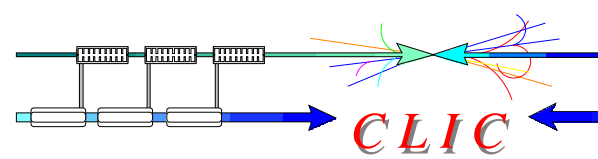


Optimum frequency and gradient for CLIC main linac

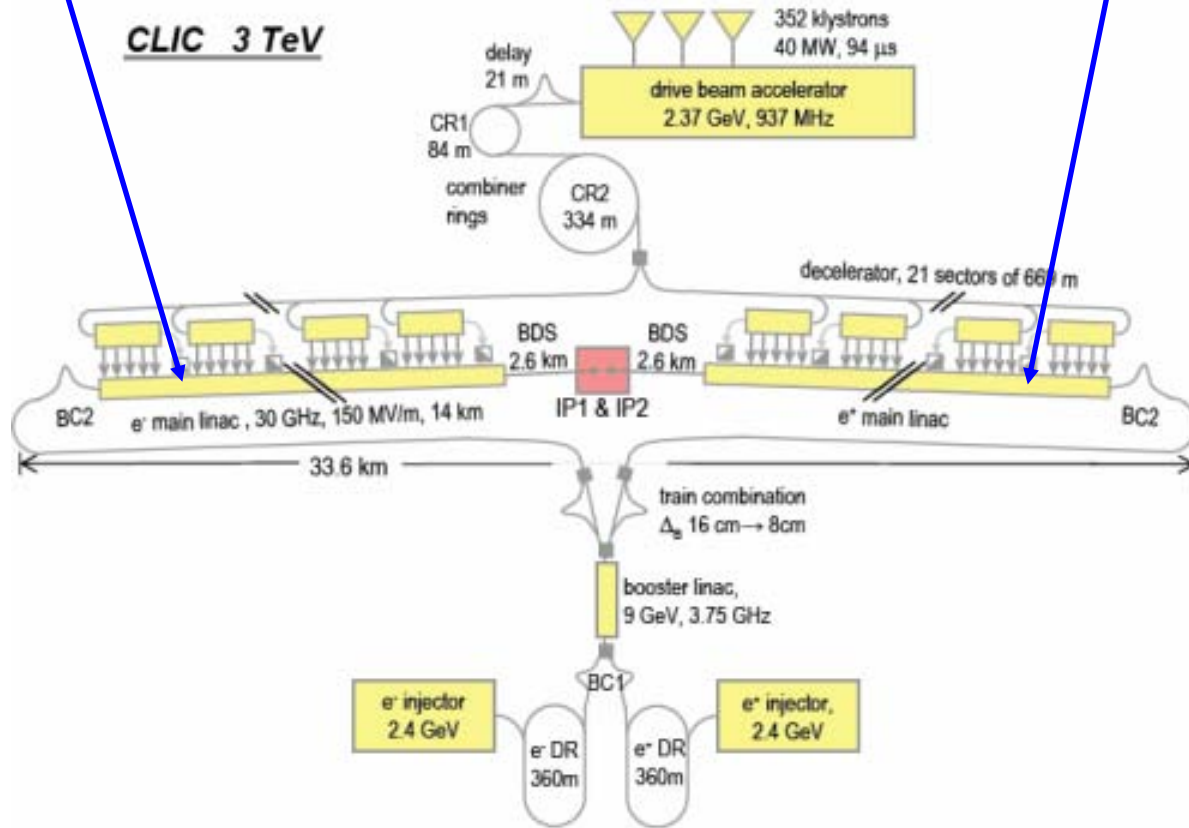
Alexej Grudiev
CERN, Geneva



- Introduction
- Optimization procedure
- Optimization results
- Conclusions

CLIC

Compact LI near Collider (CLIC) main linac



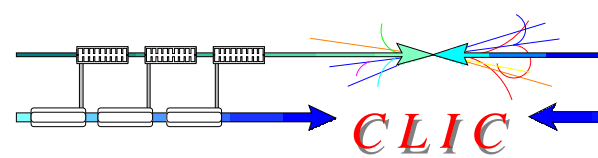
- Higher gradient ->
- Shorter linac
- Lower cost
- Better for beam dynamics

=> 150 MV/m

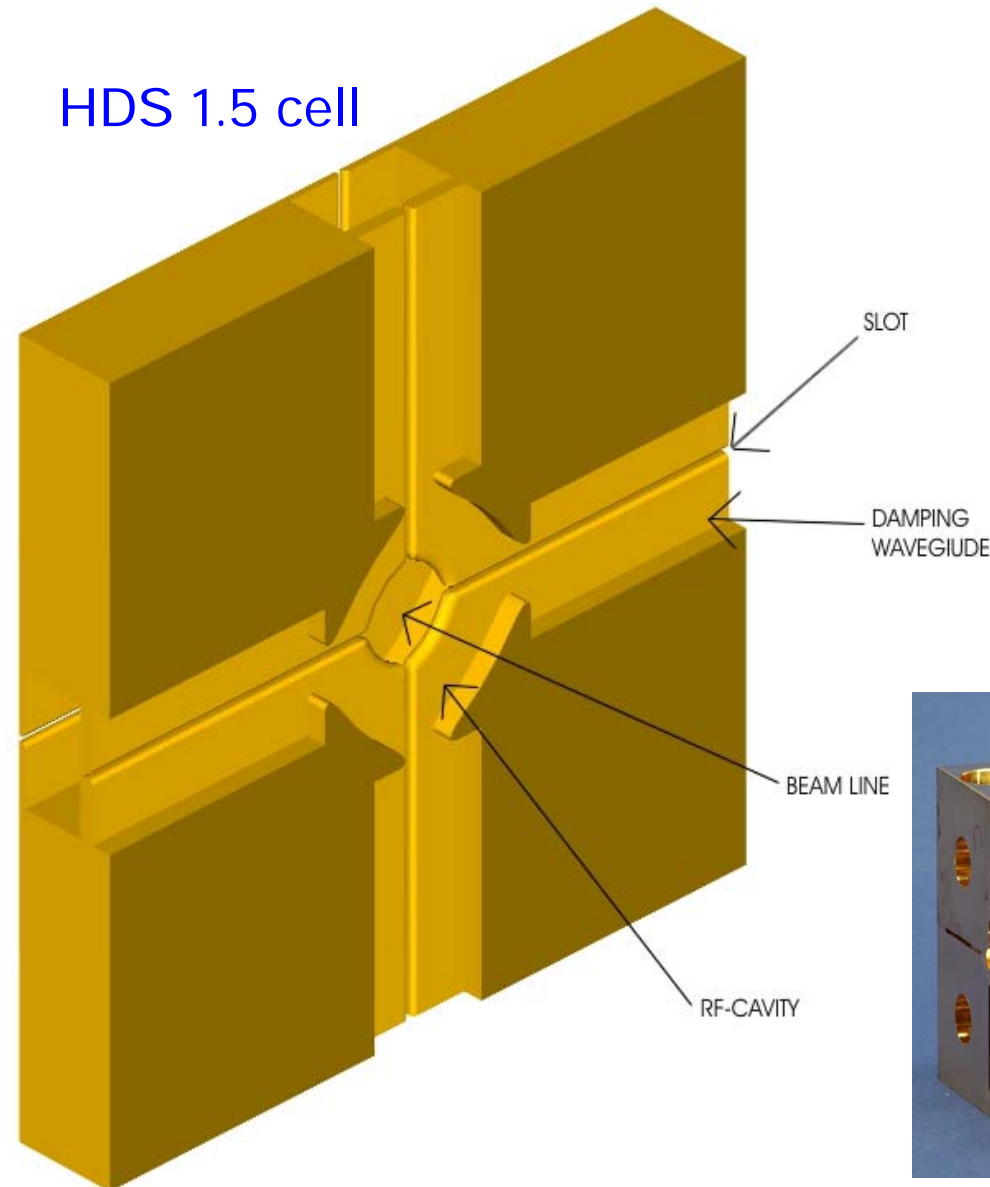
- Higher frequency ->
- Higher gradient (old)
- Lower peak power
- Higher efficiency
- More compact -> Cost

=> 30 GHz

The aim of the study is to find the best parameters for CLIC main linac performance in terms of luminosity per input power. This is not necessary the overall cost optimum (still to be done).

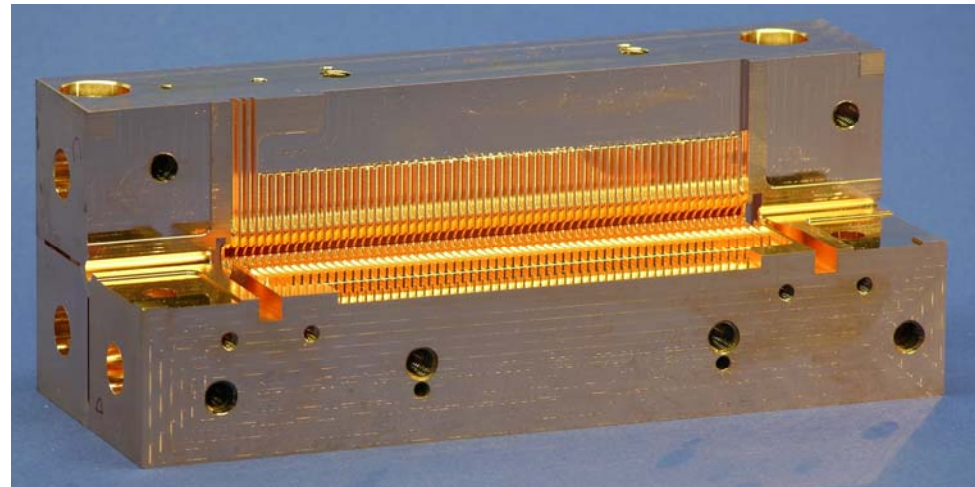


HDS 1.5 cell



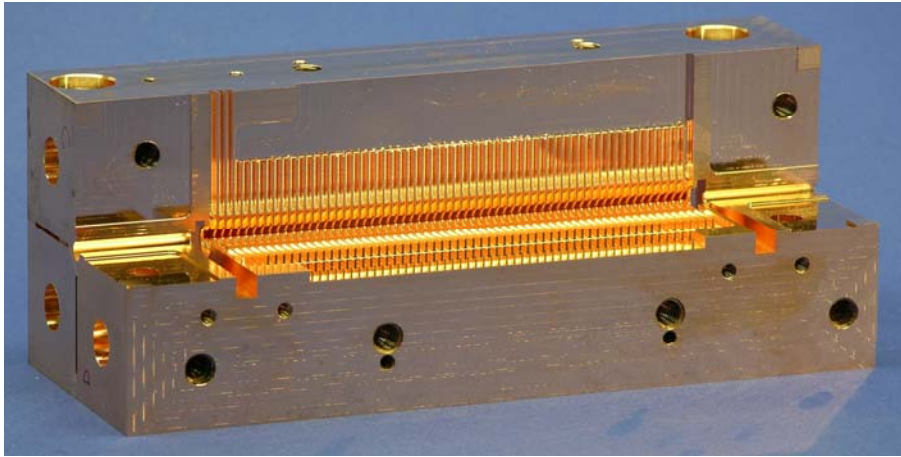
Hybrid Damped Structure (HDS)

- Excellent wakefield damping
- $E_{\text{surf}} / E_{\text{acc}}$ and $H_{\text{surf}} / E_{\text{acc}}$ are only by 7 and 9 % higher than in undamped cell, respectively
- 4 metal pieces per structure
- No brazing is necessary
- Good pumping capabilities

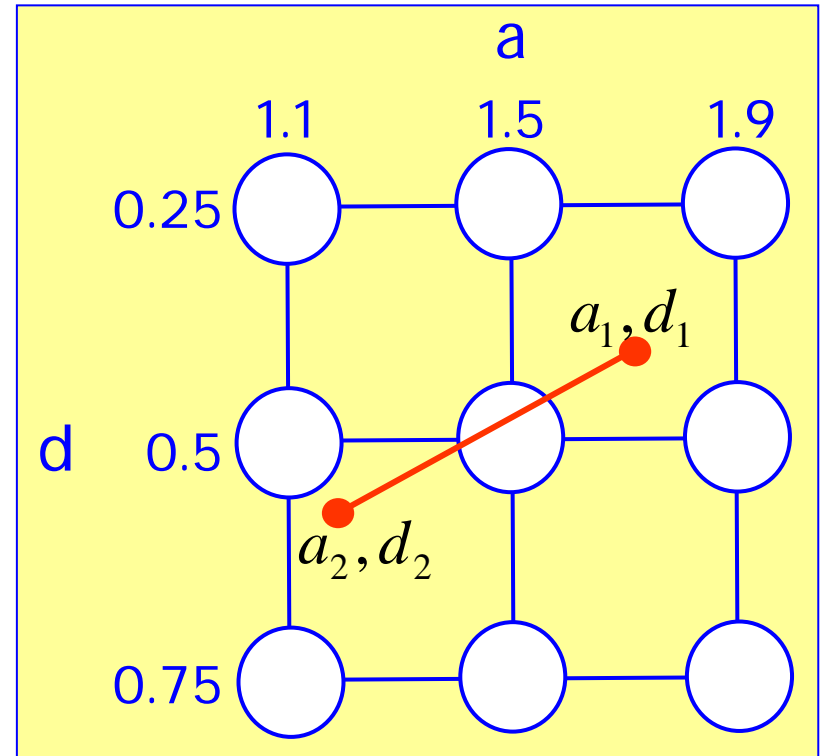


Optimization procedure

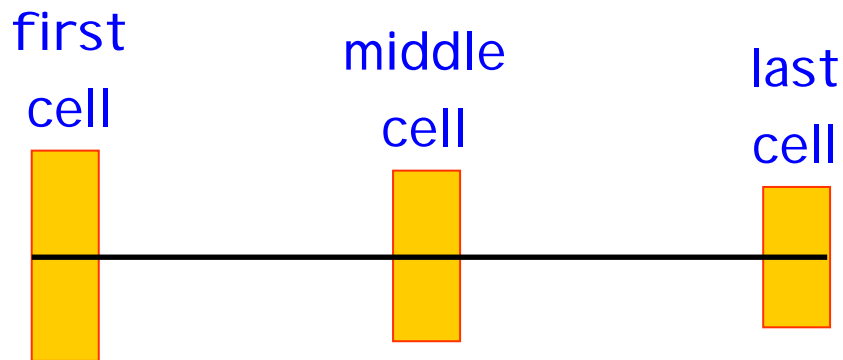
CLIC



Single cell parameter interpolation



Structure parameters are calculated using parameters of the three cells:





CLIC

All structure parameters are variable:

$$\langle E_{\text{acc}} \rangle = 90 - 150 \text{ MV/m,}$$

$$f = 12 - 30 \text{ GHz,}$$

$$\Delta\varphi = 50^\circ - 130^\circ,$$

$$\langle a \rangle / \lambda = 0.09 - 0.21,$$

$$\Delta a / \langle a \rangle = 0.01 - 0.6,$$

$$d_1 / \lambda = 0.025 - 0.1, \quad d_2 > d_1$$

$$N_{\text{cells}} = 15 - 300.$$

N structures:

7

10

9

24

60

61

4

221.356.800

CLIC

Beam dynamics constraints:

N depends on $\langle a \rangle / \lambda$, $\Delta a / \langle a \rangle$, f and $\langle E_{acc} \rangle$ because of short-range wake

N_s is determined by condition: $W_{t,2} = 10 \text{ V/pC/mm/m}$ for $N = 4 \times 10^9$

rf breakdown and pulsed surface heating (rf) constraints:

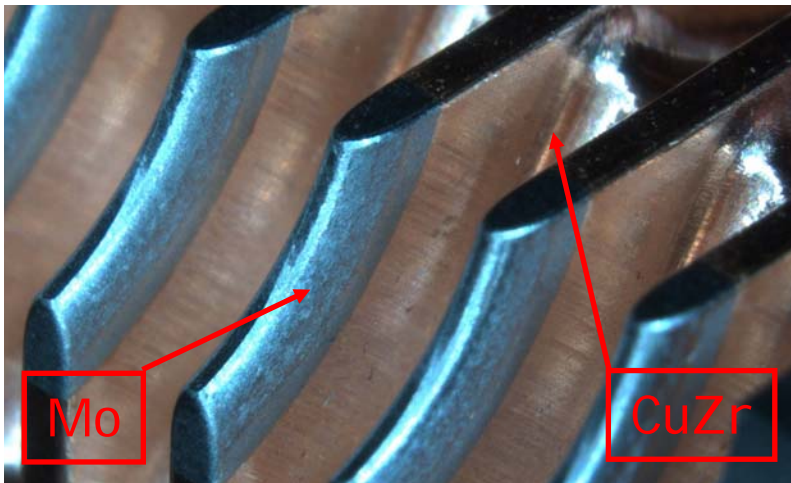
$E_{surf}^{max} < 380 \text{ MV/m}$ & $P_{in} t_p^{1/2} / C < 24 \text{ MWns}^{1/2}/\text{mm}$ & $\Delta T^{max} < 56 \text{ K}$

30 GHz, Mo

X-band, Cu \leftrightarrow 30 GHz, Mo

CuZr

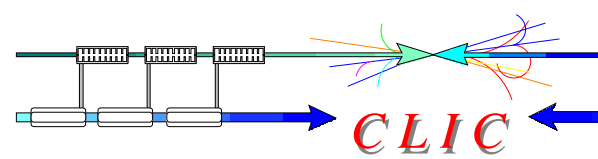
Bi-metallic HDS



Posters: MOPLS128; MOPLS103

N.B. Applying the same constraints to different structures implies that the structures are equally challenging

Optimization figure of merit



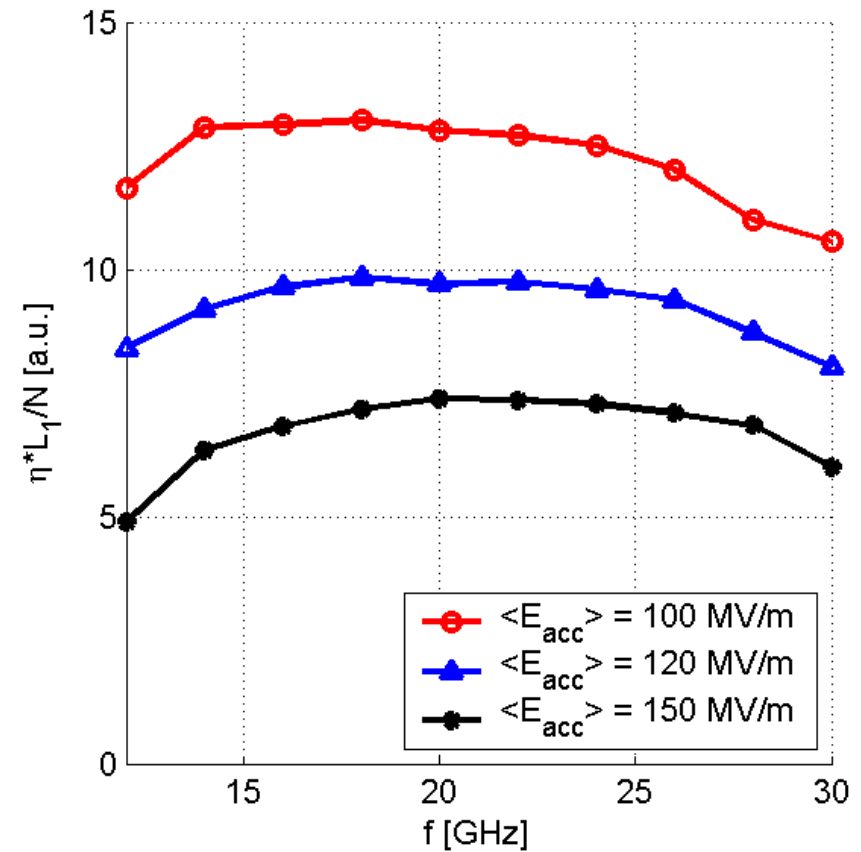
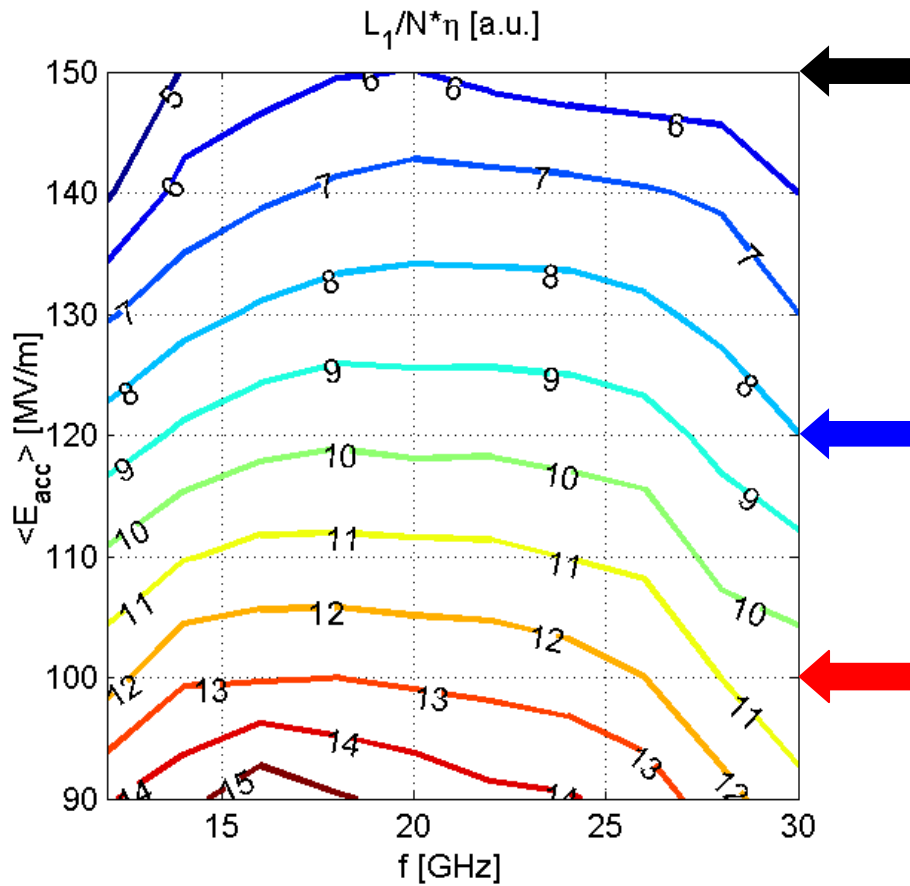
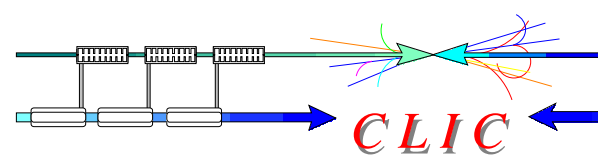
Luminosity per linac input power:

$$\frac{L}{P_l} = \frac{L_{b \times} N_b f_{rep}}{e E_c N N_b f_{rep} \eta} = \frac{1}{e E_c} \bullet \frac{L_{b \times} \eta}{N}$$

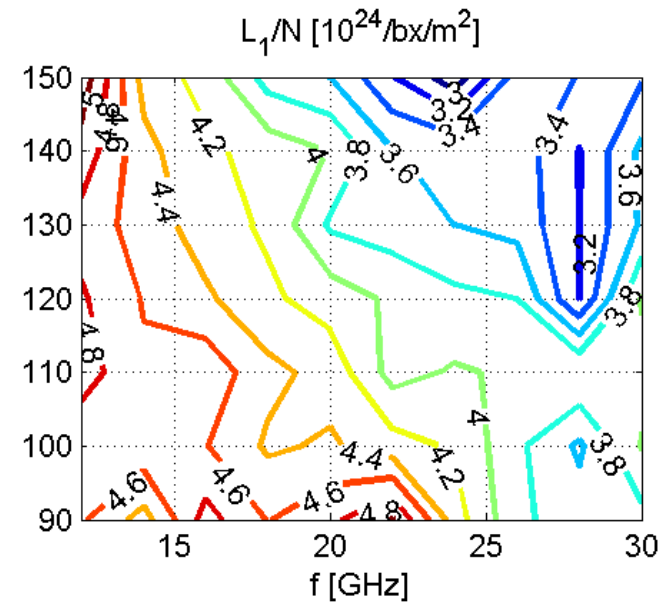
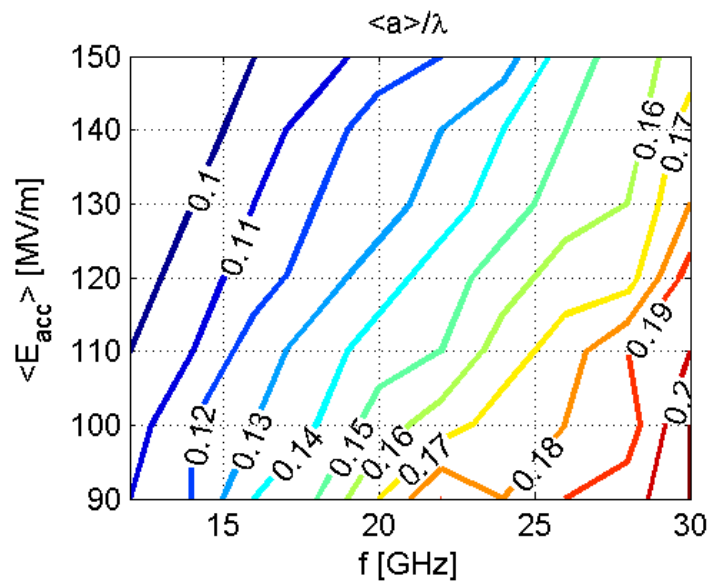
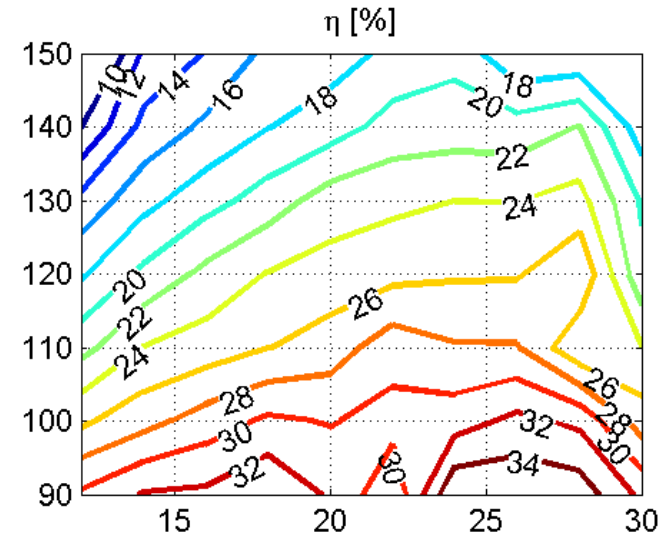
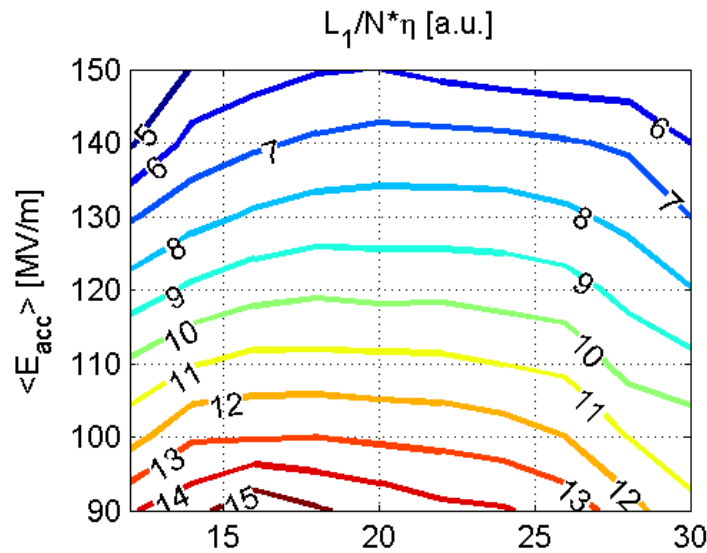
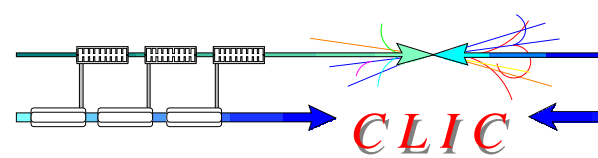
Collision energy is constant

Figure of merit

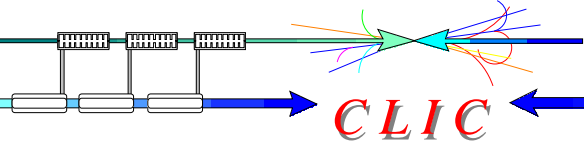
Optimization results



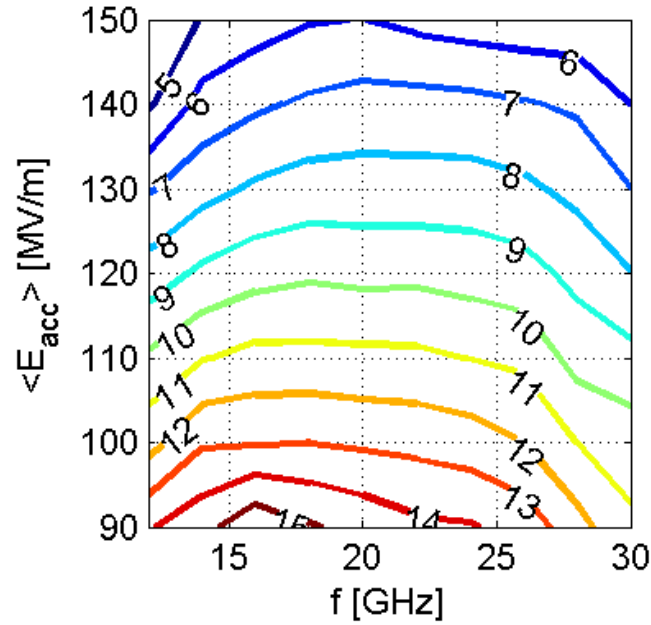
Optimization results



Optimization for different rf constraints



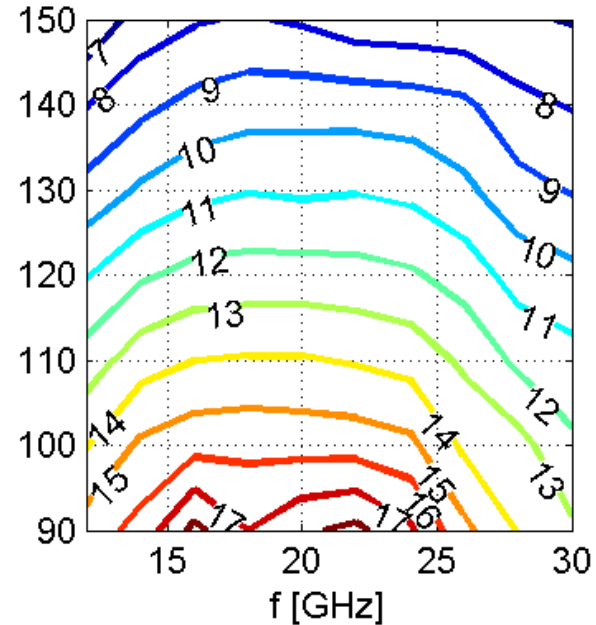
$L_1/N*\eta$ [a.u.]



$\Delta T_{max} < 56$ K
 $E_{surf}^{max} < 380$ MV/m
 $P_{in} t_p^{1/2}/C < 24$ a.u.

Nominal set of
rf constraints

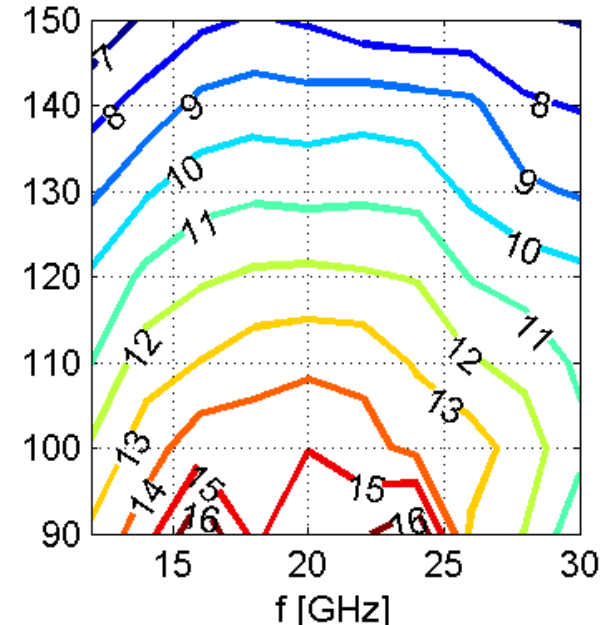
$L_1/N*\eta$ [a.u.]



$\Delta T_{max} < 56$ K
 $E_{surf}^{max} < 380$ MV/m
 $P_{in} t_p^{1/2}/C < 30$ a.u.

Increased
power limit

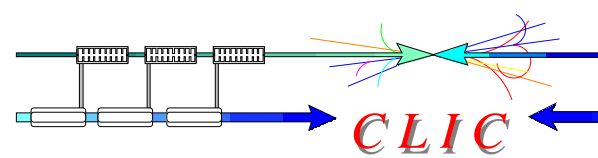
$L_1/N*\eta$ [a.u.]



$\Delta T_{max} < 40$ K
 $E_{surf}^{max} < 380$ MV/m
 $P_{in} t_p^{1/2}/C < 30$ a.u.

Reduced pulsed
surface heating limit

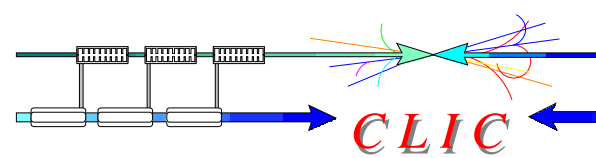
Main linac parameter list



For CLIC design luminosity: $L_1 = 3.3 \times 10^{34} \text{cm}^{-2}\text{s}^{-1}$

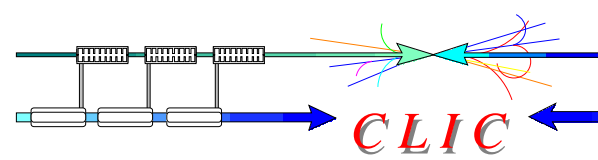
Accelerating gradient: $\langle E_{acc} \rangle$ [MV/m]	150	150	100	100
Frequency: f [GHz]	30	20	30	18
Repetition frequency: f_{rep} [Hz]	1182	538	559	243
RF input power: P_l [MW/linac]	151	132	75.1	60.9
RF energy per pulse: P_l/f_{rep} [kJ/linac]	127	245	135	250
Main linac length: l_{linac} [km/linac]	14	14	21	21

The last two rows show two parameters which have no influence on the presented figure of merit but which will have big impact on the overall cost optimization.



- Optimization of CLIC main linac parameters has been done taking luminosity per input power as a figure of merit
- Optimum gradient has not been found in the range from 90 to 150 MV/m, the lower the gradient the higher the figure of merit
- Optimum frequency is in the range of 16-20 GHz
- Optimum frequency shows weak dependence on the rf constraints
- Changing the operating frequency and gradient from the present design values of 150 MV/m at 30 GHz to the optimum frequency of 18 GHz at 100 MV/m will reduce the average linac input power by factor 2.5

Back up slides

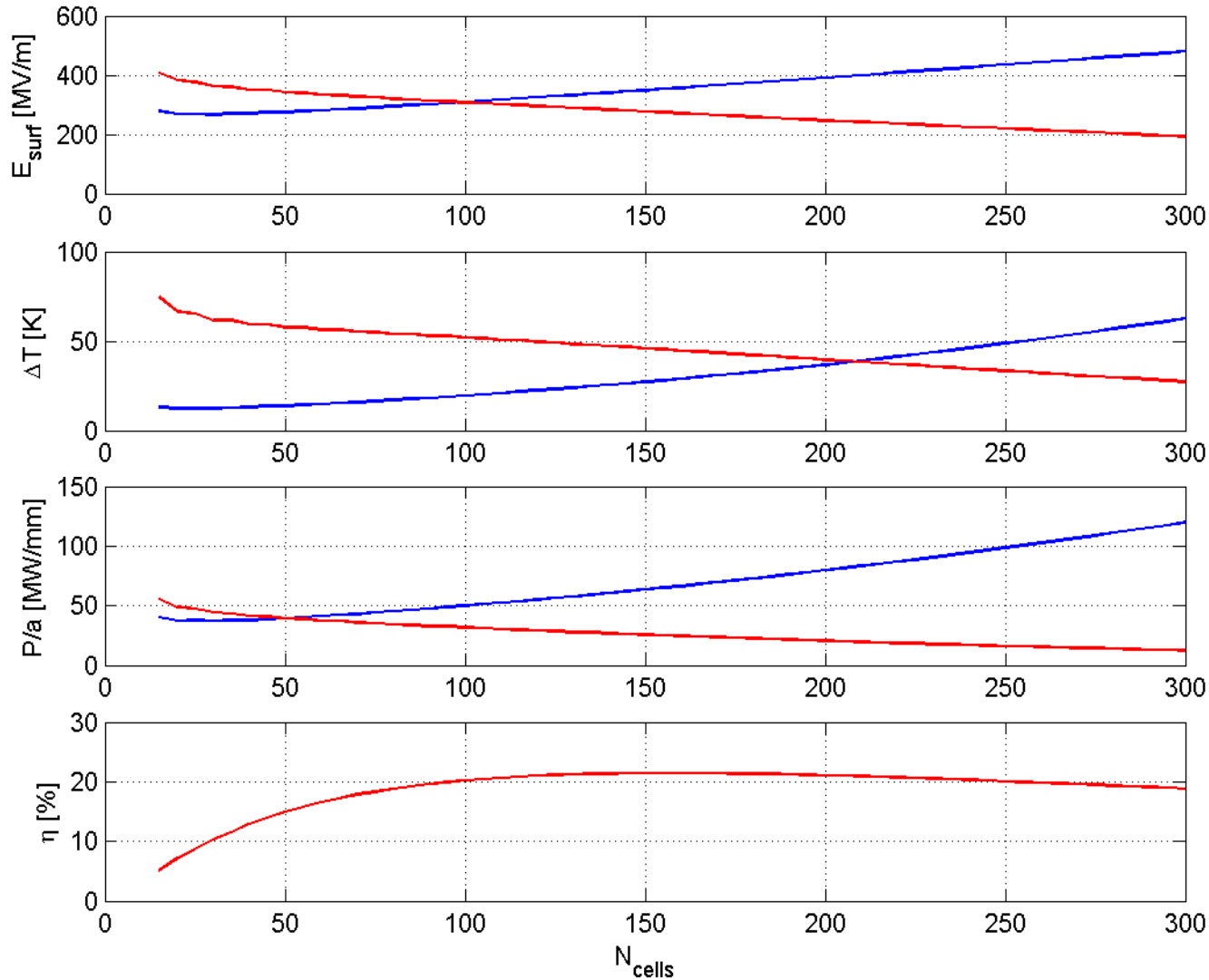


Choice of N_{cells}

CLIC

4 structures are chosen from 285.

first cell (blue), last cell (red)



For example:

$N_{\text{cells}} = 100 -$
 $E_{\text{surf}} = \text{const},$

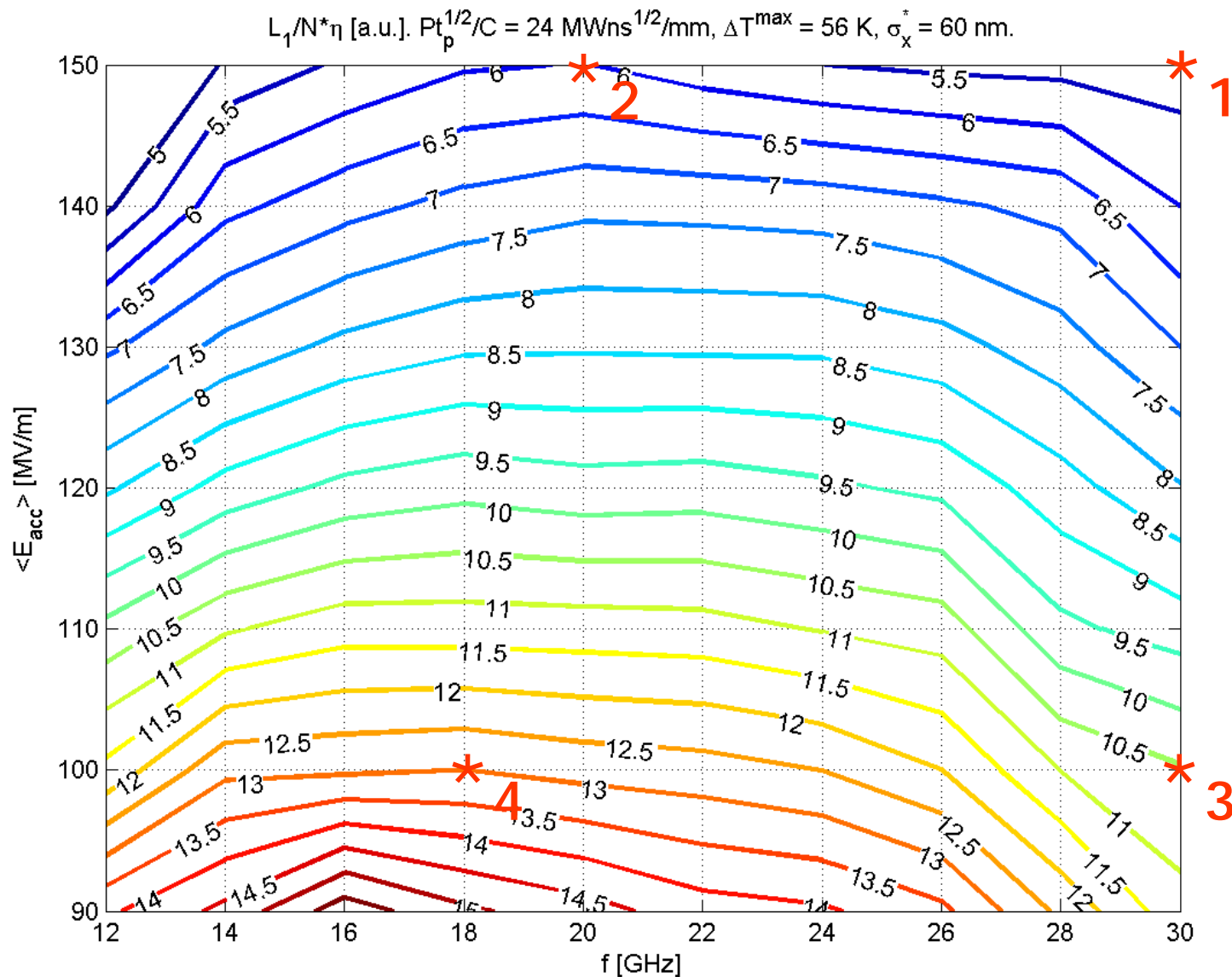
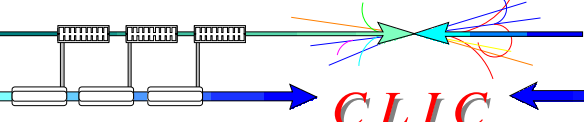
$N_{\text{cells}} = 210 -$
 $\Delta T = \text{const},$

$N_{\text{cells}} = 50 -$
 $P/C = \text{const}$

$N_{\text{cells}} = 150 -$
 $\text{Max}(\eta)$

Optimization results

CLIC

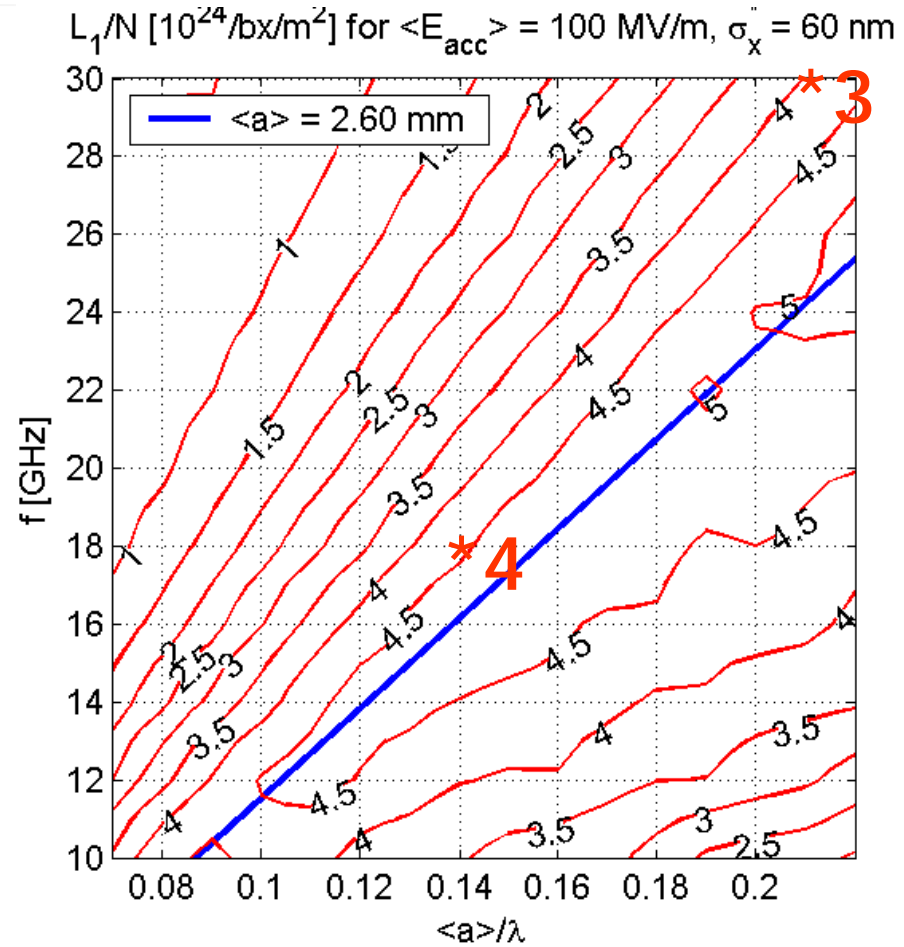
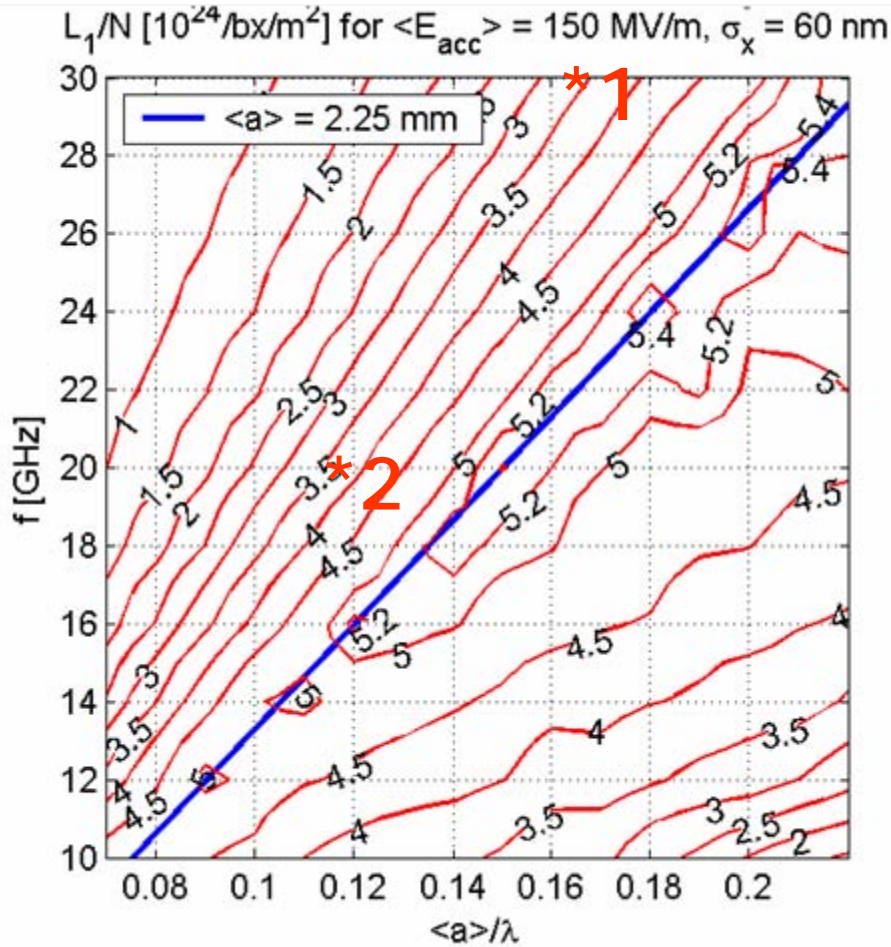


L_1/N for different gradients

CLIC

$\langle E_{acc} \rangle = 150$ MV/m

$\langle E_{acc} \rangle = 100$ MV/m



Parameter list of structures: 1-4



CLIC

Structure #	1	2	3	4
Accelerating gradient: $\langle E_{acc} \rangle$ [MV/m]	150	150	100	100
Frequency: f [GHz]	30	20	30	18
RF phase advance per cell: $\Delta\phi$ [°]	50	50	50	50
Average iris radius over wavelength: $\langle a \rangle / \lambda$	0.165	0.115	0.21	0.14
Input/Output iris radii: $a_{1,2}$ [mm]	2.14, 1.16	2.21, 1.24	2.63, 1.58	3.03, 1.63
Input/Output iris thickness: $d_{1,2}$ [mm]	0.25, 0.45	0.38, 0.38	0.25, 0.4	0.42, 0.42
Number of cells, structure length: N_c, l [mm]	69, 96	36, 75	127, 176	72, 167
Bunch separation: N_s [rf cycles]	6	5	6	5
Number of bunches in a train: N_b	42	79	59	102
Pulse length: τ_p [ns]	14.7	31.8	17.4	43.6
Input power: P_{in} [MW]	85	60	96	70
Efficiency: η [%]	16.1	17.1	26.9	30.4
Luminosity per bunch X-ing: L_{bx} [m ⁻²]	0.66×10^{34}	0.78×10^{34}	1.00×10^{34}	1.33×10^{34}
Bunch population: N	2.03×10^9	2.20×10^9	2.55×10^9	3.11×10^9
Figure of merit: $\eta L_{bx} / N$ [a.u.]	5.24	6.02	10.55	13.01

2.5 times

