

SUPERCONDUCTING RF-DIPOLE DEFLECTING AND CRABBING CAVITIES

Subashini De Silva

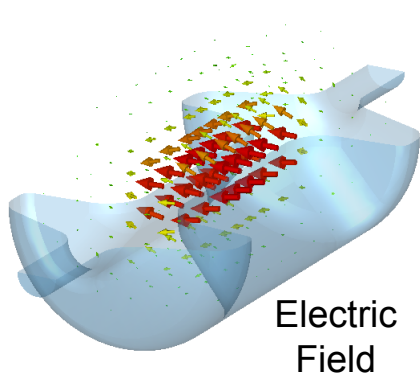
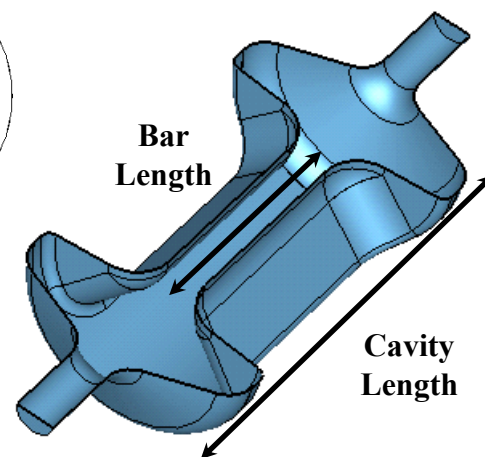
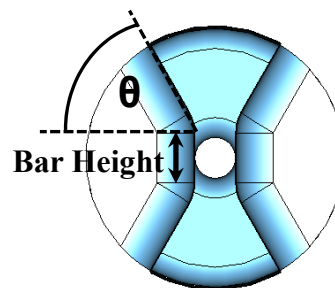
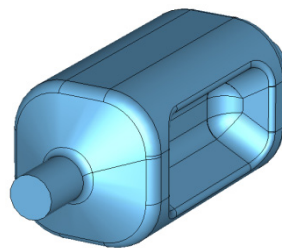
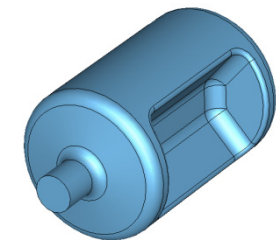
**Center for Accelerator Science
Department of Physics, Old Dominion University
and
Thomas Jefferson National Accelerator Facility**

RF-Dipole Design

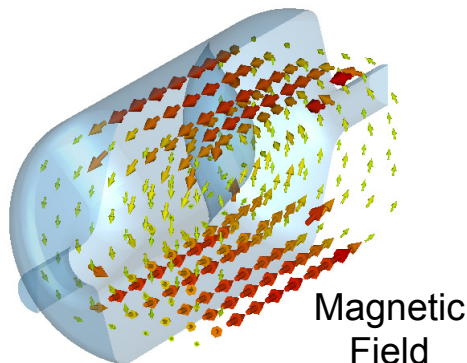
- Small size
- Square shape for additional compactness
- Lower and balanced peak surface fields
- High shunt impedance
- Wider separation in HOM spectrum and no LOMs
- Multipacting processes easily
- Cavity processing – Curved end plates for cleaning the cavity

Properties depend on a few parameters

- Frequency determined by diameter of the cavity design
- Bar Length $\sim \lambda/2$
- Bar height and aperture determine E_p and B_p
- Angle determines B_p/E_p



Electric Field

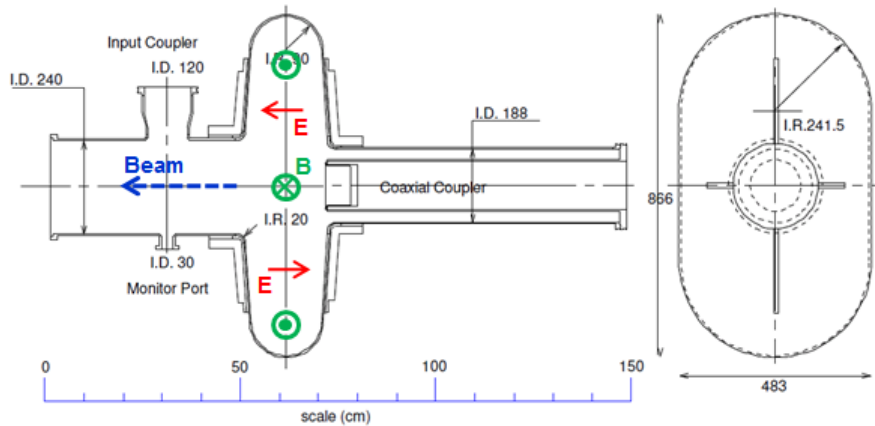


Magnetic Field

Deflecting and Crabbing Cavities

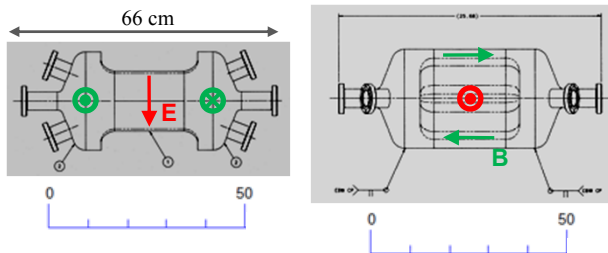
- TM_{110} type cavities

KEK Crabbing Cavity – TM_{110} mode



- RF-Dipole Cavity

499 MHz Deflecting Cavity



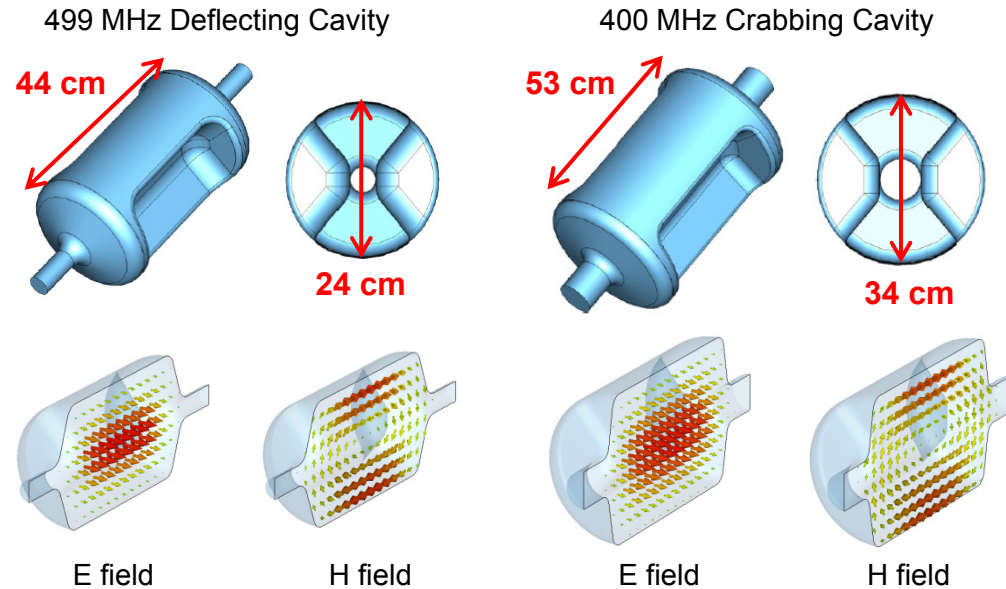
	KEK Crabbing Cavity	RF-Dipole Cavity	Units
Frequency	508.9	499.0	MHz
LOM	410.0	None	MHz
Nearest HOM	630.0	777.2	MHz
Aperture Diameter	100.0	40.0	mm
Cavity width	48.3	24.0	cm
Cavity height	86.6	24.0	cm
Cavity length	~150	66	cm
V_T^*	0.295	0.3	MV
E_p^*	4.24	2.86	MV/m
B_p^*	12.23	4.38	mT
B_p^*/E_p^*	2.88	1.53	mT/(MV/m)
$[R/Q]_T$	48.9	982.5	Ω
Geometrical Factor	227.0	105.9	Ω
$R_T R_S$	1.1×10^4	1.0×10^5	Ω^2
At $E_T^* = 1$ MV/m			

Crabbing/Deflecting Cavity Applications

- Luminosity management in linear or circular colliders
- Separation or merge of multiple beams
- Emittance exchange in beams
- X-ray pulse compression
- Beam diagnostics

Properties of Proof of Principle Cavities

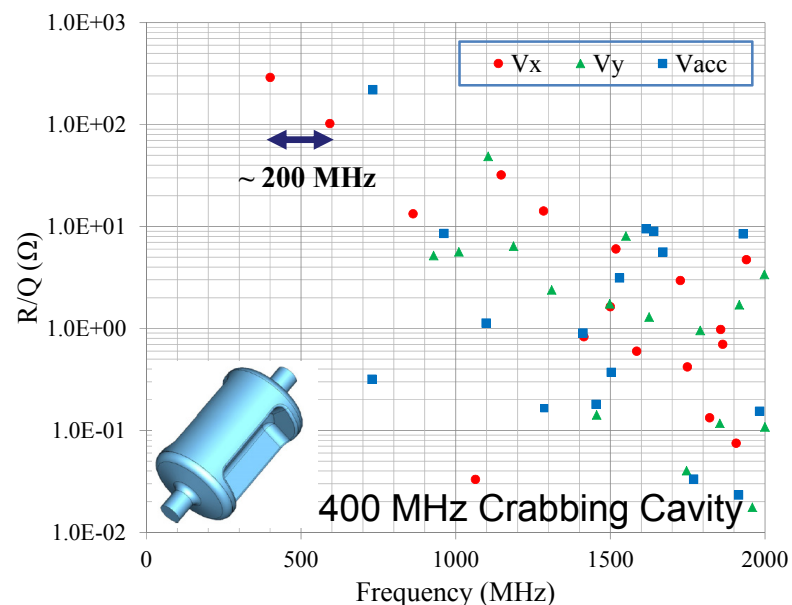
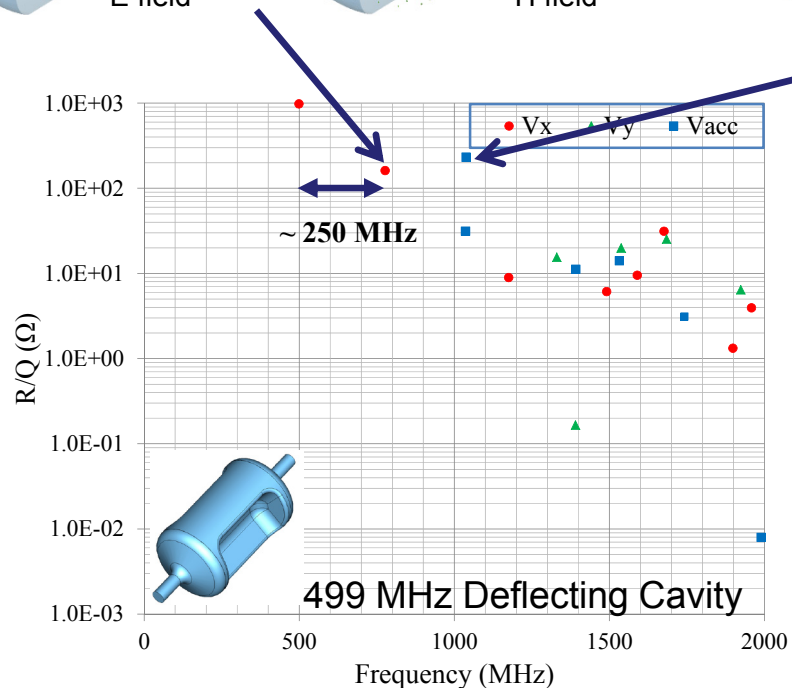
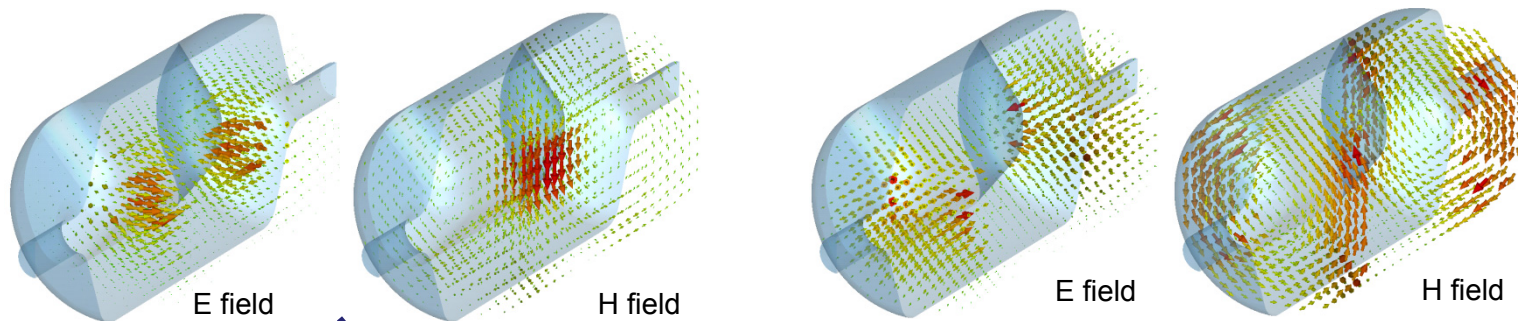
Frequency	499.0	400.0	MHz
Aperture Diameter (d)	40.0	84.0	mm
$d/(\lambda/2)$	0.133	0.224	
V_T^*	0.3	0.375	MV/m
E_p^*	2.86	4.02	MV/m
B_p^*	4.38	7.06	mT
B_p^*/E_p^*	1.53	1.76	mT/(MV/m)
U^*	0.029	0.195	J
$[R/Q]_T$	982.5	287.0	Ω
Geometrical Factor (G)	105.9	140.9	Ω
$R_T R_S = [R/Q]_T G$	1.0×10^5	4.0×10^4	Ω^2
At $E_T^* = 1$ MV/m			
V_T	5.6	5.0	MV
E_p	54	54	MV/m
B_p	82	95	mT



- Dependence of beam aperture ($d/(\lambda/2)$)
 - Peak surface fields (B_p/E_T and E_p/E_T) increase
 - Shunt impedance ($R_T R_S$) drops

Higher Order Mode Properties

- Widely separated Higher Order Modes
- No Lower Order Modes



Fabrication

- Cavity thickness = 3mm
- Frequency adjustment by trimming the center shell

499 MHz Deflecting Cavity

Fabricated at Jefferson Lab



400 MHz Crabbing Cavity

Fabricated at Niowave Inc.



Surface Treatment

- Bulk BCP of $\sim 150\ \mu\text{m}$
- Average removal
 - 499 MHz $\rightarrow 108\ \mu\text{m}$
 - 400 MHz $\rightarrow 85\ \mu\text{m}$
- Heat Treatment $\rightarrow \text{H}_2$ degassing at 600°C – 10 hours
- Light BCP – Removal of $10\ \mu\text{m}$ after heat treatment
- High pressure rinsing in 3 passes
- Assembly – with fixed coupling
- No He processing
- No in-situ baking
- Tests performed
 - 4 K high power test
 - 4 K to 2 K low power test
 - 2 K high power test

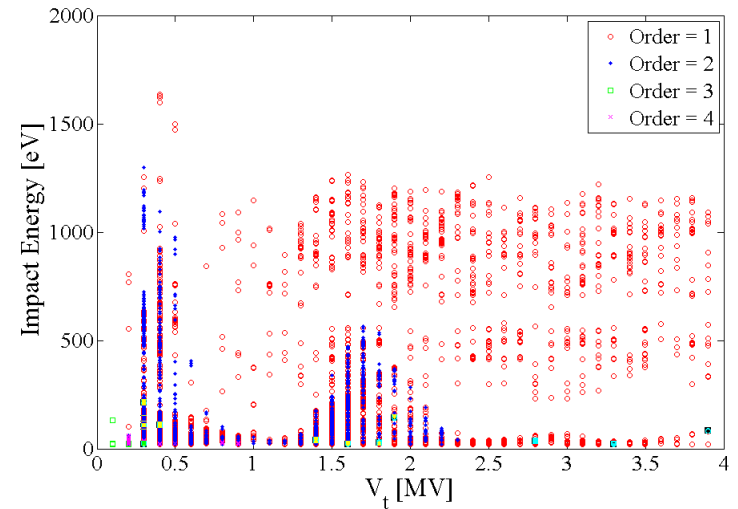
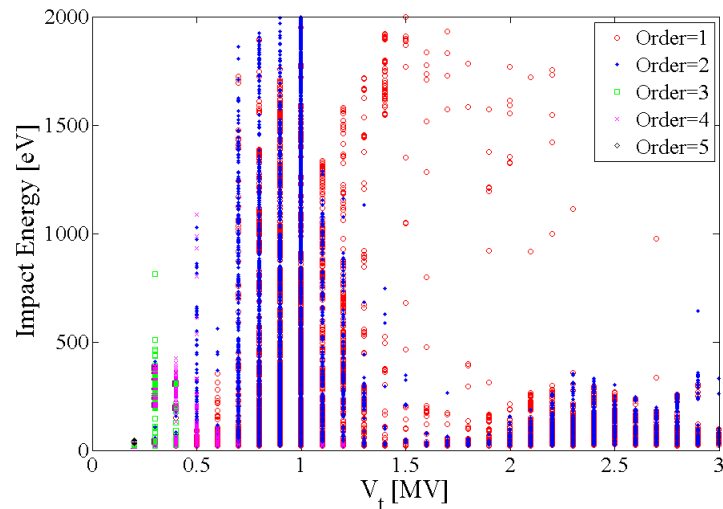
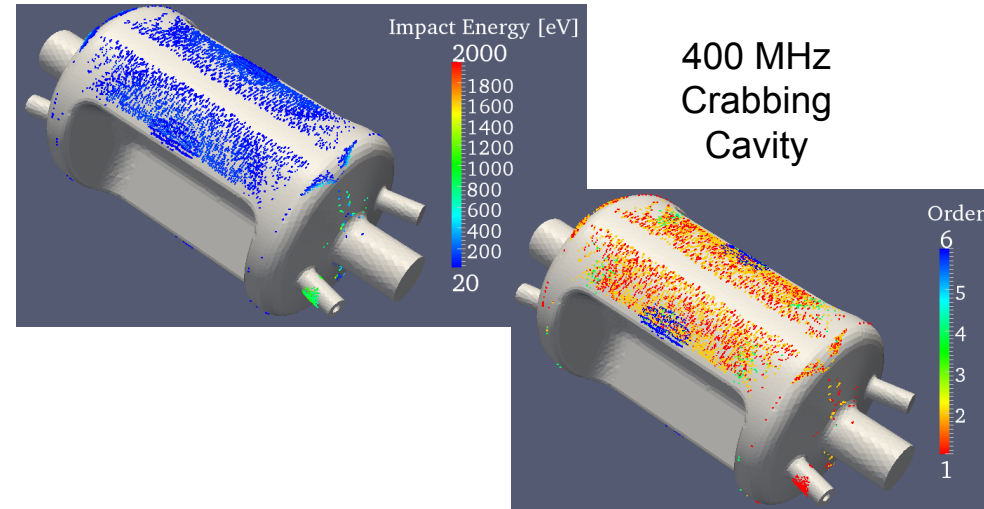
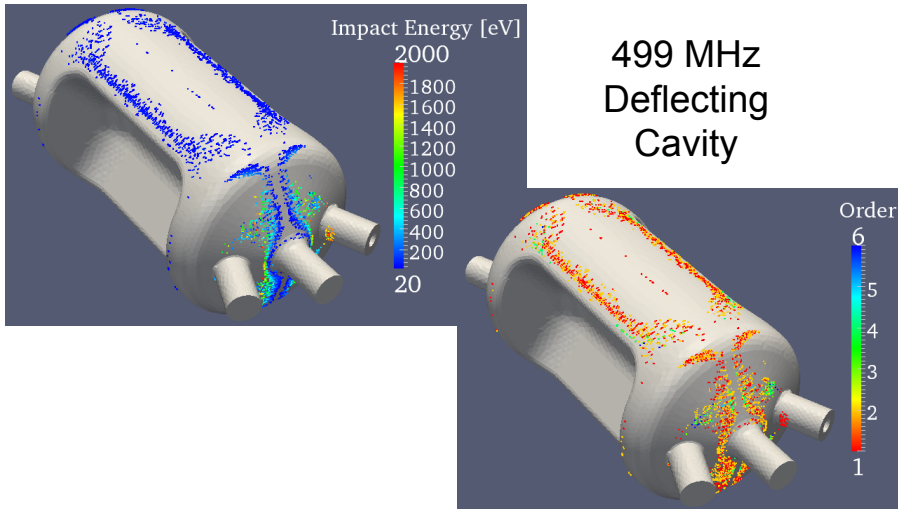
400 MHz
Crabbing
Cavity



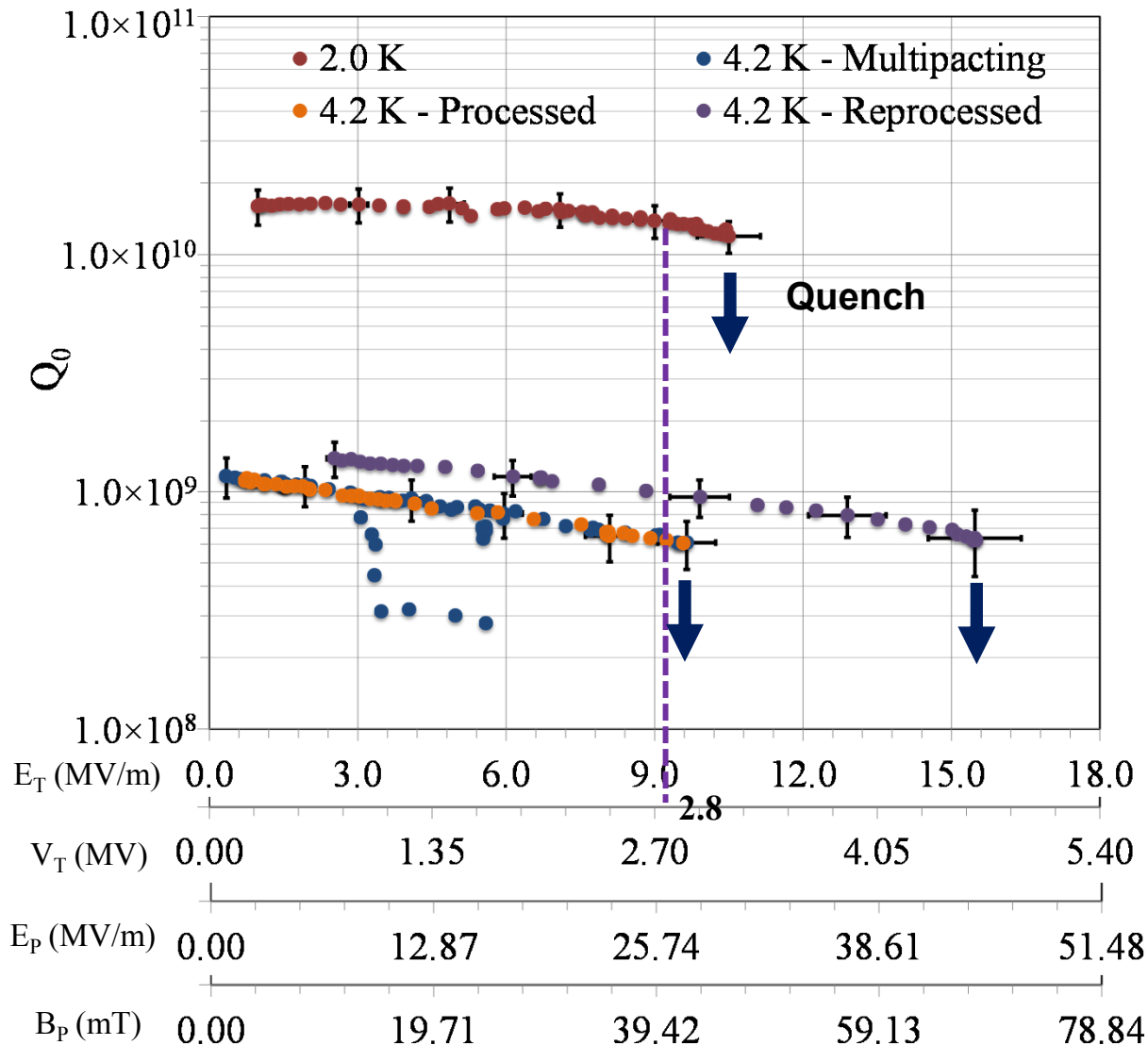
499 MHz
Deflecting
Cavity

Multipacting Analysis

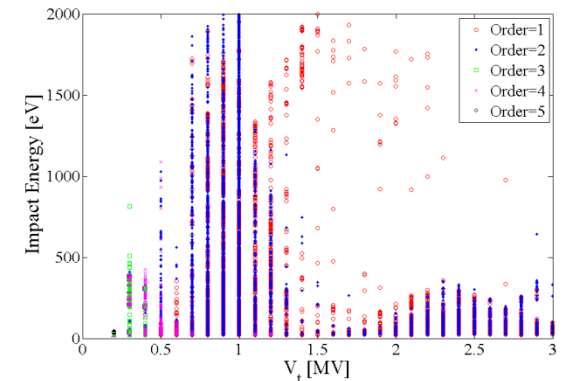
Track3P – Resonant particle tracking code in SLAC ACE3P suite



4.2 K and 2 K Test Results – 499 MHz

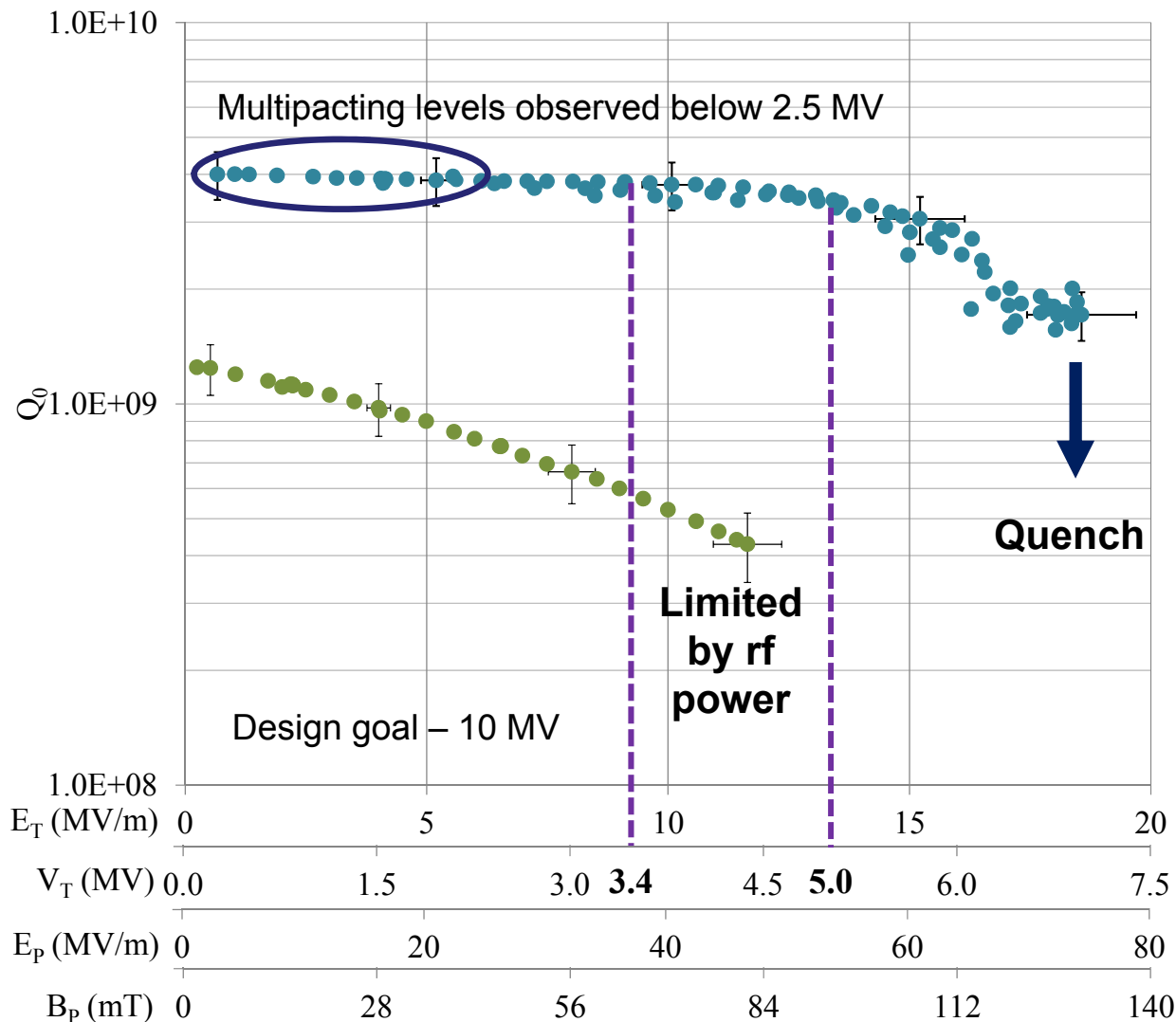


- Multipacting was easily processed during the 4.2 K rf test

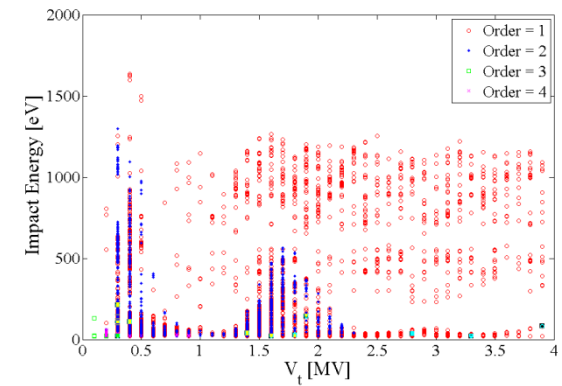


- Design requirement of 5.6 MV can be achieved with 2 cavities
- Reprocessed cavity achieved fields at 4.2 K
 - $E_T = 15.5$ MV/m
 - $V_T = 4.65$ MV
 - $E_P = 44.3$ MV/m
 - $B_P = 67.9$ mT

4.2 K and 2 K Test Results – 400 MHz

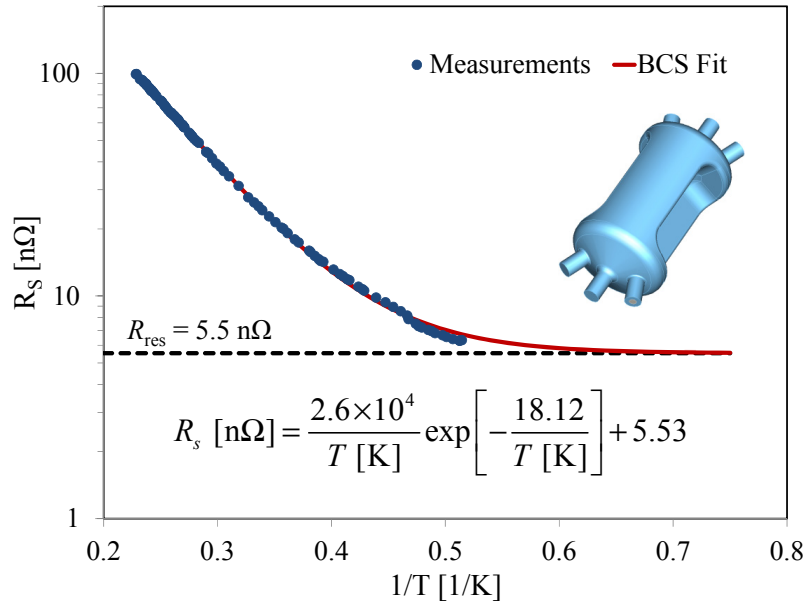


- Multipacting levels were easily processed

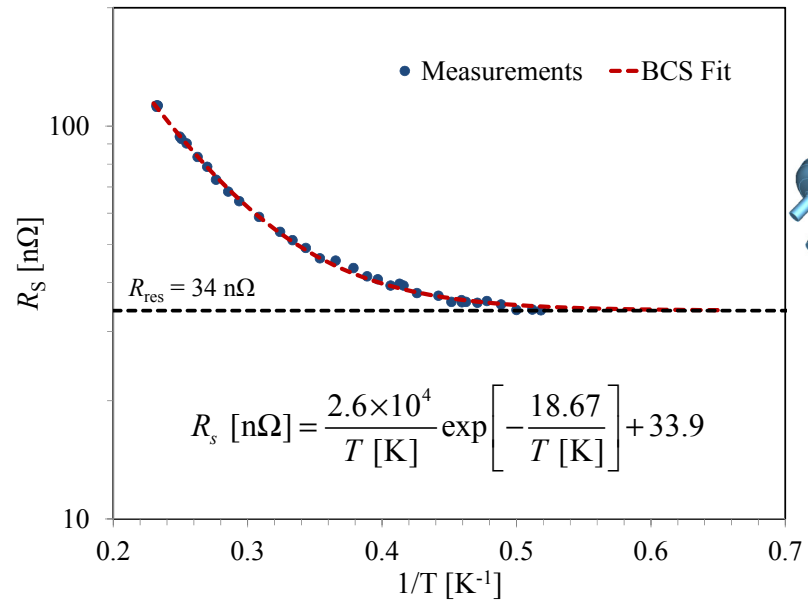


- Achieved fields at 4.2 K
 - $E_T = 11.6$ MV/m
 - $V_T = 4.35$ MV
 - $E_P = 47$ MV/m
 - $B_P = 82$ mT
- Limited by rf power at 4.2 K
- Achieved fields at 2.0 K
 - $E_T = 18.6$ MV/m
 - $V_T = 7.0$ MV
 - $E_P = 75$ MV/m
 - $B_P = 131$ mT

Surface Resistance



- 499 MHz Cavity
 - $R_{\text{BCS}} = 1.3 \text{ n}\Omega$ at 2.0 K
 - $R_{\text{res}} = 5.5 \text{ n}\Omega$

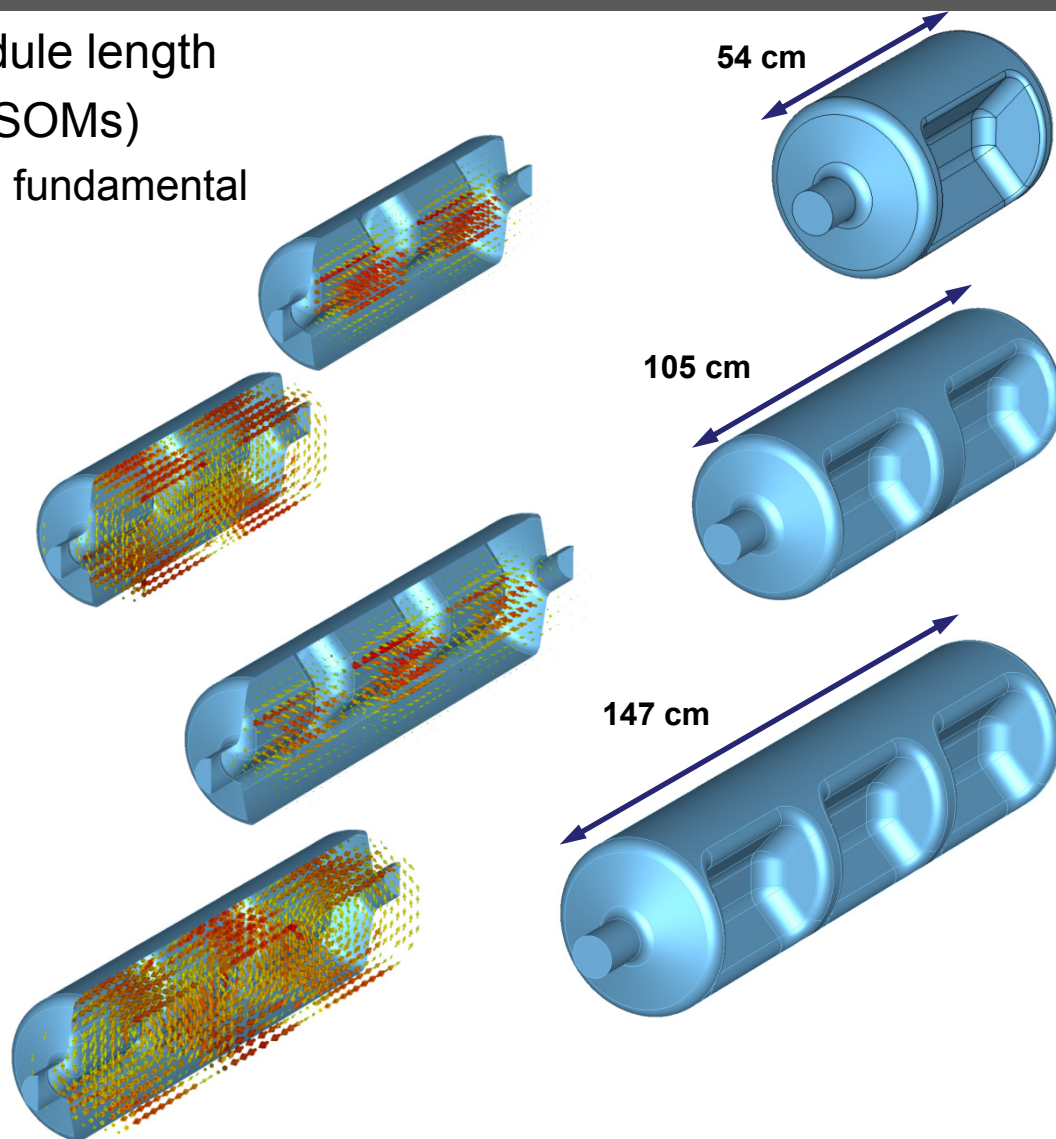


- 400 MHz Cavity
 - $R_{\text{BCS}} = 2.0 \text{ n}\Omega$ at 2.0 K
 - $R_{\text{res}} = 34 \text{ n}\Omega$
 - Measured Q_0 at 2.0 K = 4.0×10^9
 - Q_0 due to power loss at the beam ports flanges $\rightarrow 3.8 \times 10^9$

Multicell RF-Dipole Designs

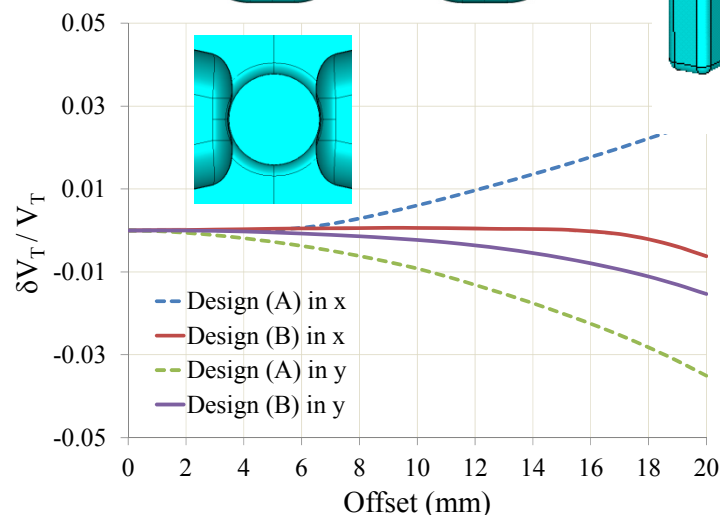
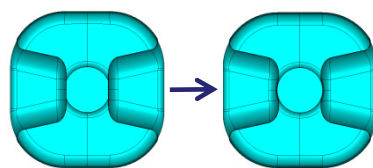
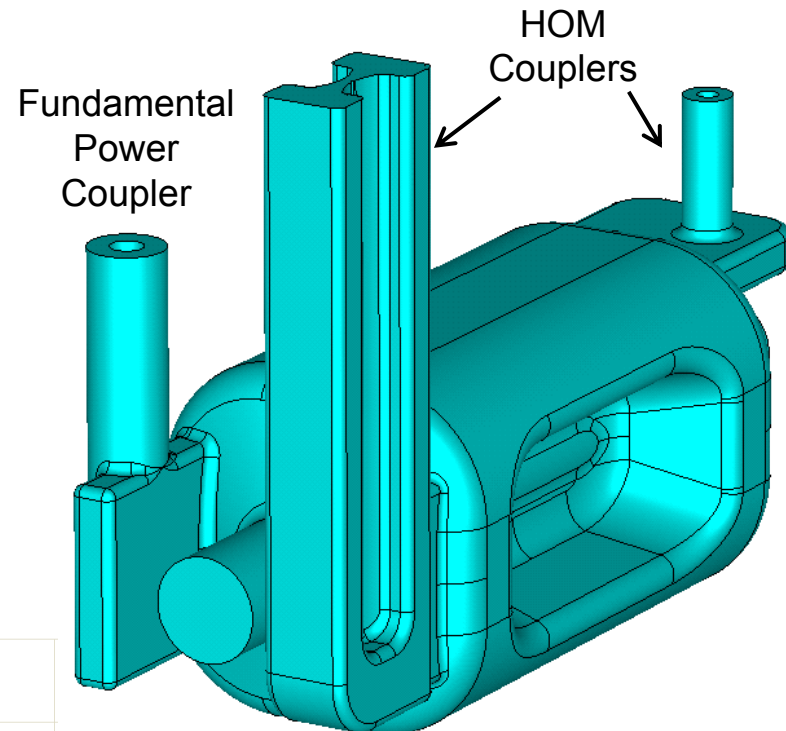
- Reduced total cavity and cryomodule length
- Existence of same order modes (SOMs)
 - SOMs have lower frequency than fundamental
 - No. of SOMs = No. of cells

	2 cell	3 cell	
Frequency	400	400	MHz
SOMs	374.5	351.6 / 376.8	MHz
Aperture	84	84	mm
Cavity length	105	147	cm
Cavity diameter	34.5	35.4	cm
V_T^*	0.375	0.375	MV
E_p^*	4.26	4.75	MV/m
B_p^*	7.4	7.77	mT
$[R/Q]_T$	488.4	708.1	Ω
Geometrical Factor (G)	127.8	131.8	Ω
$R_T R_S$	6.2×10^4	9.3×10^4	Ω^2
At $E_T^* = 1$ MV/m			

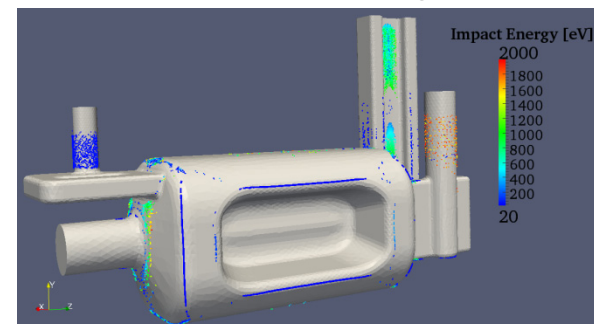


400 MHz Crabbing Cavity Prototype

- Work done in collaboration with Zenghai Li at SLAC
- With the completion of the 400 MHz cylindrical rf-dipole cavity (proof of principle cavity), now focusing on the next generation of the LHC crabbing cavity design
- Requires to deliver vertical and horizontal crabbing

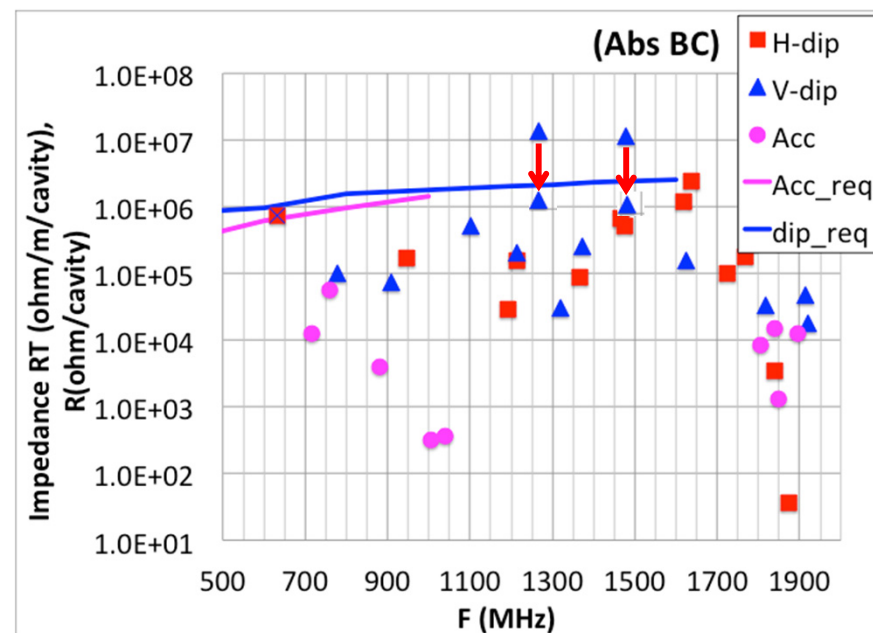
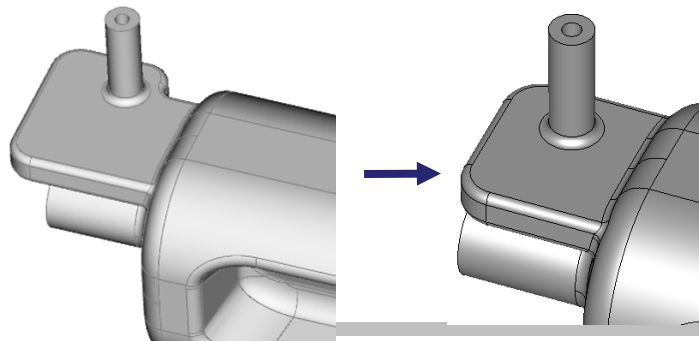
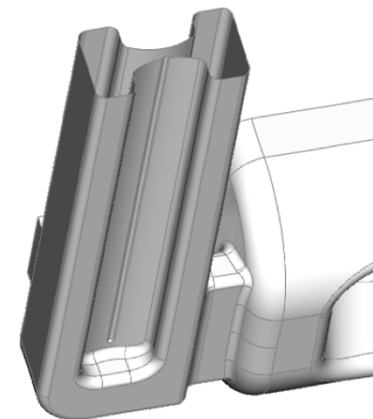


Improved multipacting levels



Damping of Higher Order Modes

- Horizontal HOM Coupler
 - Ridged waveguide coupler
 - Operating mode below cutoff – naturally reject operating mode
 - Couple to both horizontal dipole and accelerating HOM modes
 - Groove reduces multipacting levels at the waveguide
- Vertical HOM coupler
 - Selective WG-stub-coaxial coupler, does not couple to operating mode - no filter needed
 - Damps both vertical HOM and accelerating HOM modes
 - Asymmetric probe position to couple to higher HOMs (e.g. quad, etc)



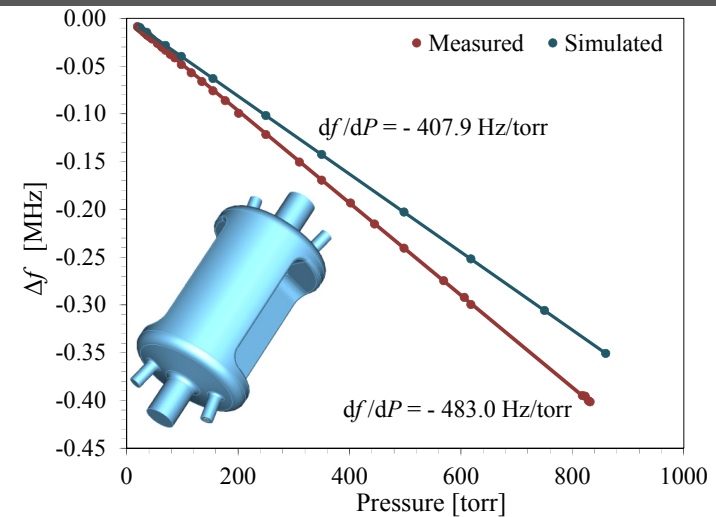
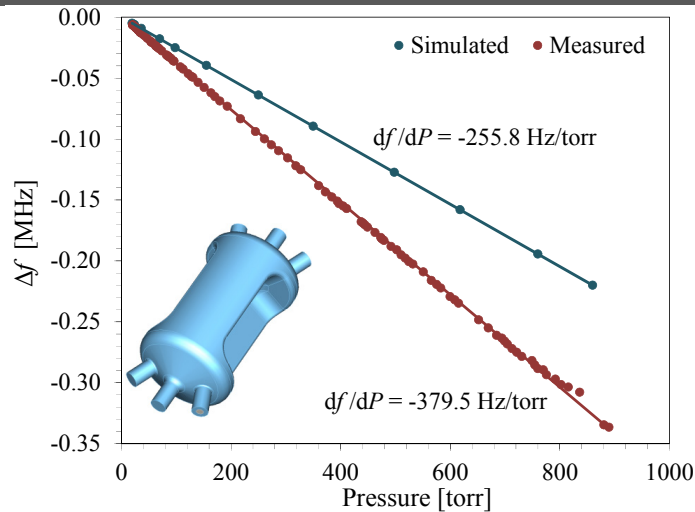
Summary

- Proof-of-Principle 499 MHz and 400 MHz cavities were tested
 - 499 MHz cavity achieved a low surface resistance and high fields
 - 400 MHz cavity achieved high surface fields (7 MV deflecting voltage cw which is twice design voltage)
 - High residual losses due losses at the stainless steel flanges
- In both cavities multipacting quickly processed and did not reoccur
- RF Dipole cavity has attractive properties compared to TM_{110} Cavity
 - Small size
 - Low surface fields
 - No lower-order modes
 - Widely separated higher-order modes
 - Disadvantage: due to its small size, probably could not be used at as high a frequency and large aperture

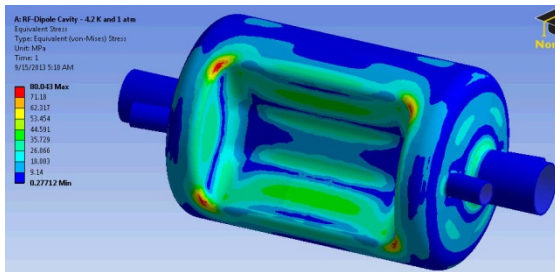
Acknowledgements

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- ODU
 - Chris Hopper
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 - Rocio Olave
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 - HyeKyoung Park
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 - Tom Powers
 - Kirk Davis
 - Pete Kushnick
 - Dave McCay
 - Casy Apeldoorn
 - Danny Forehand and his team
 - Steve Castagnola and his team

Pressure Sensitivity

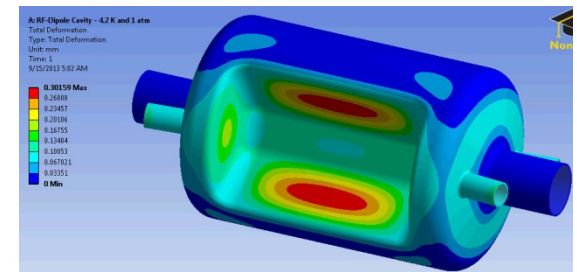


- Simulated in ANSYS with 3 mm uniform thickness
- Difference between simulation and measurements are possibly due to varying cavity thickness and material properties
- The edges of loading elements require reinforcement to reduce the stresses

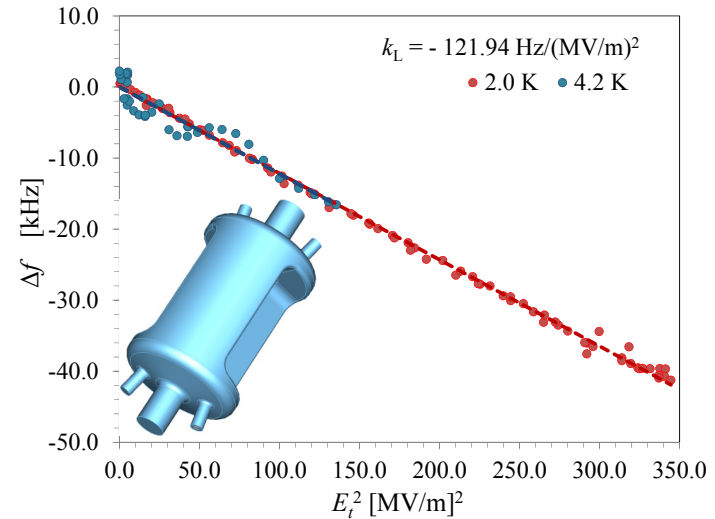
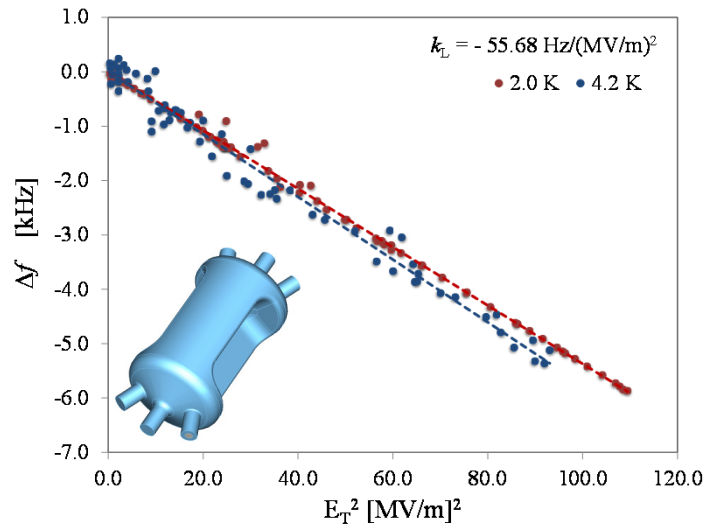


Stresses at 4 K

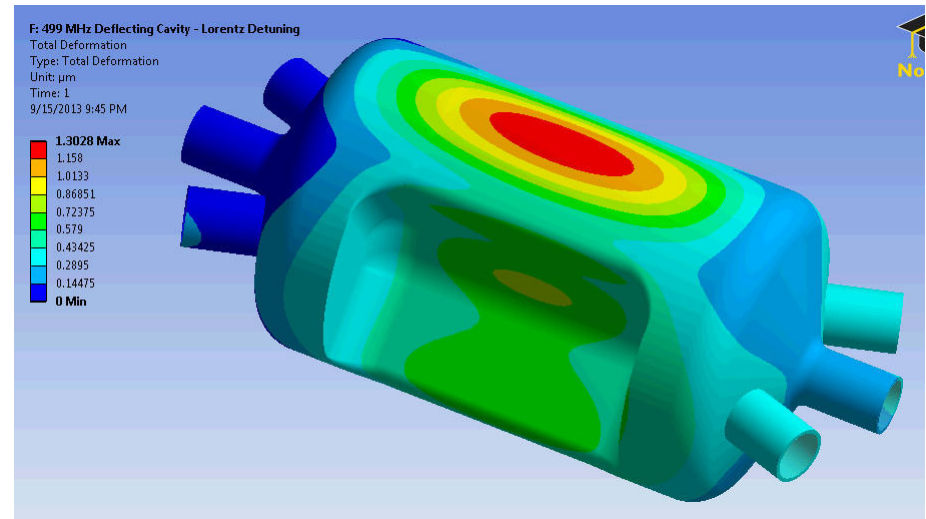
Deformation at
4.0 K due to
pressure of 1 atm



Lorentz Detuning

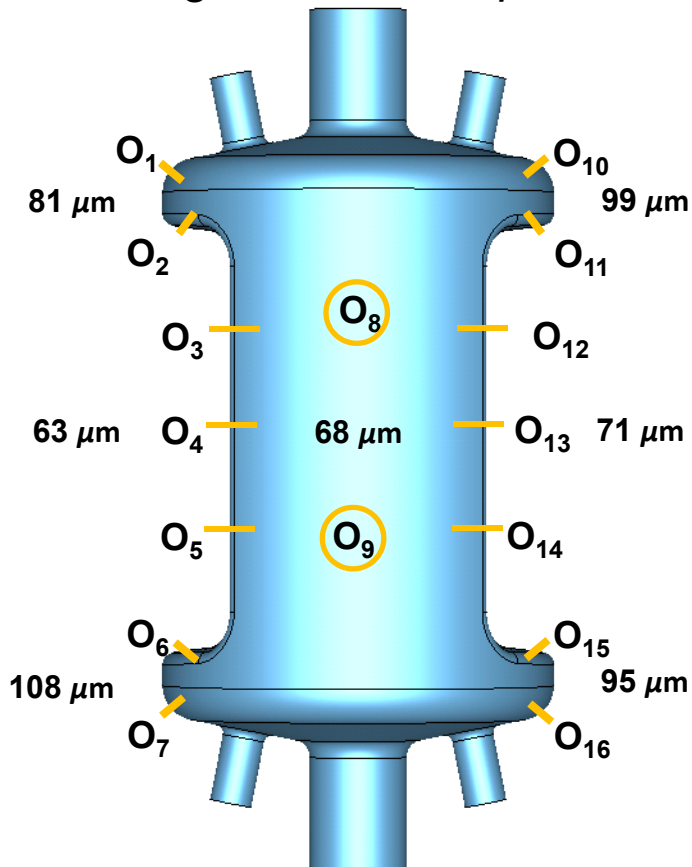


- Simulated Lorentz coefficient (k_L)
 - 499 MHz $\rightarrow -52.4 \text{ Hz}/(\text{MV/m})^2$
 - 400 MHz $\rightarrow -117.3 \text{ Hz}/(\text{MV/m})^2$



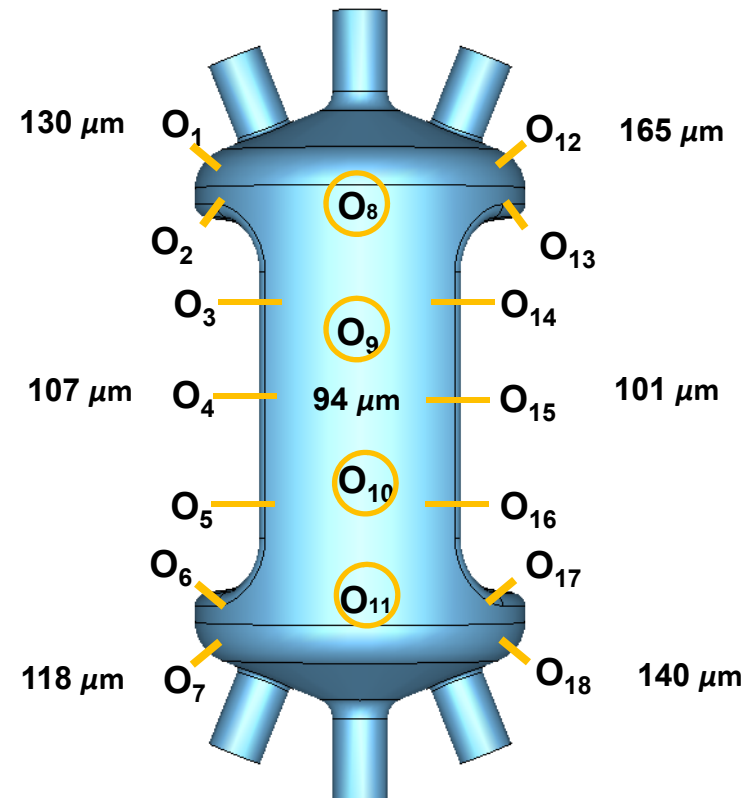
Surface Treatment – Bulk BCP

- Reduced etch rate from 2.7-2.8 $\mu\text{m}/\text{min}$ to 1.8 $\mu\text{m}/\text{min}$ due to contaminated acid mixture (with glycol)
- Average removal 85 μm



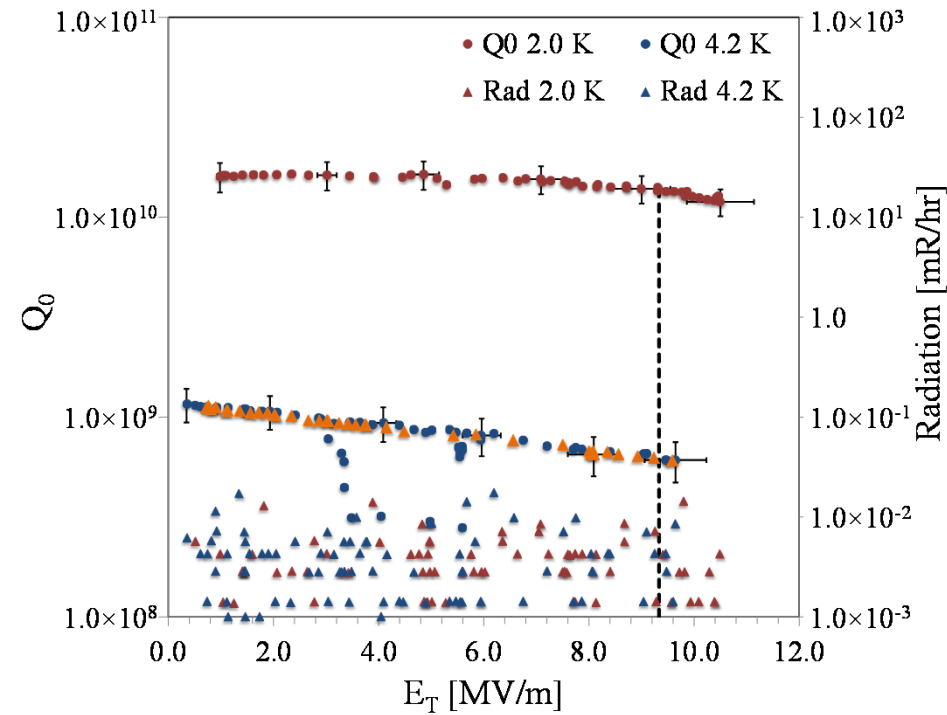
Panametrics 25DL-
Plus Ultrasonic
Precision
Thickness Gage

- Etch rate: 1.78 $\mu\text{m}/\text{min}$
- Average removal 108 μm

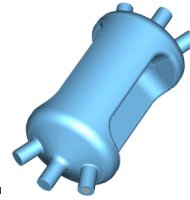


Average of O₁₉, O₂₀, O₂₁ and O₂₂ – 99 μm

Field Emission



400 MHz
Deflecting
Cavity



499 MHz
Deflecting
Cavity

