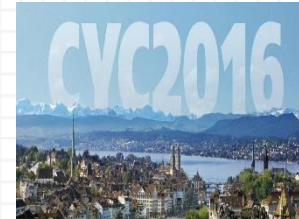




In the Name of GOD



**Amirkabir University
of Technology
(AUT), Tehran, Iran**



**21st International
Conference on
Cyclotrons and
their Applications**

Design and Simulation of Cavity for 18MeV Cyclotron

**Presenter:
Seyyed Mohsen Mousavinia**

September 2016

Content



01 Principle of Cavity

02 Resonator Design

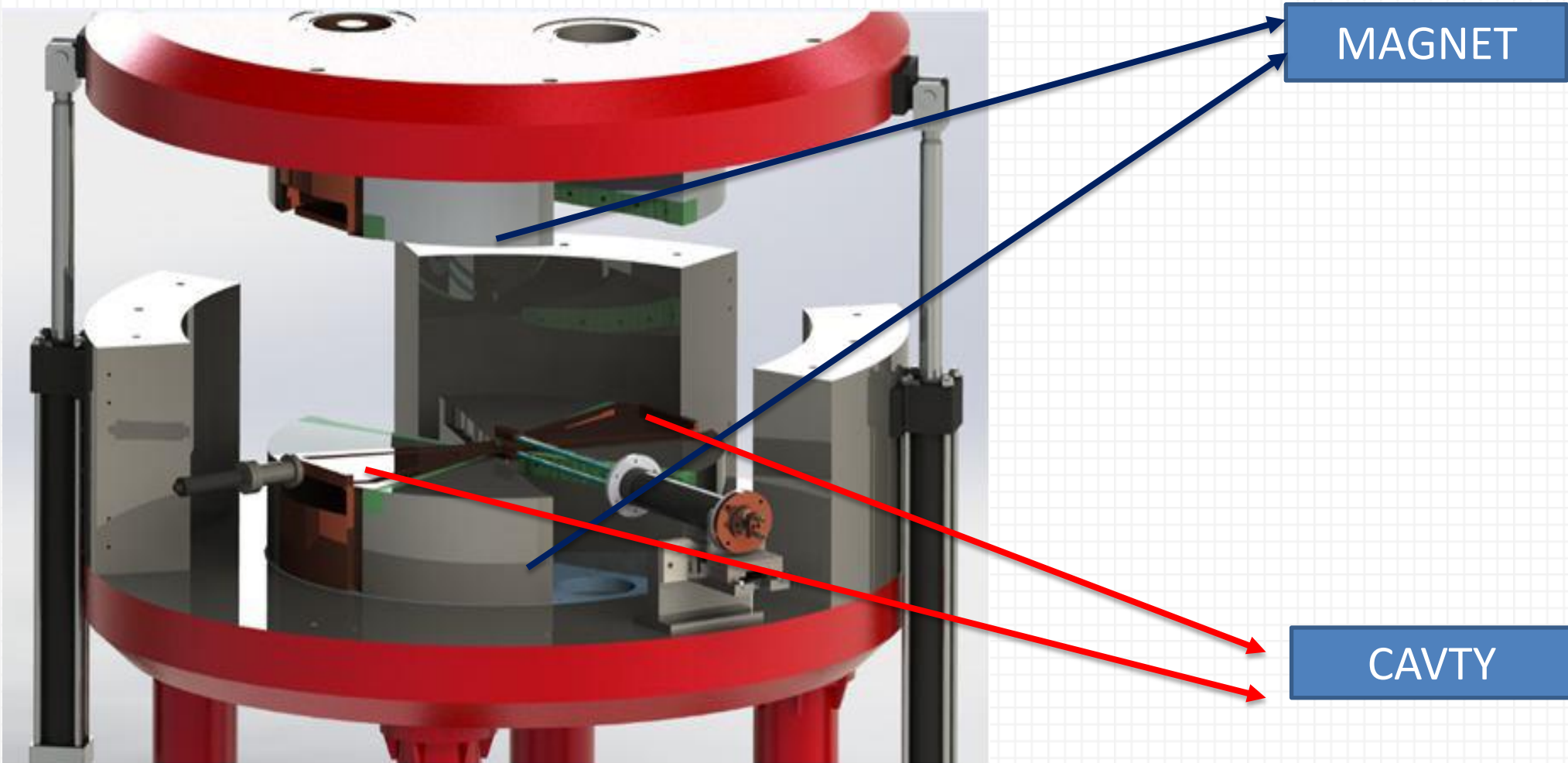
03 Simulation Results



A yellow graphic consisting of several overlapping, slanted rectangular shapes that create a sense of depth and movement. The shapes are arranged in a way that they appear to be layered, with some in front of others, creating a 3D effect. The colors range from a bright yellow to a slightly darker, more muted yellow.

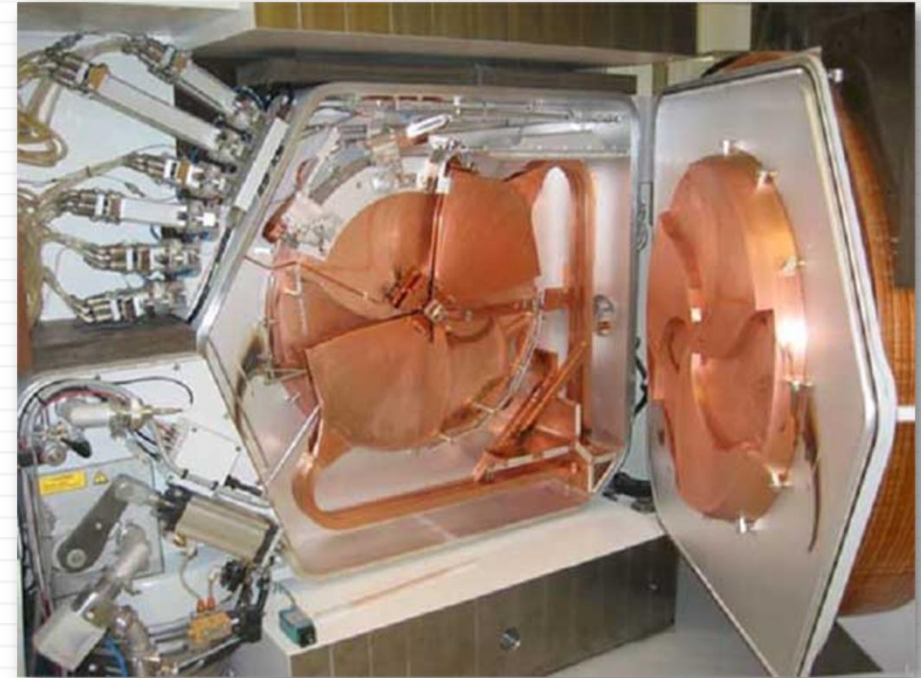
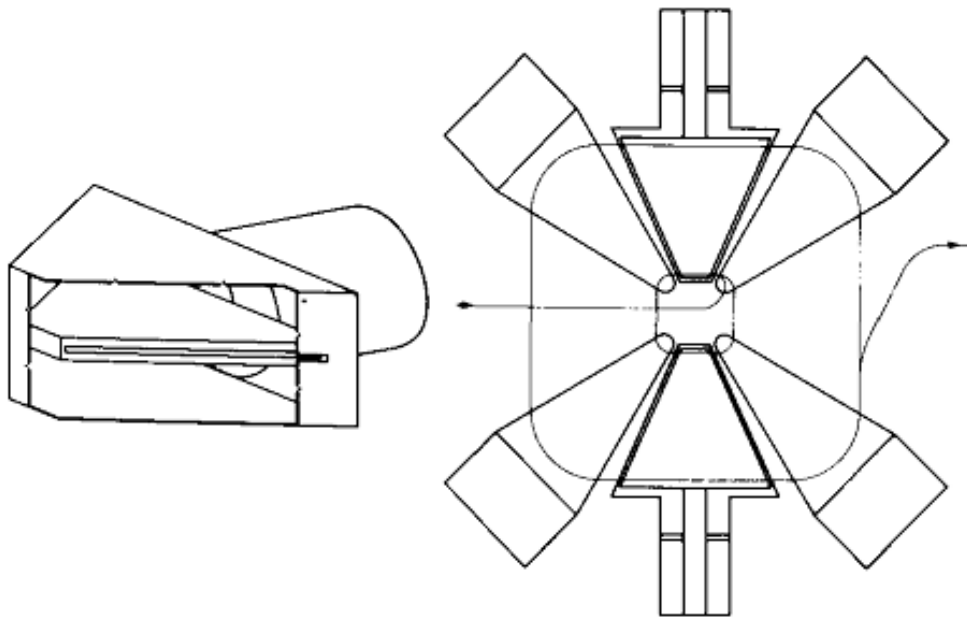
Principle of Cavity

Working principle of Cyclotron

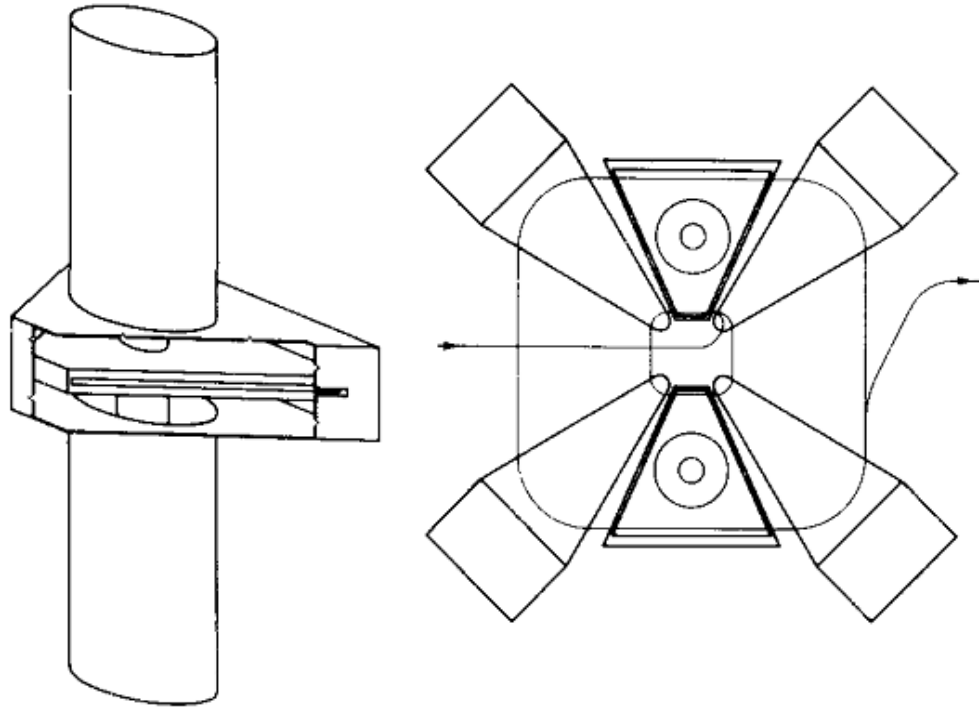


Types of Cavity

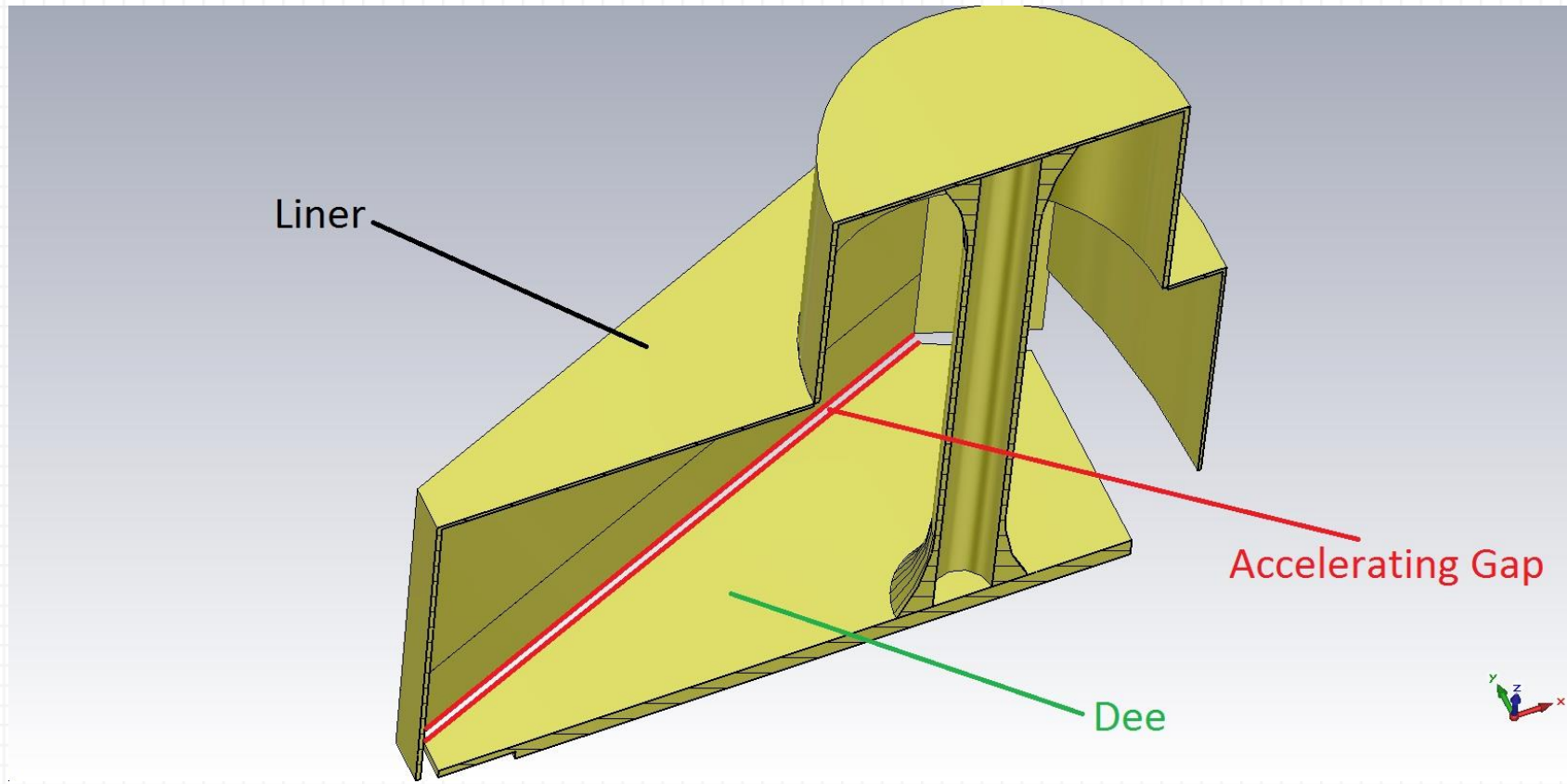
Delta Resonator with horizontal stem



Delta Resonator with vertical stem

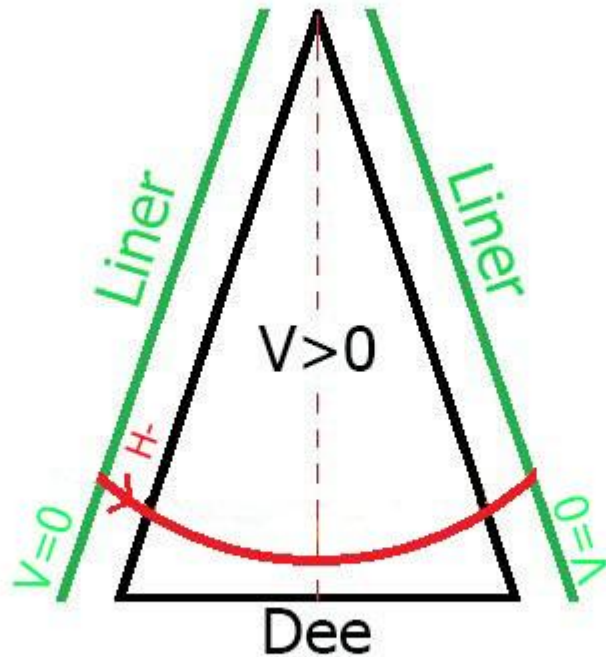


1. Electric Field Created Due to Potential Difference Between Electrodes
2. The Distance Between Electrodes Called Accelerating Gap
3. High Voltage Electrodes Called Dees
4. Ground Potential Electrodes Called Dummy Dee or Liner



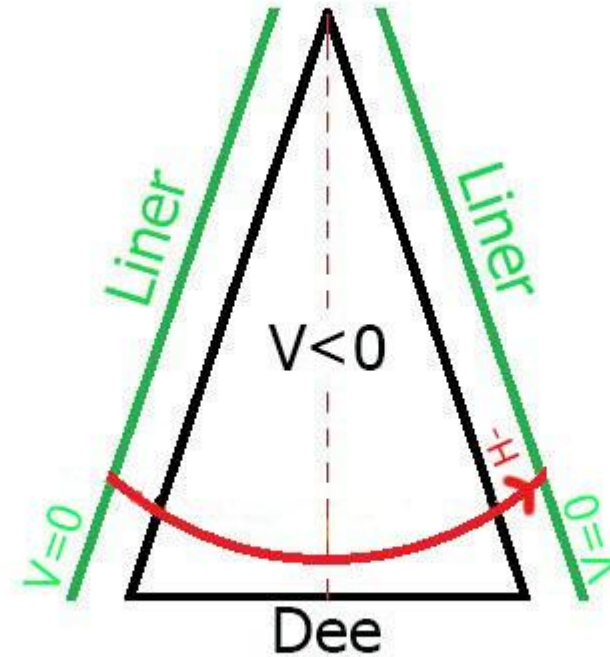
Acceleration Steps

First Acceleration
Dee Entrance

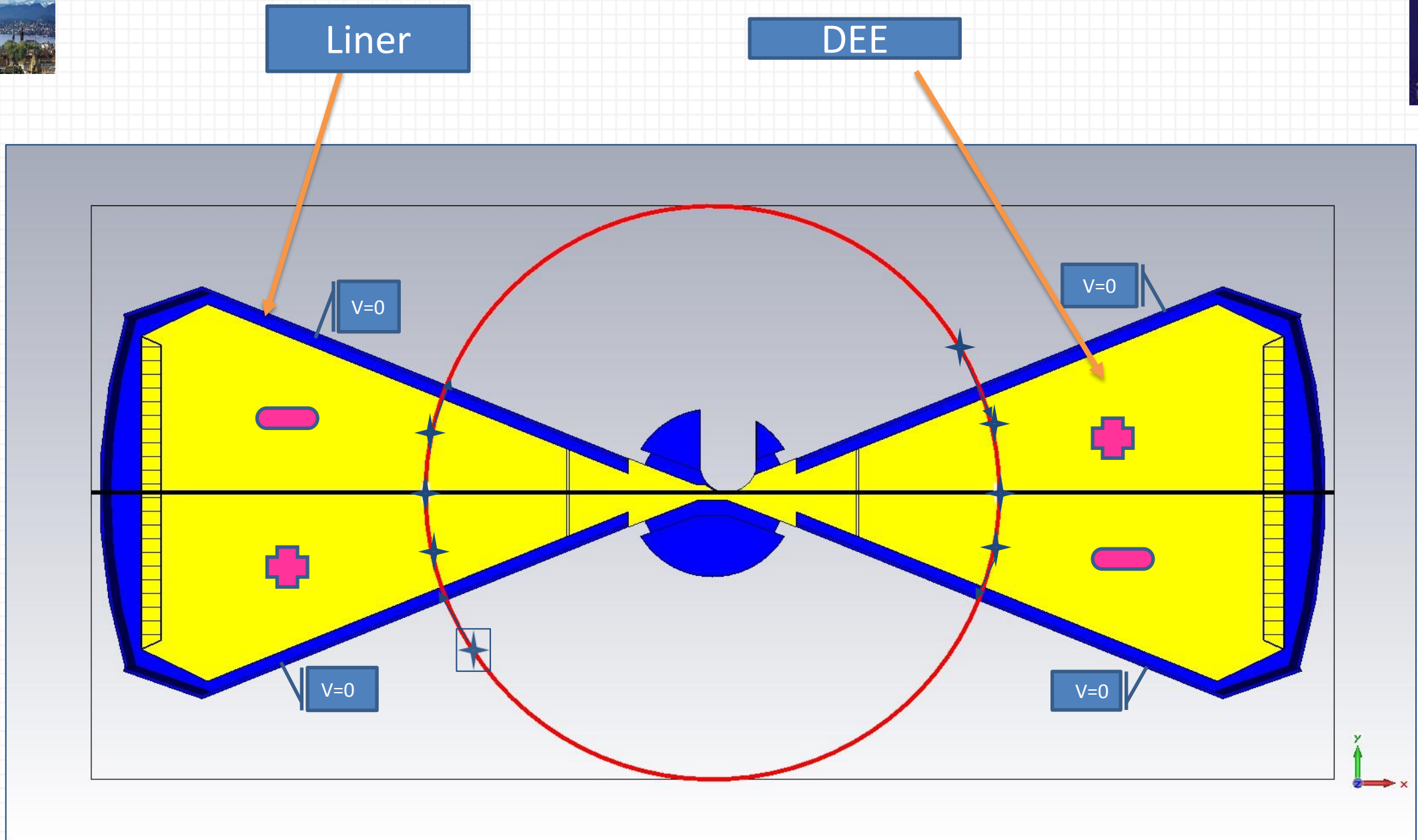


Particle Pulled in Dee Entrance
When
 $V > 0$

Second Acceleration
Dee Exit

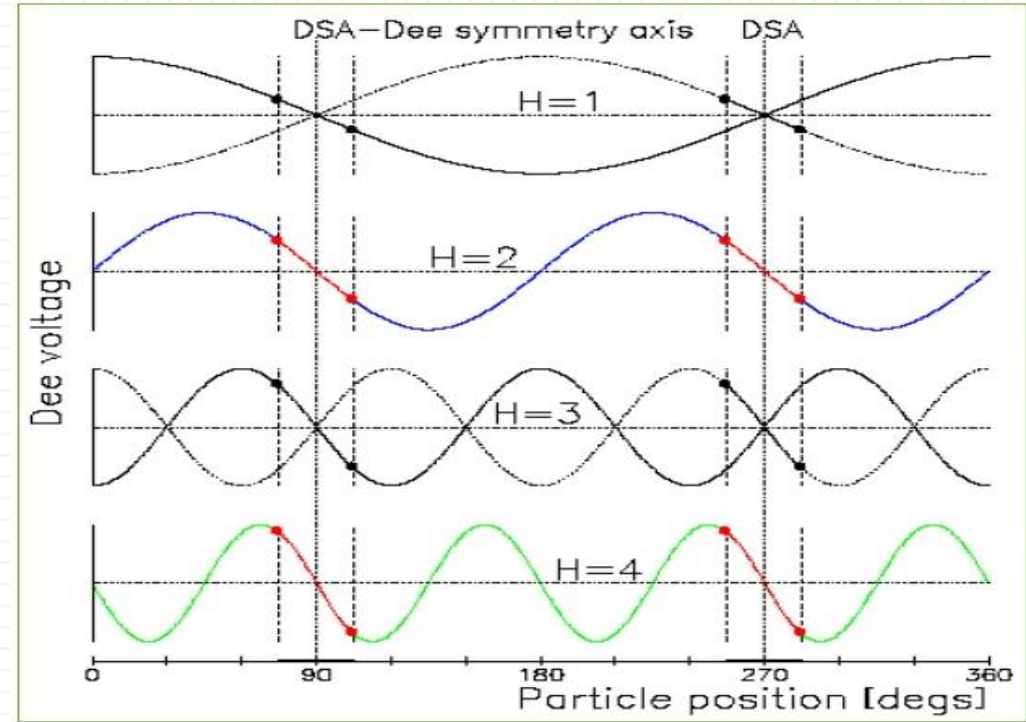
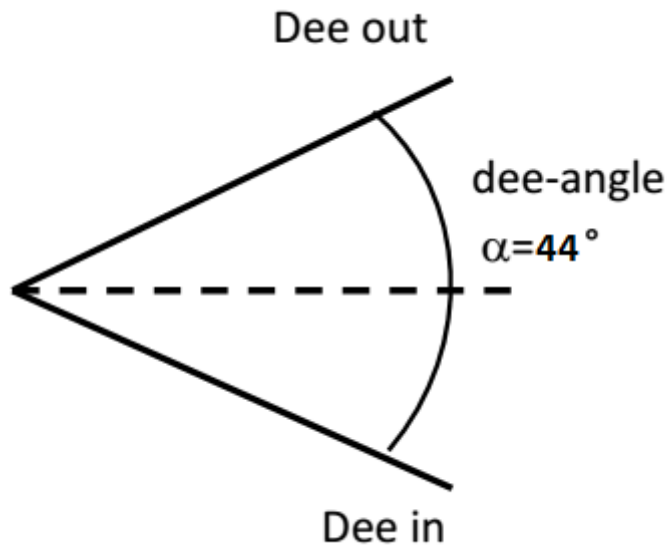


Particle Pushed in Dee Exit
When
 $V < 0$



Energy Gain per Turn

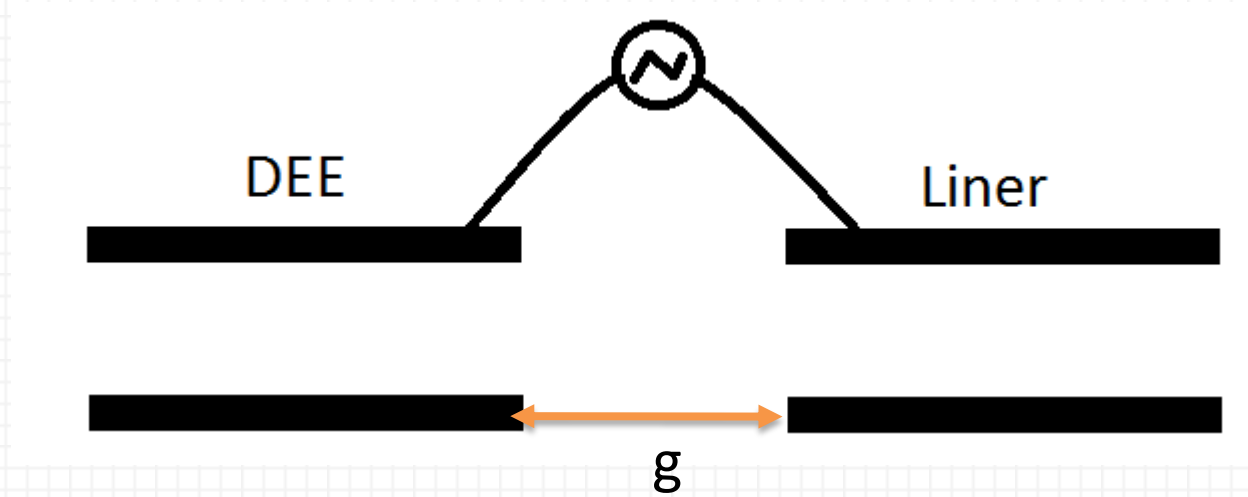
$$\Delta E_k = qV_{dee}\tau N \sin\left(\frac{h\alpha}{2}\right) \cos \Phi_{RF}$$



h=1
h=2
h=3
h=4

h	1	2	3	4	5	6	7
$\sin\left(h\frac{\theta}{2}\right)$	0.375	0.695	0.914	0.999	0.939	0.743	0.438

THE ACCELERATION GAP AND THE TRANSIT-TIME FACTOR



$$V_{eff} = V_0 \cos(\omega t) \times \frac{\sin\left(\frac{gh}{2R}\right)}{\left(\frac{gh}{2R}\right)}$$

Transit Time Factor

Kilpatrick criterion

$$f = 1.643(E_k)^2 e^{(-8.5/E_k)}$$

$$E_s = bE_k = 1.5 \times 9.7 \frac{MV}{m} = 14.55 \frac{MV}{m}$$

$$E = \frac{V}{d}$$

$$14.55M = \frac{76k}{d} \quad d_{min} = 5.22 \text{ mm}$$



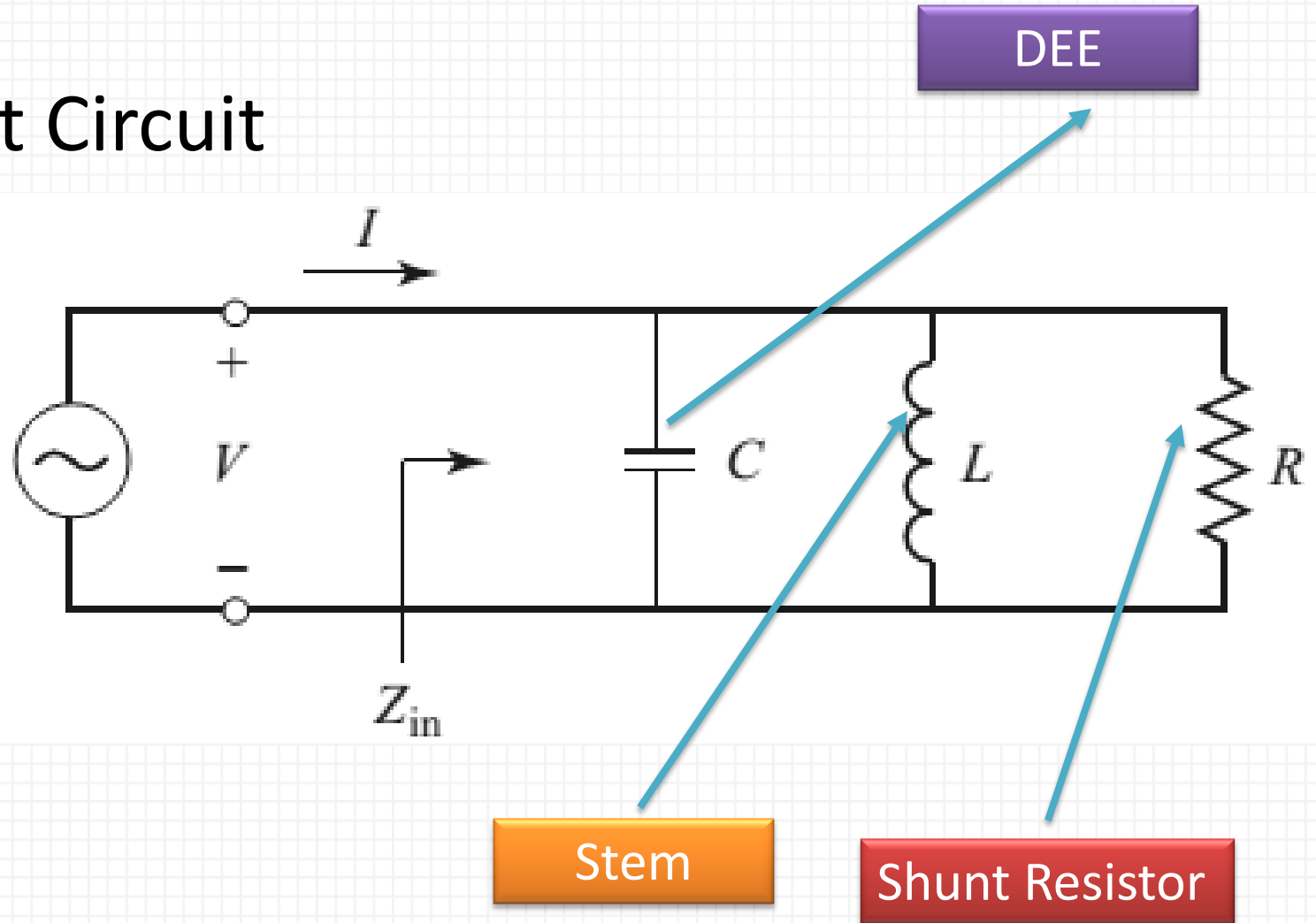
Resonator

Design

Equivalent Circuit of Resonator

Parallel Resonant Circuit

$$f = \frac{1}{2\pi\sqrt{LC}}$$



Calculate the particle rotation frequency

Proton Energy: $E_0 = 938.272 \text{ Mev}$

Cyclotron energy: $T = 18 \text{ Mev}$

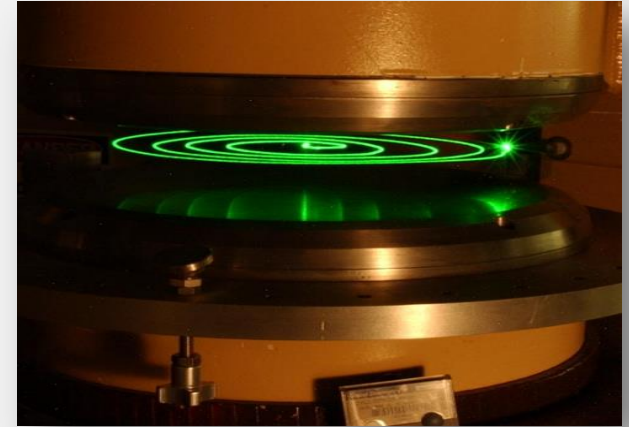
45.783 tesla meter $B \cdot r =$

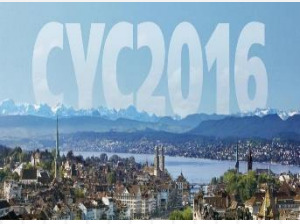
If $B = 1.7 \text{ T} \rightarrow r = 63 \text{ cm}$

According to this equation, $\omega \cdot r$ is determined:

If $r = 63 \text{ cm} \rightarrow f_{\text{particle}} = 16.075 \text{ MHz}$

$$f_{rf} = hf_{\text{particle}} = 4 \times 16.075 = 64.3 \text{ MHz}$$





Characteristics of Parallel Resonant Circuit are:

Input Impedance is : $Z_{in} = \left(\frac{1}{R} + \frac{1}{j\omega L} + j\omega C \right)^{-1}$,

Complex Power Delivered to the Resonator is:

$$P_{in} = \frac{1}{2}|V|^2 \left(\frac{1}{R} + \frac{j}{\omega L} - j\omega C \right).$$

power dissipated by the resistor, R , is $P_{loss} = \frac{1}{2} \frac{|V|^2}{R}$

Average Electric Energy Stored in the capacitor, C , is

$$W_e = \frac{1}{4}|V|^2 C$$

Average Magnetic Energy Stored in the Inductor, L , is

$$W_m = \frac{1}{4}|I_L|^2 L = \frac{1}{4}|V|^2 \frac{1}{\omega^2 L}$$

Resonance Occurs
when

$$W_m = W_e$$

Quality Factor

$$Q = \omega \frac{\text{average energy stored}}{\text{energy loss/second}}$$

Q of the parallel resonant circuit can be expressed as

$$Q_0 = \omega_0 \frac{2W_m}{P_{\text{loss}}} = \frac{R}{\omega_0 L} = \omega_0 RC,$$

This result shows that the Q of the parallel resonant circuit increases as R increases.

Coupling and Matching

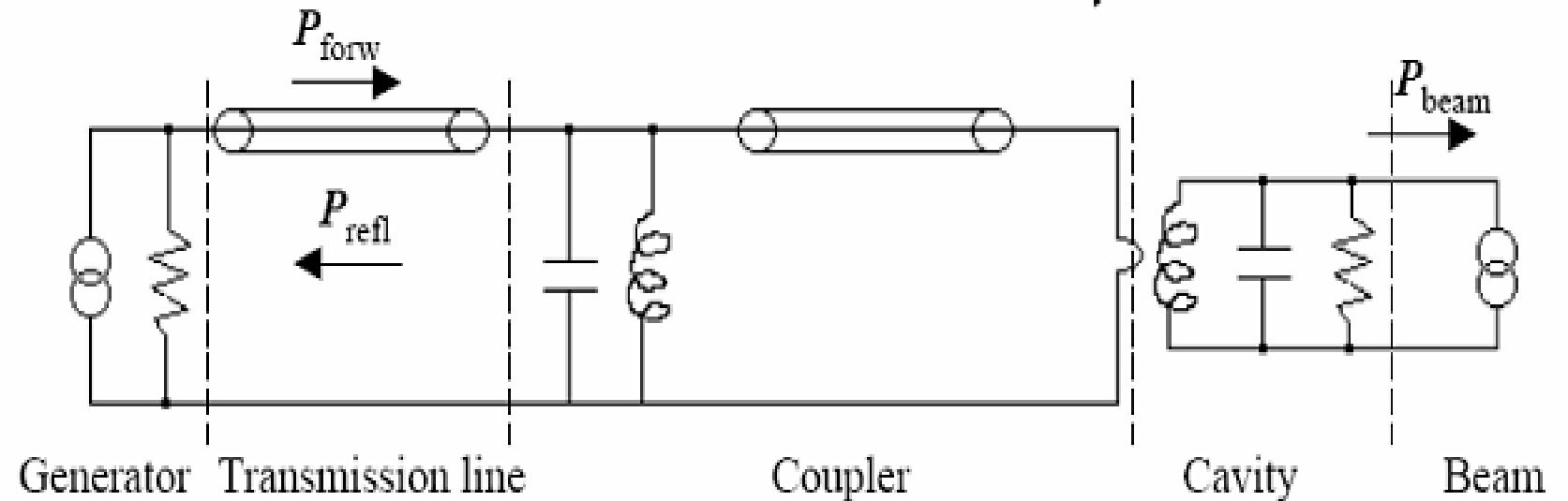
Tasks:

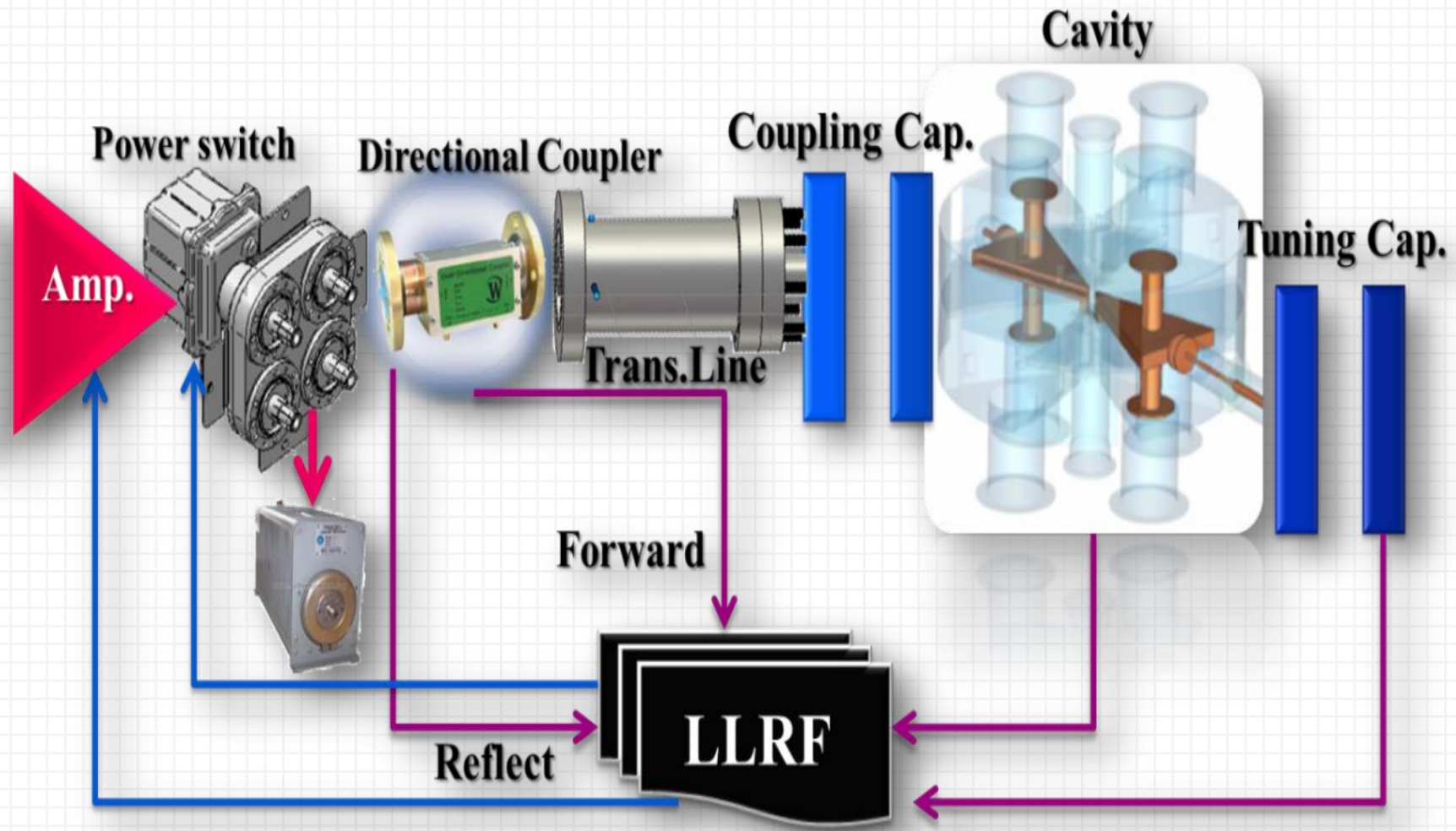
Maximum power transfer and impedance matching of line to cavity

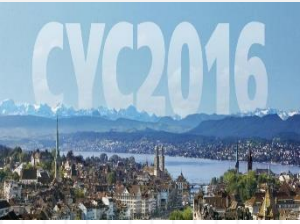
Types of cavity:

Capacitive(Electric)

Inductive(Magnetic)





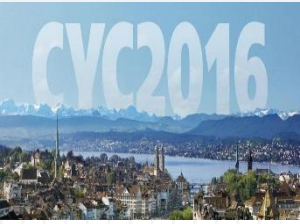


Possible problems during operation of the cyclotron



Mismatch Leads to:

- a. the transmitter may not be able to supply enough power to maintain the desired accelerating voltage if the cavity's resonant frequency drifts too far from the driving frequency;
- b. the power supply could be damaged by dissipation of excessive power reflected back from the load;
- c. breakdown and sparking could occur
- d. the phase and amplitude response of the transmitter may be severely affected by the change in the load

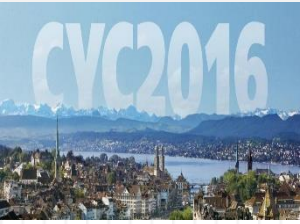


The factors that can cause changes in the cavity's geometry and loading are

1. Thermal expansion and contraction of the cavity structure, which will greatly affect the cavity's resonant frequency;
2. Electrical discharge phenomena such as sparking which will lower the cavity's quality factor and which may also slightly detune the cavity
3. Multipacting

And changes cavity geometry leads to changes in:

Resonant Frequency, Quality Factor and Input Impedance



Calculate the required power

Beam power

$$P_b = V_f \times I_b = 18 \text{ MV} \times 150 \mu\text{A} = 2.7 \text{ KW}$$

Resonator dissipated power

$$P_r = \frac{V_{dee}^2}{2R_s} = \frac{44 \text{ KV}^2}{2 \times 151 \text{ K}\Omega} = 6.411 \text{ KW}$$

Total power

$$P_t = 2.7 \text{ KW} + 6.41 \text{ KW} = 9.11 \text{ KW}$$

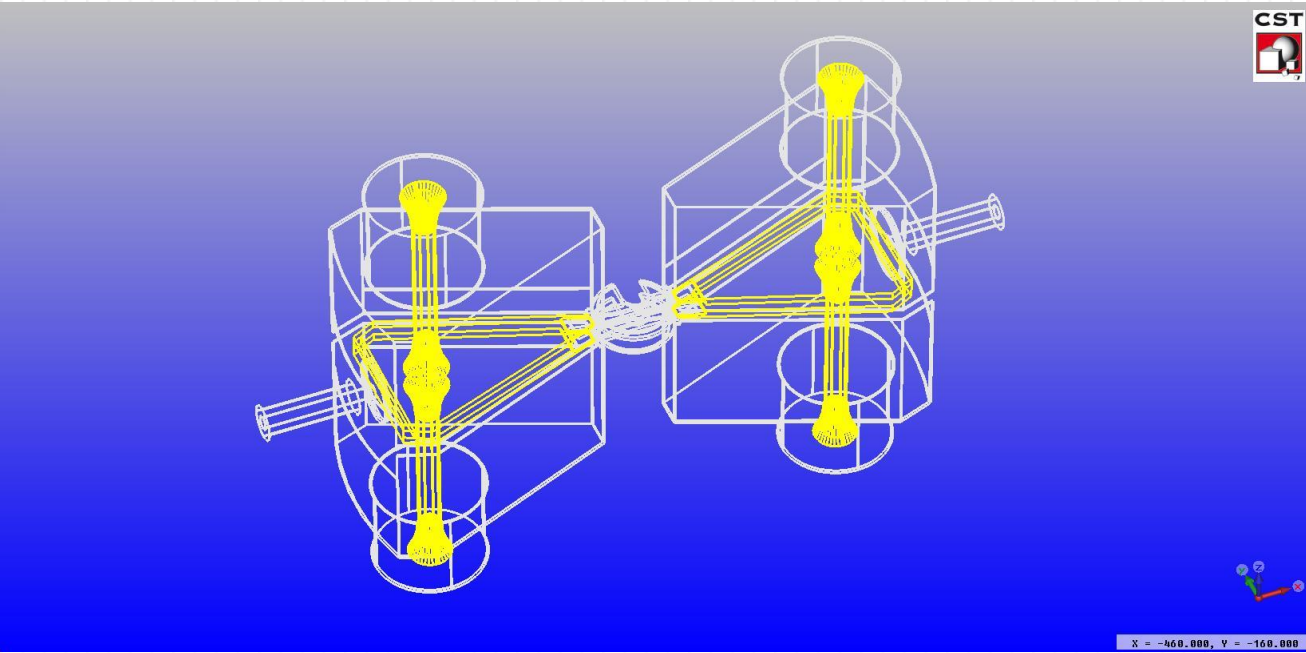
Adding 20% safety margin

$$9.11 \text{ KW} * 1.2 = 10.93 \text{ KW}$$

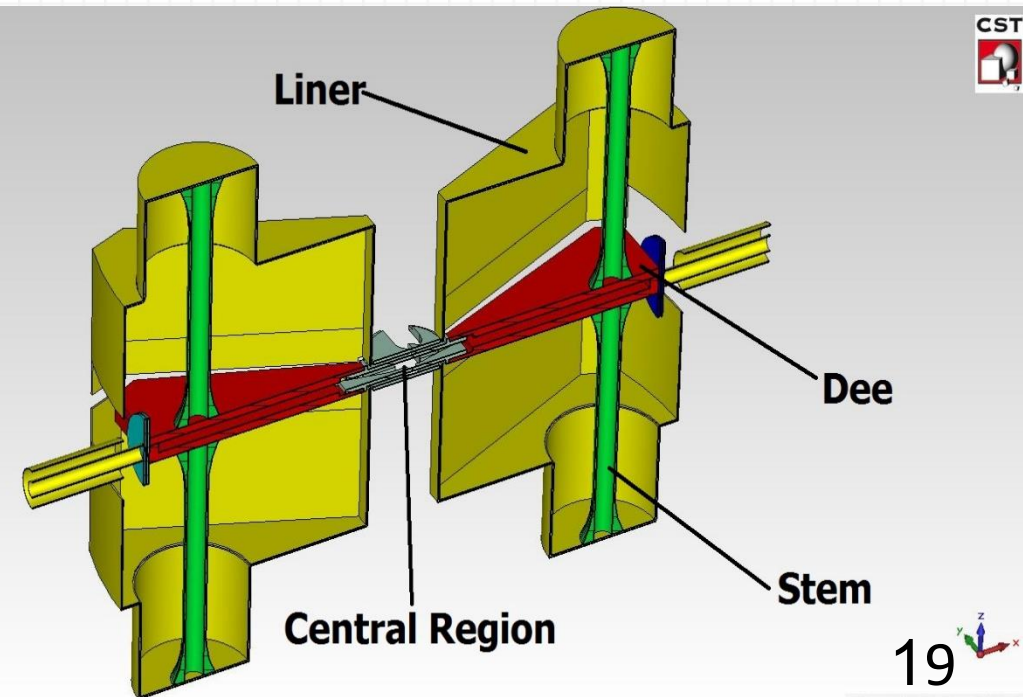
A yellow parallelogram graphic with a horizontal line, set against a dark background. The graphic consists of several overlapping, semi-transparent yellow parallelograms that create a sense of depth and movement. The central text is positioned within the most prominent, solid yellow parallelogram.

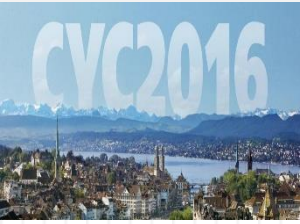
Simulation

Results



Geometry designed in CST MWS





Design Items

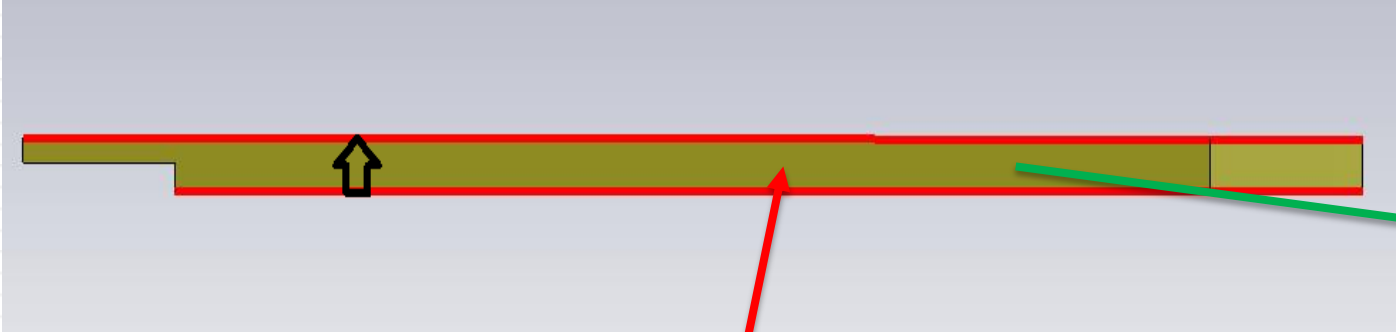
Items that should be considered in the design of dee

1. Angle and width of the Dee
2. Gap between the Dee and Liner
3. Dee thickness

Items that should be considered in the design of stem

1. Radius
2. Length

The effects of changing the thickness of the dee

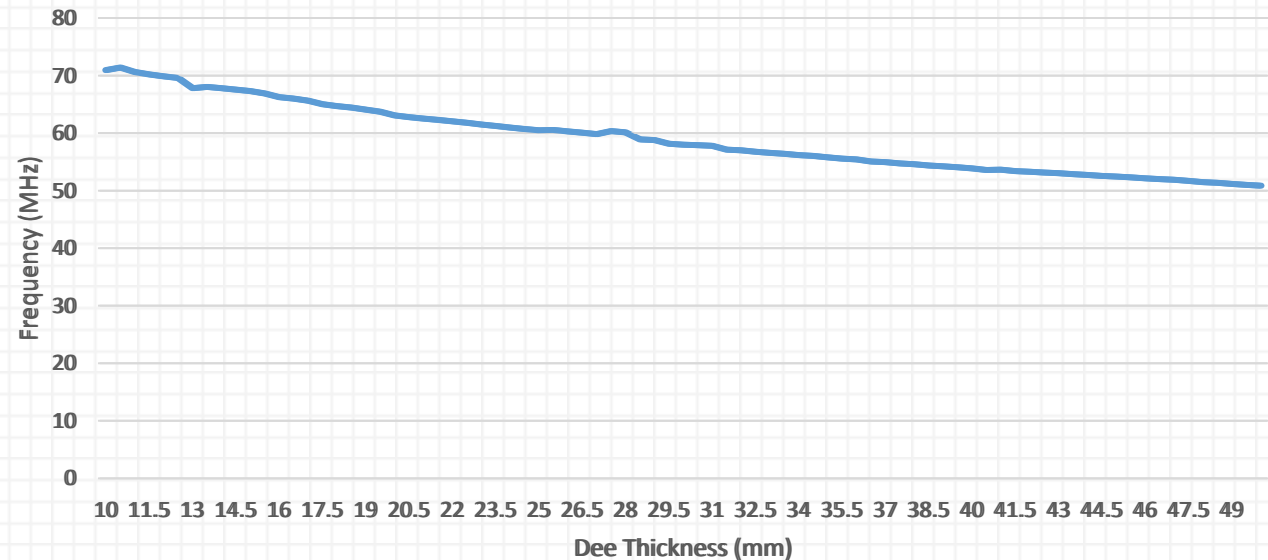
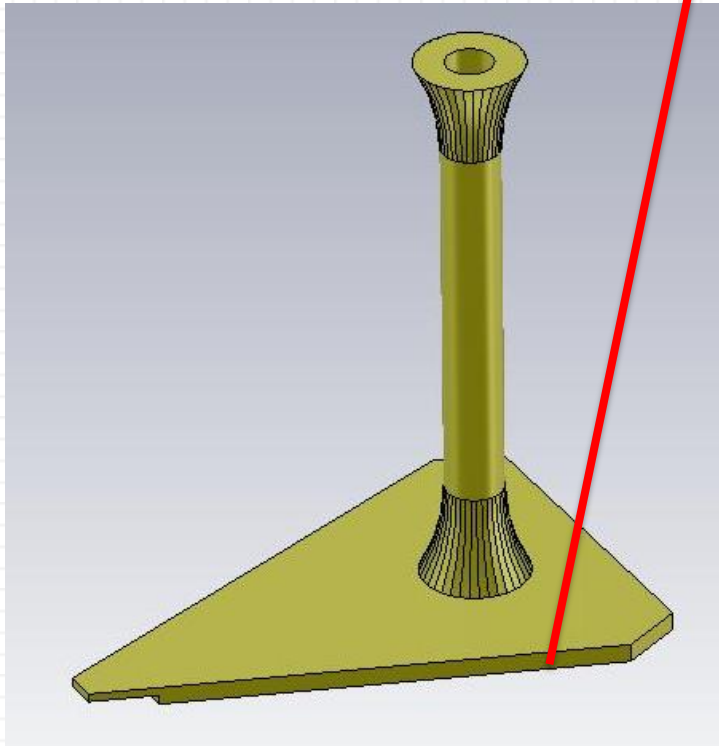


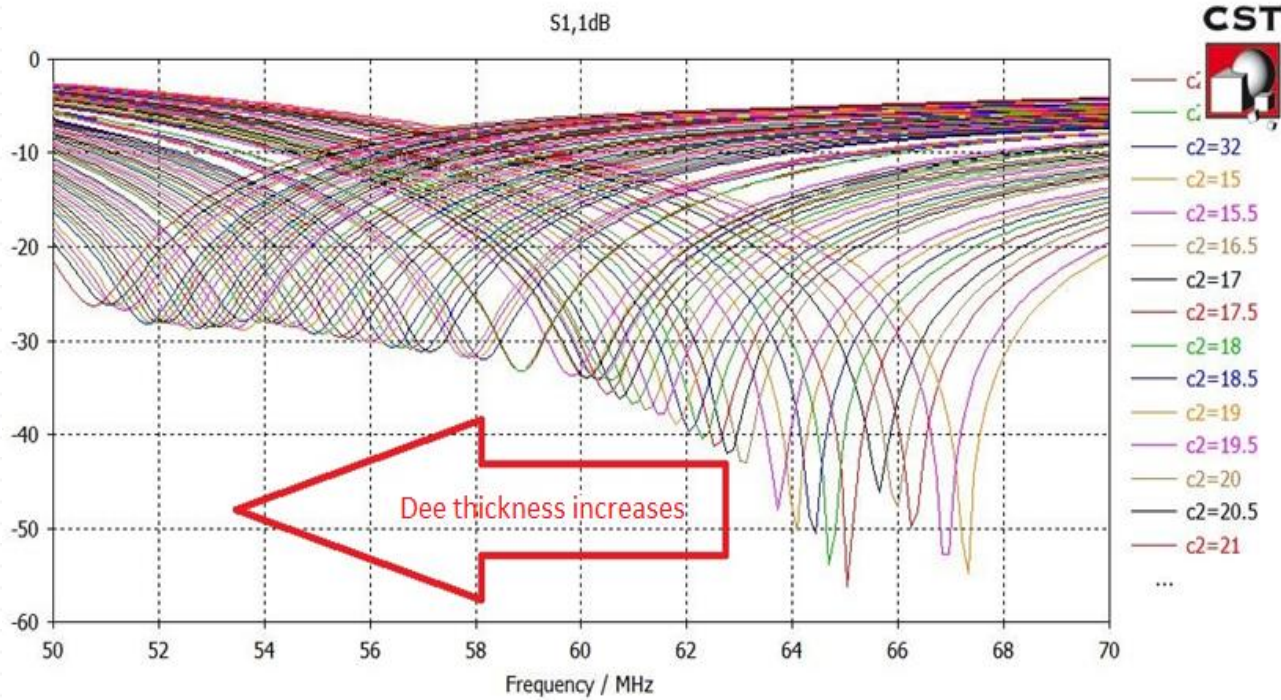
$$C \approx \frac{A}{d}$$

and

$$f = \frac{1}{2\pi\sqrt{LC}}$$

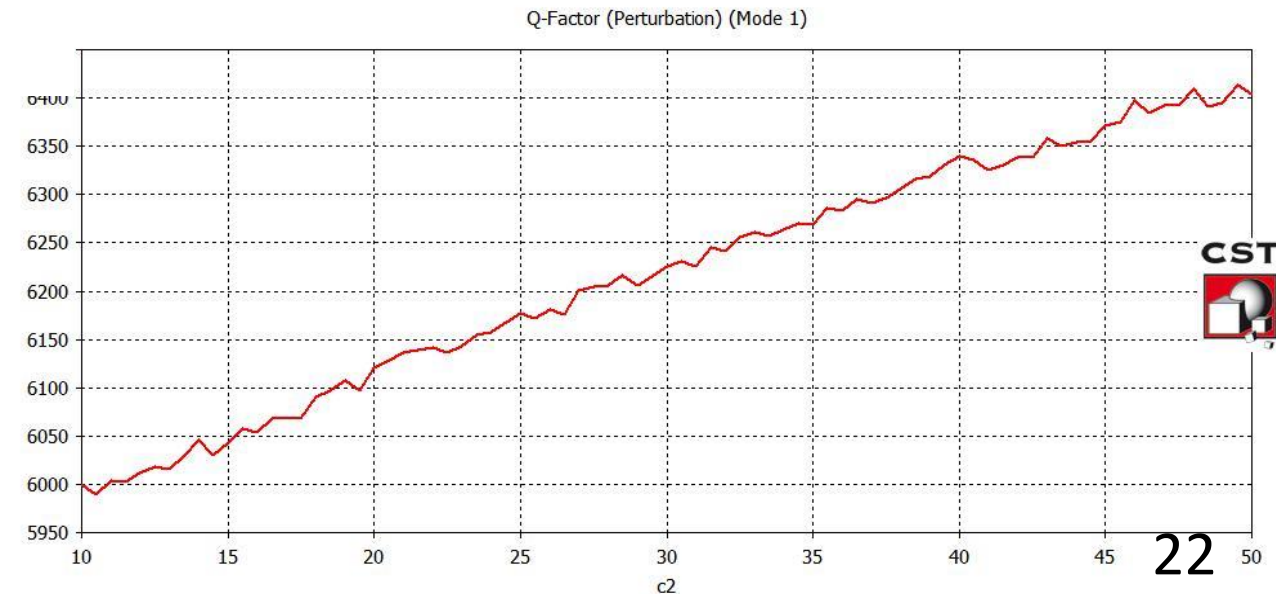
$$A \uparrow \rightarrow C \uparrow \rightarrow f \downarrow$$





The effect of Dee thickness variation on return loss

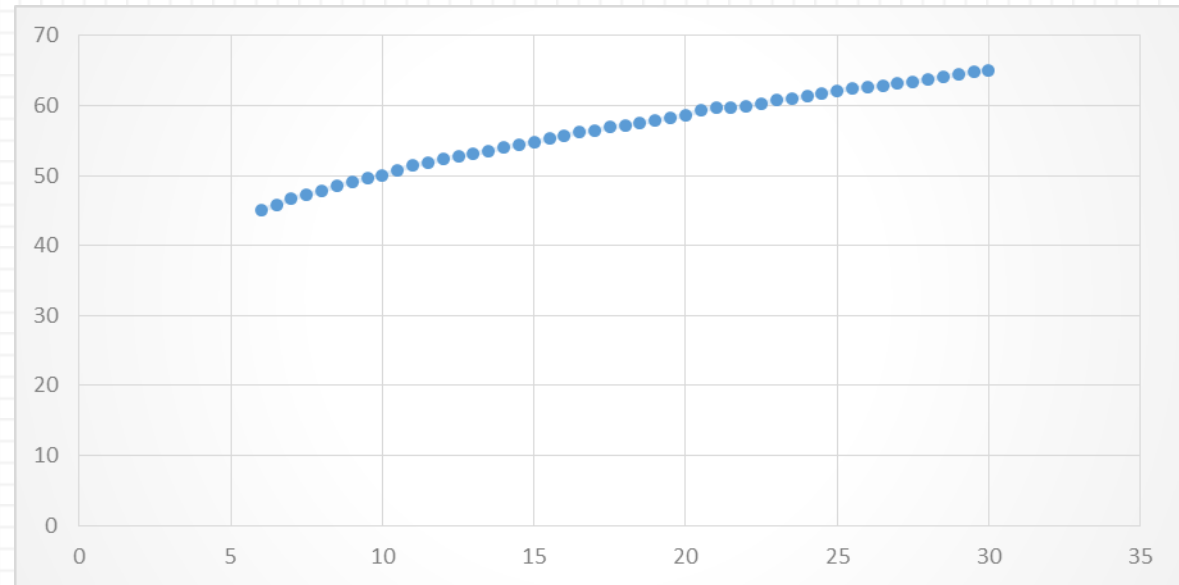
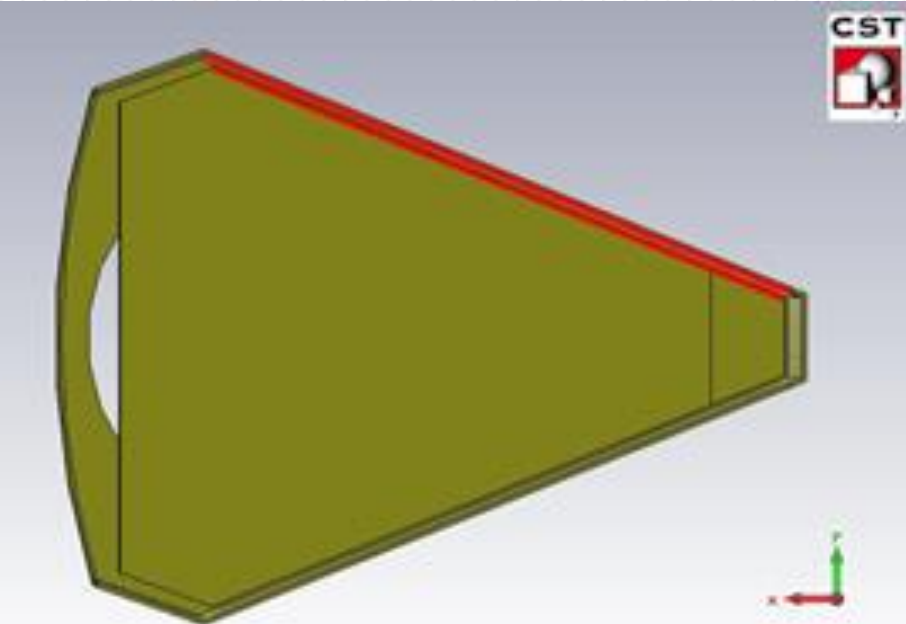
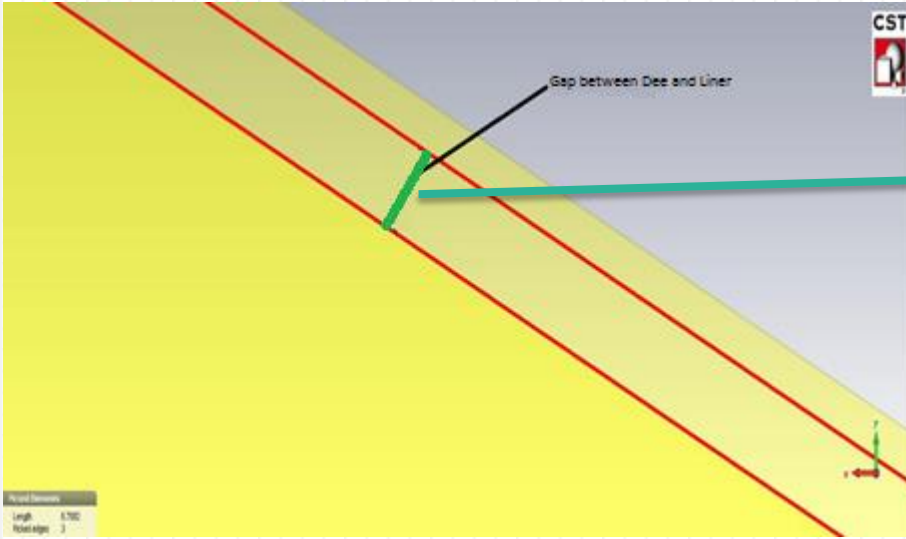
The effect of changing thickness of the Dee on quality factor



The gap between dee and liner

$$C \approx \frac{A}{d} \quad \text{and} \quad f = \frac{1}{2\pi\sqrt{LC}}$$

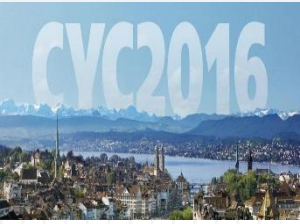
$$d \uparrow \rightarrow C \downarrow \rightarrow f \uparrow$$



frequency

Gap distance

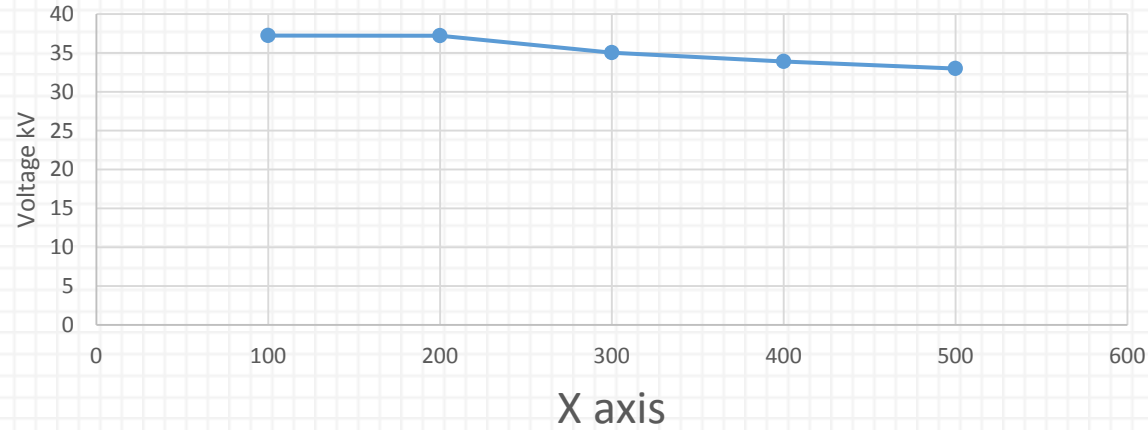
The effect of changing the gap On the frequency



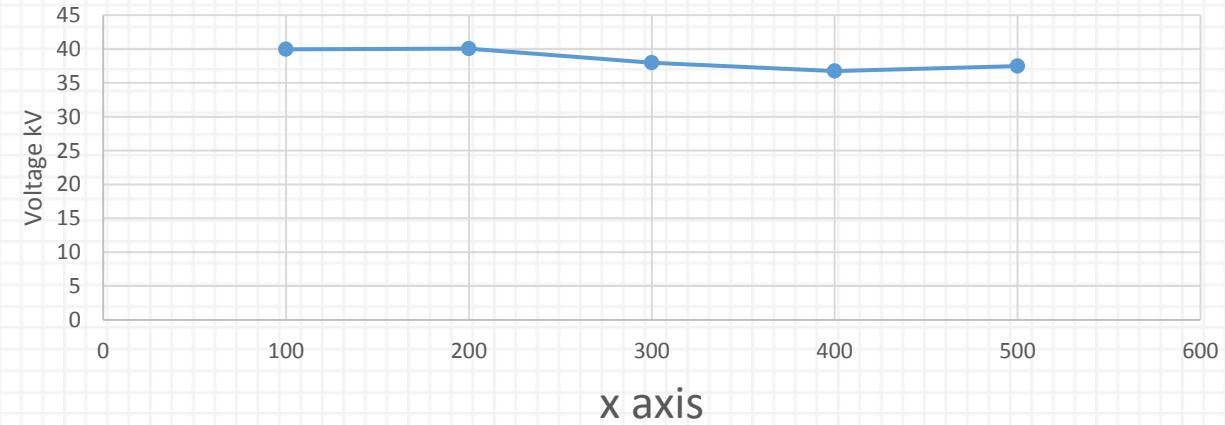
Voltage distribution in size of different gaps



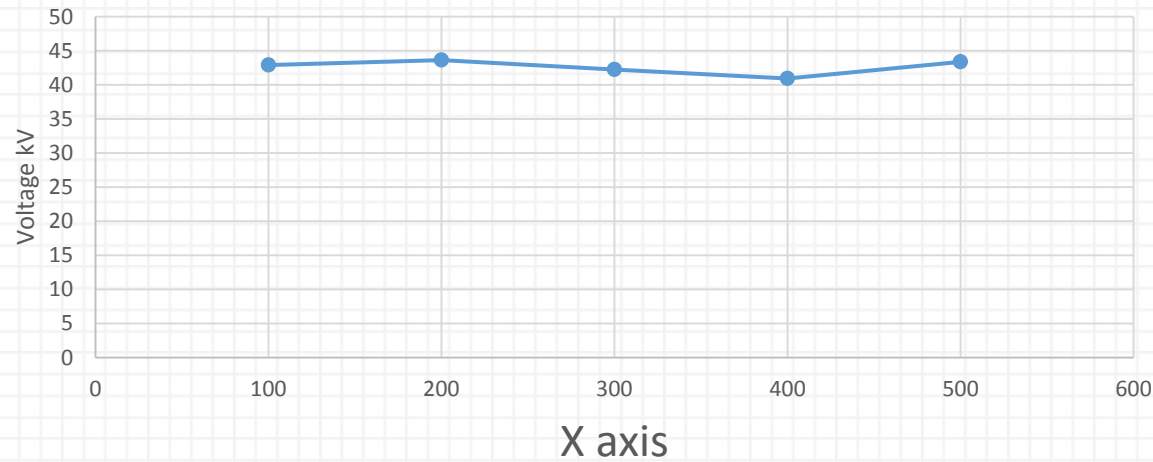
Gap of 16mm



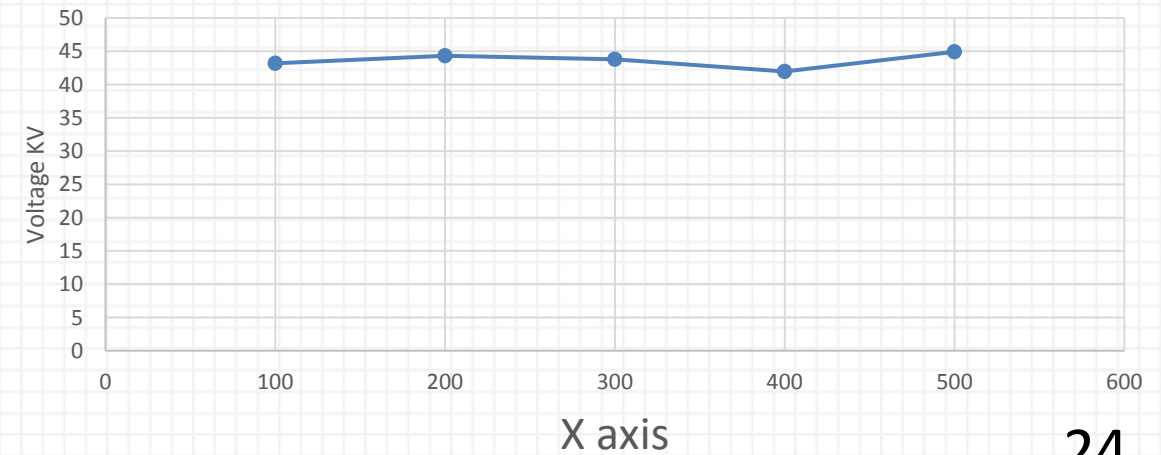
Gap of 14mm



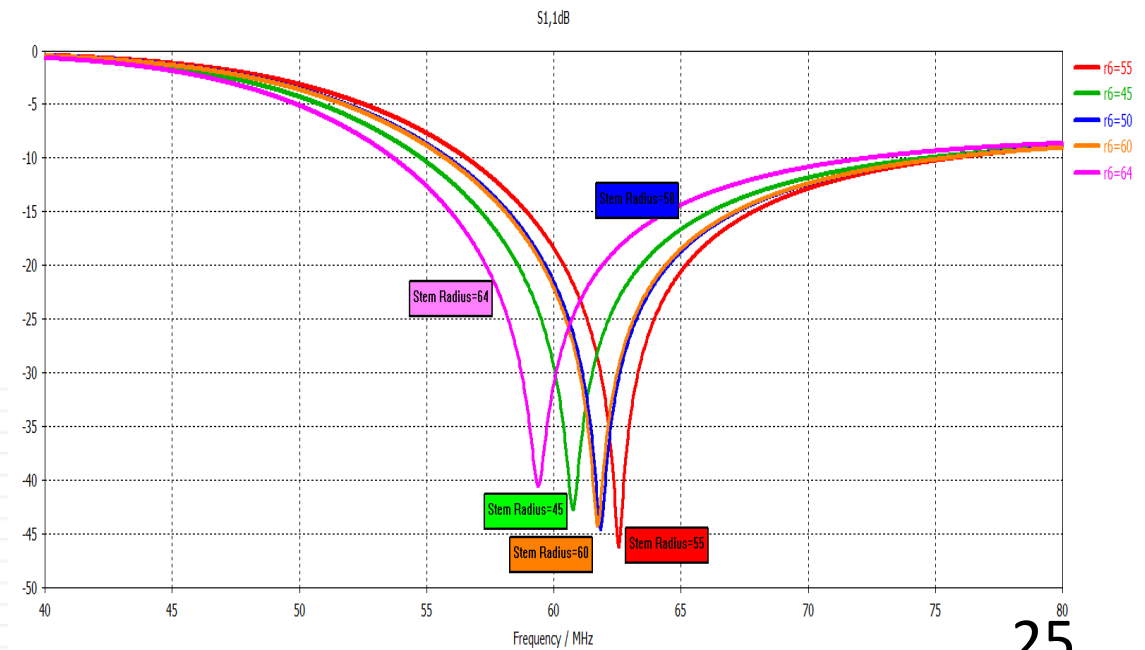
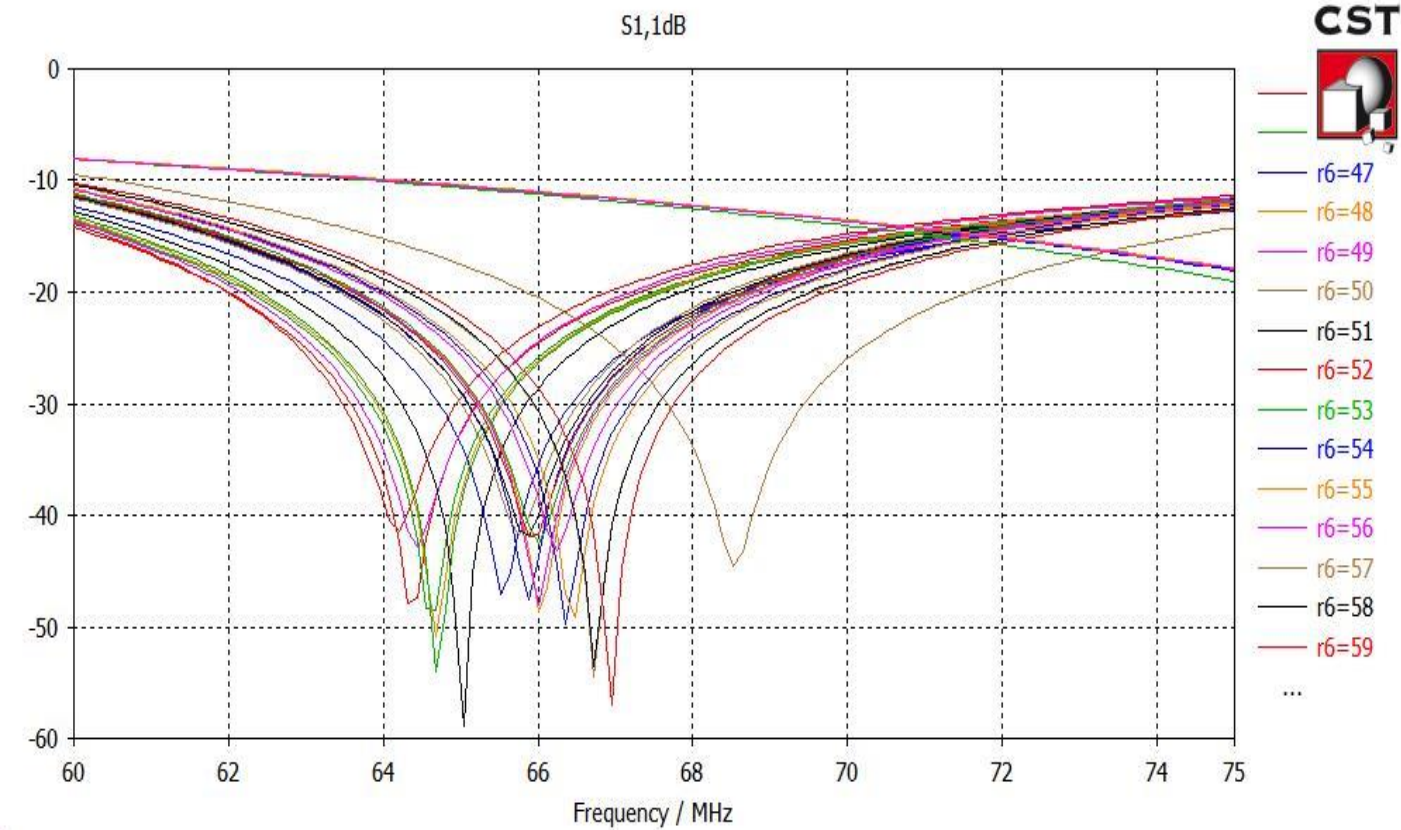
Gap of 12mm



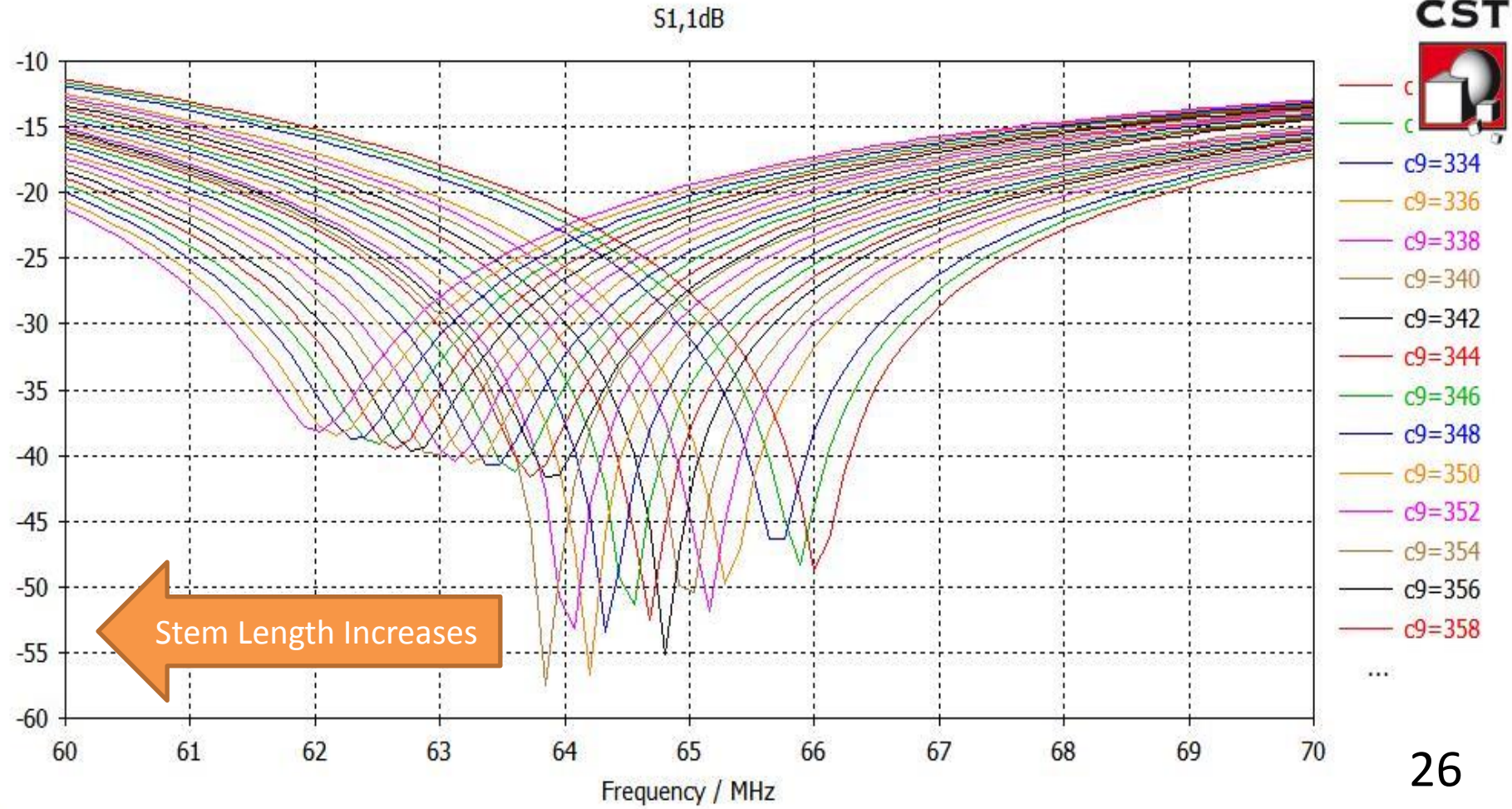
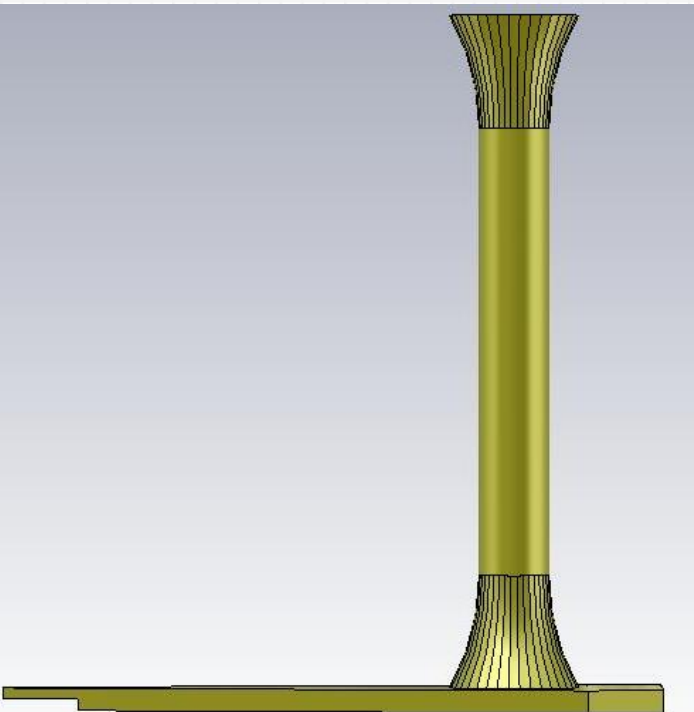
Gap of 10mm



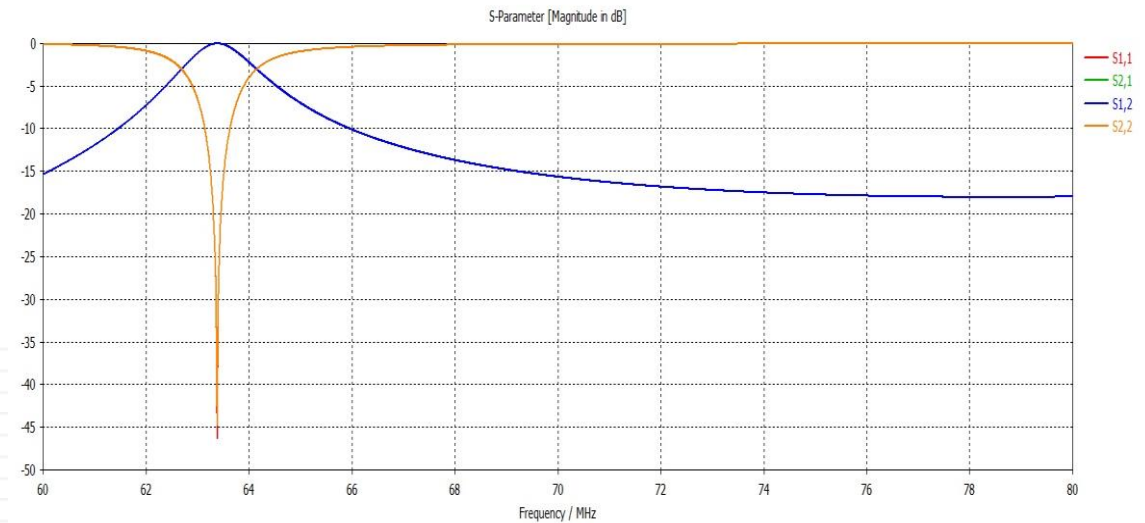
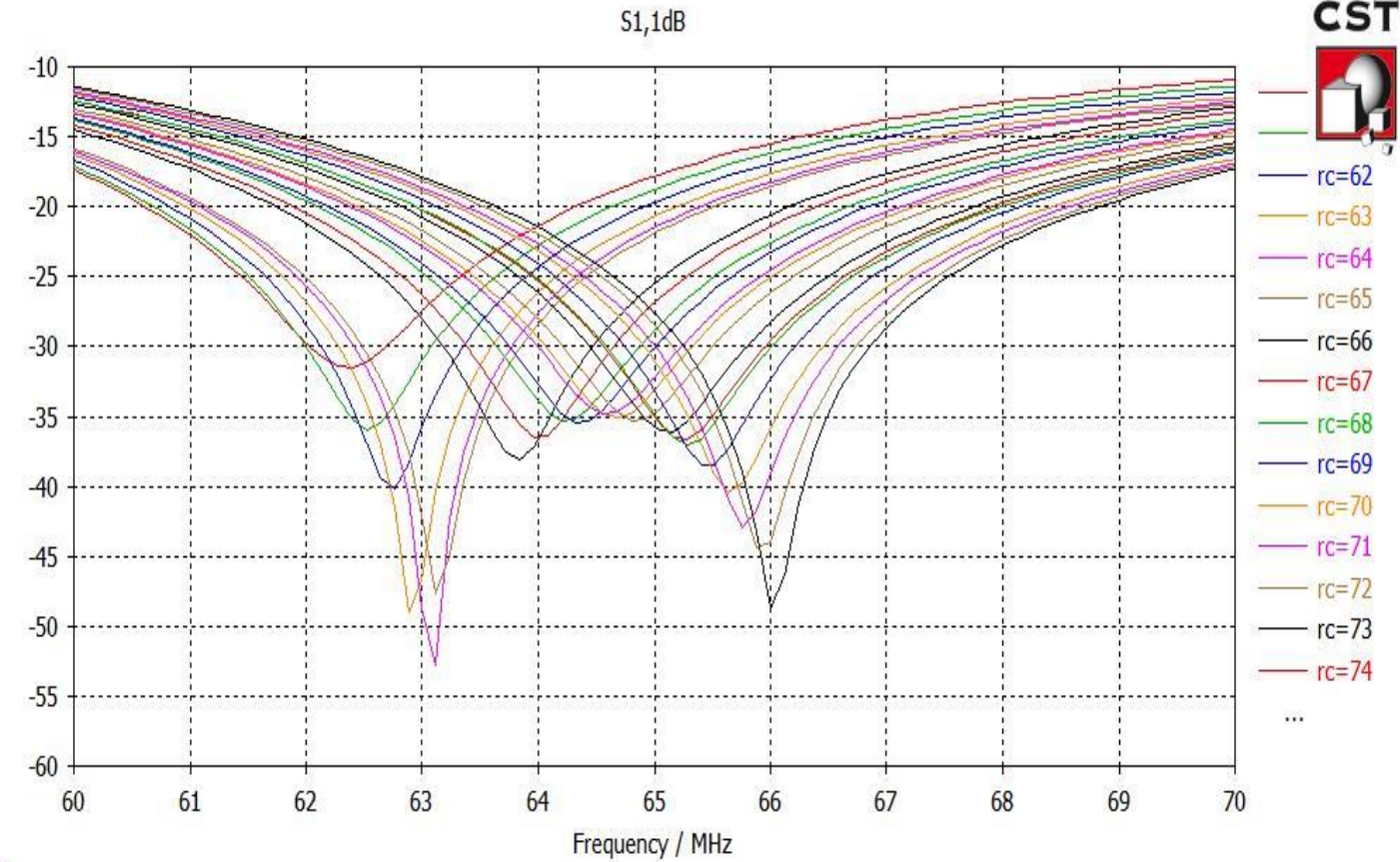
The effect of changing the stem radius



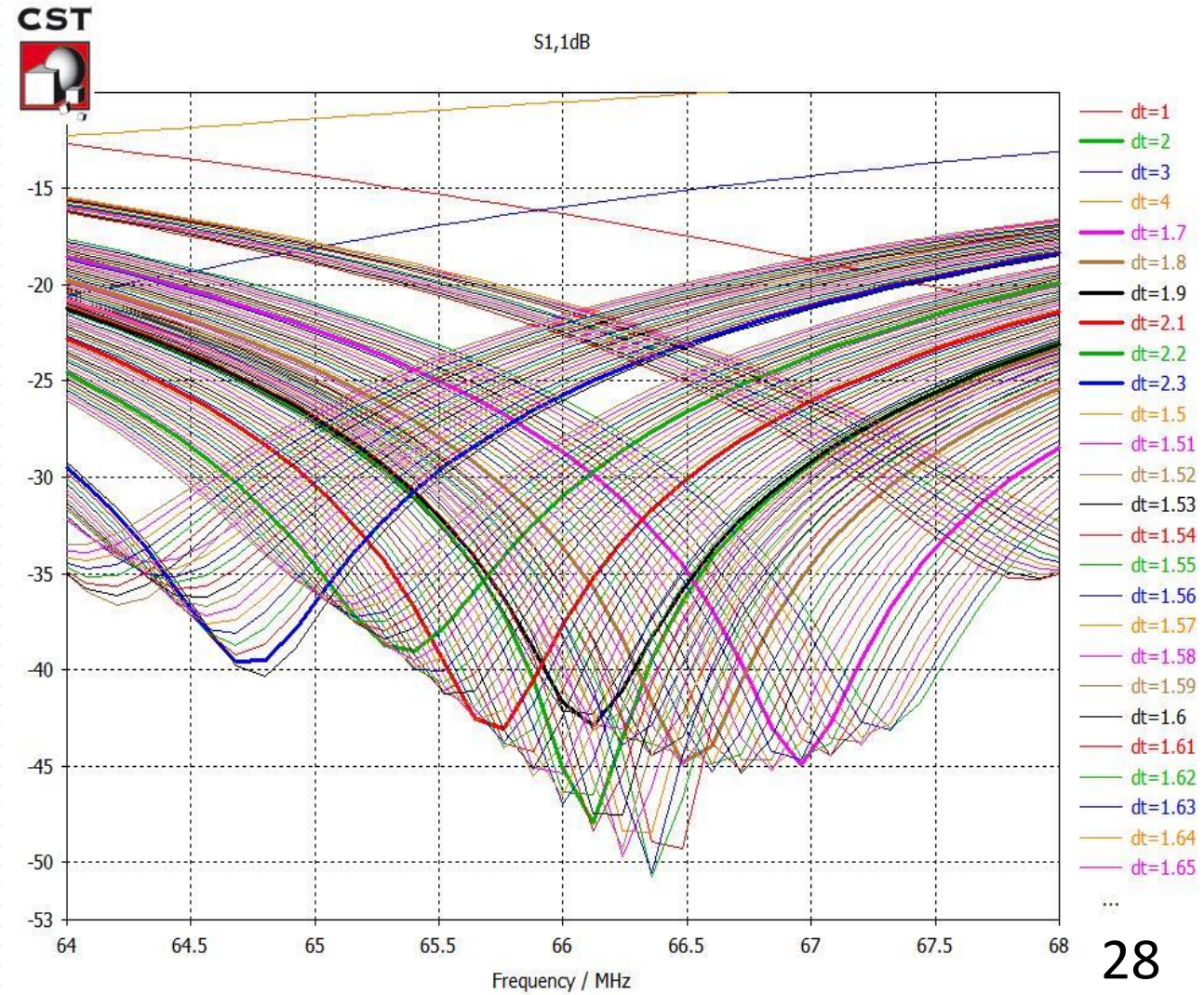
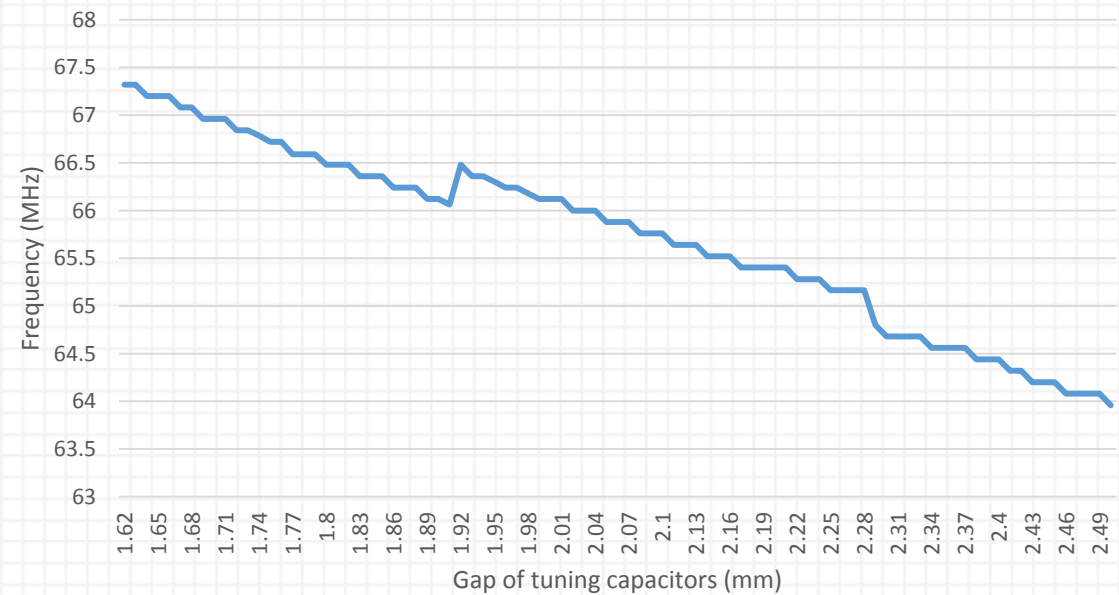
The effect of changing the stem length on the frequency and return loss



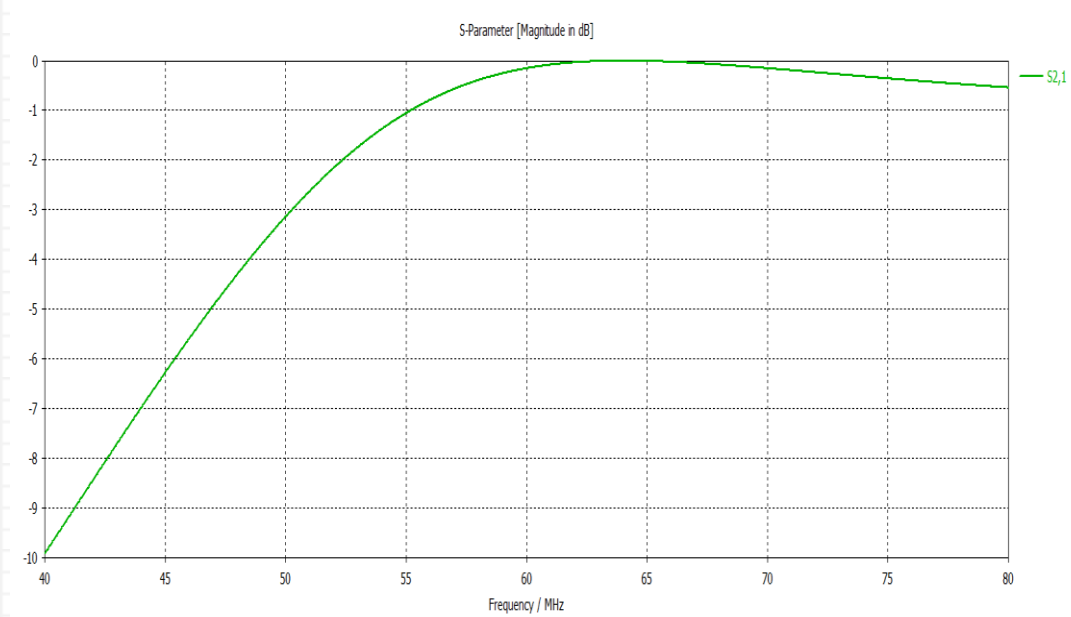
Coupling Result



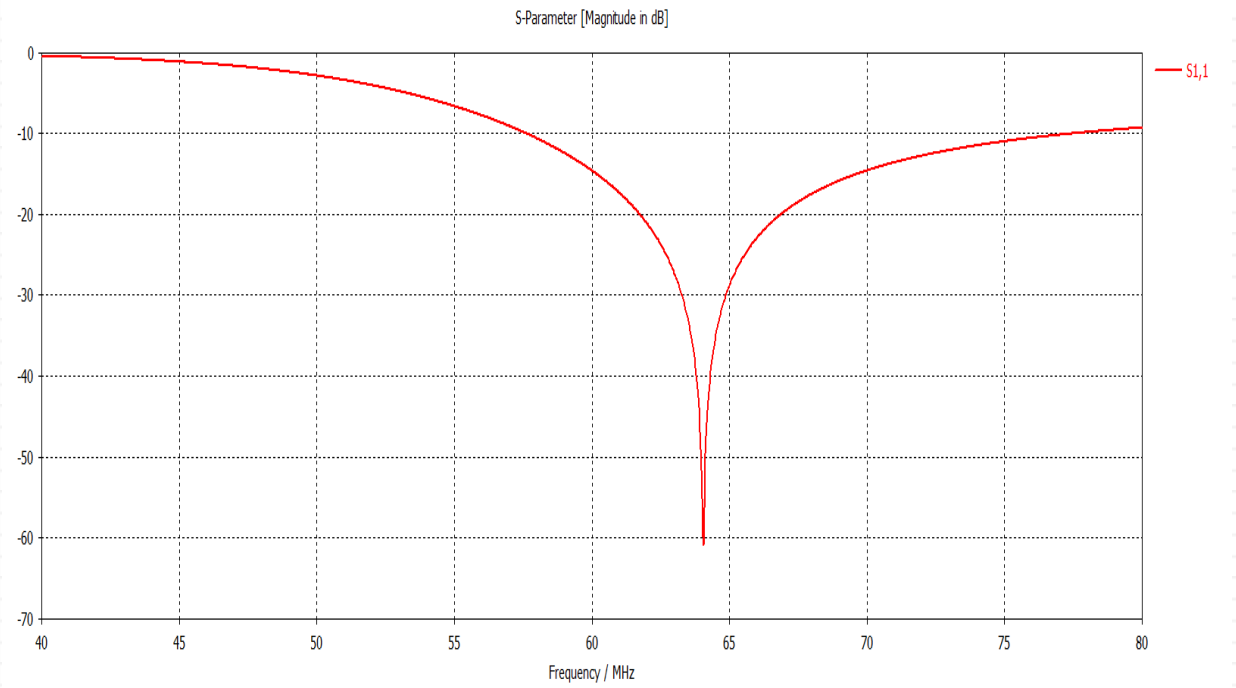
Tuning Result



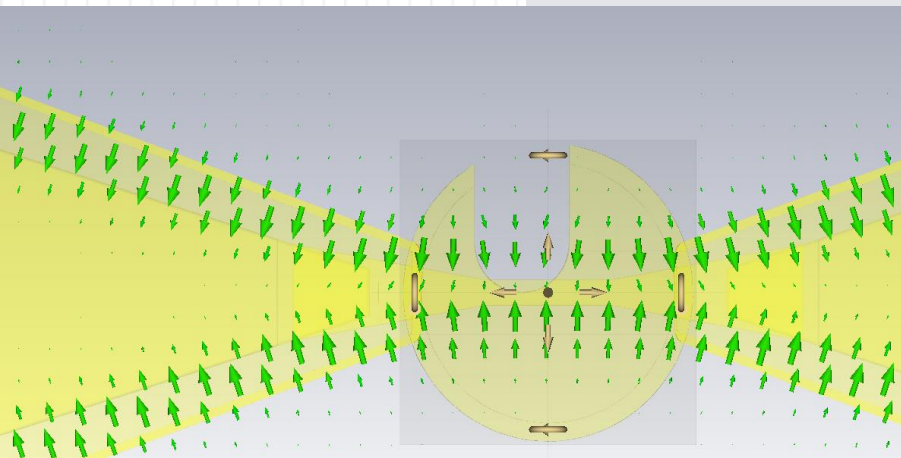
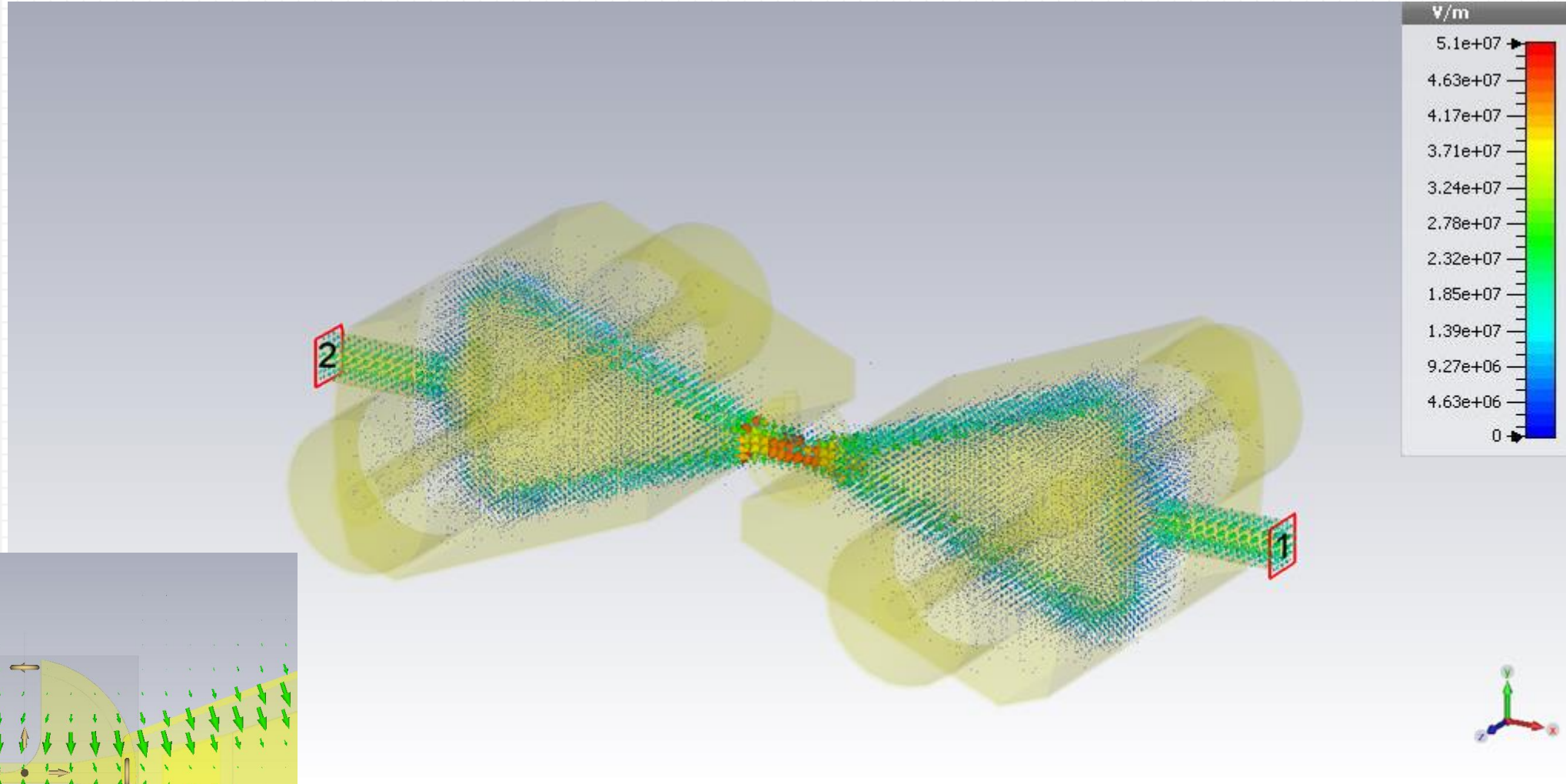
Final S_{21} Parameter

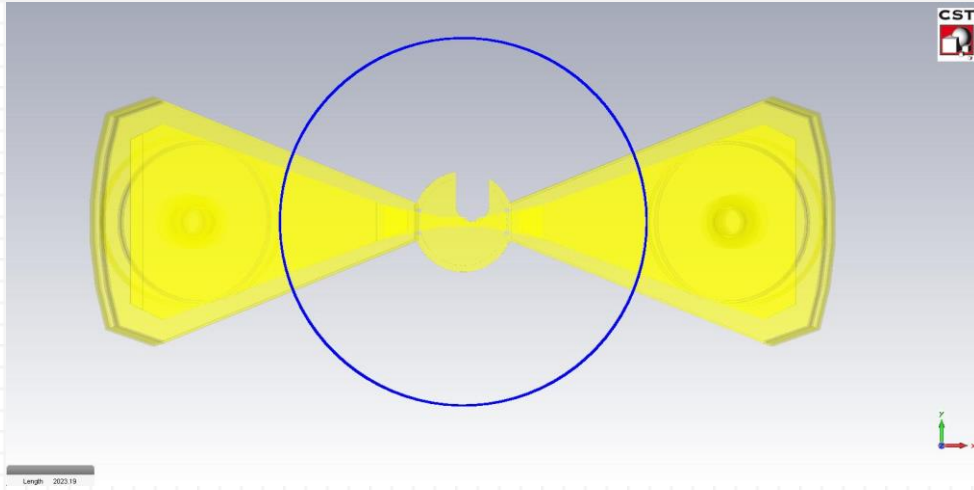


Final S_{11} Parameter

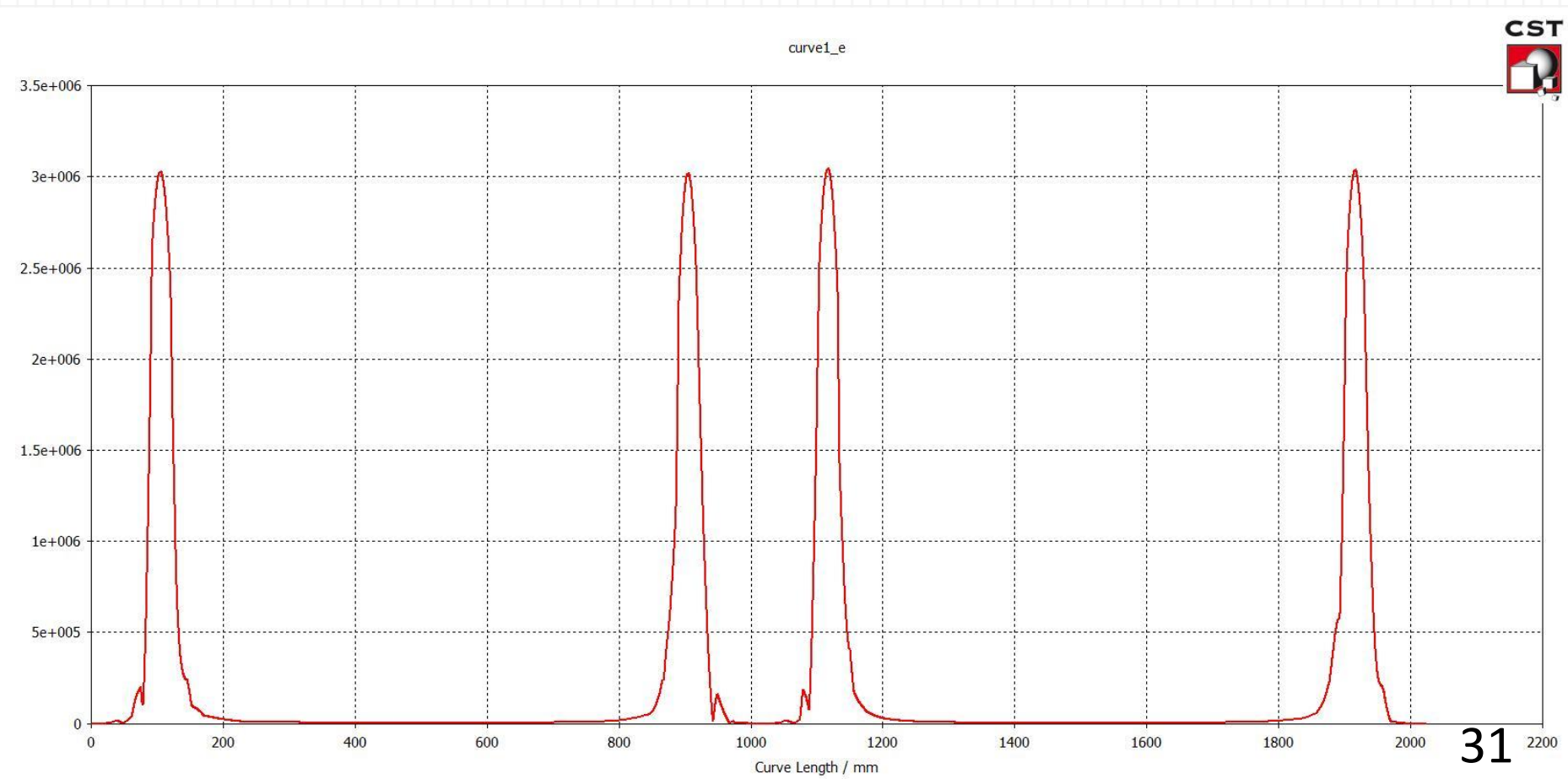


Electric field view

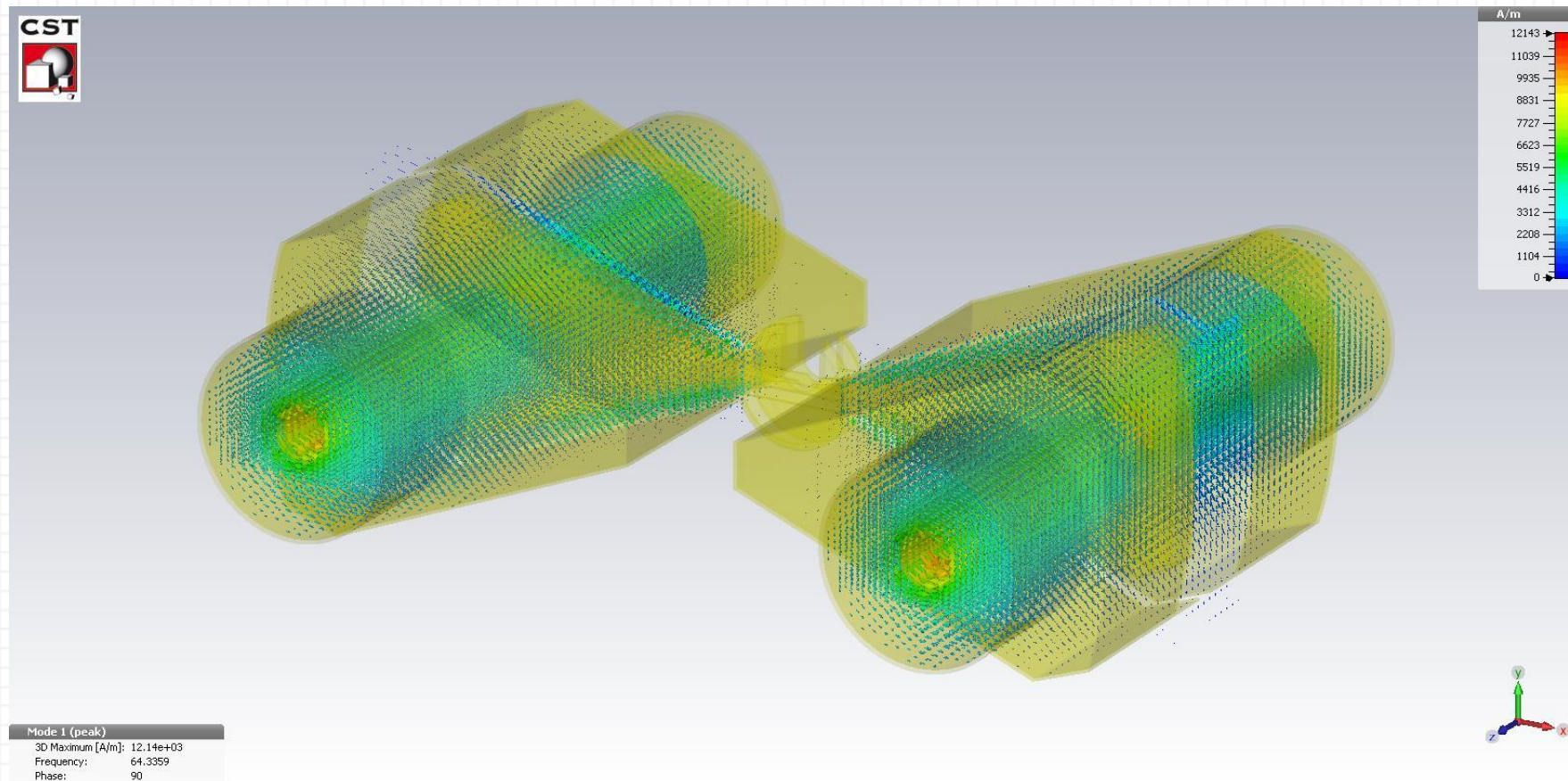


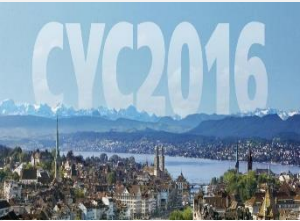


Electric field strength in an arbitrary radius

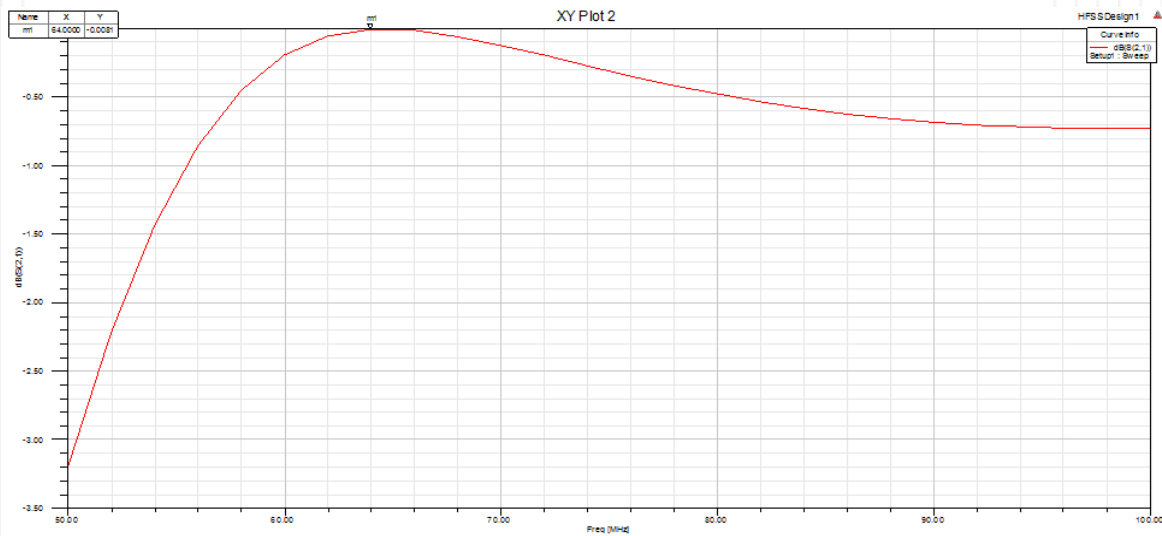
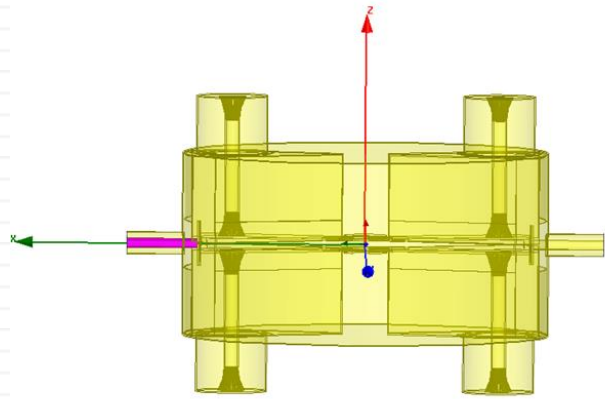


Magnetic field view

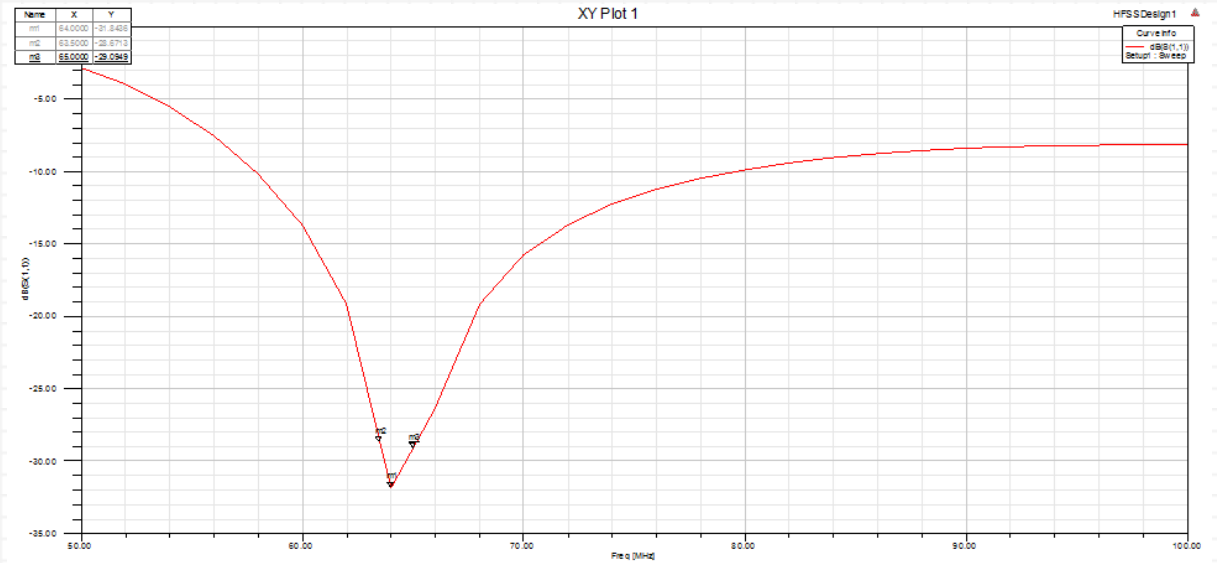




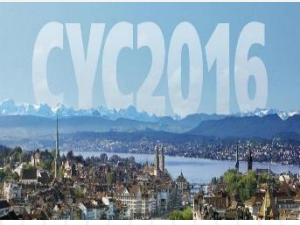
Verify the results with the HFSS software



S_{21} with hfss



S_{11} with hfss



Final specifications of cavity simulated



Parameter	Value
Number of Dees	2
Dee Angle	44
Harmonic Number	4
Resonant Frequency	64.3 MHz
Dee Voltage	45 kV
RF Power	11 kW
Coupling	Capacitive, fixed
Tuning	Capacitive, variable
Quality Factor	6220

**THANK YOU FOR YOUR
ATTENTION**

ANY QUESTIONS?