

## High-Q Operation of SRF Cavities:

# The Impact of Thermocurrents on the RF Surface Resistance

*J. Vogt, O. Kugeler, J. Knobloch, Phys. Rev. ST Accel. Beams 18, 042001 (2015)*

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Helmholtz-Zentrum Berlin

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## Why bother?

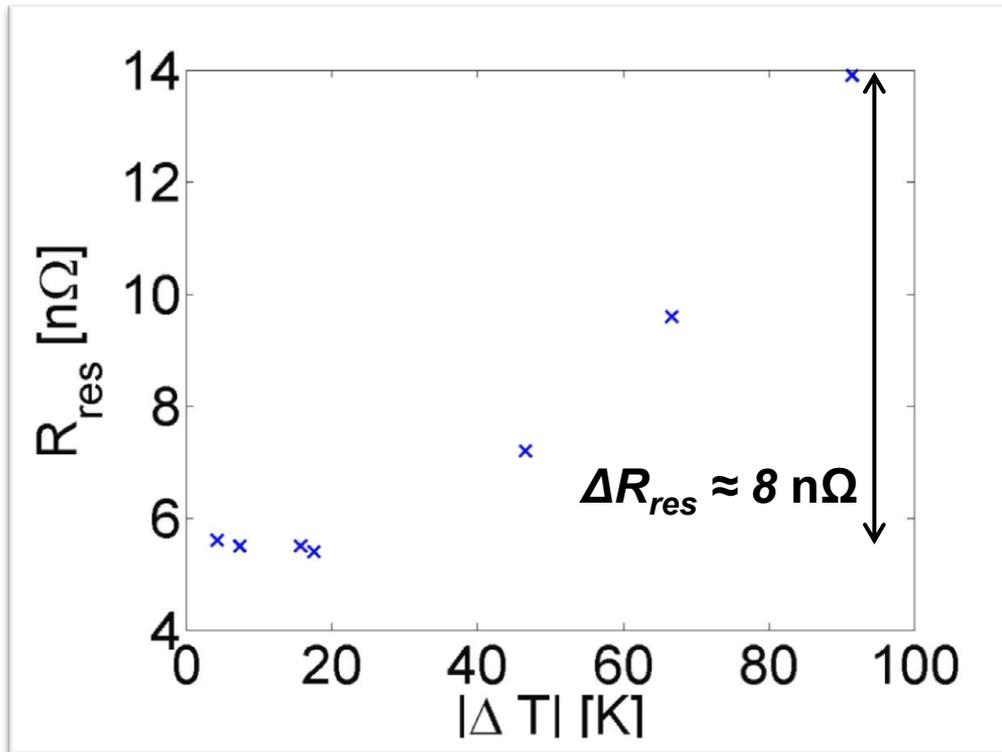
- Demand for high duty cycle or **cw beams** in modern application (LCLS-II, XFEL, bERLinPro...)
- Elevated **dynamic losses**
- Refrigeration efficiency  $\approx 1/1000$ 
  - **Minimization of power loss and costs**
- BCS resistance decreases with temperature, residual resistance not
- General interest in understanding loss mechanisms in sc cavities



bERLinPro

## Status SRF 2013:

Cooling conditions and thermal cycle can significantly impact and degrade the quality factor



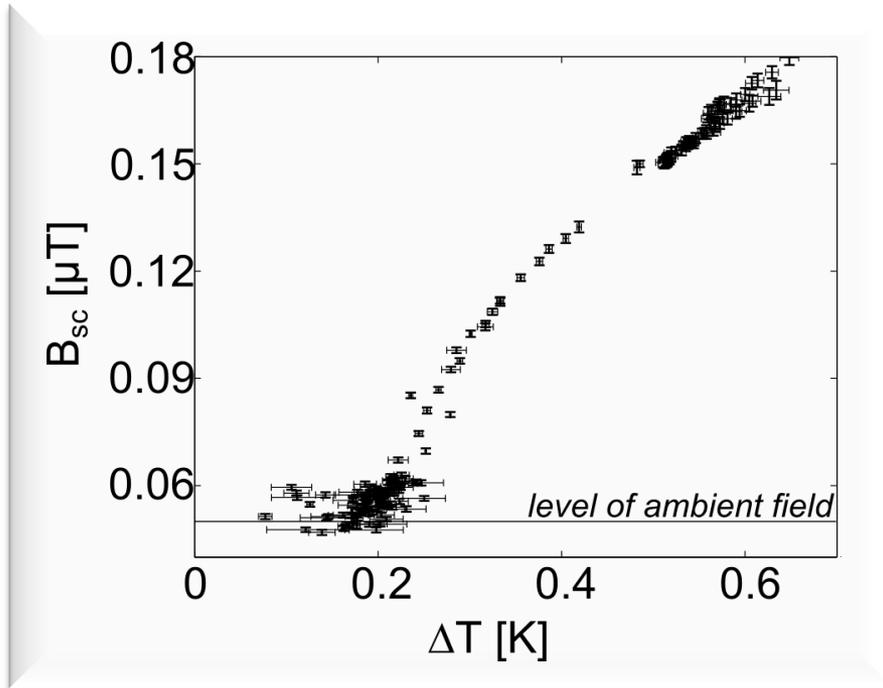
- Thermal cycle can decrease as well as increase the residual surface resistance (low ambient magnetic field)

*O. Kugeler et al.,*

*"Influence of the Cooldown at the Transition Temperature on the SRF Cavity Quality Factor", SRF'13, Paris, France, p. 370 (2013)*

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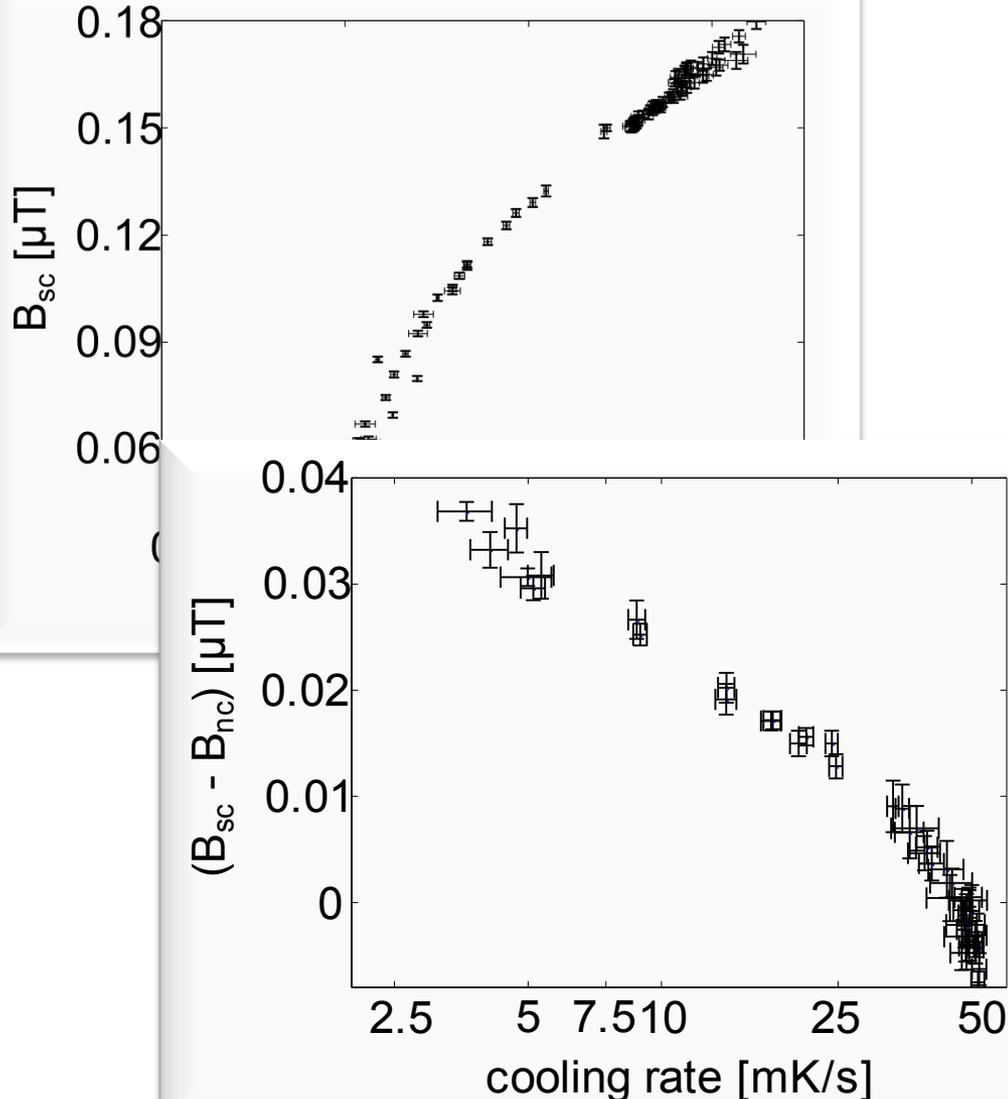
- Sample test indicate major impact of cooling dynamics (gradient/rate) on flux expulsion

*J.M. Vogt et al.,*

*"High Q0 Research: The Dynamics of Flux Trapping in Superconducting Niobium", SRF'13, Paris, France, p. 374 (2013)*

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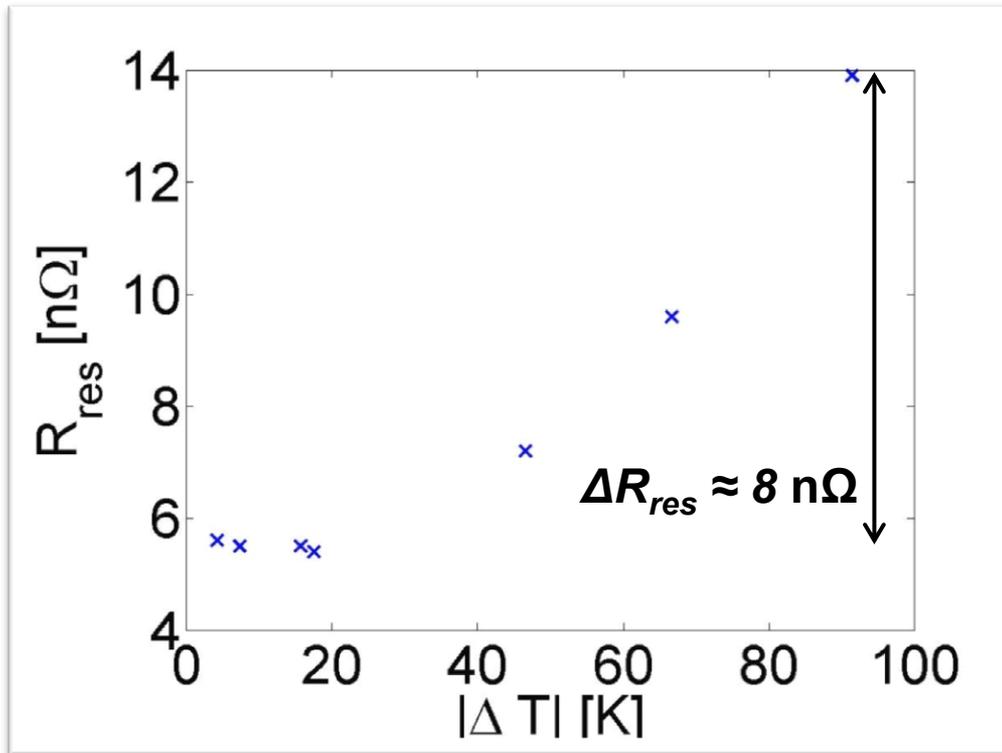
Thermocurrents

Flux expulsion

*Aull et al., PRSTAB 15, 062001 (2012)*

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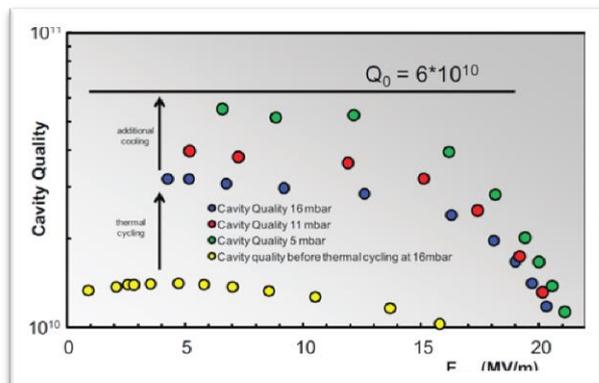
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- First reported 2009

*O. Kugeler et al.,*

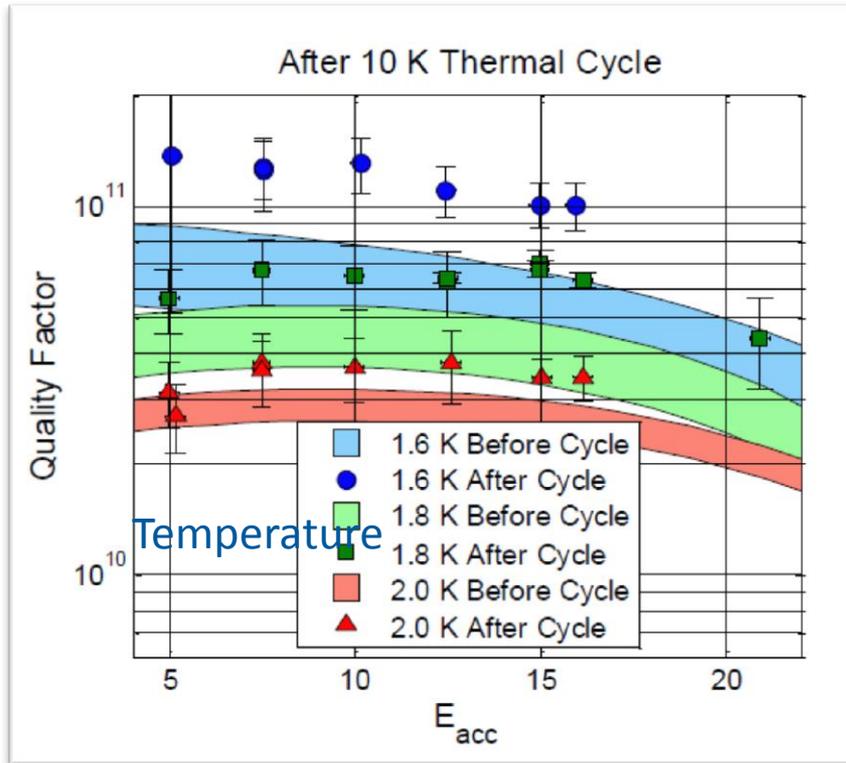
*"Manipulating the intrinsic quality factor by thermal cycling and magnetic fields", SRF'09, Berlin, Germany, p. 352 (2009)*

## Status SRF 2013:

Cooling conditions can significantly impact and degrade the quality factor

Cornell confirmed: Thermal cycle improves Q

Courtesy R. Eichhorn



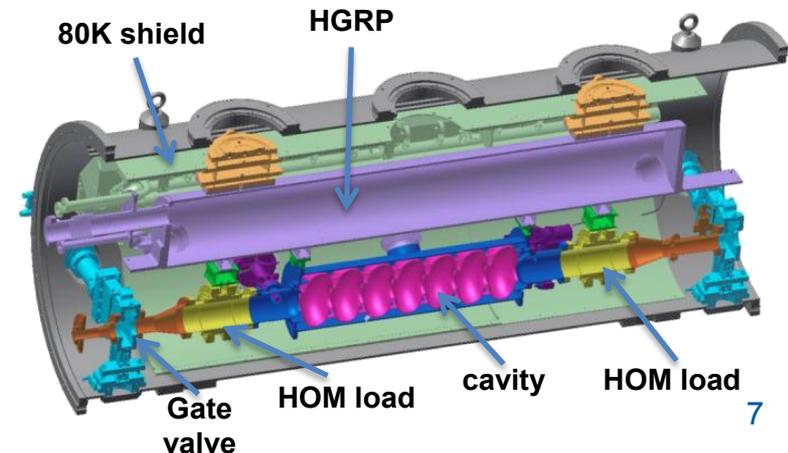
Temperature

Time

- After a 10 K thermal cycle significant increase in the Q (up to a Q of  $6 \cdot 10^{10}$  design operation parameters being three times higher than targeted)
- measurements suggest that effect is related to magnetic fields

G.R. Eichhorn et al.,

"High Q Cavities for the Cornell ERL Main Linac",  
SRF'13, Paris, France, p. 844 (2013)



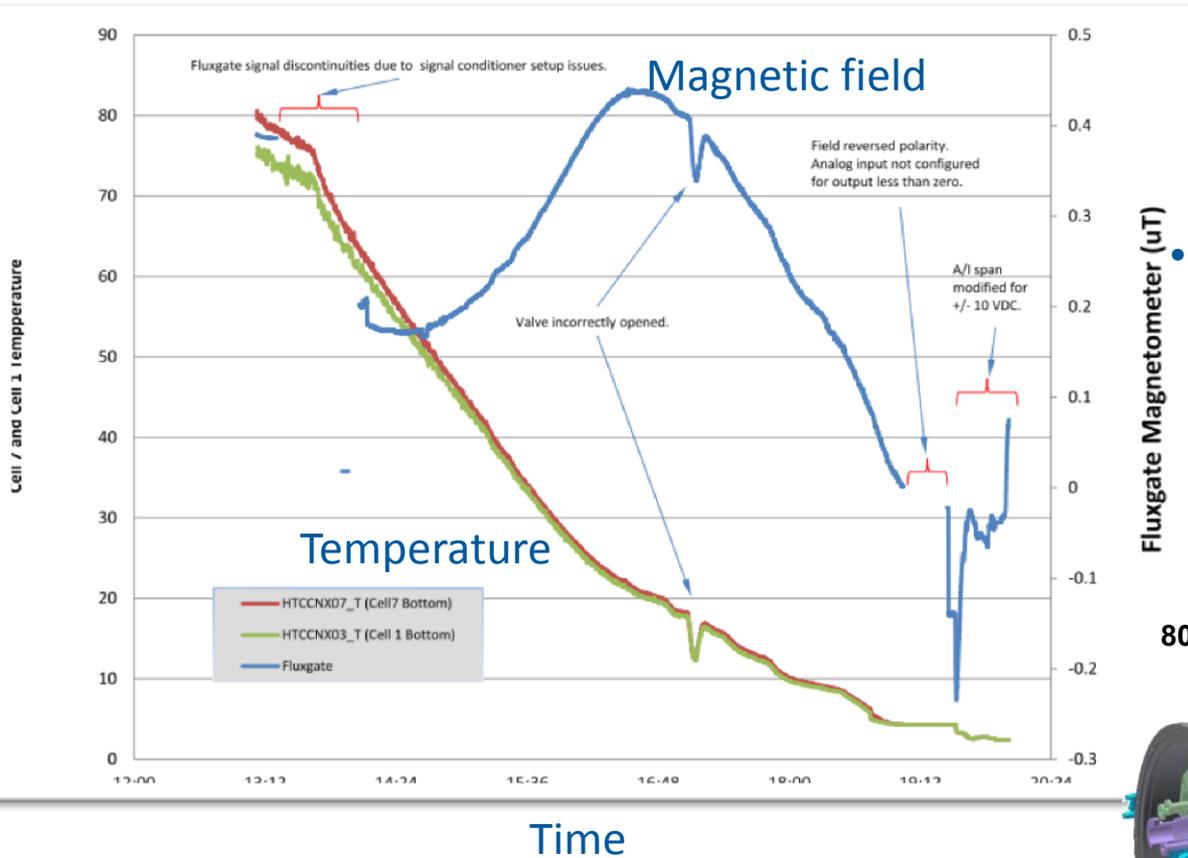
Remark: only one flux direction was measured

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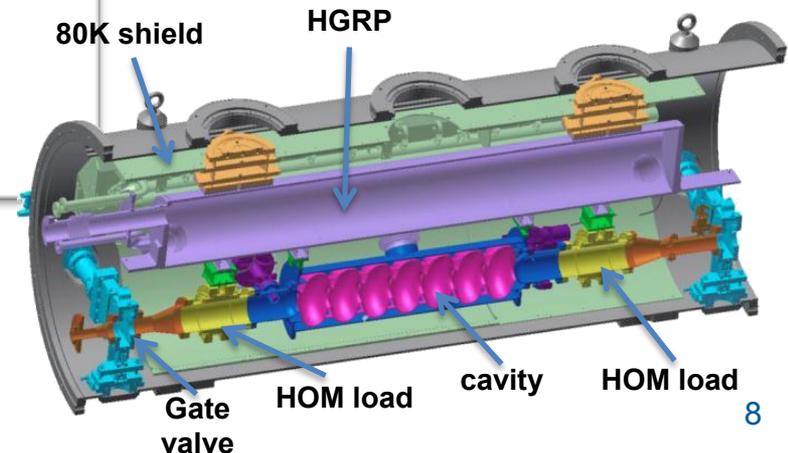
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**Open questions:**

1. More detailed study of the impact of **temperature difference** on the **surface resistance**
2. Exact **Seebeck coefficients** in the temperature regime of interest to analyze magnitude of thermocurrents
3. **Geometry and distribution** of thermocurrents
4. Direct measurement of the **magnetic field** in the cavity tank system and **especially** on RF surface

# 1. More detailed study of the impact of temperature difference on the surface resistance

$$R_S(T) = \underbrace{A \cdot \exp\left(\frac{-B}{T}\right)}_{\text{BCS resistance}} + \underbrace{R_{\text{res}}}_{\text{Depends on amount of trapped flux}} = G/Q_0$$

$G_{\pi} = 271.2 \Omega$   
 $G_{8\pi/9} = 271.5 \Omega$   
 $G_{\pi/9} = 268.3 \Omega$   
 $A = (31.8 \pm 2.2) \mu\Omega$   
 $B = (15.7 \pm 0.2) K$

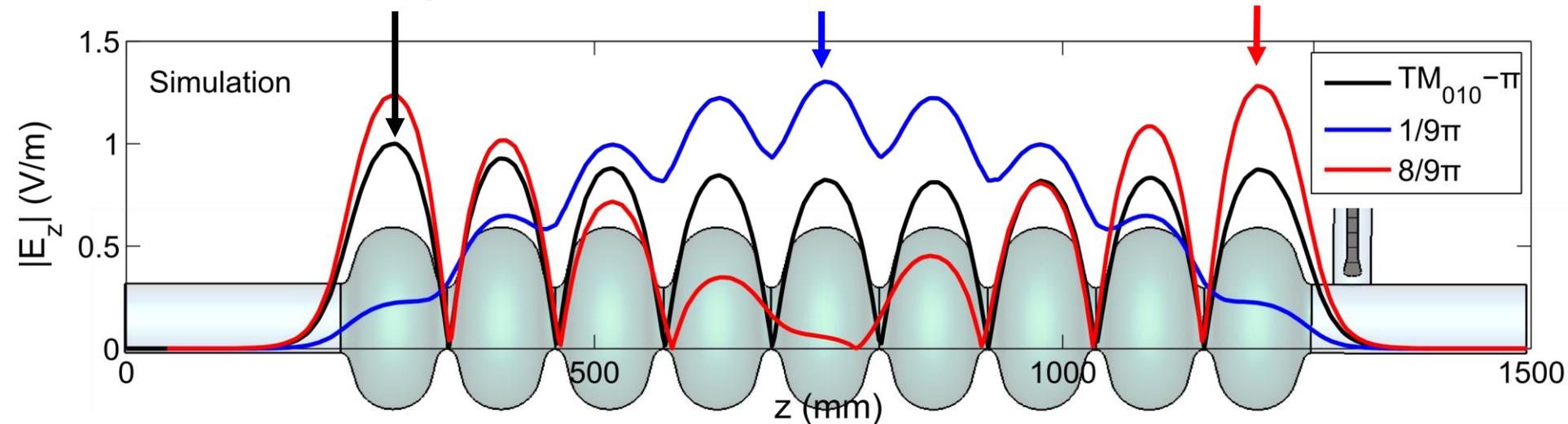
BCS resistance is the same for all modes (at fixed  $E_{\text{acc}}$ ), depends on T

Depends on amount of trapped flux but not on T

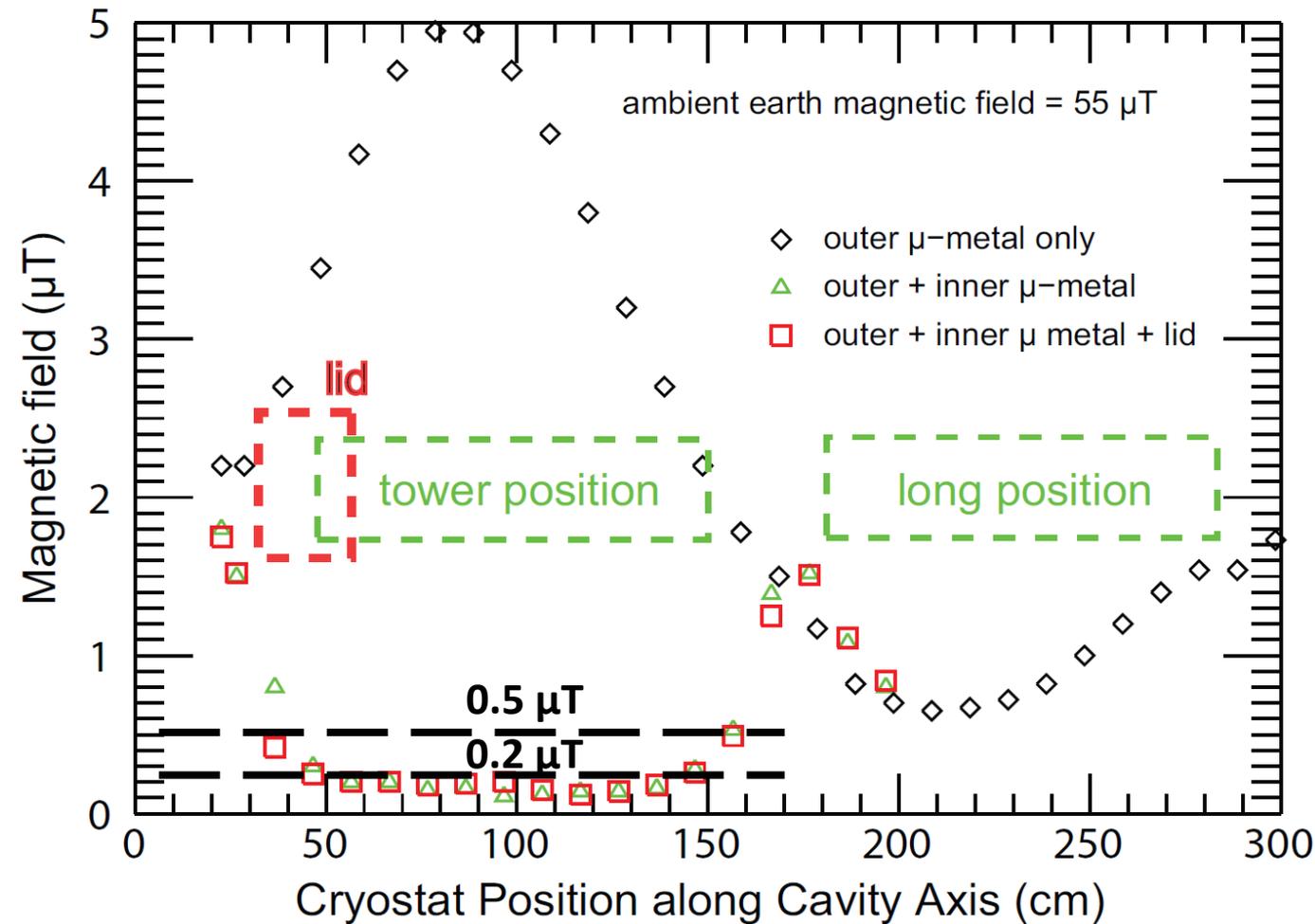
“accelerating mode”

“mid cell mode”

“end cell mode”



# 1. More detailed study of the impact of temperature difference on the surface resistance



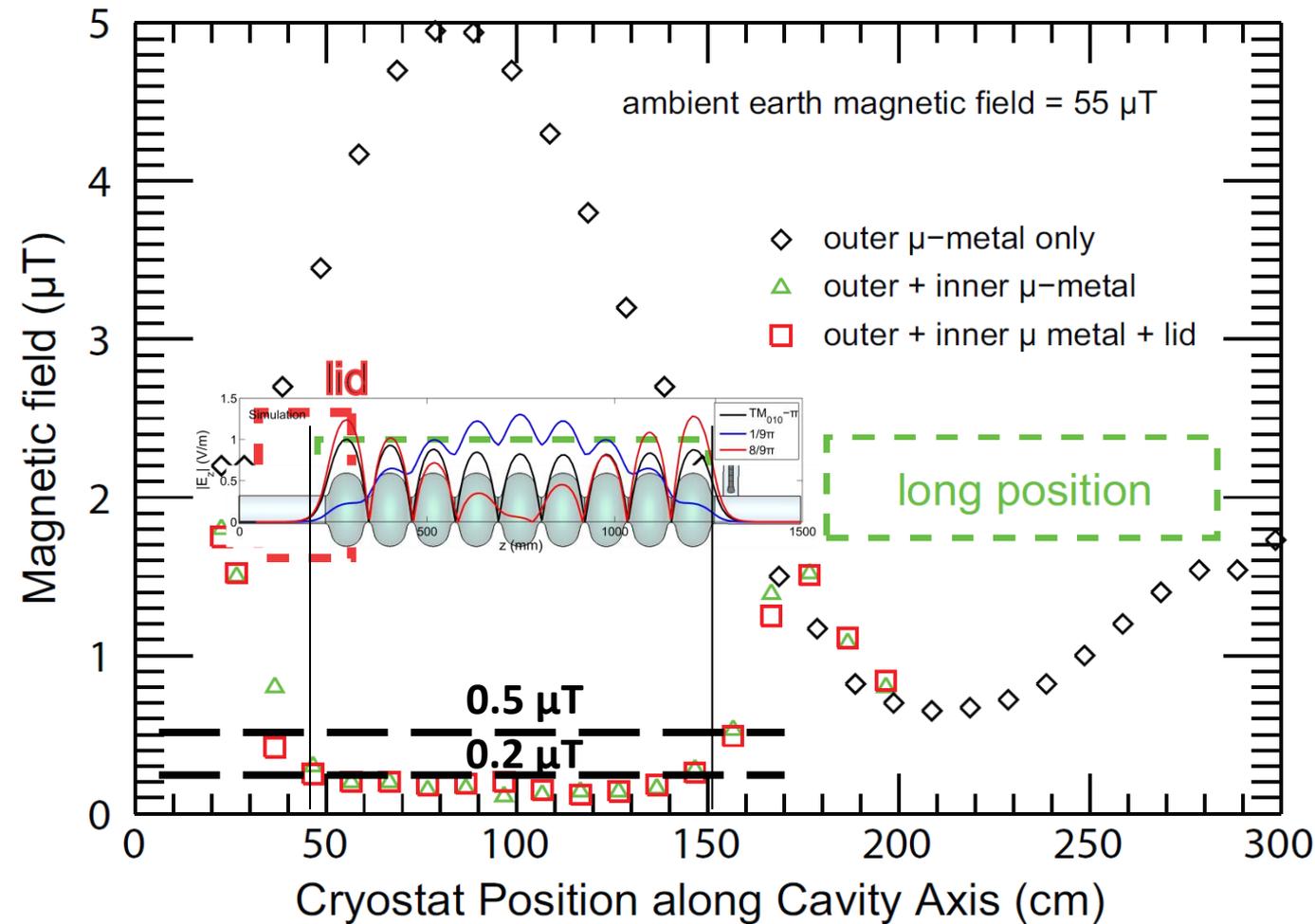
Ambient field in the HoBiCaT cryostat:

- less than 0.2  $\mu\text{T}$  at the center cells
- about 0.5  $\mu\text{T}$  maximum in the end cells



Evaluation of  $\langle R_{\text{res}} \rangle$  and hence **the change in trapped flux** in different cells of the cavity

# 1. More detailed study of the impact of temperature difference on the surface resistance



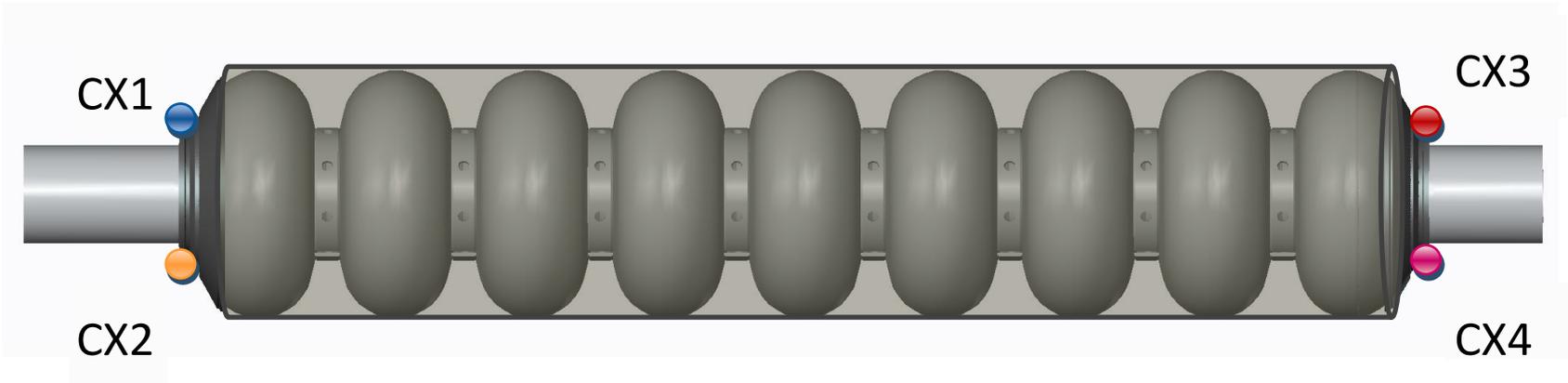
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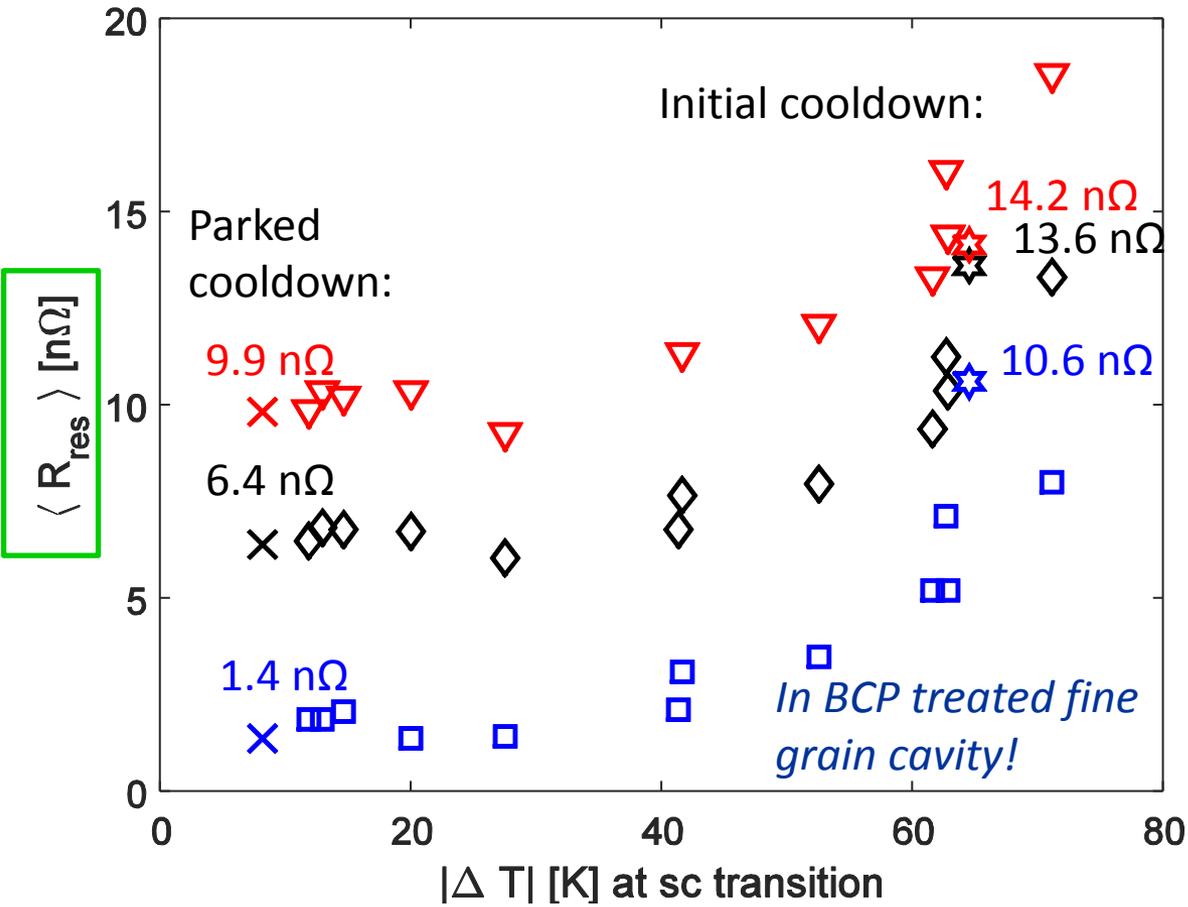
- Temperature difference at the start of the phase transition:

$$\Delta T = \left| \frac{T_{Cx1} + T_{Cx2}}{2} - \frac{T_{Cx3} + T_{Cx4}}{2} \right| \quad \text{when the first sensor drops below 9.2K}$$

- Drives thermoelectric current through the system

# 1. More detailed study of the impact of temperature difference on the surface resistance

$$R_S(T) = A \cdot \exp\left(\frac{-B}{T}\right) + R_{\text{res}}$$

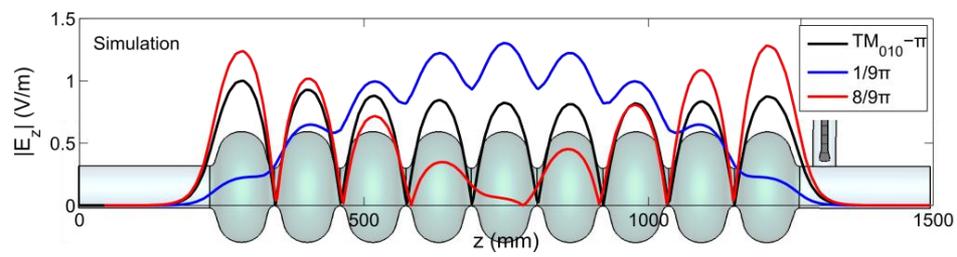


8/9  $\pi$  mode

$\pi$  mode

1/9  $\pi$  mode

A smaller temperature difference (10 - 30K) reduces the RF losses significantly. Even when cooled down from room temperature, low residual resistance is achievable when the cavity is parked above  $T_c$  for several hours (here 48h).

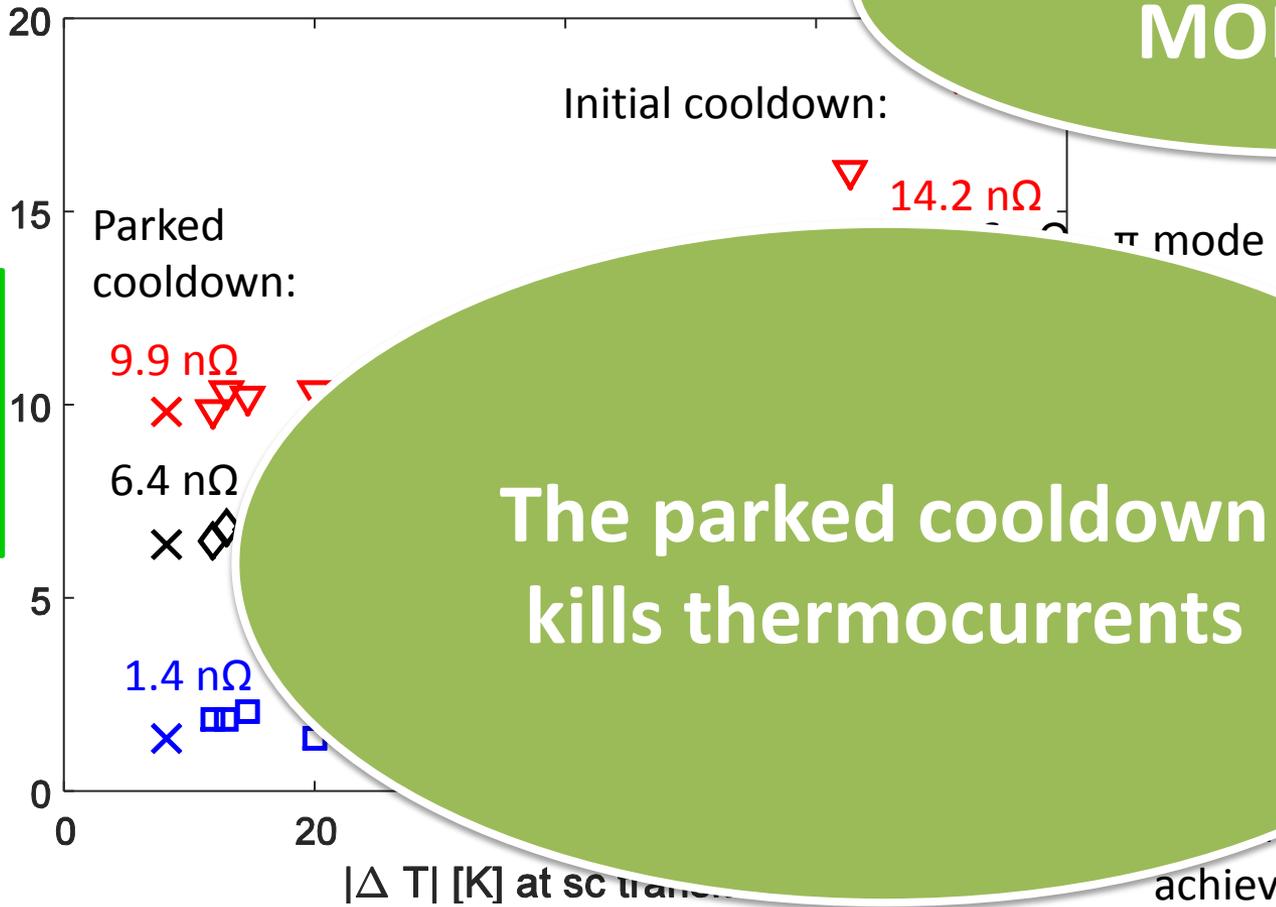


Mark: all modes are mirror symmetric

1. More detailed study of the impact of the surface resistance

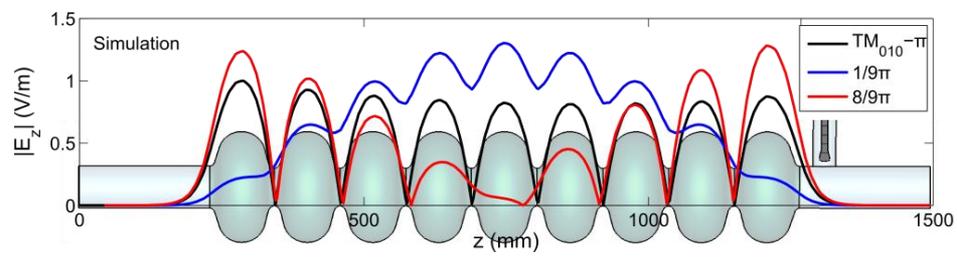
See poster MOPB017

$\langle R_{res} \rangle$  [nΩ]



The parked cooldown kills thermocurrents

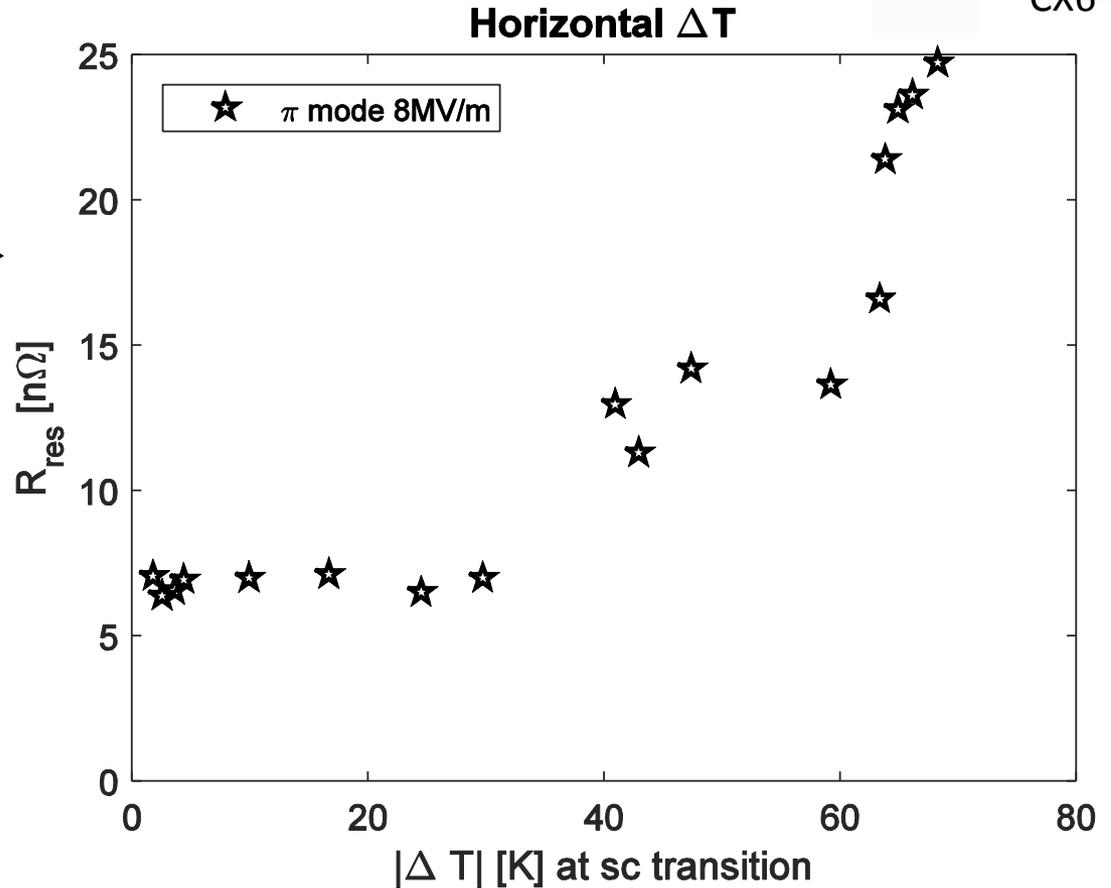
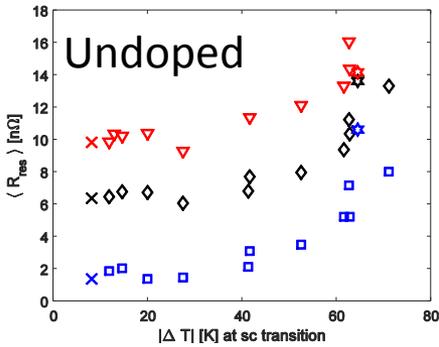
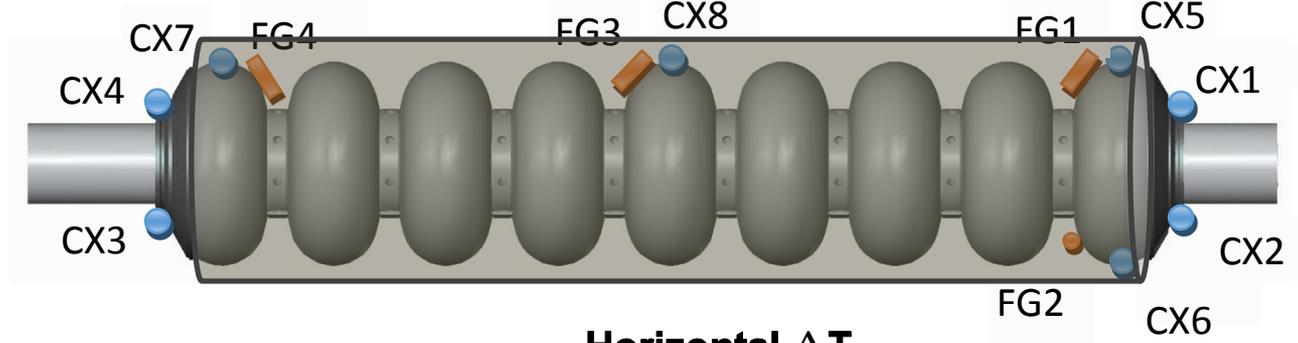
temperature (K) reduces significantly. Cooled down to low temperature, low surface resistance is achievable when the cavity is parked above  $T_c$  for several hours (here 48h).



Mark: all modes are mirror symmetric

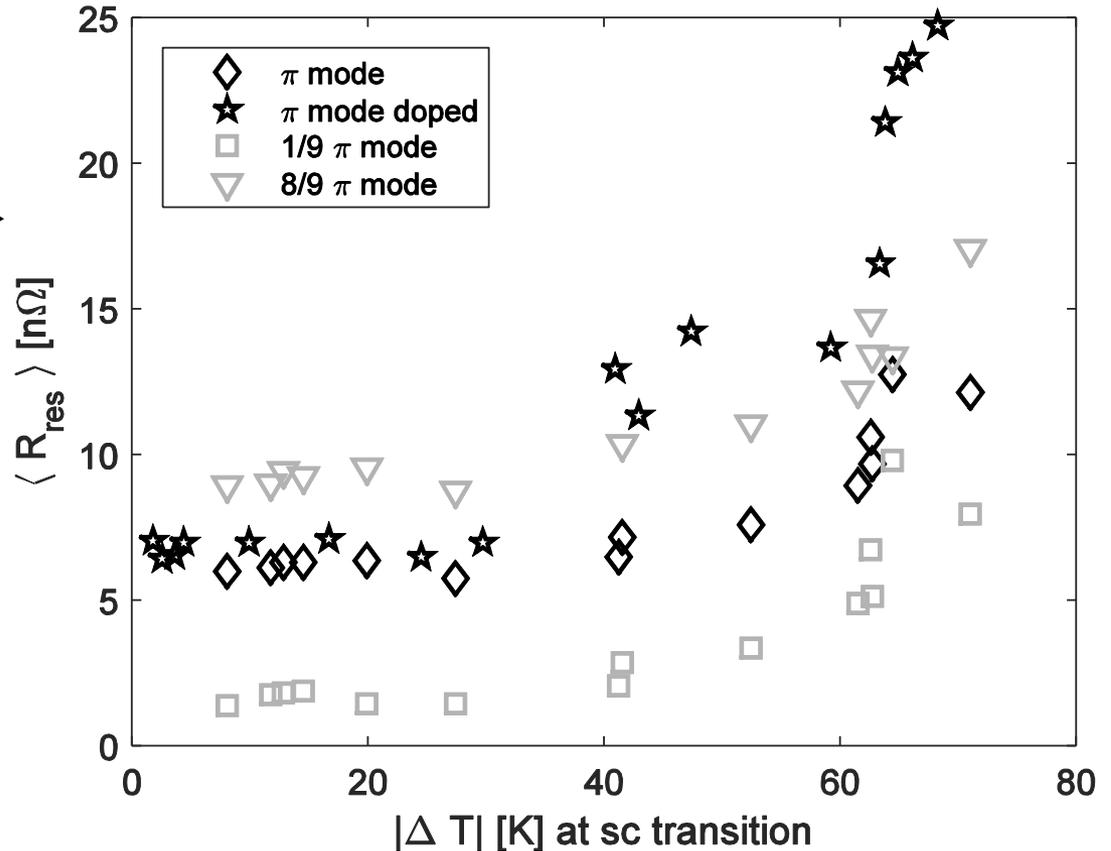
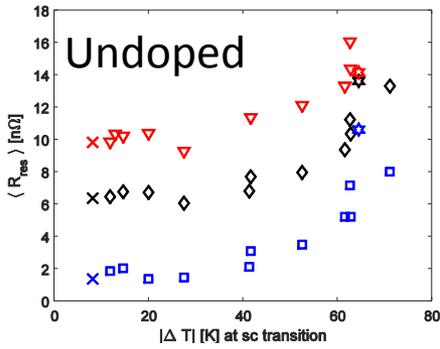
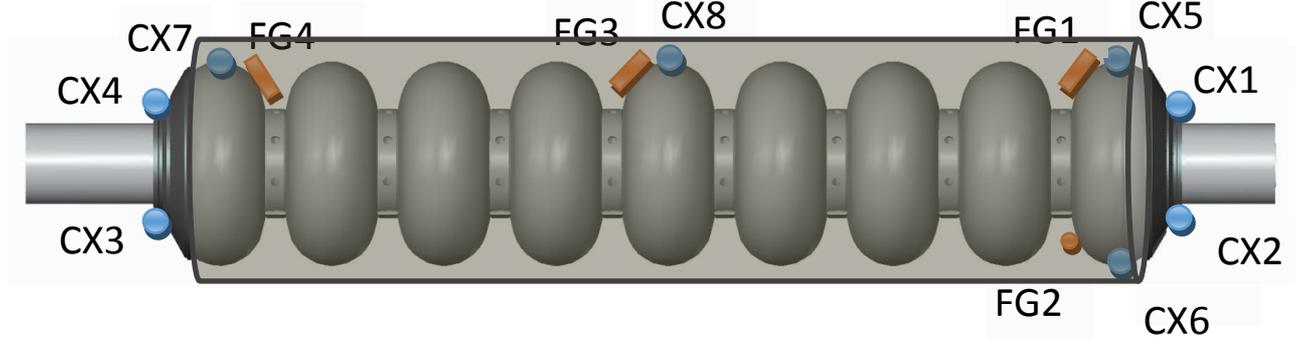
# Additional question: How does it apply to a doped cavity?

Doped cavity at Fermilab:  
60min N doping  
with 10 $\mu$ m final EP



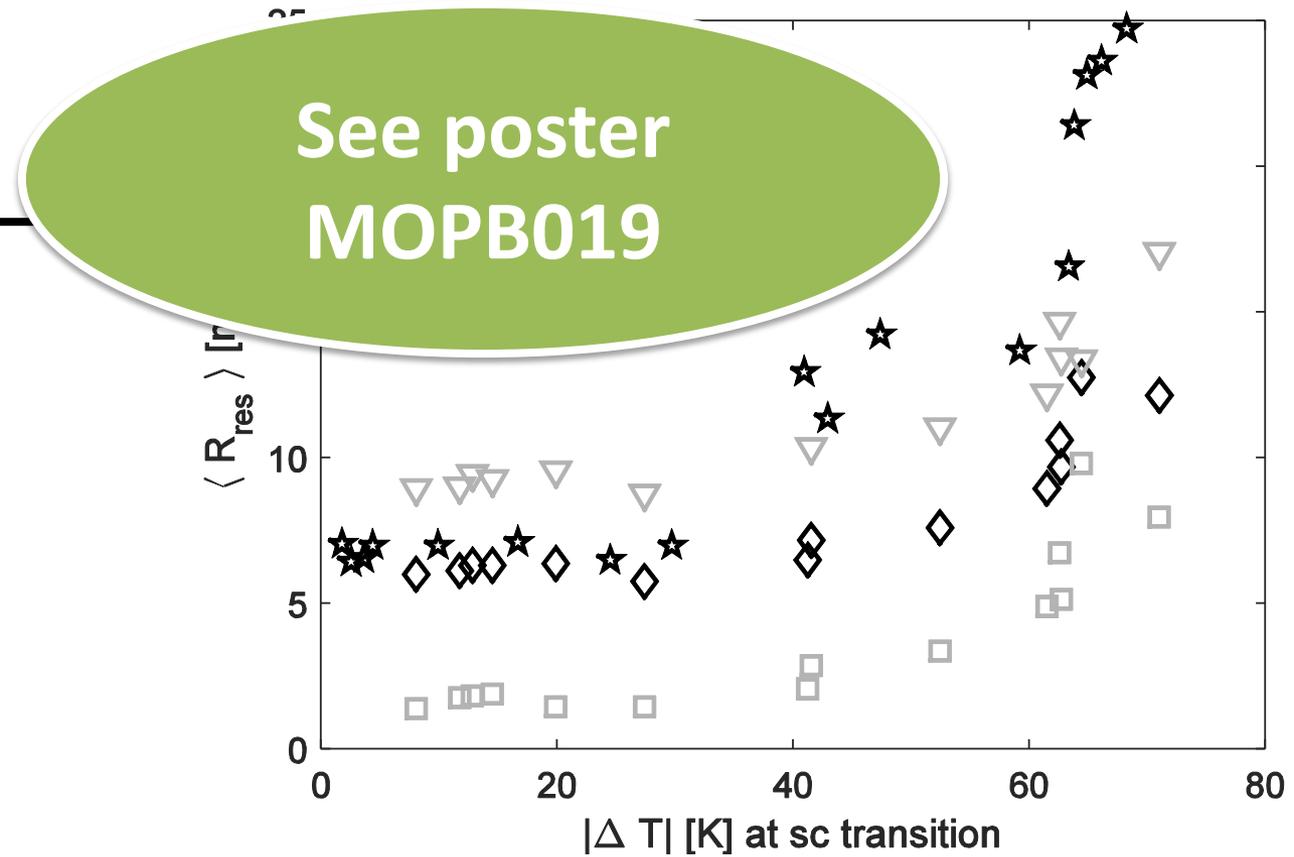
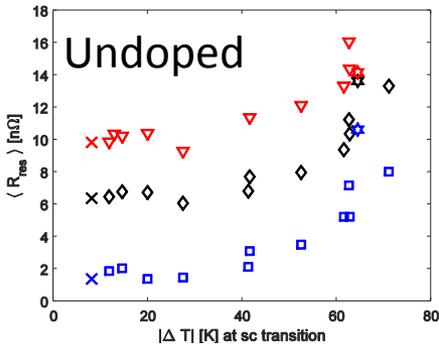
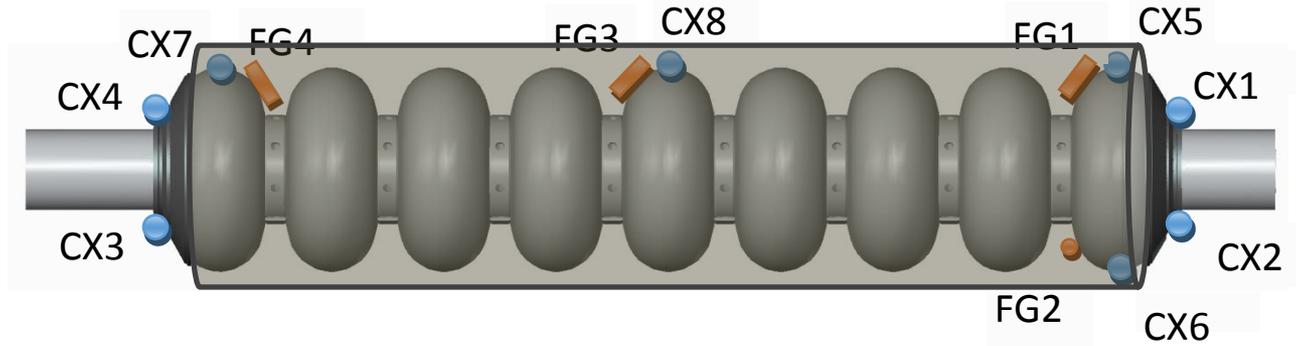
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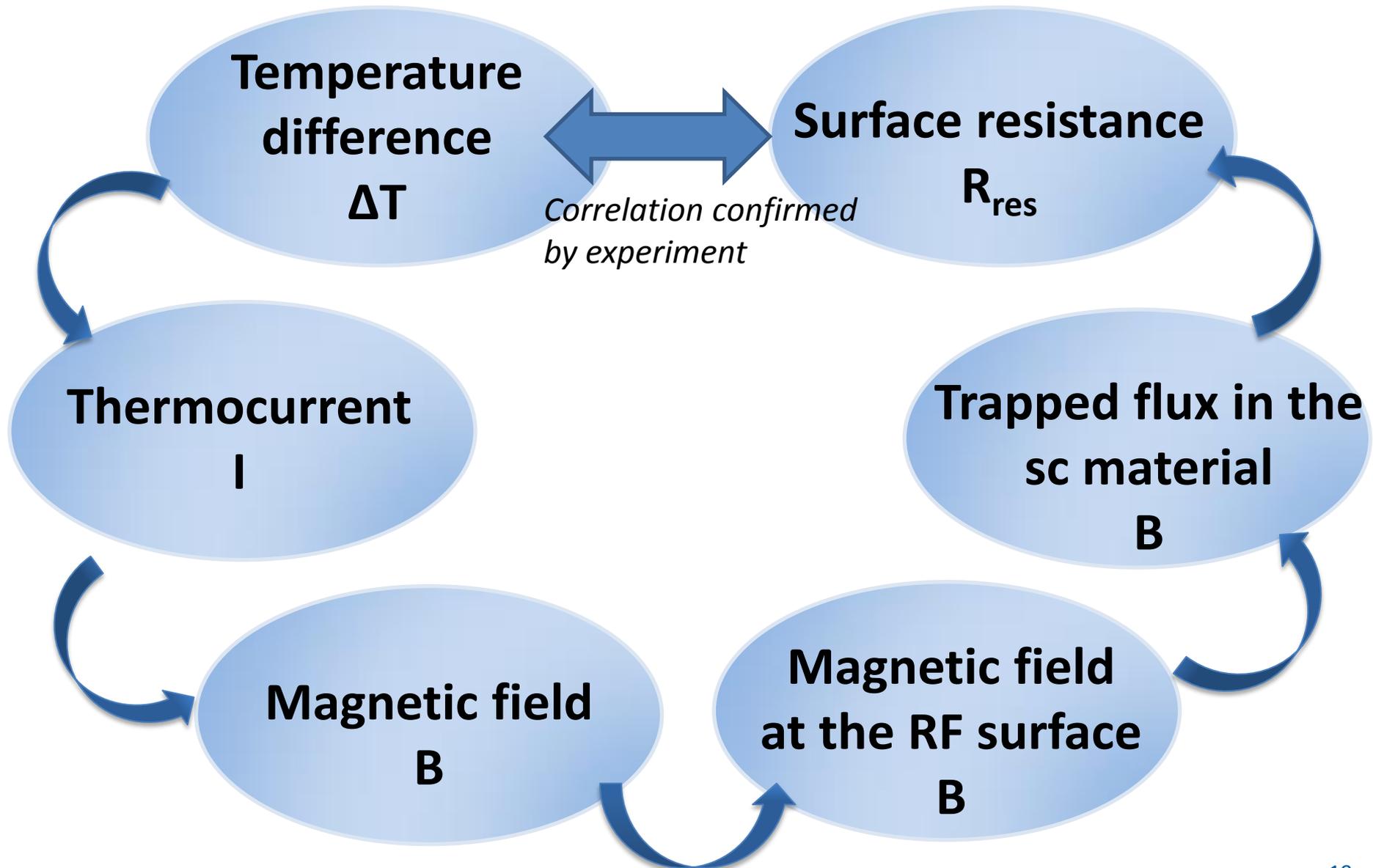


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Doped cavity at Fermilab:  
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## How can we validate the thermocurrent hypothesis?



# How can we validate the thermocurrent hypothesis?

**Temperature difference**

**Surface resistance**

$R_{res}$

*Correlation confirmed by experiment*

2. Exact Seebeck coefficients in the temperature regime of interest

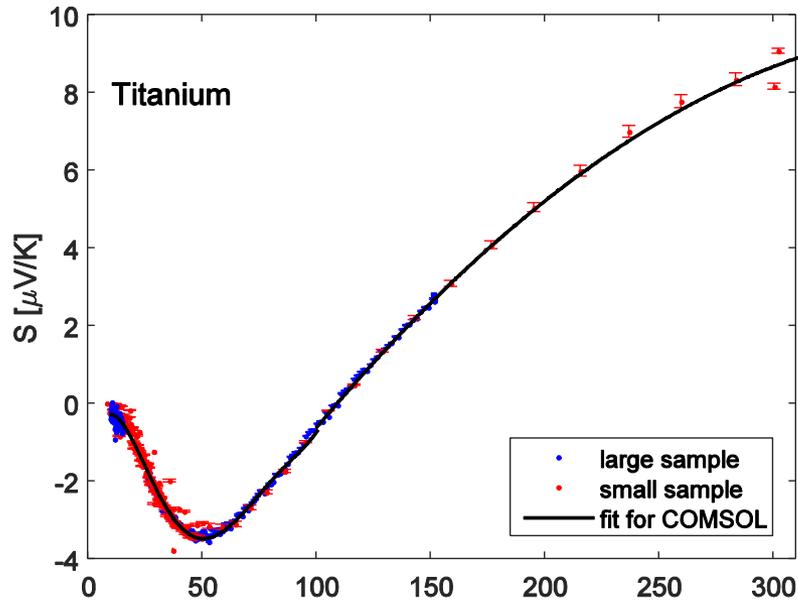
**Thermocurrent**  
**I**

**Trapped flux in the sc material**  
**B**

**Magnetic field**  
**B**

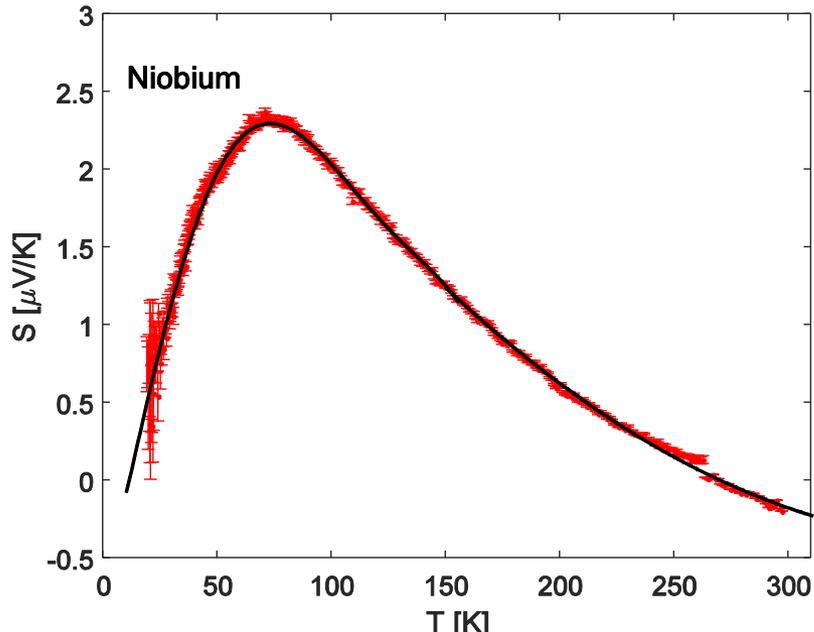
**Magnetic field at the RF surface**  
**B**

## 2. Exact Seebeck coefficients in the temperature regime of interest

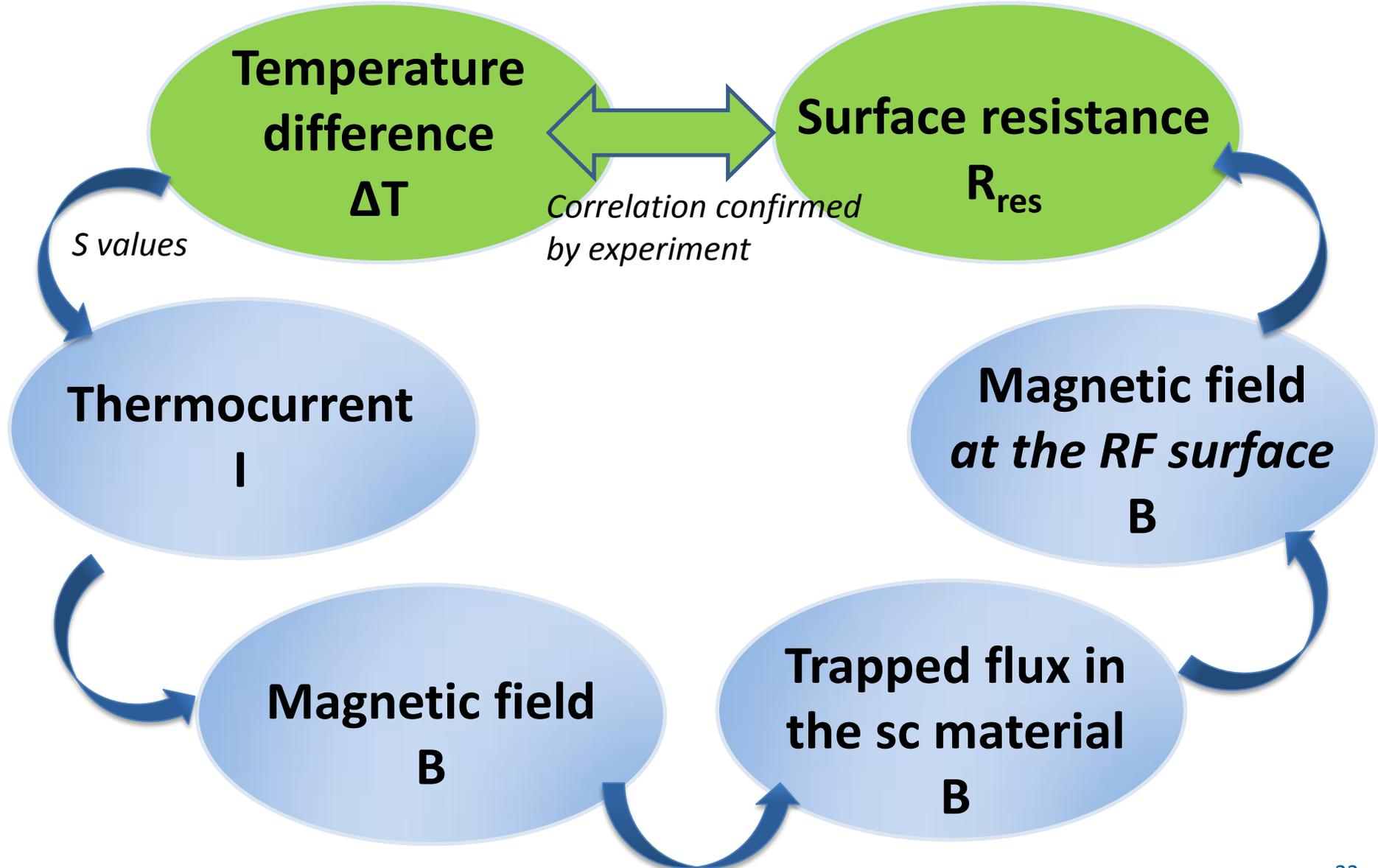


Samples from material as used in cavity fabrication:

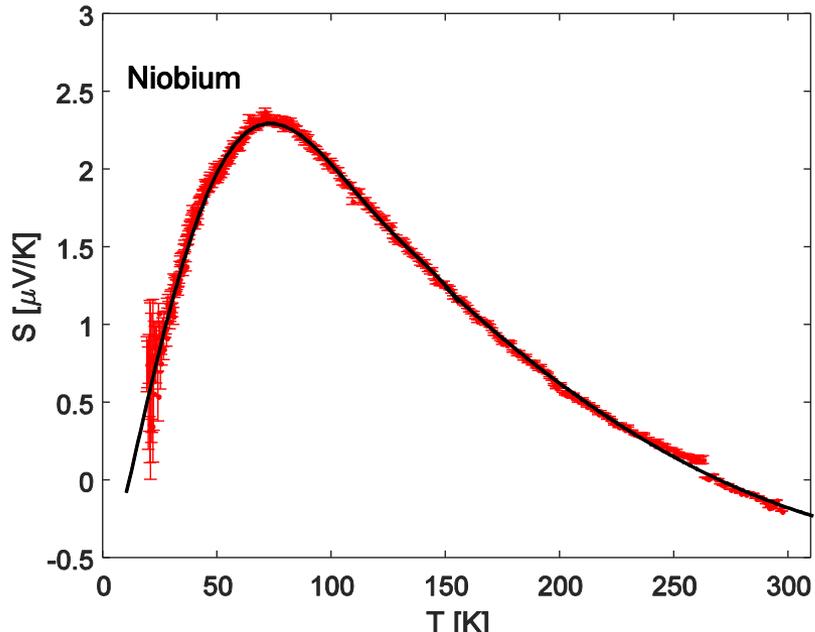
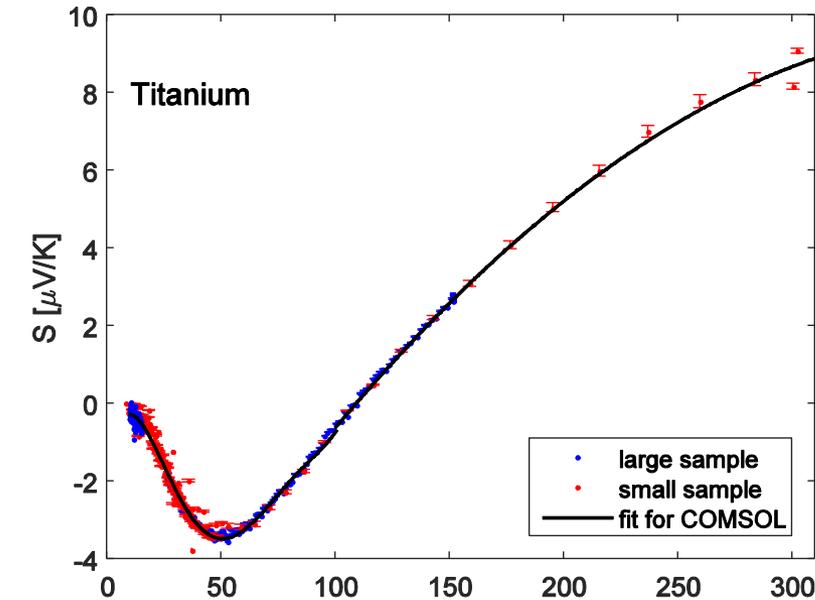
- Niobium (RRR = 300)
- Titanium (grade 2)



# How can we validate the thermocurrent hypothesis?



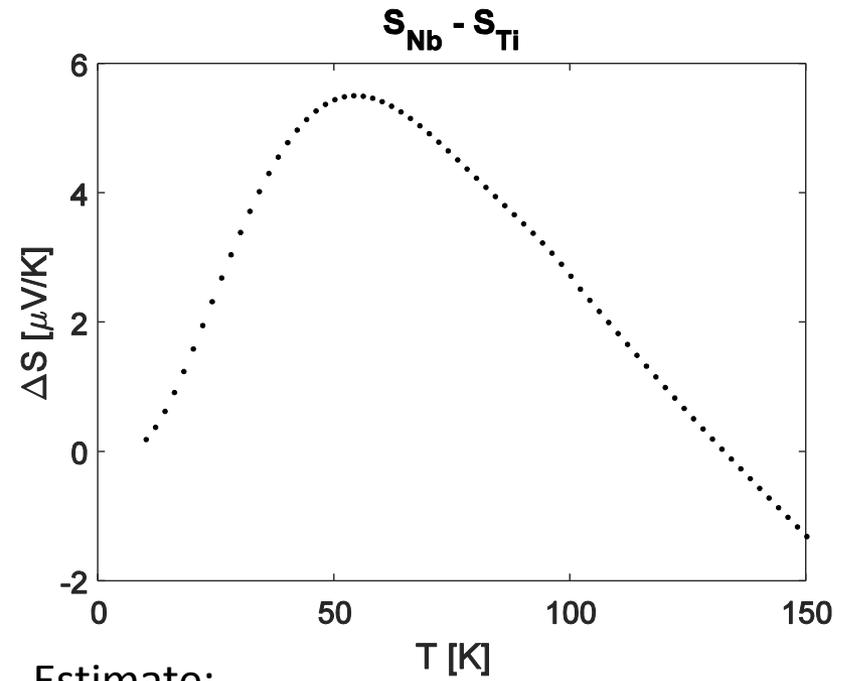
## 2. Exact Seebeck coefficients in the temperature regime of interest



Samples from material as used in cavity fabrication:

- Niobium (RRR = 300)
- Titanium (grade 2)

$\Delta S$  has maximum between 50K and 100K

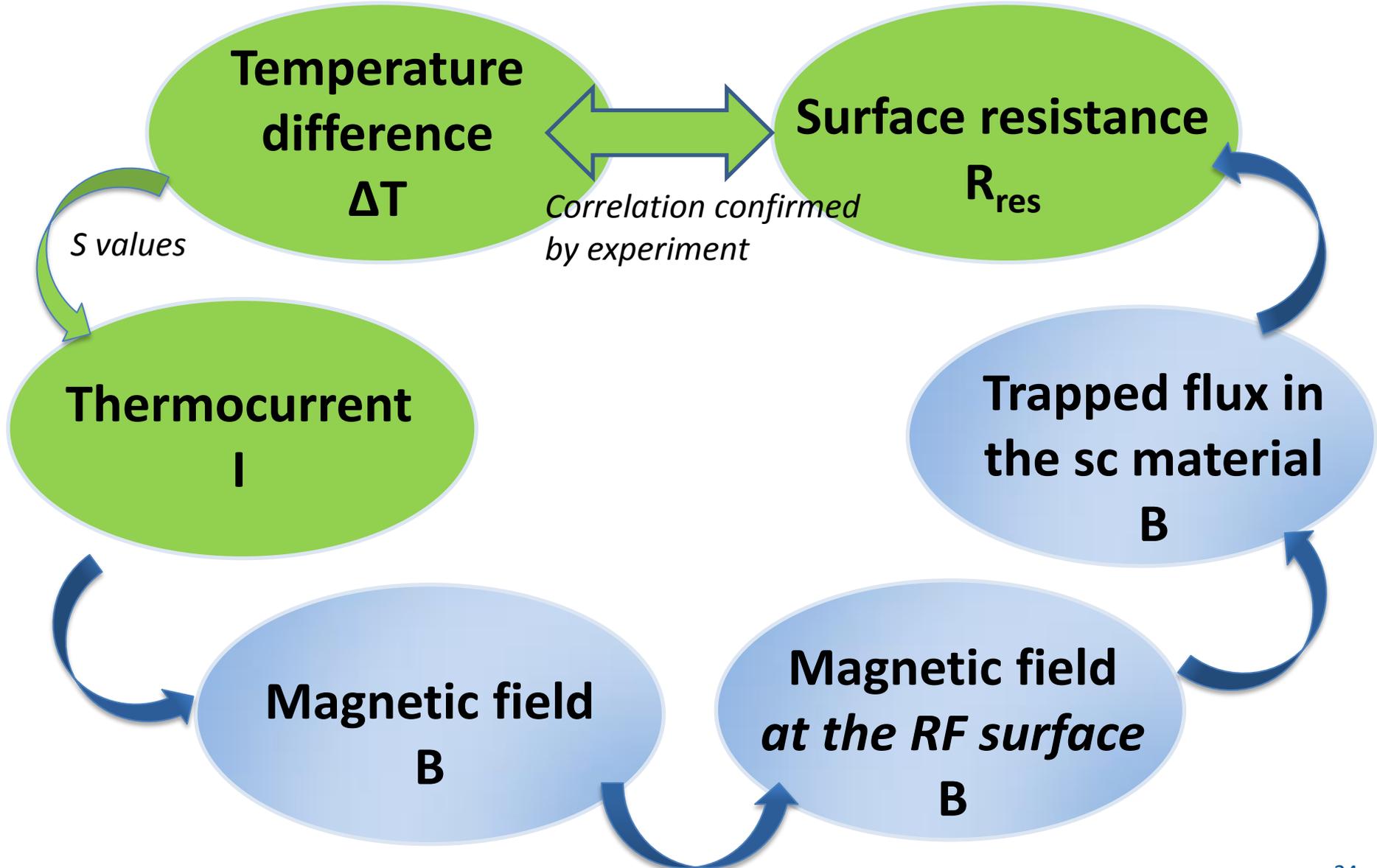


Estimate:

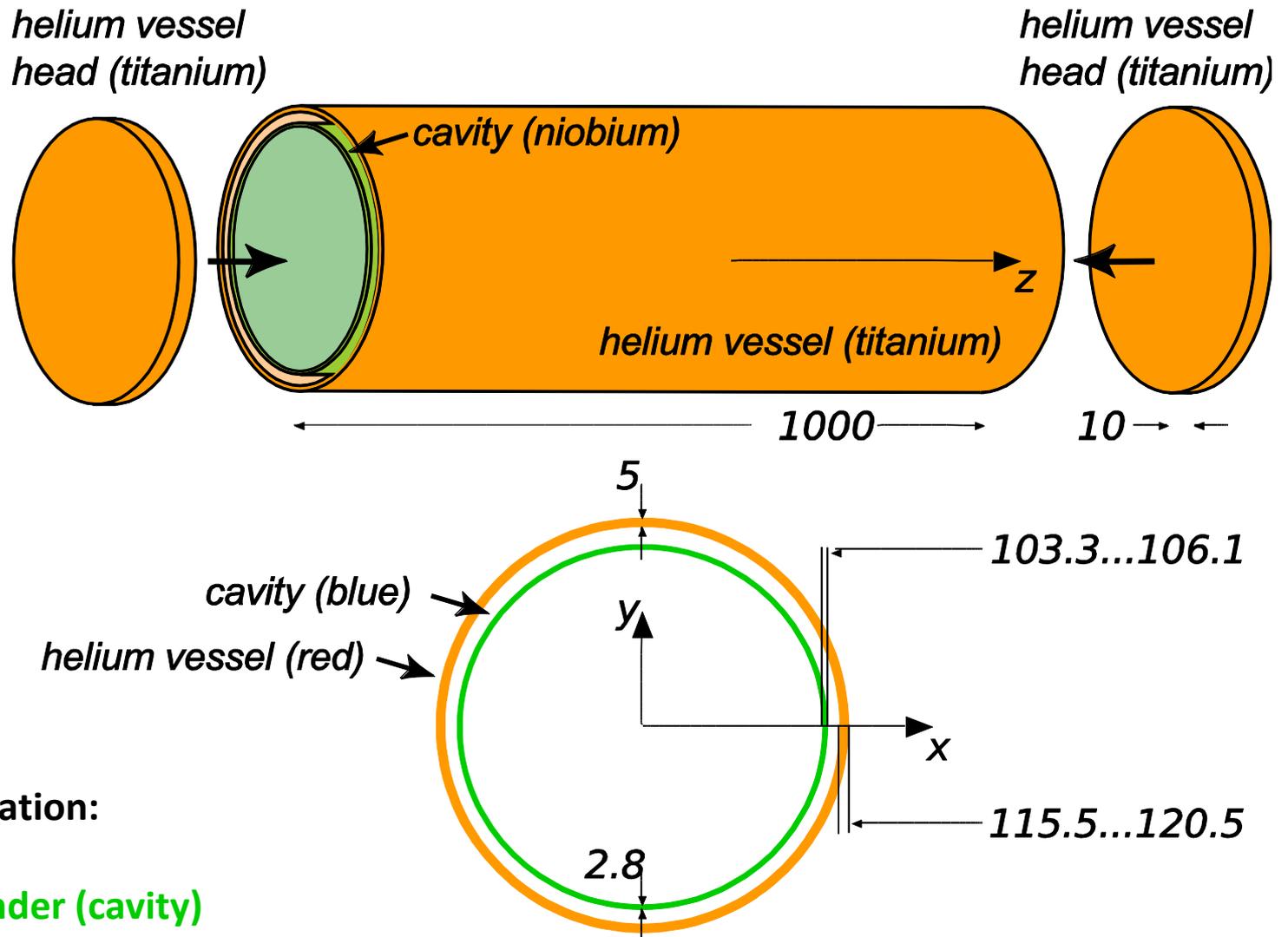
$$I = \Delta S \cdot \Delta T / R = 1 \mu\text{V/K} \cdot 100 \text{ K} / 100 \mu\Omega = 1 \text{ A}$$

10cm distance of a 1 A line current:  $2\mu\text{T}$

# How can we validate the thermocurrent hypothesis?



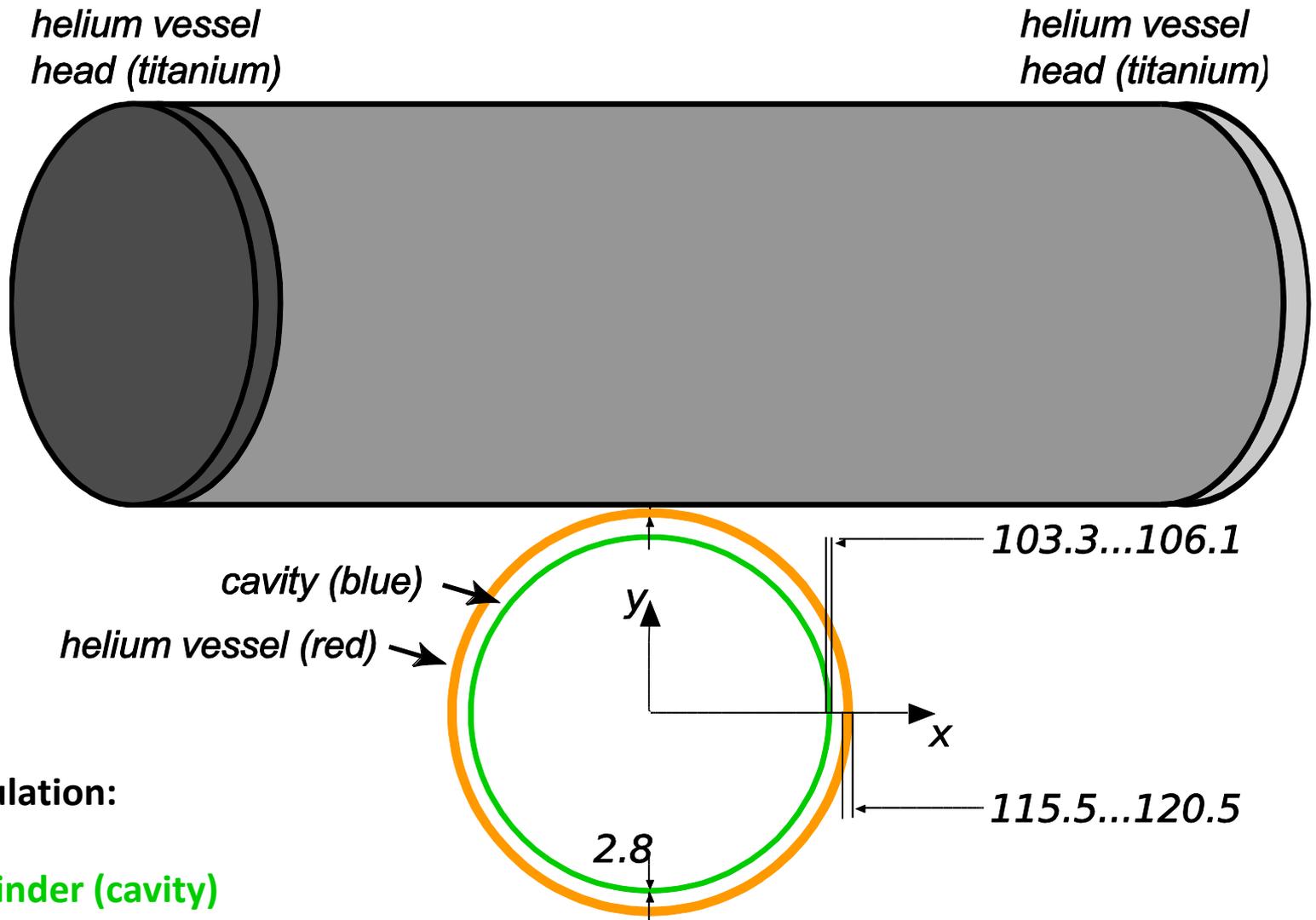
### 3. Geometry of thermocurrents



COMSOL simulation:

- **Niobium:**  
Inner cylinder (cavity)
- **Titanium:**  
Outer cylinder (He vessel)  
End plates (vessel head)

### 3. Geometry of thermocurrents



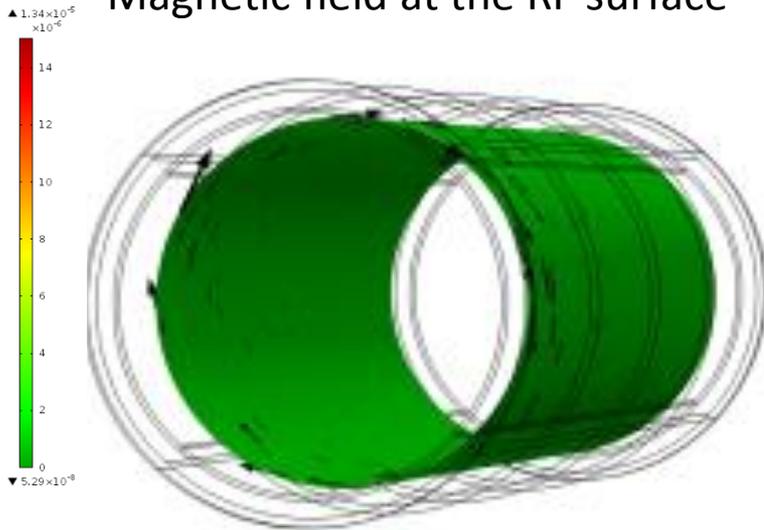
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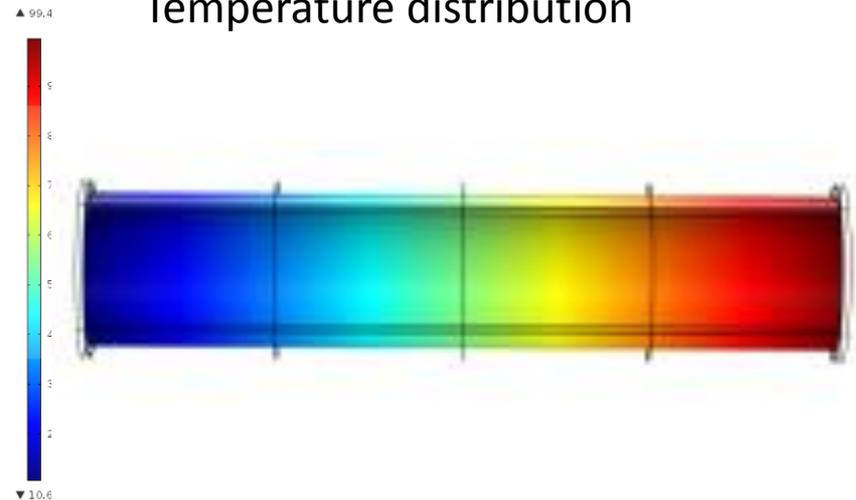
### 3. Geometry of thermocurrents



Magnetic field at the RF surface



Temperature distribution

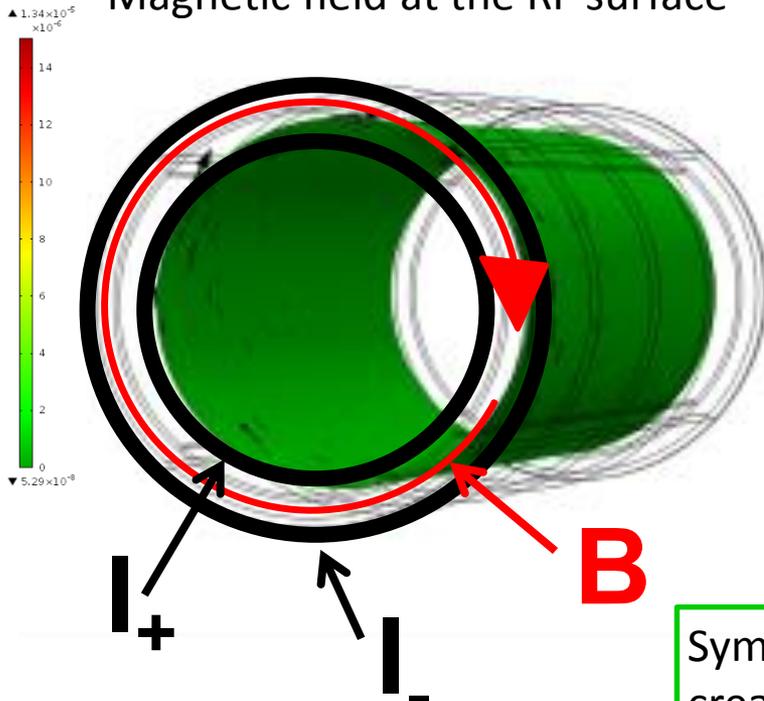


Symmetric current configuration creates no field on the RF surface.

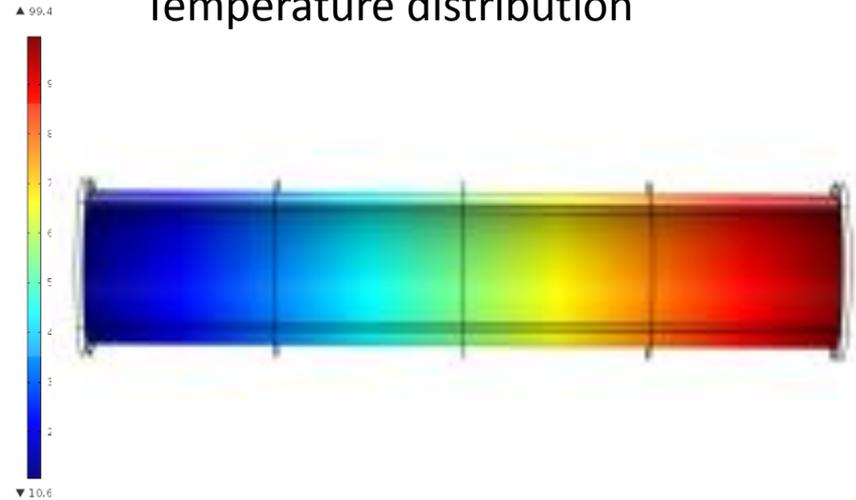
### 3. Geometry of thermocurrents



Magnetic field at the RF surface



Temperature distribution



Symmetric current configuration creates no field on the RF surface.

### 3. Geometry of thermocurrents: Breaking the symmetry



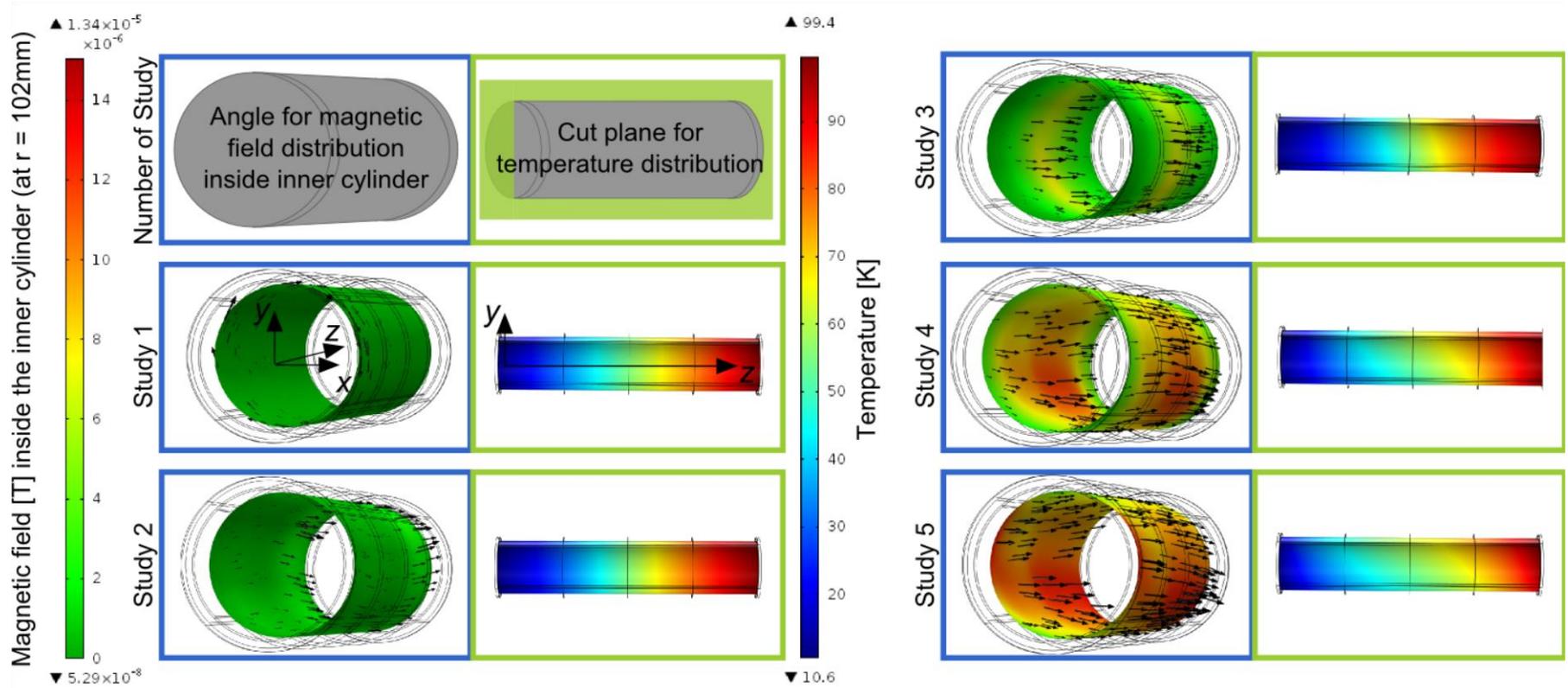
Symmetry can be broken by:

- Mechanical errors: *A. Crawford, "A Study of Thermocurrent Induced Magnetic Fields in ILC Cavities", <http://arxiv.org/abs/1403.7996>*
- Temperature dependance of electrical resistance:

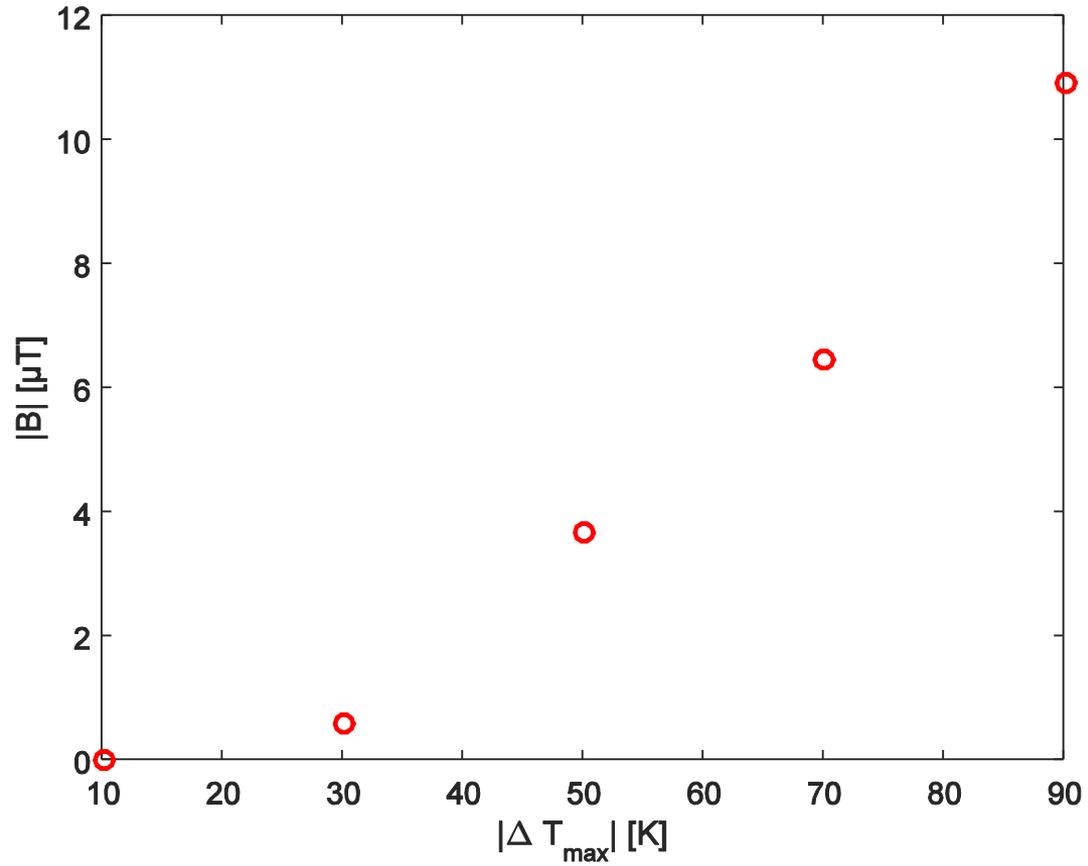
Tank is filled from bottom to top →

Additional temperature difference bottom to top

### 3. Geometry of thermocurrents: Additional temperature difference bottom to top

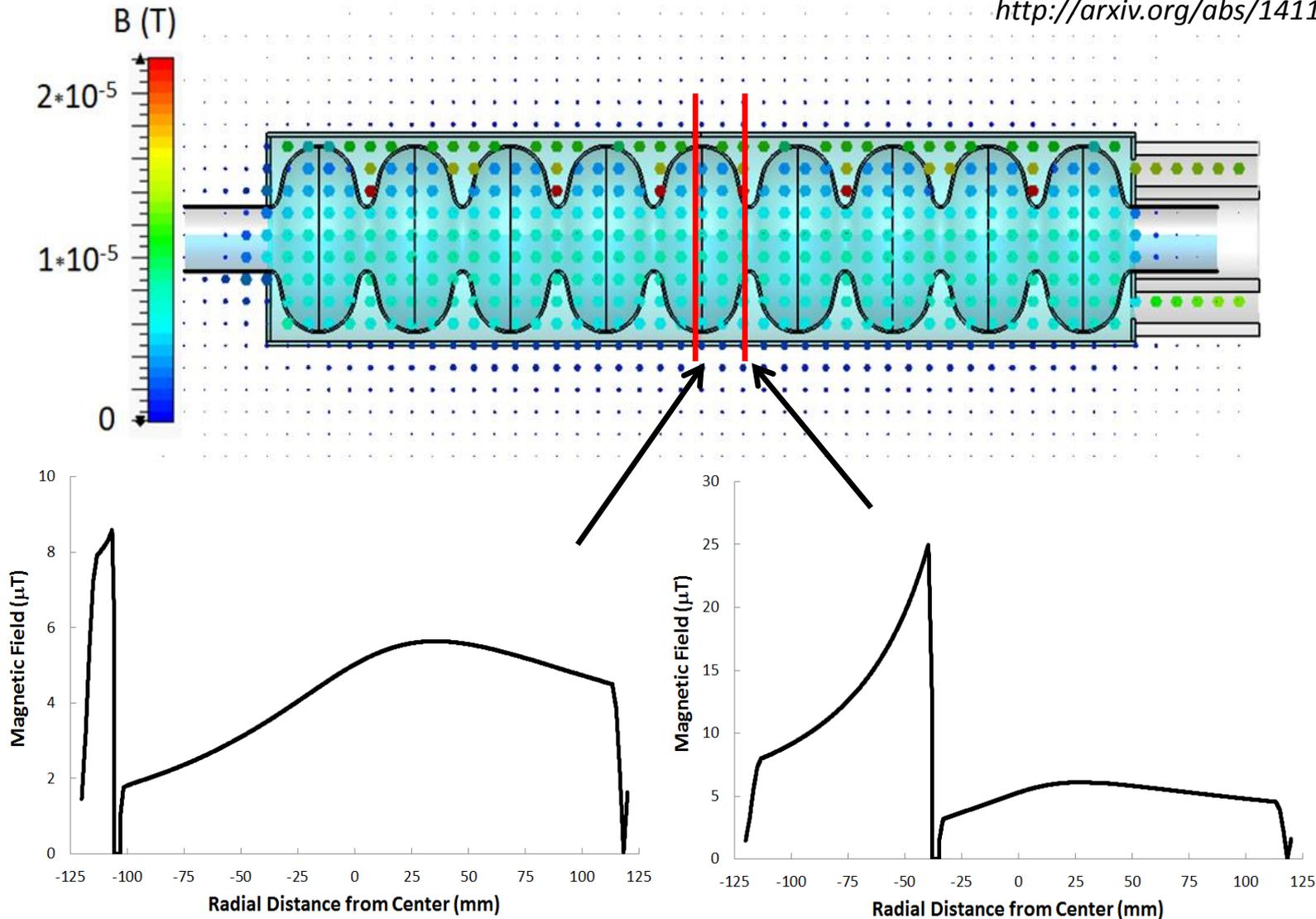


### 3. Geometry of thermocurrents

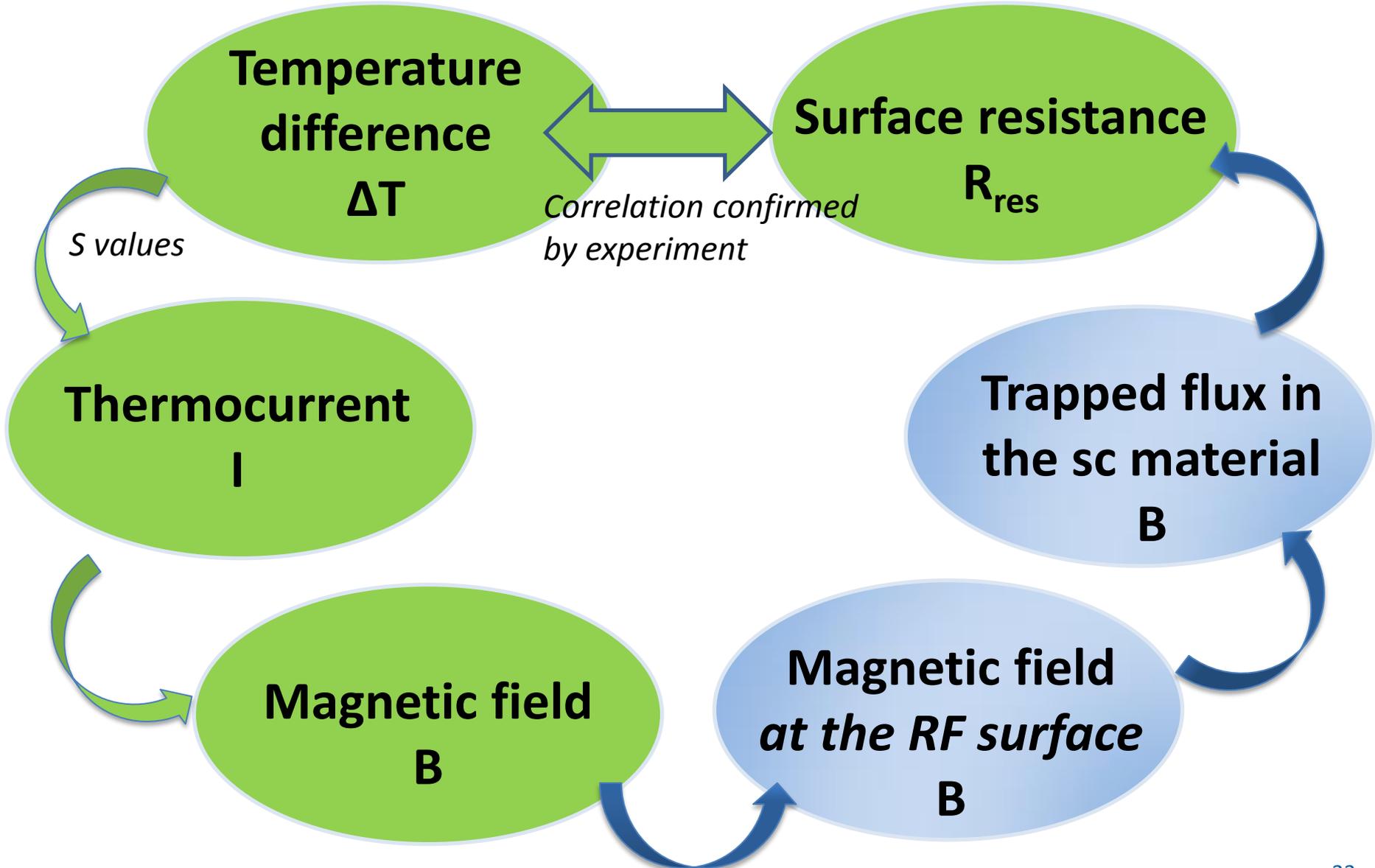


### 3. Geometry of thermocurrents: Highest degree of asymmetry when parts of the cavity are superconducting *Courtesy R. Eichhorn*

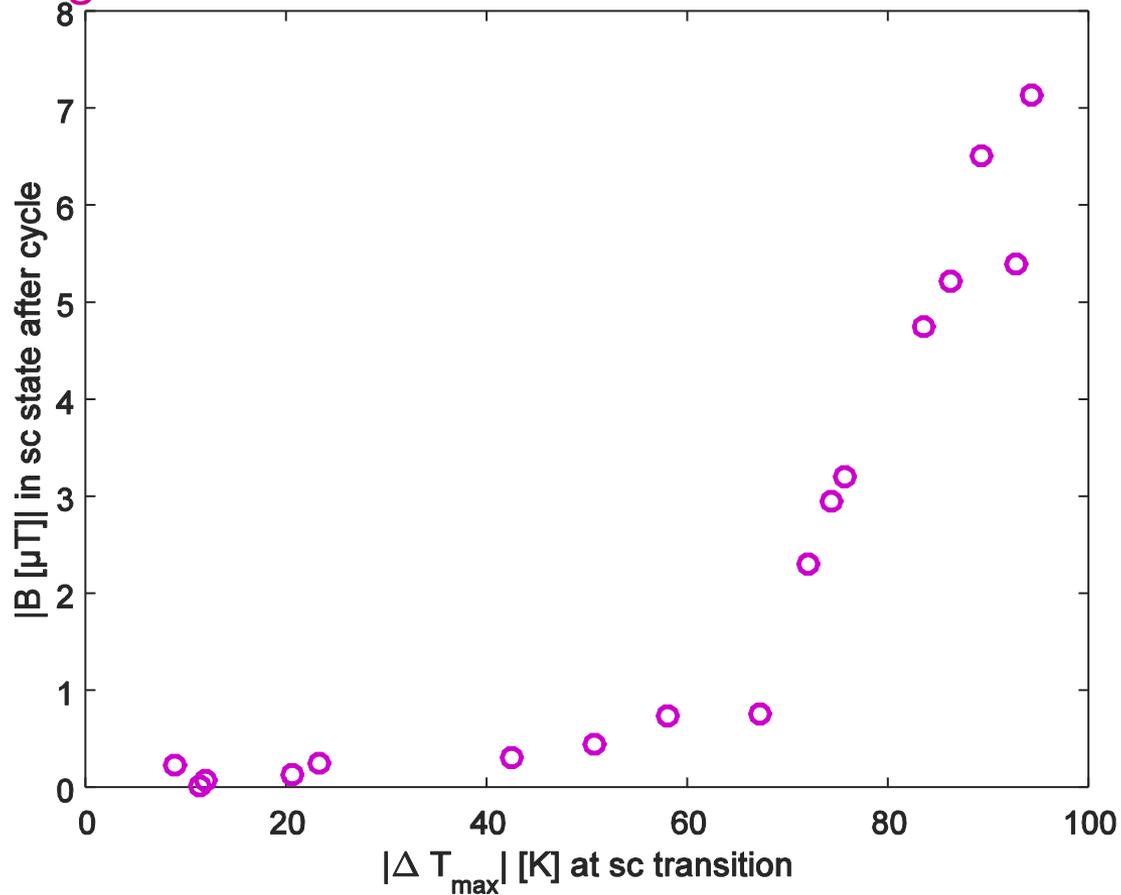
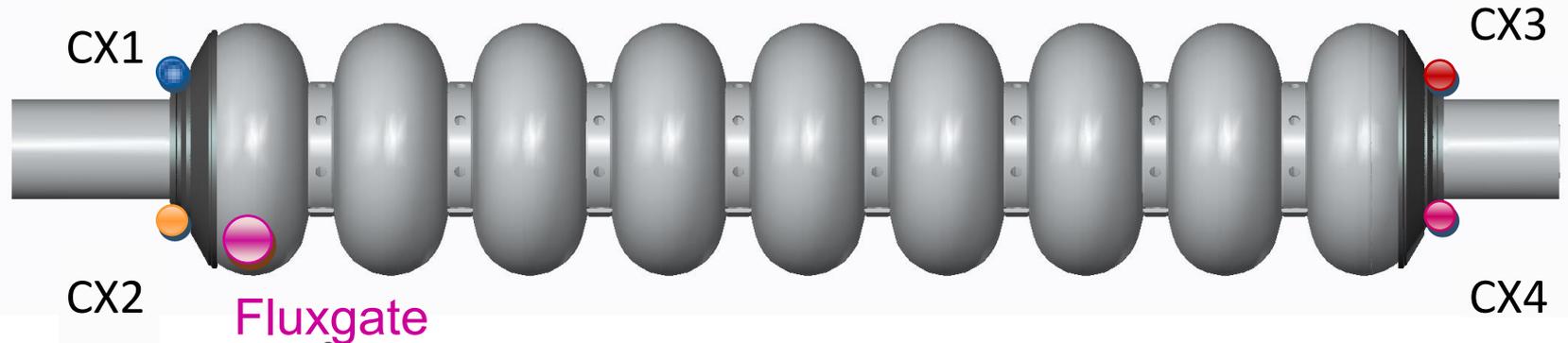
R. Eichhorn et al.,  
"Thermocurrents and their Role in high Q Cavity Performance",  
<http://arxiv.org/abs/1411.5285>



# How can we validate the thermocurrent hypothesis?

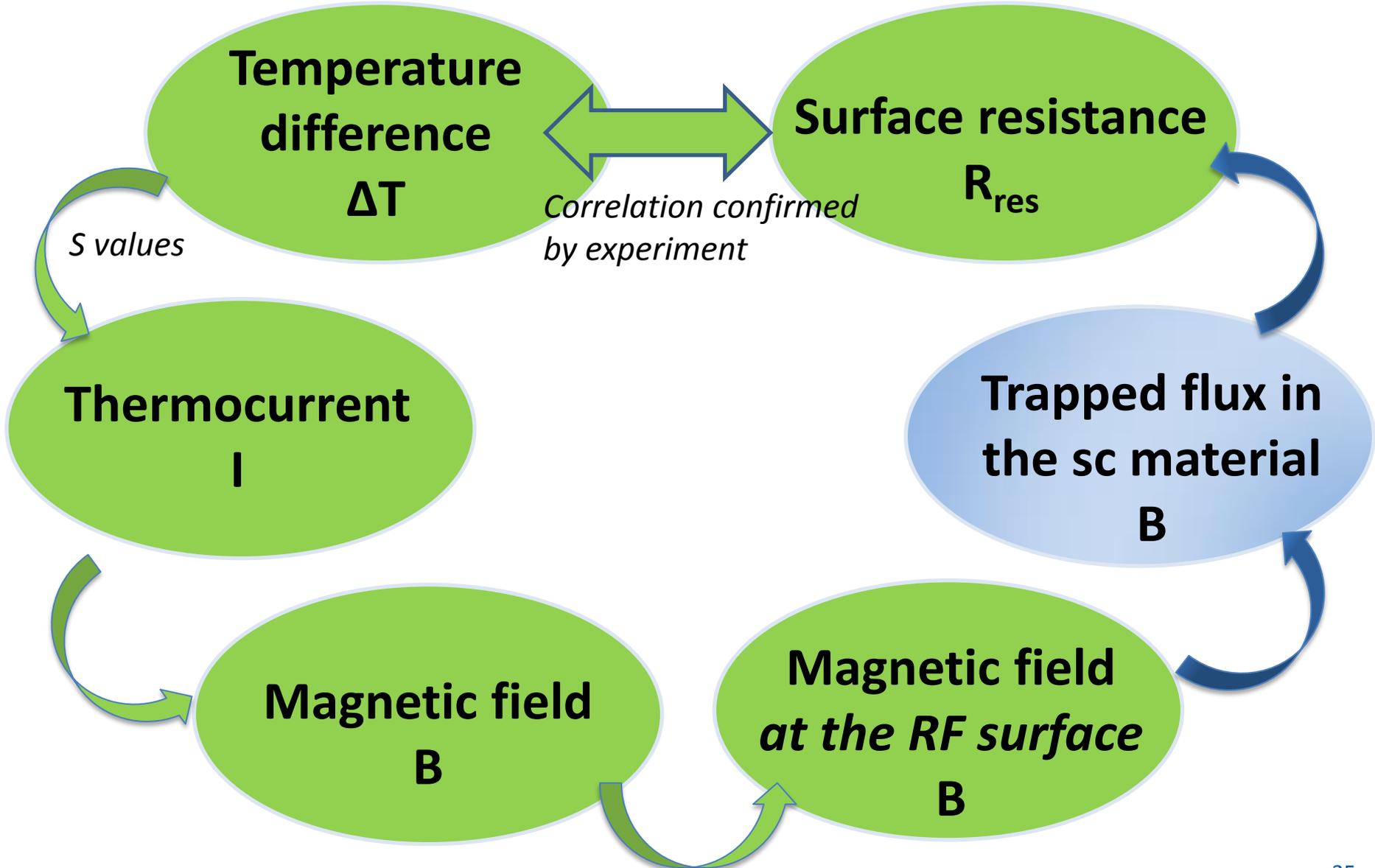


## 4. Direct measurement of the magnetic field on RF surface

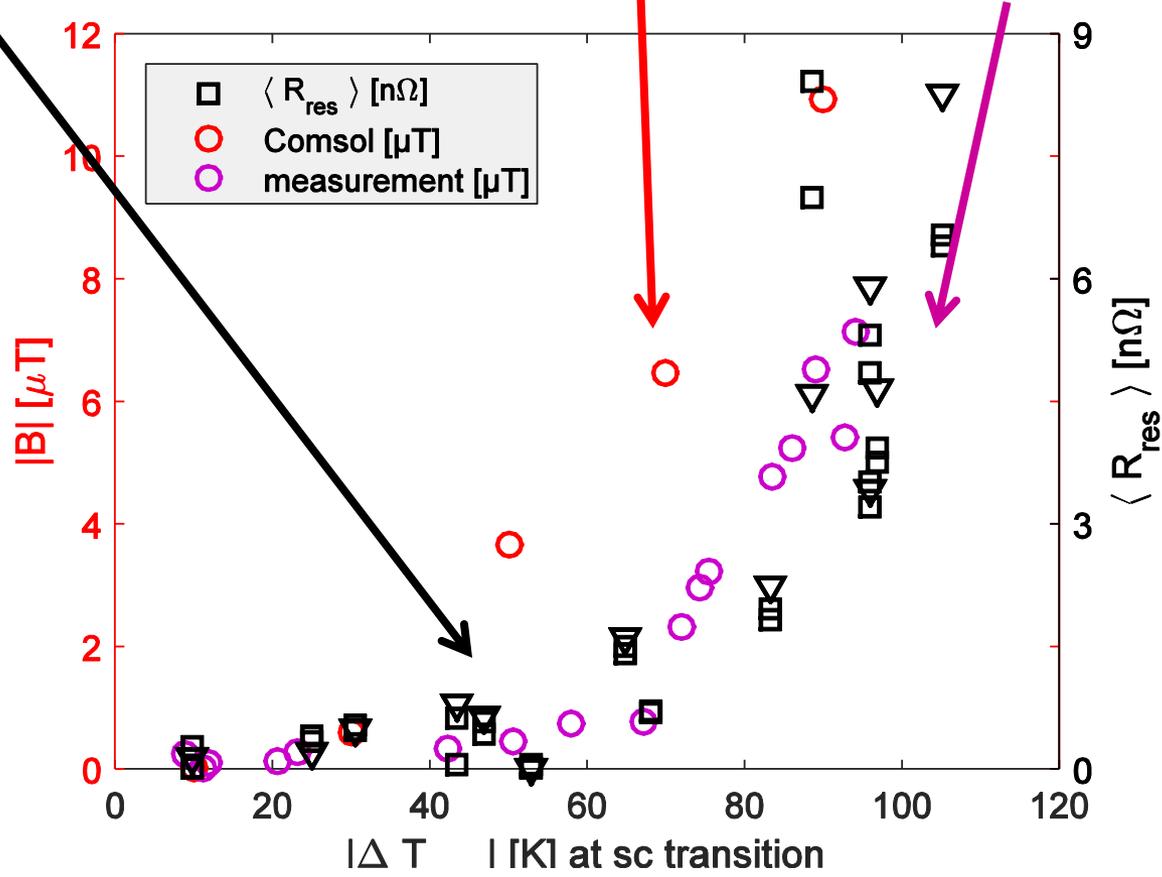
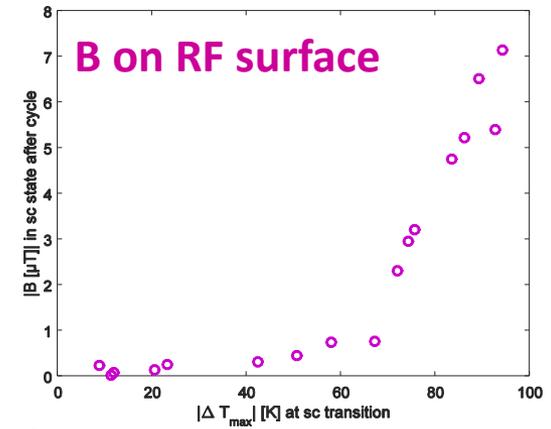
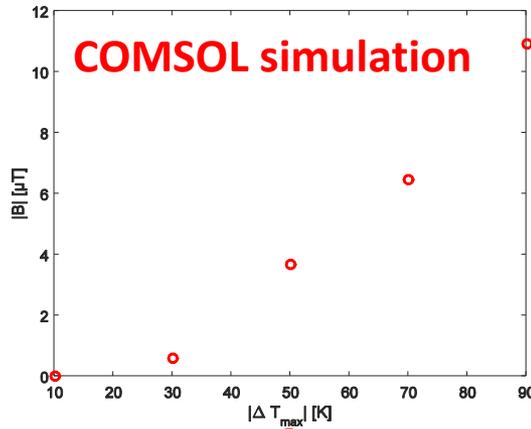
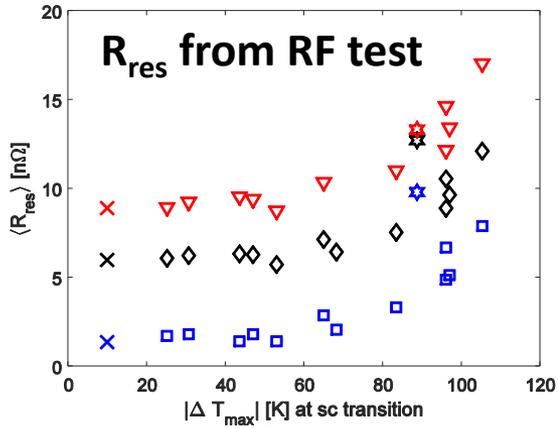


*Mark:  $\Delta T$  is not mean but maximum value*

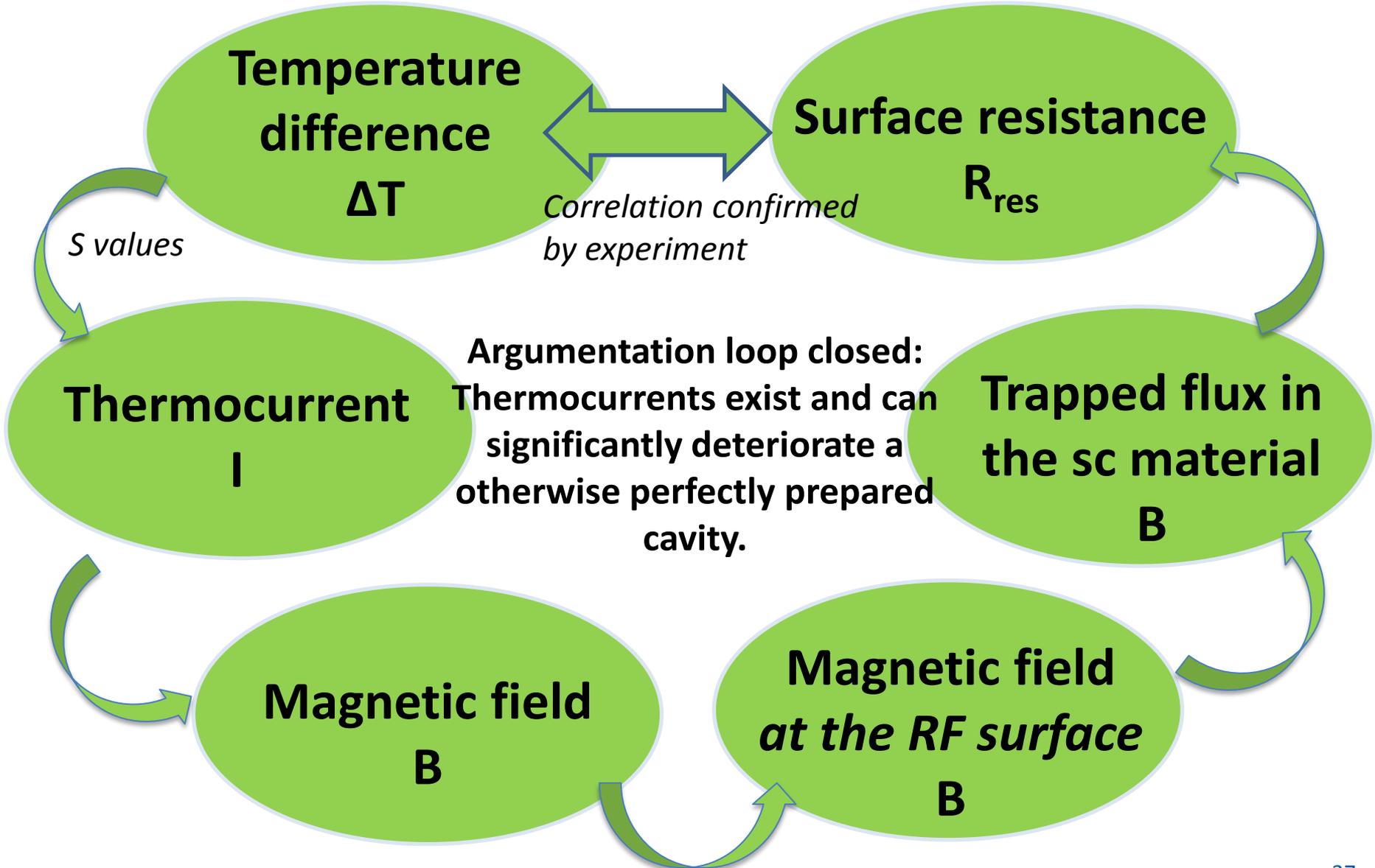
# How can we validate the thermocurrent hypothesis?



# Summary: Thermocurrents in horizontal cavity test



# How can we validate the thermocurrent hypothesis?



## Does the effect apply to every setup?

**Not, if...**

... **only one aspect is satisfied**

... There is no LHe tank (undressed vertical test)

→ *no closed circuit*

... The system is (electrically) symmetric (vertical test)

→ *no gradient across cavity*

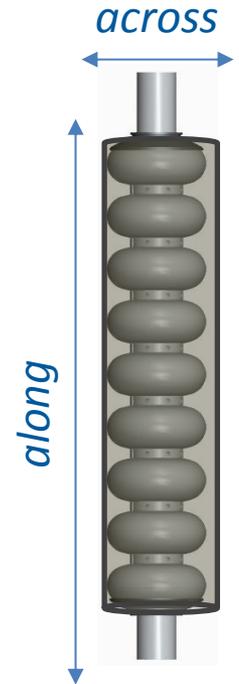
... The system allows for symmetric LHe fill (modified LHe tank)

→ *no gradient along cavity*

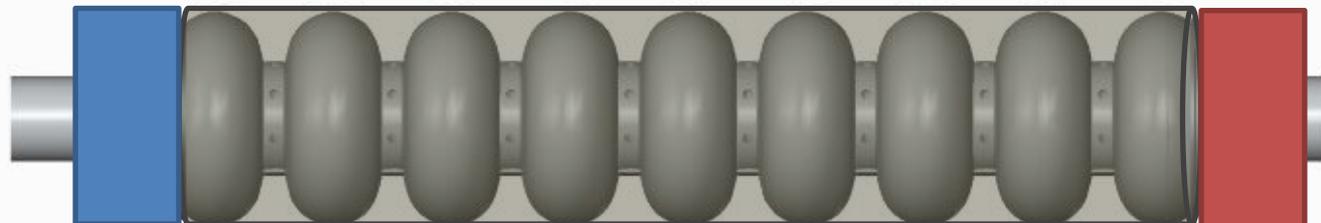
**Yes, if...**

... **both aspects are satisfied**

... especially with couplers and tuners!



*Well cooled  
input side*



*Poorly cooled  
component  
(e.g. "Saclay"  
tuner)*

*across*

*along*

# Thank you for your attention!

## Acknowledgement

**To the Fermilab Team, in particular Anna Grassellino, Alexander Romanenko, Curtis Crawford, Dmitri Sergatskov who provided the doped and equipped cavity for the test, as well as everybody who provided material for the slides.**

**We would like to thank our engineers *André Frahm, Michael Schuster, Sascha Klauke, Dirk Pflückhahn and Stefan Rotterdam* for patient support.**

## References

- J. Vogt et al., “High-Q operation of superconducting rf cavities: Potential impact of thermocurrents on the rf surface resistance”, Phys. Rev. ST Accel. Beams 18, 042001 (2015)
- O. Kugeler et al., “Manipulating the intrinsic quality factor by thermal cycling and magnetic fields”, SRF’09, Berlin, Germany, p. 352 (2009)
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- D. Gonella et al., “Nitrogen-doped 9-cell cavity performance in a test cryomodule for LCLS-II”, Journal of Applied Physics 117, 023908 (2015)