

Fokker-Planck Description of Transverse Stochastic Cooling

F. Nolden
GSI, Germany
Cool15
October 2015

Classical Cooling Rate

$$\frac{1}{\tau} = \frac{2\dot{W}}{N} \left(gB - g^2 (M + U) \right)$$

system bandwidth
 ↓
 $2\dot{W}$
 system gain
 ↙ ↘
 gB g^2
 ↑ ↑
 undesired „bad“ desired „good“ thermal
 mixing mixing heating
 (Schottky noise) (thermal noise)

↑
 τ
 cooling rate

↑
 N
 particle number

↑
 B
 system bandwidth

↑
 M
 desired „good“ mixing (Schottky noise)

↑
 U
 thermal heating (thermal noise)

Transverse Action J

J is a kind of single particle emittance

$$x = D \frac{\delta p}{p} + \sqrt{2J_x \beta_x} \sin(\mu_x)$$

Fokker Planck Equation

a continuity equation in action space

$$\frac{\partial \Psi(J_x, J_y, \delta p/p; t)}{\partial t} + \nabla \cdot \Phi(J_x, J_y, \delta p/p; t) = 0$$

flux in action space

$$\Phi_m = -F_m \Psi + \frac{1}{2} D_{mn} \frac{\partial \Psi}{J_n}$$

drift (coherent cooling effect)

$$F_m = \frac{1}{\tau} \langle \Delta J_m \rangle$$

diffusion (incoherent cooling effect)

$$D_{mn} = \frac{1}{\tau} \langle \langle (\Delta J_m \Delta J_n) \rangle \rangle$$

Assumptions and Simplifications

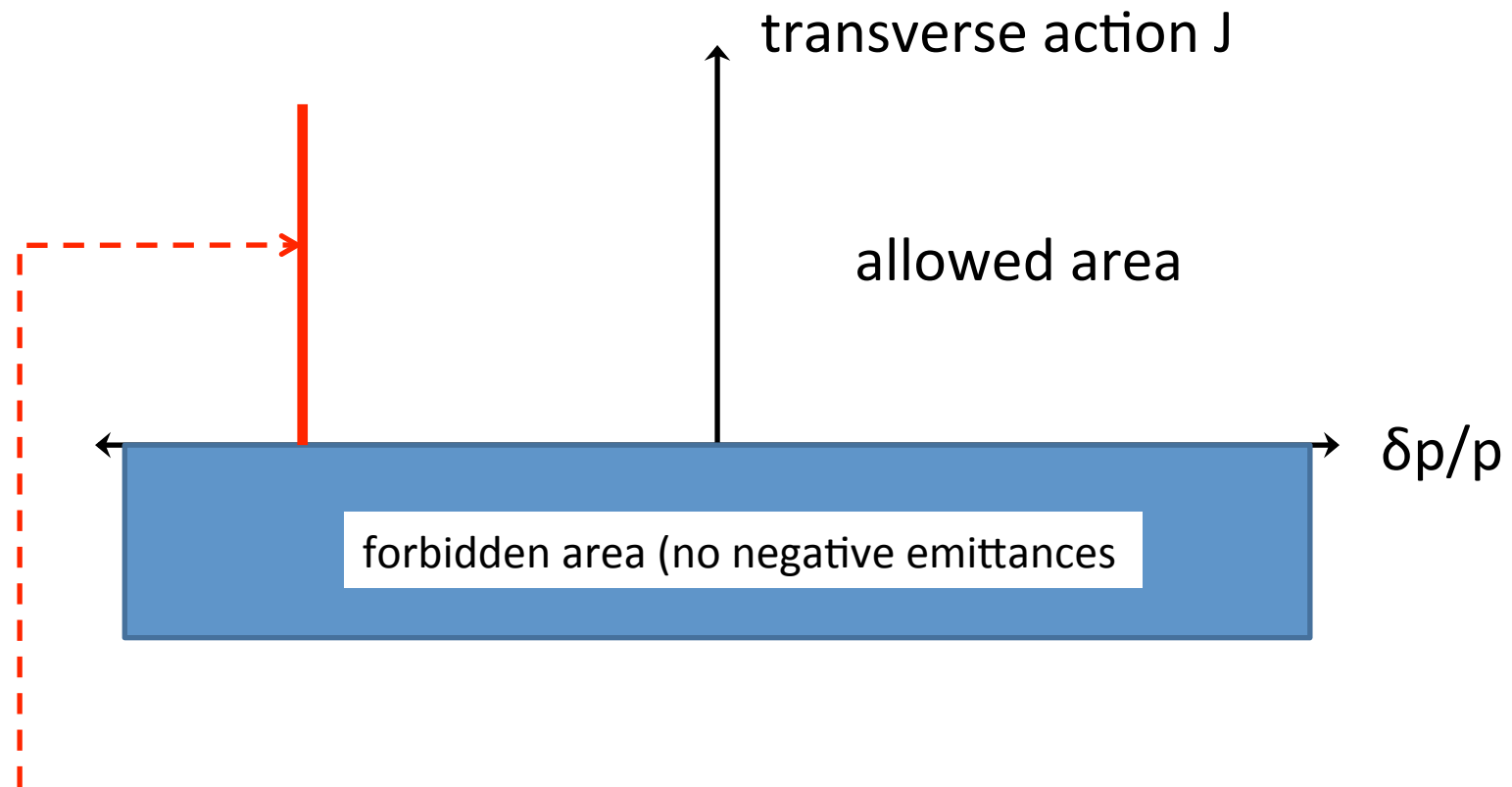
- Zero dispersion at pick-ups and kickers
- Linear response for pick-ups and kickers
- No Schottky overlap
- No Chromaticity

accelerating voltage: $U_k(\Omega) = S_k(x, y, \Omega)V_k(\Omega)$

pick-up response: $V_p(\Omega) = \frac{Qe\omega}{2} S_p(x, y, \Omega)j_p(x, y, \Omega)$

transverse sensitivity: $S(x, y, \Omega) = xS'(0, 0, \Omega)$

2D Phase space



In the following we shall study the 1D distribution function $\psi(J)$ of transverse actions at a given $\delta p/p$

Pick-up Signal for Transverse Cooling

$$V_p(\Omega) \propto \frac{QeZ_l \sqrt{2J_x \beta_x} \partial S_p / \partial x}{4i}$$

at the frequencies $\omega_{m,\pm} = (m \pm Q_x) \omega_{rev}$

in the following: $\frac{\partial S_{pk}}{\partial x} := S'_{pk}$

Voltage Power Densities (1)

The voltage spectral power density $C(\Omega)$ is by definition the Fourier transform of the voltage autocorrelation $R(t) = \langle V(\tau)V(t + \tau) \rangle$.

In a coasting beam it does not depend on τ , i.e. $V(t)$ is a *stationary process*.

The dimension of $C(\Omega)$ is V^2s .

Voltage Power Densities (2)

Voltage power density due to Schottky noise:

$$C_p(\Omega) = \frac{(QeZ_l)^2 \omega \beta_x |S'_p|^2}{16\pi |m\eta|} \langle J \rangle \psi(\delta p / p)$$

average emittance

$$\langle J \rangle = \frac{\int_0^{\infty} J_x \Psi_x dJ}{\int_0^{\infty} \Psi_x dJ}$$

Voltage Power Densities (3)

Voltage power density due to thermal noise:

$$C_n(\Omega) = \frac{1}{2} Z_l k_B T_{eff}$$

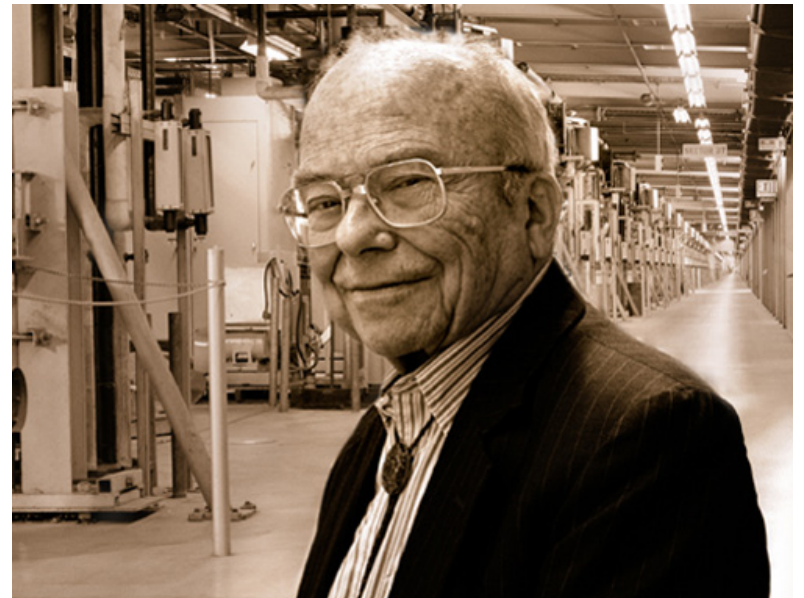
Transverse Kicks

The transverse kicks are described by the Panofsky-Wenzel theorem:

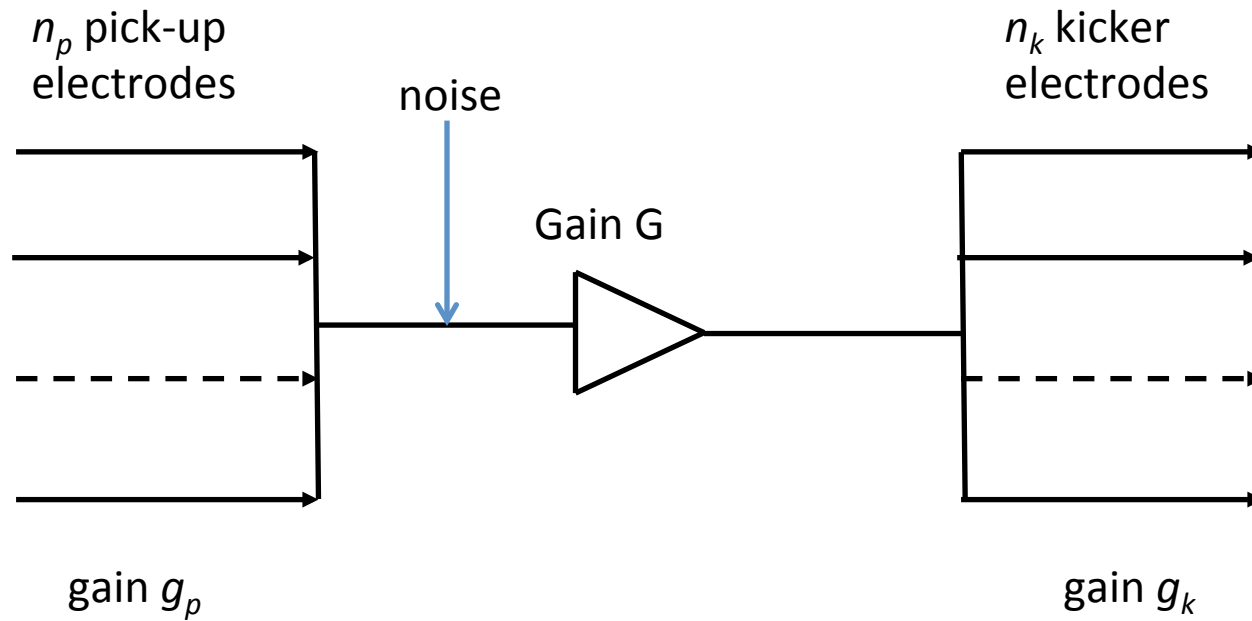
$$\delta p_x = \frac{Qe}{i\Omega} S'_k(\Omega) V_k(\Omega)$$

The kick strength is

- proportional to the transverse gradient of the longitudinal electric field
- inversely proportional to frequency
- max at the zero transition of the electric field



Gain Factors



$$g_{pk} = \sqrt{n_{pk}}$$

Fokker Planck flux

$$\Phi = -F \Psi + \frac{1}{2} D \frac{\partial \Psi}{\partial J}$$

$$F = -C J$$

$$D = (S \langle J \rangle + H) J$$

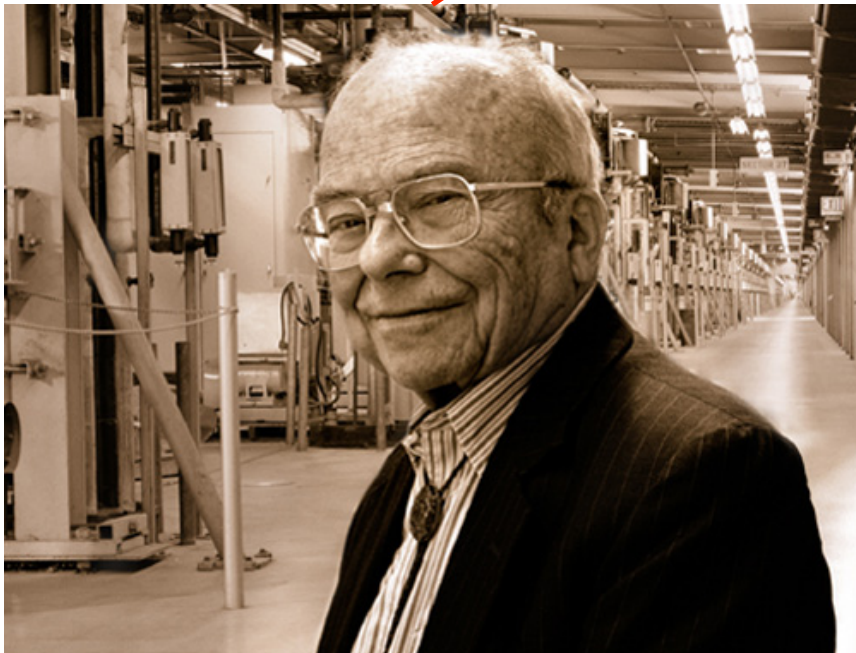
The terms **C (cooling)**, **S (Schottky noise)**, and **H (thermal noise)** do not depend on J.

Therefore the flux is proportional to J.

No flux towards J<0!

Transverse System Gain

$$g_{\perp} = \frac{(Qe)^2 \omega Z_l}{8\pi p \Omega} \sqrt{\beta_p \beta_k} S'_k G g_p S'_p$$



frequency dependent!

Cooling Coefficient

$$C = \frac{\omega}{2\pi} \sum_{m,\pm} \pm g_{\perp} \exp \left[i(\mu_k - \mu_p) - (m \pm Q)\omega T_{pk} \eta_{pk} \frac{\delta p}{p} \right]$$

betatron
phase advance

undesired
mixing

Schottky Noise Coefficient

Schottky power density depends on longitudinal distribution

$$S = \frac{\omega \psi(\delta p / p)}{2\pi} \sum_{m, \pm} \left| \frac{g_{\perp}^2}{m\eta} \right|$$

Schottky power density decreases with harmonics

Thermal Heating Coefficient

$$H = \frac{4k_B T_{eff}}{(Qe)^2 Z_l \beta_p |g_p|^2} \sum_{m,\pm} \left| \frac{g_{\perp}^2}{S'_p} \right|$$

Equilibrium Distribution

condition: $\frac{\partial \Psi}{\partial t} = 0$

The equilibrium distribution turns out to be an exponential:

$$\Psi(J) = \Psi_0 \exp\left(-\frac{2C - S}{H} J\right)$$

with average emittance $\langle J \rangle_\infty = \frac{H}{2C - S}$

Time Dependent Solution

$$\Psi(J, t) = \alpha(t) \exp(-\alpha(t)J)$$

It turns out that this ansatz is a time-dependent solution to the transverse Fokker-Planck equation if

$$\frac{\dot{\alpha}}{\alpha} + \left(-C + \frac{S + \alpha H}{2} \right) = 0$$

If C, S, and H are constant in time, then

$$\langle J \rangle(t) = \left(\langle J \rangle_0 - \langle J \rangle_\infty \right) \exp\left(-\frac{t}{\tau} \right) + \langle J \rangle_\infty$$

with $\tau = C - \frac{S}{2}$ not the instantaneous cooling rate!

Instantaneous Cooling Rate

$$\frac{1}{\tau_{\perp}} = C - \frac{S}{2} - \frac{H}{2\langle J \rangle}$$

$$g_{\perp} = \frac{(Qe)^2 \omega Z_l}{8\pi p \Omega} \sqrt{\beta_p \beta_k} S'_k g_k G g_p S'_p$$

$$C = \frac{\omega}{2\pi} \sum_{m,\pm} \pm g_{\perp} \exp \left[i(\mu_k - \mu_p) - \eta_{pk} (m \pm Q) \omega T_{pk} \frac{\delta p}{p} \right]$$

$$\frac{S}{2} = \frac{\omega \psi(\delta p/p)}{4\pi} \sum_{m,\pm} \left| \frac{g_{\perp}^2}{m\eta} \right|$$

$$\frac{H}{2\langle J \rangle} = \frac{2k_B T_{eff}}{(Qe)^2 Z_l \beta_p |g_p|^2 \langle J \rangle} \sum_{m,\pm} \left| \frac{g_{\perp}^2}{S'_p} \right|$$

Naive Approximation

- constant system gain:

replace $\omega \sum_{m,\pm}$ by $4W$

- rectangular longitudinal distribution:

replace $\psi(\delta p/p)$ by $\frac{N}{\Delta p/p}$

full momentum width

The diagram consists of a rectangular box at the bottom containing the text "full momentum width". An upward-pointing arrow originates from the top center of this box and points to a rounded rectangular box above it. This upper box contains the mathematical expression $\Delta p/p$. This visualizes that the full momentum width is the parameter used to define the width of the rectangular distribution.

Almost Textbook Cooling Rate

$$\text{cooling rate: } \frac{1}{\tau_{\perp}} = 2W \left[2B g_{\perp} - (M N + h) |g_{\perp}|^2 \right]$$

$$\text{undesired mixing: } B \approx \cos \left(m_c \omega T_{pk} \eta \frac{\delta p}{p} \right)$$

$$\text{desired mixing: } M \approx \left(m_c \left| \eta \right| \frac{\delta p}{p} \right)^{-1}$$

$$\text{thermal heating: } h \approx \frac{8k_B T_{eff}}{(Qe)^2 \omega Z_l \beta_p |g_p S'_p|^2 \langle J \rangle}$$

What's „new“?

- Equilibrium distribution is exponential.
- Exponential initial distribution remains exponential during the cooling process.
- In that case, a cooling rate equation for each frequency in the cooling band can be derived.
- If this can be made frequency-independent somehow, one gets to the standard van der Meer/Möhl description.
- Why not modify it (particle number N)?