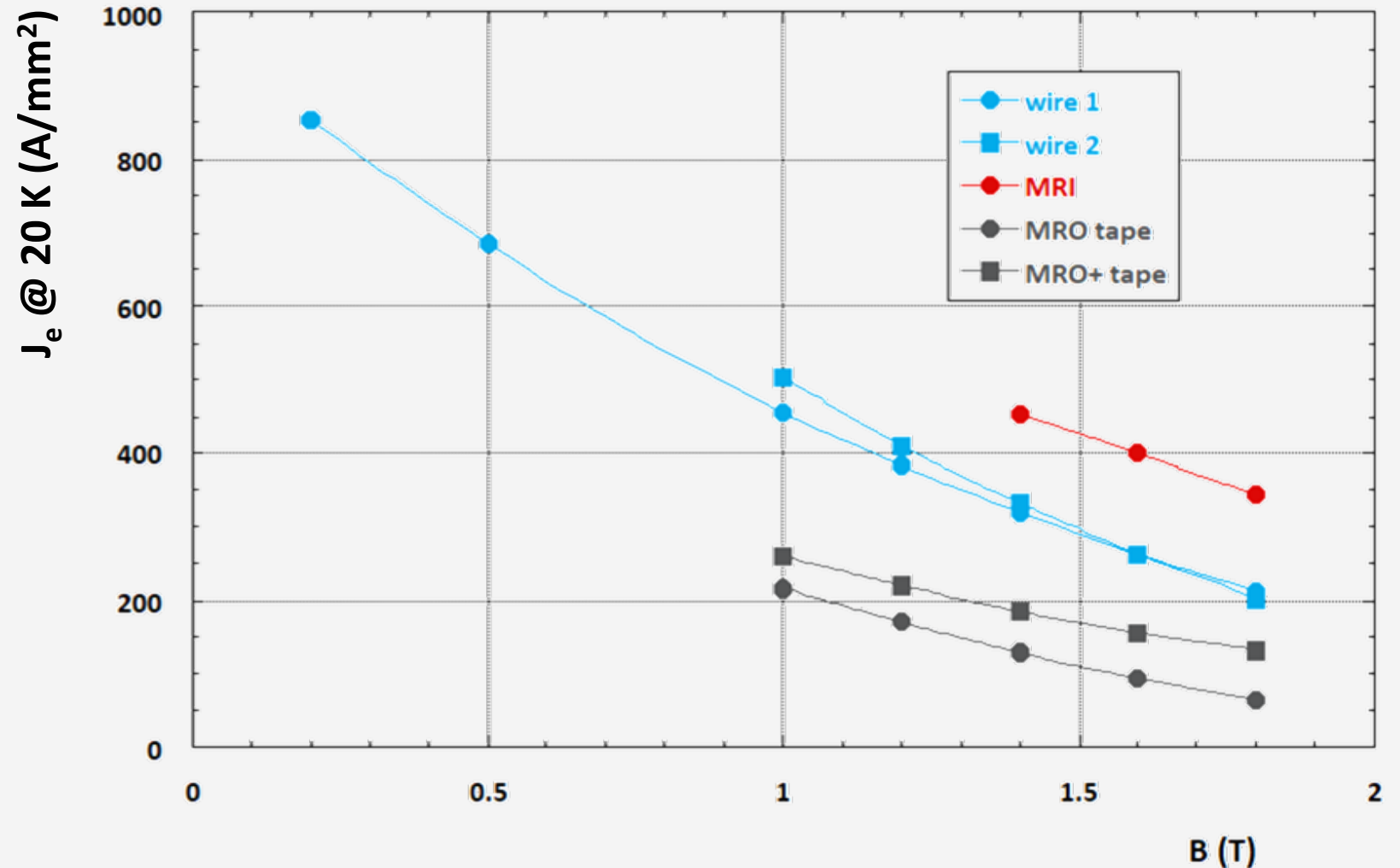


Problems occurred during aluminum tape soldering due to different thermal contractions.

Due to tight schedule and limited funds, no further attempts were made to solder the aluminum tape.



## Present status of ex-situ MgB<sub>2</sub> conductors



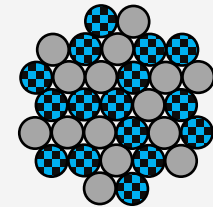
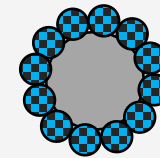
$$J_e(15K, 2T) \approx 400 - 600 \text{ A/mm}^2$$

In MgB<sub>2</sub> magnets operating at  $T > 10 K$  stability is due to the high specific heat

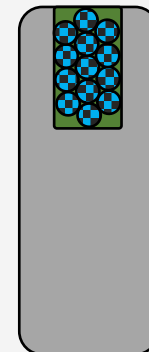


Close contact between the superconducting composite and aluminum is not necessary

- In principle, it is possible to use conductors obtained by cabling MgB<sub>2</sub> wires and aluminum wires



- Limited deformation is possible before heat treatment to obtain an almost flat cable



- MgB<sub>2</sub> detector magnets could be protected via controlled insulation technique



## A remarkable example of cabling of MgB<sub>2</sub> wires: the LHC superconducting links

A. Ballarino, Supercond. Sci. Technol. 27 (2014) 044024



a)



b)



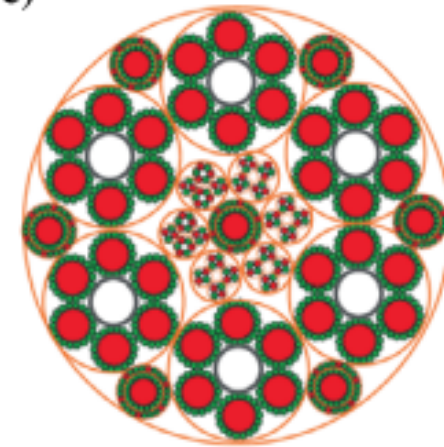
c)



d)



e)



**Figure 5.** Cables made with MgB<sub>2</sub> round wire. (a) Sub-unit of 20 kA cable,  $\Phi \sim 6.5$  mm ; (b) 20 kA cable,  $\Phi \sim 19.5$  mm; (c) concentric 2x3 kA cable,  $\Phi \sim 8.5$  mm; (d) 0.4 kA cable (top) and 0.12 kA cable (bottom),  $\Phi < 3$  mm ; (e) 165 kA cable assembly for LHC P1 and P5 (6x20 kA, 7x2x3 kA, 4x0.4 kA, 18x0.12 kA),  $\Phi \sim 65$  mm.





## Conclusions

- Detector magnets based on MgB<sub>2</sub> conductors can be operated at  $T > 10\text{ K}$
- Consequences of higher operative temperature are:
  - higher stability
  - higher thermal conductivity (better indirect cooling)
  - higher refrigerator COP
- R&D is necessary to develop suitable conductors
- Detector magnet design must be rethought based on MgB<sub>2</sub> conductor features (as an example, the quench issue of MgB<sub>2</sub> detector magnets could be faced via controlled insulation technique)