Status Report on the CERN Synchrocyclotron Improvement Programme

M.S.C. Staff CERN, Geneva, Switzerland

Presented by N. Vogt-Nilsen

ABSTRACT

In order to increase the internal beam current of the CERN SC from its present value of $\sim 1 \,\mu$ A to $\sim 10 \,\mu$ A and to improve its radial quality, the pulse repetition rate will be raised from 54 Hz to ~ 500 Hz and the dee voltage increased to 30 kV and the present open Penning source will be replaced by a hooded arc source. The principal features and the expected performance of the design are outlined and the modification of extraction and pulse stretching are indicated.

1. INTRODUCTION

In common with other projects raising the beam intensity of synchrocyclotrons the CERN SC improvement programme relies on the use of a hooded arc source, a narrow-gap geometry and an increased accelerating voltage. These were first proposed by McKenzie^{1, 2} as means of overcoming the space charge limitations of the conventional open ion source. Practical experience with accelerators^{3,4} and central region studies^{5,6,7} have shown the effectiveness of such an arrangement. Its adoption still leaves several possibilities for further acceleration, i.e.

- (1) retention of weak focusing and full range frequency modulation,
- (2) partial isochronism with limited sector focusing,
- (3) full isochronism, i.e. conversion to a relativistic cyclotron.

The merits of the different solutions have recently been compared by Blosser.⁸ He showed that conversion to isochronism need not lead to a drastic loss of maximum energy and that its difficulties are not necessarily greater than those of options (1) and (2).

CERN has adopted the first possibility. The reasons for this choice and the basic concepts of the project have been outlined in a number of documents.^{9,10} These show that the principal motives for CERN were the wish to limit the

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length of the shutdown needed for a modification, the decision to retain internal targets and the present beam layout, and the conviction that the existing installation would make it difficult to use the higher beam currents potentially furnished by a partially or fully isochronous machine.

The continued use of internal targets appears justified in view of recent measurements^{11,12} showing that their efficiencies are considerably higher than previously assumed,¹³ while the efficiencies of external targets must be limited to a few per cent if good secondary optics and resolution are required.

2. BASIC CONCEPTS FOR THE IMPROVEMENT OF THE CERN SC

2.1. Aims

The aims of the CERN design is a machine

- (1) capable of accelerating about 10 times the present number of protons to the present energy of ~ 600 MeV,
- (2) fitted for operation with internal targets and an extracted proton beam,
- (3) possessing an extraction efficiency large compared with the present 5-7%,
- (4) providing beams of large and possibly also of very small duty cycle,
- (5) capable of being used and serviced for a period of five to ten years.

2.2. General features

The principal characteristics and the main numerical parameters of the project are listed in Table 1. Some details on the design and performance of individual elements are given in the following sections.

3. PRESENT STATUS

3.1. Ion source

Galiana¹⁴ has obtained instantaneous proton currents of the order 100 mA from hot cathode sources of the dimensions given in Table 1. Limitations arising from filament lifetime have been overcome by new types of composite and coaxial filaments, the latter avoiding electrical torques during pulsing.

The improved machine will have the source mechanically integrated into a rigid source assembly comprising the source itself, the puller electrode or electrodes, and the conical accelerating electrodes out to a radius of ~ 6 cm where electrical contacts are made with the dee and dummy dee (see Fig. 3, reference 14). This source assembly is positioned by and supplied through a vertical support of eccentric cylinders introduced through an axial hole in the lower pole face.

Various source assemblies have been tested in the CERN SC Central Region Model using rf extraction. This places the source off-centre and requires different assemblies for field-up and field-down operation.

A d.c.-biased source capable of operating with the magnetic field in either direction 15 is under study.¹⁴

 Table 1. CHARACTERISTICS AND BASIC PARAMETERS FOR THE IMPROVED

 CERN SC

	Maximum proton Average internal o	energy: 600 MeV current: 10 µA					
Magnetic field (reversible):							
At centre	19.7 kG	At extraction radius	18-1 kG				
Extraction radius	2·25 m	K value for $r < 0.2$ m	2				
Ion source:							
Hot cathode hooded ar	c, rf extraction, axial	support, and positioning.	1 1 1 0 2				
Outer diam.	6 mm	Chimney slit	1 × 10 mm ²				
Plasma column diam	4 mm 2 mm	Arc current Pulse length	2 to 5 A				
i lasina columni ulam.	2 1111	i uise iength	- 35 μs				
Rf system:							
Modulation range	30-0-16-77 MHz	Peak accelerating voltag	e 30 kV				
Acceleration time	1383 µs	$(df/dt)_{min}$	–15•65 MHz/ms				
Repetition rate	466 Hz						
Adiabatic beam stackin	g between 16.87 and	17-30 MHz.					
Resonator							
$\lambda/2$ capacity loaded. m	odulated by rotary ca	nacitor electrical length 🛩 m					
Characteristic impedan	ce: maximum 25 Ω . r	ninimum 2 Ω .	•				
Rotary capacitor (3 ro	ws of 16 teeth):						
Outer diam.	1-5 m	Voltage at minimum ga	p 15 kV				
Rotor speed	1747 rpm	Electrical gap	1 to 4 mm				
Maximum voltage	35 K V	Capacitance	0.5 to \sim 7 nF				
Counling capacitor to s	tub:						
Constant capacitance	20 nF	Electrical gap	0·3 mm				
•							
Oscillator (self-excited	tetrode, amplitude me	odulated):					
Variable coupling capa	citor to oscillator:	max. \approx 700 pF, min. \approx 100 pF	-				
Constant voltage at osc	illator:	10 kV	, ,				
Maximum oscillator po	wer:	150 KW	V				
Main dee							
180° to $r = 0.6$ m.							
Cut back by 15° at 0.6	, 0.95, and 1.3 m from	vertical symmetry plane.					
Aperture: 60 mm for r	<1.89 m, 120 mm in	target region.					
Maximum radius	2•35 m	d.c. bias	$\sim 2 \text{ kV}$				
Central dummy dee:							
Radius	0.40 m	d.c. bias	as main dee				
	Intown	al taxaata:					
Internal largets:							
Universal target ranges.	1401ai 2.0-2.5 iii, azii						
	Extractio	on system:					
Non-linear regenerative, first channel section electromagnetic, others iron. Regenerator 56°							
behind channel entranc	e, computed efficienc	y ≲85%. [−]					
Electromagnetic section	1:	Pield and set	210				
Septum thickness	2.5 mm	rield reduction	2 kG				
Current	12 KA	Power consumption	~86 КW				

Table 1. CHARACTERISTICS AND BASIC PARAMETERS FOR THE IMPROVED CERN SC (continued)

	Periphe	ral cee:	
Single sweep operation (provisional design).		
Dimensions: angular	ີ 45°	Modulation range	~160 kHz
radial	200 mm	Tuning range	16.87-17.30 MHz
Axial aperture	120 mm	Power consumption	~50 kW
Stacking radii	2.15-2.25 m	Installed newer	$\sim 100 \mathrm{LW}$
Peak voltage	2·10-2·20 III	instance power	100 KW
reak voltage	\sim 18 kV		
	Extraction coil (p	rovisional design):	
Angular extension	18°	Peak current	~3.2 kA
Axial aperture	120 mm	Peak magnetic field	200 G
Slow operation		East operation (1 us)	•
Peak voltage	20 V	Post voltoro	. 16 1-37
Demon of a manual and	50 V	reak voltage	
Power consumption	5 K W	Power consumption	40 kW
	Expected proton	beam properties:	
Long burst extracted pro	oton beam:		
By cee:		By coil:	
Energy spread	0.5 MeV	Energy spread	<3 MeV

By cee:		By coil:	
Energy spread	0.5 MeV	Energy spread	$\lesssim 3 \text{ MeV}$
Micro duty cycle	10-20%	Micro duty cycle	100%
Macro duty cycle	80%	Macro duty cycle	85%
Emittances: radial <1	5 mm mrad, vertical <	25 mm mrad.	
Short burst extracted	proton beam by coil:		_
Pulse length	1 μs	Energy spread	≲3 MeV
Duty cycle	0.05%		
Long burst on internal	targets by cee:		
Duty cycle	10-20%		

3.2. Central region studies

The behaviour of the beam in the central region has been subject to extensive theoretical studies¹⁶⁻²⁰ and various geometries have been designed with the aim of optimising the range of rf phases available for capture. Several assemblies have been tested experimentally in the Central Region Model,⁷ where beam intensities somewhat in excess of the calculated values have been observed. Recent measurements have given equivalent currents of ~20 μ A for the improved SC.

Shadow measurements of radial betatron amplitudes at 22 cm radius confirm the existence of an amplitude build-up introduced by a movement of the orbit centre at small radii and large phase angles.⁷ This effect may be weakened at the expense of internal beam current and technical difficulties in the rf system by operating with initial equilibrium phases φ_s at values of $\cos \varphi_s$ larger than 0.1 at which the beam current is optimised.^{7,17}

3.3. Rf system

The new main rf system has to furnish 30 kV on the dee gap over a frequency range from 30.0 to 16.7 MHz with a repetition rate of \sim 500 Hz. To comply

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Fig. 1. Principal equivalent circuit for the new rf system



Fig. 2. Principal mechanical arrangement for the new rf system

with these requirements a system based on a rotary capacitor of a rather sophisticated design has been proposed.²¹⁻²⁴

To minimise the dee capacity the cut-back form indicated in Table 1 was adopted. Computer studies have shown that the proposed form does not give a significant contribution to the radial betatron amplitude such as has been predicted and observed at the Harwell Synchrocyclotron.²⁵

Fig. 1 shows the equivalent circuit of the rf system. In it the dee and dee stem are represented by a transmission line with a carefully designed tapered impedance distribution, into which the rf power is fed through a system consisting of the rotary modulation capacitor $C_{\rm mod}$ and the rotary coupling capacitor $C_{\rm cos}$ synchronised on the same shaft, and the fixed coupling capacitor $C_{\rm CL}$. The role of $C_{\rm cos}$ is to provide a constant load to the oscillator over the whole frequency range. A schematic view of the layout is shown in Fig. 2.

The designer's problem is to find an impedance distribution in the line section which achieves the required variation of the resonant frequency (see Table 1) for practicable values of C_{mod} while keeping the potentials across the capacitors within tolerable limits. Numerical studies of the problem have provided a range of acceptable solutions, of which some have been tested on a one-fifth scale model of the entire system. A separate study of breakdown phenomena in rf fields has shown that the calculated potentials across the small capacitor gaps can be maintained if suitable precautions are taken with regard to the surface

treatment of the electrodes and by avoiding traces of hydrocarbon vapours in the vacuum. The latter necessitates a separate turbomolecular pump system for the rotary capacitor.

The shapes of the stator and rotor blades have been chosen to provide a frequency vs time function (Fig. 3) which fulfils the following three requirements²⁶ (Fig. 4):

- (1) $\cos \varphi_s$ should start close to its theoretical optimum, 0.1.
- (2) In order to be sure to retain all captured particles, even in the presence of unforeseeable errors, the canonical bucket area A should be given a 5% increase during the first 100 μ s and a further 5% increase during the rest of the modulation cycle.

(3) The flyback time should be as short as technically feasible.

Provisions will be made to deposit the beam adiabatically at a radius chosen within certain limits for further acceleration or displacement by one of the proposed beam stretching devices.

A study of the beam loading problem is envisaged. As a preliminary a theoretical model capable of describing the various cross modes in the cut-back dee has been worked out.²⁷ A study to define the local impedances of the dee is in progress.

The observation of parasitic resonances in the one-fifth scale model²⁸ necessitated the redesign of the rotary capacitor, which is now cantilevered and fed coaxially. Its design also attempts to minimise the rf currents flowing through the ball bearings by letting these be parts of bridge circuits.

The manufacture of the entire accelerating system, consisting of oscillator, modulator, rotary capacitor, and resonator, including the dee, is being undertaken by a contractor. Delivery is scheduled for August 1971 and will determine the date of the shutdown.

3.4. Beam extraction

Beam extraction by a non-linear regenerative system in weak focusing



Fig. 3. Frequency vs time function for the improved CERN SC. It is chosen to minimise the acceleration time (1.383 ms)

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Fig. 4. Bucket parameters for the improved CERN SC. The bucket area A (right scale) is chosen to increase by 10% over the acceleration period. The resulting $\cos \varphi_8$ (left scale) rises from 0-13 to 0-52. The small minimum in the A curve stems from the desire to have a smooth f(t) curve (Fig. 3)



Fig. 5. Details at end of acceleration period showing the nominal rf vs time (lower full curve) as well as frequency (upper full curves) and voltage (dashed curve) functions for adiabatic stacking. The regenerative extraction occurs at 15.82 MHz

synchrocyclotron fields has been subject to orbit studies by Paul²⁹ and by Lindbäck,³⁰ who have shown the deleterious effect of pre-existing betatron amplitudes and of field distortions in the vicinity of the magnetic channel.

The present betatron amplitudes $A_r \sim 10$ cm and $A_z \sim 1.5$ cm observed in the CERN SC should both be reduced to less than 1 cm with the introduction of the calutron source. According to Lindbäck this alone would at least double

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the extraction efficiency and improve the energy resolution of the extracted beam considerably.

A further gain can be expected if the strong disturbance of the field near the channel can be avoided, since it leads to a rapid growth of the vertical amplitude in the last turn before extraction. To minimise the effect of the stray field we therefore plan to use an electrical channel of coaxial type similar to that proposed by Morpurgo³¹ in the first section of the extraction channel.

À tentative design of a curved concrete insulated channel has been made by Susini and Giannini.³² Copper conductors are arranged to produce a field distribution similar to that of a coaxial cable; a 2.5 mm septum and an anti-septum produce stray field cancellation. A similar channel has been proposed by Cohen *et al*³³ for the Columbia SC.

Blosser⁸ has recently suggested preceding the magnetic channel by an electrostatic deflector and has predicted extraction efficiencies of up to 80% for such a system. Unfortunately the presence of internal targets and the associated beam transport makes the adoption of this idea difficult at CERN.

3.5. Long and short burst

Long burst operation is at present provided by a peripheral cee operating on the beam deposited at storage radius by the main rf. Duty cycles exceeding 30% are obtained with internal targets; for the extracted beam 10% is a normal value. The capture efficiency of the cee is about 50-60%. A pulsed magnetic field perturbation, such as the system developed by Danilov *et al*³⁴ at Dubna is considerably more efficient and produces an output free from rf structure.

However, it is difficult at the CERN SC to find a coil position which will give a long burst operation for internal targets as well as for the extracted proton beam. Our coil will be positioned for proton extraction opposite the regenerator.

Lindbäck³⁵ has shown that the capture efficiency of a cee system can be large (90-100%) if the beam storage is performed by reducing both the rf voltage and frequency slope adiabatically to zero (Fig. 5). Provided that the radial amplitudes in the stored beam are <1 cm the cee will be capable of giving an extracted beam of greatly reduced energy spread (≈ 0.5 MeV).

In an attempt to combine the advantages of a cee system and a pulsed coil Susini^{36,37} has recently proposed to place a pulsed coil inside a cee. Operated with a suitable power supply such a coil would also permit a very fast beam ejection in ~20 turns (~1 μ s). This possibility is of interest for very low count-rate experiments in which the background is not due to the machine.

3.6. External beams

The external beam system of the CERN SC is highly developed and we do not envisage any fundamental change. However, most beam lines will have to be re-designed; to permit servicing of the beam transport elements we plan to place them on rails and to withdraw them through the shielding wall. We shall use this opportunity to add an inflector magnet to the present low-energy pion beam from internal targets, thereby increasing its versatility. We are also studying the possibility of very low energy pions from an external target. Pion beams of good quality of 50 MeV or less would have considerable research potential. Present beam intensities, which are of order 10^5 particles/s for pion beams and 5×10^{11} for the extracted proton beam should increase by an order of magnitude. We hope for larger gains in the extracted proton beam and secondary beams derived from it.

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