TRANSVERSE BEAM GROWTH DUE TO LONGITUDINAL COUPLING IN LINEAR ACCELERATORS

Robert L. Gluckstern
Physics Department, University of Massachusetts
Amherst, Massachusetts

I. Introduction

The usual approximation for treating orbit dynamics in linear and circular accelerators is to consider the longitudinal and two transverse motions to be uncoupled and to treat the development of the corresponding 2 x 2 phase spaces independently. It has long been recognized that the orbit motions are coupled.

In linear accelerators the source of this coupling is the dependence of the rf defocusing term in the transverse motion on the longitudinal phase and the dependence of the transit time factor in the longitudinal motion on the transverse position (these coupling terms arise from the same term in the Lagrangian). An effort to include the effect of these coupling terms to the two lowest orders was made in order to determine their influence on transverse beam size. Comparison of these results with orbit computations, indicated agreement for the lowest order term, but not for the term which would be resonant if the longitudinal and transverse oscillation frequencies were equal.

The present report reviews the analysis, yielding a result for the second order term which takes into account higher order terms in the first coupling term. This result now appears to be in general agreement with the orbit computations and can be used as the basis for predicting transverse beam growth due to this coupling.

II. Growth of Transverse Oscillations

The basic coupled equations for motion in the longitudinal and one transverse direction, including only the first two coupled terms, are

\[ \frac{1}{\beta^3 \gamma^3} \frac{d}{ds} \left( \beta^3 \gamma^3 \frac{dX}{ds} \right) + k^2 L X = \frac{\gamma^2}{\beta^3 \gamma^3} y \left( 2gx + x^2 \right) \]

\[ \frac{d}{ds} \left( \beta^3 \gamma^3 \frac{dX}{ds} \right) + k^2 L X = g \beta \gamma^3 \left( x^2 - k^2 \gamma^3 (g + x) \right) \]

(1)

These equations differ from those in References 3 and 4 by the inclusion of the \( \chi^2 \) term in the equation for \( \chi \), and by treating \( y \) as an actual displacement. The notation is:

\[ \lambda = \text{rf wavelength} \]

\[ \phi_s = \text{synchronous phase} (\leq 0) \]

\[ x = \phi - \phi_s \]

\[ y = \text{transverse displacement} \]

\[ k_t = \text{smoothed transverse oscillation number} \]

\[ \beta \gamma = \text{longitudinal momentum of the synchronous particle in units of } mc \]

Equations (1) and (2) contain several approximations. These are:

1) Only terms of order up to \( y^2 \) are included in the Lagrangian. This appears to be valid for beam sizes currently considered.

2) The transverse oscillation, which is usually of the strong focusing type, has been smoothed. This should be reasonable for the present coupling effects but not for any coupling effects arising at magnet boundaries.

3) Only terms of order up to \( \chi^3 \) and \( \chi y^2 \) are included in the Lagrangian. Stability limits are not correctly obtained in this approximation but the coupling effects will be consistent to the order shown.

4) Only that rf wave component traveling with the beam is included. Inclusion of other components is equivalent to taking into account the velocity dependence of the transit time factor, which has little relevance to the coupling effects.

The solutions of the uncoupled linearized part of Equations (1), (2) in
the JWKB approximation are:
\[ y = A \left( \frac{\beta y}{s} \right)^{-1/2} k \left( \frac{s}{s} \right) + \alpha t \]
\[ x = A \left( \frac{\beta y}{s} \right)^{-3/2} k \left( \frac{s}{s} \right) + \alpha t \]
\[ y = A \left( \frac{\beta y}{s} \right)^{-1/2} k \left( \frac{s}{s} \right) + \alpha t \]
\[ x = A \left( \frac{\beta y}{s} \right)^{-3/2} k \left( \frac{s}{s} \right) + \alpha t \]

In order to compare with numerical results, we consider collections of points of fixed \( A_t \), \( A_s \), and distributed values of \( a_t \), \( a_s \). The most convenient coordinate systems for observing the motion of these phase points are the polar coordinates \( A \), \( A_s \) and \( A_{\alpha}, A_{s} \) which are equivalent to the Cartesian coordinates:
\[ y = \left( \frac{\beta y}{s} \right)^{1/2} \left( \frac{\beta y}{s} \right)^{-1/2} \]
\[ \frac{\beta y}{s} \]
\[ \frac{\beta y}{s} \]
\[ \frac{\beta y}{s} \]
\[ \frac{\beta y}{s} \]

where \( \beta y \) is Courant and Snyder's \( \beta \).

The uncoupled oscillations correspond to motions of phase points in circles in the coordinate systems represented by Eq. (5). Amplitude increases then appear as (elliptical) distortions in these coordinate systems.

In the iterative scheme for solving Equations (1) and (2), the typical equation will contain oscillatory driving terms of decreasing amplitude. Integration of such an equation over the course of acceleration will then be done approximately and will only involve the starting amplitude, frequency and phase of the driving term. Specific damping variations will not appear explicitly. To simplify the presentation, therefore, we shall ignore damping, except where necessary to discard terms at the end of acceleration. With this understanding we then write
\[ y = y(0) + y(1) + y(2) + \ldots \]
\[ x = x(0) + x(1) + x(2) + \ldots \]

with
\[ y(0) = y_o \sin t = y_o \sin(k \left( \frac{s}{s} \right) + \alpha t) \]
\[ x(0) = x_o \sin \theta = x_o \sin(k \left( \frac{s}{s} \right) + \alpha t) \]

\[ y(1)^{\prime} + \frac{\beta y}{s} y(1) = \frac{k}{2} \cos(t - \xi) \]
\[ x(1)^{\prime} + \frac{\beta y}{s} x(1) = \frac{k}{2} \cos(t - \xi) \]

\[ x(2)^{\prime} + \frac{\beta y}{s} x(2) = \frac{k}{2} \cos(t - \xi) \]

We have here separated the \( x(1) \) contribution into a part proportional to \( y_0 \) and a part proportional to \( k^2 \) and have treated the second order terms consistently. The solutions for \( y(1), x(1) \) and \( x(1) \) (which are defined to vanish and have vanishing derivatives at \( s = 0 \)) are:
\[ y(1) = \frac{\beta y}{s} y_o \left[ \frac{2k \cos(t - \xi)}{2k^2 - k} \right] + \frac{k \cos(t - \xi) + a_t}{2k - k^2} \]
\[ x(1) = \frac{\beta y}{s} y_o \left[ \frac{2k \cos(t - \xi)}{2k^2 - k} \right] + \frac{k \cos(t - \xi) + a_t}{2k - k^2} \]

\[ y(1)^{\prime} + \frac{\beta y}{s} y(1) = \frac{k}{2} \cos(t - \xi) \]
\[ x(1)^{\prime} + \frac{\beta y}{s} x(1) = \frac{k}{2} \cos(t - \xi) \]

\[ x(2)^{\prime} + \frac{\beta y}{s} x(2) = \frac{k}{2} \cos(t - \xi) \]

\[ y(1)^{\prime} + \frac{\beta y}{s} y(1) = \frac{k}{2} \cos(t - \xi) \]
\[ x(1)^{\prime} + \frac{\beta y}{s} x(1) = \frac{k}{2} \cos(t - \xi) \]

\[ x(2)^{\prime} + \frac{\beta y}{s} x(2) = \frac{k}{2} \cos(t - \xi) \]
The cos(t + a) terms in Eq. (14) and the 1 and cos2t terms in Eq. (15) decrease with increasing s, whereas the remaining terms are present only to satisfy the boundary conditions at s = 0 and represent permanent deformations which persist at s = ∞. These latter terms give rise to a change in transverse amplitude which comes only from the coefficient of sin t in Eq. (14):

\[
\frac{\delta A(x)}{A(0)} \sim g k^2 \frac{\sin(2a - a)}{8k^2} \left[ \frac{1}{2k - k_a} + \frac{1}{2k + k_a} \right].
\]

The contribution of \( y^{(2)} \) to the transverse amplitude change can similarly be calculated from Eq. (12). We shall here only evaluate the effect of the term which dominates for \( k_t \) and \( k_a \) almost equal. The result (which can also be obtained by the phase amplitude method of Reference 3) is

\[
\frac{\delta A(\omega)}{A(0)} \sim \frac{k^2}{32k_a^2(2k - k_a)} \left[ 1 - g^2 \left( \frac{1}{3} + \frac{k_a}{2k - k_a} \right) \right].
\]

The factor proportional to \( g^2 \) represents the contribution of the first order terms in Eq. (12) which was not previously included.

The dominant term in the sum of Equations (17) and (18) is expected to be the first term in Eq. (17) unless \( k_t - k_a \) is particularly small. This term represents, for a given \( a \), an elliptical distortion of the transverse phase space by a factor

\[
\frac{A(\omega)}{A(0)} \sim 1 + \frac{g k^2}{8k^2(2k - k_a)} x_0
\]

with orientation such that the maximum transverse amplitude occurs for

\[
2a_t - a_1 = \pi/2.
\]

If one now considers a collection of all values of \( a \), the occupied phase space will consist of the superposition of ellipses of distortion given by Eq. (19) with all orientations, and, for all intents and purposes, will appear to be a growth in the transverse amplitude by the factor given in (19).

The situation is more complicated for the sum of Equations (17) and (18) since the distortion in general depends on \( a \). However, the maximum distortion occurs for a value of \( a_1 \) such that all terms are in phase. The maximum transverse amplitude growth is therefore

\[
\frac{\delta A(\omega)}{A(0)} \left[ \frac{1}{2k - k_a} + \frac{1}{2k + k_a} \right] + \frac{2k_a^2}{32k_a^2} \left[ \frac{g^2}{3} + \frac{k_a^2}{2k - k_a} - 1 \right].
\]

The result in Eq. (21) gives the transverse amplitude growth at the end of acceleration (after coupling terms are unimportant). One expects to see wider variations and oscillations during acceleration, and each term can be expected to reach a peak approximately twice that represented by the individual terms in Eq. (21). Although these peaks will not occur at the same energies, a rough upper limit to the maximum distortion is given by twice the result in Eq. (21), namely,

\[
\frac{\delta A(s)}{A(0)} \left[ \frac{1}{2k - k_a} + \frac{1}{2k + k_a} \right] \left[ \frac{g^2}{3} + \frac{k_a^2}{2k - k_a} - 1 \right].
\]

III. Comparison with Orbit Computations

Computations have been performed\(^6,7\) to determine the seriousness of the transverse beam growth due to coupling with the longitudinal oscillations.\(^8\) Comparisons have been made, essentially with the forms in Equations (17) and (18) with the following conclusions:

1) The main contribution to the effect comes from the first term in Eq. (17), as expressed in Eq. (19). For \( k_t \) and \( k_a \) equal at the start of acceleration, \( x_0 = \pi/2 \) and \( x_0 \sim 30^\circ \), Eq. (19)
predicts a 15% increase in amplitude at 
$s = 0$ and a 30% increase at some inter-
mediate value of $s$, according to Eq. (22). 
This is the order of magnitude of the ef-
fect observed.

2) A Fourier analysis of the distor-
tion in the variable $a_k$ leads to excel-
 lent agreement with the two terms in 
Eq. (17). (The second term is roughly 
$1/3$ of the first.) The agreement with 
Eq. (18) is not quite so good, primarily 
because of the difficulty in assigning 
an accurate value to $2k_t - 2k_1$ in the 
presence of the highly nonlinear and 
coupled oscillations. The order of mag-
nitude and sign of this term, however, 
appear to be correctly given by Eq. (18).

3) The longitudinal wave number de-
creases more rapidly than the transverse 
wave number. In those designs where $k_t$
starts out below $k_1$, the two become 
equal at some intermediate value of $s$ and 
the analysis in Section II is no longer 
applicable. Reference 3 contains a treatment 
of the resonant behavior for an assumed 
variation of $k_t$ and $k_1$ and indicates the 
magnitude of Eq. (18) should be increased 
by a large factor if resonance takes 
place shortly after the start of accel-
eration. Even in those cases where re-
sonance does not occur, the rapid varia-
tion of $k_t$ - $k_1$ with $s$ makes the result 
in Eq. (18) only approximate. For these 
reasons the magnitude and phase of the 
term proportional to $x_6$ is used as 
parameters in fitting the computations. 
Indications are that the term in Eq. (18) 
depends sensitively on the starting value 
of $k_1$ in the design of the transverse 
 focusing system, but that it is not as 
important as the first term in Eq. (17).

IV. Application of Liouville's Theorem

In the course of numerical computa-
tions,7 to ascertain the seriousness of 
the transverse amplitude growths, it was noticed that the two-dimensional 
transverse projection of the four- or 
six-dimensional phase space did not 
exactly satisfy conservation of phase-
space area. For a distribution in all 
phase-space directions, this is not sur-
prising and is just the effect predicted 
in Equations (17) and (18). For a 
single starting point in longitudinal 
phase, however, the transverse area 
appeared to fluctuate by several percent.

The first order (in $x_6^2$) results in 
Equations (17) and (18) vanish if one 
averages over all values of $a_k$ for fixed 
$a_1$. It now appears that higher order 
effects modify this conclusion. This 
section is therefore a re-examination of 
the conditions which apply in general 
and the extent to which the new notions 
affect the choice of beam aperture.

The basic coupled equations for the 
motion in the longitudinal and one trans-
verse direction are given in Equations 
(1) and (2). The following conclusions 
are apparent from these equations:

1) For uncoupled motion all two-
dimensional space trajectories are circles 
(ellipses) of constant area. The pro-
dected phase-space areas are obviously 
conserved.

2) If the right sides of Equations 
(1) and (2) are approximated by using the 
uncoupled values of $y$ and $x$, the indi-
vidual phase-space areas are distorted 
but retain their original values. How-
ever, the distortions depend on the ini-
tial values of the oscillations and for a 
distribution of initial values there will be an apparent increase in the pro-
dected phase-space area. This is the 
situation discussed previously, and 
treated in Section II.

3) If the uncoupled solution for $x$ 
is used in Eq. (1), one obtains the 
equivalent homogeneous equation

\[ \frac{d}{ds} \left( s \cdot \frac{dy}{ds} - s \cdot y \frac{q_2}{s} \right) = 0 \]  

(23)

where $q_2$ is a known function of $s$. Once 
again phase-space area must be conserved 
in a particular two-dimensional projec-
tion for a point in the other projections. 
(The determinant of the infinitesimal 
transformation is still 1.)

4) If one includes in the $x$ on the 
right side of Eq. (1) that part of the 
solution of Eq. (2) which depends on $y$, 
the arguments which lead to conservation 
of area no longer apply. It is this 
case which is explored now in greater 
detail.

It is clear from Equations (17) and 
(18) that, to first order in $y_0$, the 
change in transverse phase-space area 
vanishes. In order to see whether this 
is true to second order in $y_0$, it is 
necessary to perform a more careful in-
tegration of Equations (1), (2). We 
shall, however, accomplish this same goal 
by using the fact that the sum of the 
phase-space projections in the transverse 
and longitudinal projections remains con-
stant.16 The longitudinal projection can 
more easily be calculated to second order 
since it starts as a point at $s = 0$. In 
fact one can just solve Eq. (13) to the 
order shown to obtain the desired area 
change.
As in Section II, we shall include all first order (in $x_0$) terms and only those second order terms which are important for $k_t$ almost equal to $k_l$. The terms in Eq. (15) which persist at $s = \infty$, and which lead to a distortion from a point to an ellipse, are the last two. The terms on the right side of Eq. (13) which contribute for $k_l$, near $k_l$ include the $\cos (t - \phi)$ term of $y(1)$ from Eq. (14) and the $\cos 2t$ term of $x(1)$ from Eq. (15). After considerable algebra, one finds that the point in longitudinal phase space has become an ellipse of major and minor axes given by

$$
\pi y_0^2 k_l^3 \frac{(k_l + k_t)}{4k_t^2 - k_l^2} \left\{ \frac{g}{2k_t - k_l} - \frac{1}{2} \right\}
$$

This ellipse is actually traversed twice as $t$ goes from 0 to $2\pi$. One therefore uses the Poincare Invariant \(^{10}\) to obtain

$$\delta \text{Area}(t) = -2 \delta \text{Area}(t)$$

and finally

$$\frac{\delta \text{Area}(t)}{\text{Area}(t)} = -\frac{k_l^3 \pi y_0^2}{32k_t (8\pi \lambda)} \left\{ \frac{g}{2k_t - k_l} - \frac{1}{2} \right\}
$$

$$- \frac{1}{2} \frac{x_0 e^{2} g^2 k_l (k_l + k_t)}{4k_t^2 - k_l^2} \left\{ \frac{g}{2k_t - k_l} - \frac{1}{2} \right\}
$$

Equation (26) expresses the decrease in transverse phase-space area for a fixed starting point in longitudinal phase and a "matched" beam in transverse phase space. This must be included with any apparent increase in phase-space area due to a distribution of points in longitudinal phase space. It should be noted that Eq. (26) predicts an area change even in the absence of longitudinal oscillation, a phenomenon observed in the numerical results. However, this area change appears to be substantially smaller than that due to the distortions discussed in Section II, and is primarily of academic interest only.

Numerical computations \(^{6,7,9}\) illustrate the area changes discussed here, although precise agreement has not been obtained for the term proportional to $x_0$. Nevertheless the transverse area does decrease by the order of magnitude specified in Eq. (26), and the effect is clearly proportional to the square of the transverse displacement. Precise agreement is not expected because of:

1) The possibility of contribution of terms for $j \geq 3$, and of terms of higher order in $x_0$.

2) The fact that the values of $k_l$, $k_t$ used in the denominators of Eq. (26) should be those appropriate to the actual longitudinal and transverse oscillations, not the linearized version appropriate to $x_0 = 0$, $y_0 = 0$.

3) The possibility of contributions from resonances of the form $2k_t = jk_l$.

4) The limited accuracy of the numerical calculations.

One last point should be discussed. Courant \(^{11}\) has shown that a coupled dynamical system satisfying certain conditions \(^{12}\) conserves the area of its two-dimensional projections along particular axes. In the uncoupled case these are the normal axes for the separate coordinates. In the coupled case these special axes are linear combinations of the longitudinal and transverse coordinates. The conclusions in this note, applying only to the simple coordinate axes, are therefore not in violation of the theorem proved by Courant.

V. Summary and Conclusions

1) Coupling of the longitudinal and transverse motion takes place through the phase dependence of the rf defocusing
force and the radial dependence of the longitudinal transit time factor. Both of these effects arise from the same term in the Lagrangian.

2) The coupling forces decrease rapidly with increasing $s$. Consequently the seriousness of the effect depends primarily on the parameters at the start of acceleration.

3) The main contribution to the growth in transverse dimension (and phase-space area) comes from the first coupling term in Equations (1) and (2). The prediction is for an amplitude increase

$$\Delta a(t) = \frac{k_z^2 \cot |\phi|}{2(4k_t^2 - k_z^2)} x_0$$  \hfill (27)

at the end of acceleration (actually this increase takes place within the first 10 MeV of acceleration). The growth will be approximately twice as large in the course of reaching the final value in Eq. (27).

4) For comparable $k_z$ and $k_t$, at the start of acceleration, Eq. (27) predicts a 15 - 20% transverse amplitude increase, and a 30 - 45% increase in transverse emittance. The effect increases for lower $k_t$ (weaker transverse focusing) and suggests transverse focusing designs which make $k_t$ as large as possible at injection.

5) The effect of that part of the second coupling term which dominates for small $2k_t - 2k_z$ has also been taken into account, and the result is given in Eq. (18). Numerical computations of orbits indicates that Eq. (18) overestimates the effect. The following considerations are relevant, however:

a) For small $2k_t - 2k_z$, one should use a resonant treatment, which leads to a finite result at $k_t = k_z$.

b) Equation (18) is sensitive to the actual values of $k_t$ and $k_z$ used. For nonlinear coupled oscillations these will be different enough from the linear uncoupled values to make the prediction of Eq. (18) uncertain.

c) There will also be contributions of order $x_0^2$ and higher which have been omitted here, but which can be important.

In spite of these uncertainties, Eq. (18) does predict a contribution to the distortion which has been observed in the numerical computations to be of the same sign and order of magnitude as predicted.

6) If one considers a collection of starting points in phase space, each having the same $x_0$, $y_0$, but with different $a_t$, the transverse phase-space area can change. This change (usually a decrease in transverse area) is relatively small and unimportant compared to the distortion, but it does not violate Liouville's Theorem. Analytic results for this area change are given in Eq. (26)

VI. Acknowledgments

The author would like to acknowledge several helpful conversations with Drs. R. Chasman and E. D. Courant of BNL, S. Ohnuma of Yale, and D. Swenson of LASL.

References

6. Private communication from R. Chasman, BNL; S. Ohnuma, Yale.
7. Private communication from D. Swenson, LASL.
8. In Equations (1), (2), $\phi$ is taken to be the momentum of the synchronous particle. The derivation of these equations requires changing variables in the Lagrangian from $y, y', z, z'$ to $y, y', x, x', s$ where

$$t = \int_0^s \frac{ds}{v_s^2}, \quad z = s.$$

This transformation is similar to that discussed in Reference 1, and actually leads to additional terms on the right side of Equations (1) and (2), whose origin is the difference between the actual and synchronous momenta. These terms can safely be neglected in the present application, being of relative order the square of the ratio of cell
length (SA) to oscillation wavelength $(2\pi/k_f)$.

9. These were described in greater detail in reports at the LASL Linear Accelerator Conference, October 3-7, 1966.

10. See, for example, L. Goldstein, "Classical Mechanics," p. 247ff, 1st edition, Addison-Wesley Publishing Co. By use of the Poincare Invariants, Goldstein shows that, in a Hamiltonian system, the quantity

$$\sum \int \int dp_i dq_i$$

is an invariant if the surface $S$, bounded by a closed curve, is allowed to move with the points in phase space. The individual terms in the sum over $i$ are the projections, if one takes into account the sign and multiplicity of the contributions.

11. E. D. Courant, private communication. The author is grateful to Dr. Courant for calling his attention to this point.

12. Hamiltonian system, with the motion given by a linear transformation matrix which is symplectic.

* Supported in part by the NSF and AEC.

This paper is also being issued as BNL Internal Report AADD-120 Sept. 1966.