

HEIMHOITZ

HOM damping concept

**Zentrum Berlin** 

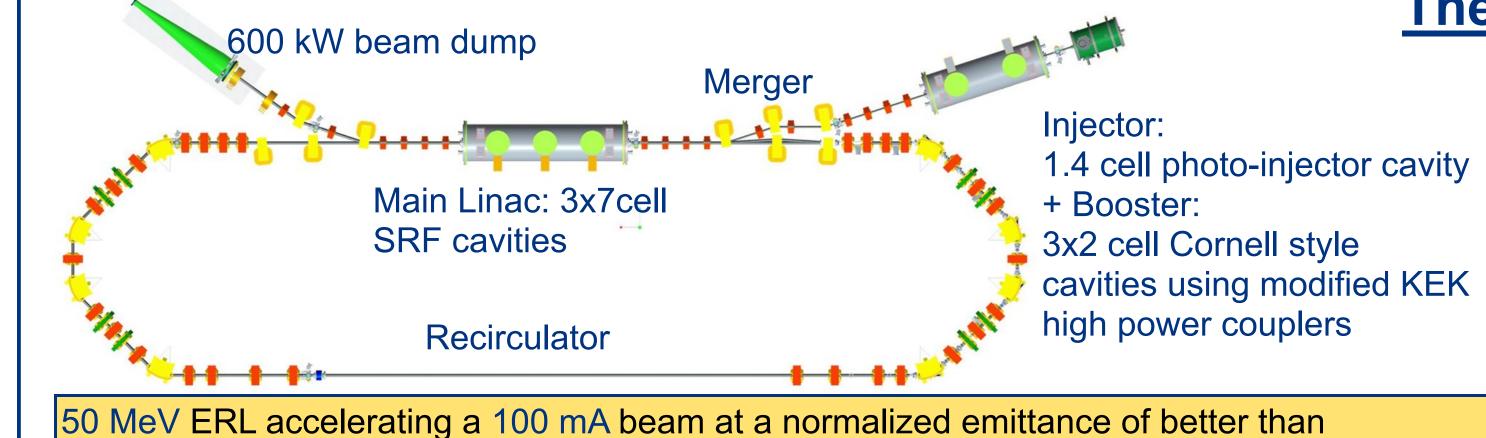
**bERLinPro** 

A.Neumann<sup>\*</sup>, J. Knobloch- Helmholtz-Zentrum Berlin, 12489 Berlin, Germany B. Riemann, T. Weis- University Dortmund, Dortmund, Germany

K. Brackebusch, T. Flisgen, T. Galek, U. van Rienen- University Rostock, Rostock, Germany



## The bERLinPro Energy Recovery Linac



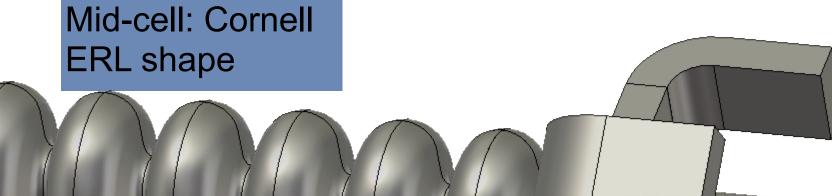
# **The Linac Cavity design**

CW-modified TTF-III fundamental power coupler (FPC) for variable loaded  $Q(Q_{\rm L})$ 

tube

5 waveguides close to he cavity iris

by JLab:



mm mrad filling every RF bucket at 1.3 GHz [1]. The main Linac cavities have to accelerate and on second pass decelerate the beam from 6.5 MeV injection energy to 50 MeV and vice versa.

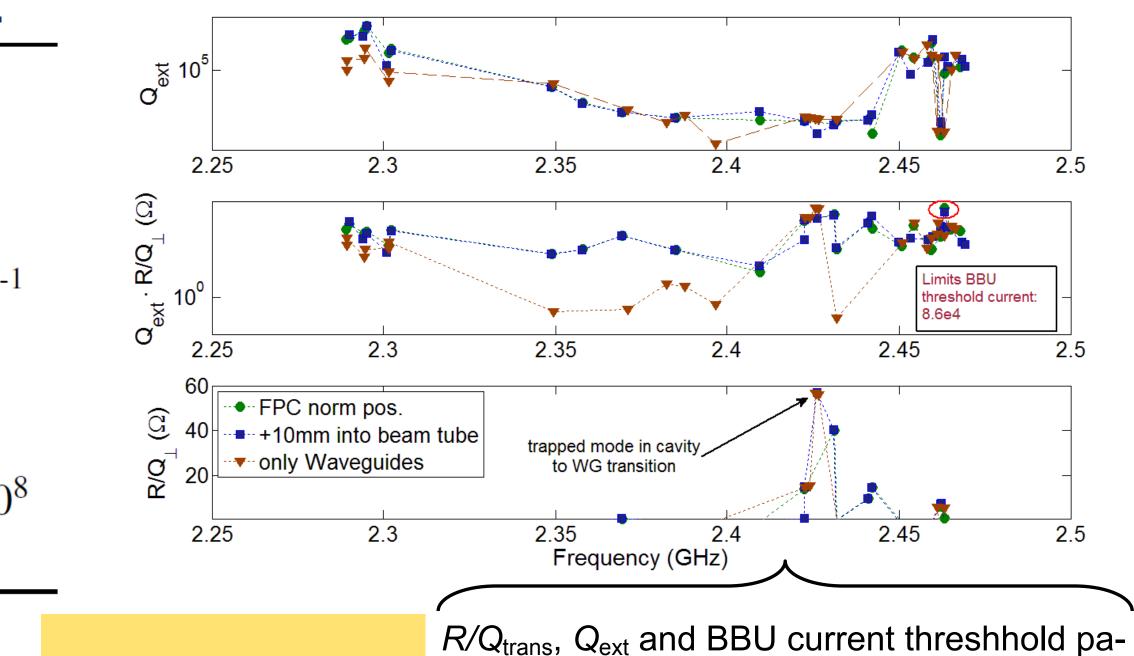
Thus, the cavities operate at high CW accelerating gradient of about 20 MV/m and interact with two 180 deg. in phase shifted high current beams.

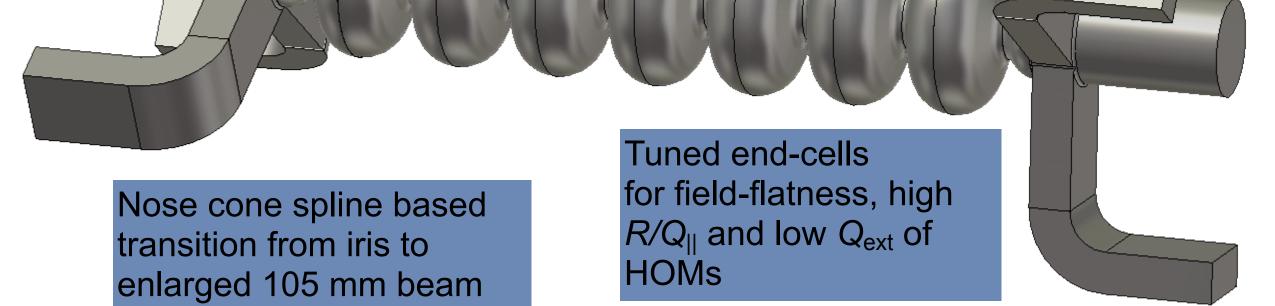
The cavity design therefore requires excellent RF properties as high R/Q and low peak field ratios for the fundamental, but also good propagation of higher order modes (HOM) and subsequent damping.

Any unwanted coupling between the beam and dipole-like field patterns of any HOM can contribute to the beam-break-up (BBU,[2]) instability.

## **RF and HOM damping performance**

Number of cells  $788 \Omega$  $R/Q_{\parallel}$ 1.3 GHz  $f_{\rm TM_{010}} - \pi$  $E_{\rm peak}/E_{\rm acc}$ 2.08  $4.4 \text{ mT/MVm}^{-1}$  $B_{\rm peak}/E_{\rm acc}$  $\leq 8 \cdot 10^3$  $Q_{\text{ext}} \operatorname{TM}_{110}$  dipole 1.596 GHz Beam tube  $TE_{01}$  cutoff 1.576 GHz Waveguide  $TE_{10}$  cutoff  $1 \cdot 10^7 - 1 \cdot 10^8$  $Q_{\rm L}$  for TM<sub>010</sub>- $\pi$  $P_{\text{forward}}$  at  $Q_{\text{L}} = 5 \cdot 10^7 (\Delta f = 0)$ 1.4 kW 10°



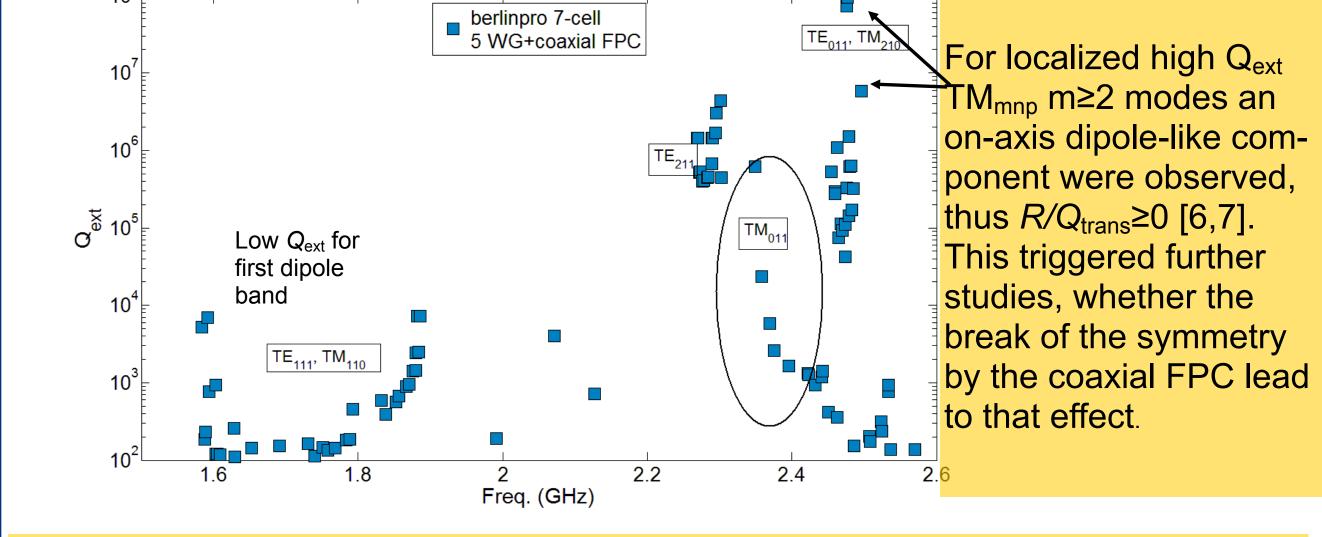


### Convergence studies:

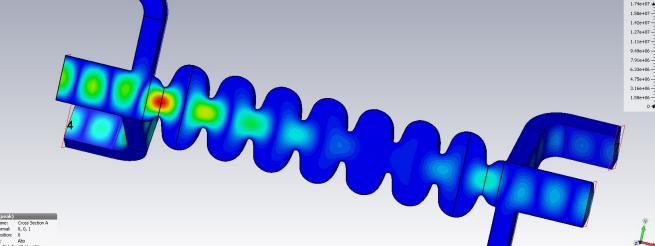
Optimization and calculations up to high frequencies of up to 10 GHz using 2D codes is prohibited by the non-symmetric design. To reliably predict a BBU limit, Q<sub>ext</sub> should be at least determined with an accuracy below an order of magnitude. Thus, convergency studies were conducted for the  $Q_{ext}$  of HOMs, especially of the limiting quadrupole passband. Using CST's 2014 new mesh type, a convergence for the rather low Q TM mono- and dipole modes was demonstrated.

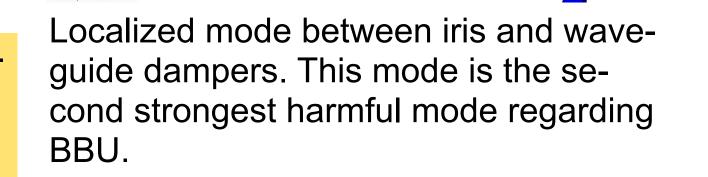
However, high Q quadrupole modes still show a variation with mesh density. At higher mesh density computational time was increasing and the solution itself would not converge.

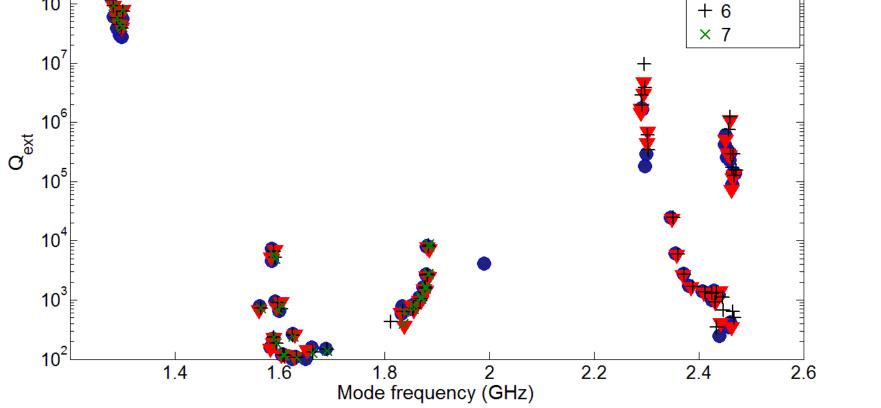




rameter  $R/Q_{trans} x Q_{ext}$  for an all WG system compared to the 5WG+coax. system for two different coupling strength of the FPC. The limit is set by a TM<sub>210</sub> mode for the sysrems with coaxial FPC.







#### **Conclusion:**

Due to the localized mode in the endgroup and a nonvanishing dipole component of high Q<sub>ext</sub> quadrupole modes, the endgroups have to be reworked accompanied by a thorough multipole analysis of the HOMs.

HOM damping of the RF design after a particle swarm based optimizatin of the endcells while keeping peak field ratios low, field-flatness above 98% and  $R/Q_{\parallel} \ge 110 \Omega/$ cell [9,10].

### **Coupler kick and emittance dilution calculations**

