

## PLANS FOR A SUPERCONDUCTING H<sup>-</sup> LINAC (SPL) AT CERN

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### Abstract

As part of the upgrade of the LHC injector complex at CERN, the construction of a 4 GeV Superconducting Proton Linac (the SPL, in fact an H<sup>-</sup> accelerator) is planned to begin in 2012. Depending upon physics requests, it should be upgradeable to 5 GeV and multi-MW beam power at a later stage. The construction of Linac4, its low energy front end, has started at the beginning of 2008. A full project proposal with a cost estimate for the low power version of the SPL aimed at improving LHC performance has to be ready for mid-2011. As a first step towards that goal, essential machine parameters like RF frequency, cooling temperature and accelerating gradient have recently been revisited and plans have been drawn for designing and testing critical components.

### INTRODUCTION

The foreseen upgrade of the LHC injector complex [1] will entail the construction of PS2, a new 50 GeV synchrotron and of the SPL as its injector. The SPS will not be replaced, but it will be significantly upgraded. The layout of these new accelerators on the CERN site has been decided [2] and Linac4 [3], the SPL front-end, is being built at its final location (Fig. 1).

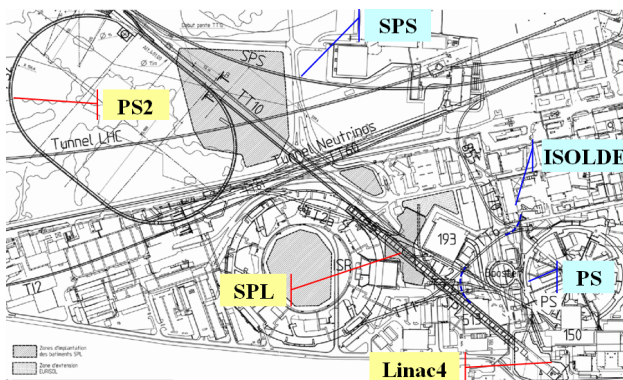


Figure 1: Layout of the new injector complex.

The flexibility and the potential of evolution of the SPL will make it an important asset for physics in the future [4]. As injector of PS2, only a 4 GeV low power version of the SPL is needed (“the “LP-SPL”). For a neutrino facility, the LP-SPL would have to be upgraded to 5 GeV and 4 MW of beam power, and accompanied with an accumulator and a compression ring to meet the required time structure of the beam [5]. For a Radioactive Ion Beam Facility of the next generation [6], a similar beam power would also be required at 2.5 GeV. A summary of the specifications of the accelerator in its different possible phases of implementation is given in Table 1.

As a first step in the preparation for the project proposal to be submitted to the CERN Council by mid-2011, the

choice of the basic parameters of the SPL [7] has been revisited during the past months in view of optimizing synergy with the worldwide development effort on superconducting accelerating structures cavities. The RF frequency was therefore reconsidered, as well as the cooling temperature of the superconducting cavities and the foreseeable accelerating gradients [8, 9, 10].

Table 1: Main Characteristics of the Successive Phases of Realization of the SPL

	LP-SPL	SPL (5 GeV)	SPL (2.5 GeV)
Users	PS2 ISOLDE	+ ν facility	+ RIB facility
T [GeV]	4	5	2.5
P <sub>beam</sub> [MW]	0.2	4	4
F <sub>rep</sub> [Hz]	2	50	50
I <sub>source</sub> [mA]	40	80	80
Chopping	yes	yes	no
I <sub>av</sub> [mA]	20	40	40
T <sub>pulse</sub> [ms]	1.2	0.4	0.8

### DESIGN OPTIONS

The RF frequency of 352 MHz has been selected for Linac4, because it is very well matched for use in the low energy front end of a proton linac and because of the large inventory of RF hardware available at that frequency since the decommissioning of LEP. Hence only harmonics of 352 MHz can be considered for acceleration after Linac4 (160 MeV). The three design options which have been compared [9] (Table 2) were especially aimed at analysing the interest of 1408 MHz which is close to the frequency used in the ILC and X-FEL projects.

An updated survey of recent experimental results, confirmed the 2006 conclusion [7, 10] that the maximum accelerating gradient of bulk Niobium cavities only depends on geometry ( $\beta_{\text{geometrical}}$ ) and on the quality of the surface treatment techniques, and not on the RF frequency. It is therefore assumed when comparing the length of the different options that the superconducting elliptical cavities operate at an accelerating gradient corresponding to the same peak surface field of 50 MV/m, as in a  $\beta=1$  cavity with an accelerating gradient of 25 MV/m. Their characteristics are given in Table 3.

The “Nominal” option in Table 2 is a slightly improved version of the SPL design published in 2006 [7]. It uses only 2 types of 5 cell elliptical cavities and has a length of 439 m.

Table 2: SPL Design Options

	Nominal	High frequency	Hybrid
Frequency [MHz]	704	1408	352/1408
Type of cavities	elliptical	elliptical	spoke/elliptical
$\beta_{\text{geometrical}}$	0.65/0.92	0.6/0.76/0.94	0.67/0.8/0.94
Number of cells/cavity	5/5	7/9/9	4/5/9
Input energies/section [MeV]	160/581	160/357/884	160/392/758
Accelerating gradient* [MV/m]	19.4/24.2	18.1/21.7/24.2	8.5/9.5/24.2
Number of cavities/focusing period	3/8	2/4/8	3/4/8
Number of cavities	42/200	30/40/208	27/24/216
Total number of cavities	242	278	267
Length of sc linac	439	499	485

\* Normalized for elliptical cavities to a peak surface field of 50 MV/m.

Table 3: Estimated Characteristics of SC Cavities

f [MHz]	$\beta_{\text{geometric}}$	R/Q [ $\Omega$ ]	$Q_0$ [ $10^9$ ] @4.5/2 K	$E_{\text{acc}}$ [MV/m]
704	0.65	285	0.3/5.8	19.4
704	0.92	501	0.4/7.7	24.2
1408	0.60	441	0.1/2.3	18.1
1408	0.76	671	0.12/2.5	21.7
1408	0.94	931	0.15/3.2	24.2

In the “High frequency” option, 1408 MHz elliptical cavities are used immediately after Linac4. To preserve comparable real-estate gradient, cavities with more cells must be used, which reduces their energy range and forces to have three different types. Moreover, the accelerator length has to be 60 m longer because of the longer matching section needed by the x4 frequency jump.

In the “Hybrid” option, the transition to 1408 MHz is done at 758 MeV only, using spoke cavities operating at 352 MHz immediately after Linac4. Two different types of Spoke and one type of elliptical cavities are needed. The total length remains 46 m longer than in the nominal case.

## ANALYSIS

### Beam Dynamics

Similar design principles are used in all options, using similar focusing periods and avoiding space charge resonances by keeping an approximately constant ratio between transverse and longitudinal phase advances. Beam dynamics performance is compared in terms of r.m.s. emittance growth and sensitivity to RF field errors.

Transverse emittance growth is small in all cases [between 1.5 (5.3) and 5.6 (8.2) % for  $\epsilon_x$  (resp.  $\epsilon_y$ )], with a slight advantage for the “hybrid” option. The situation is

more contrasted in the longitudinal phase plane where the “high frequency” option is clearly worse (12 % blow-up instead of 6.8 % and 2.5 % in the “nominal” and “hybrid” cases). This is confirmed by the analysis of the effect of RF field errors and energy/phase jitter of the Linac4 beam, 4.2 % of the simulation runs showing particle loss with the “high frequency” option.

### Impact of Frequency on Cavity Parameters

The characteristic impedance R/Q of a one cell elliptical cavity with a given geometry is independent of its resonant frequency f. The impedance per unit of length is then proportional to f.

The stored energy, for the same accelerating gradient, scales like the volume as  $1/f^3$ . Hence the energy stored in a 1408 MHz multi-cell cavity is  $1/4$  of the energy stored in a 704 MHz cavity of the same length (and less cells). Since SPL cavities are pulsed, filling them with RF field uses four times more wall-plug power at 704 MHz.

For longitudinal High Order Modes (HOM), similar reasoning shows that the short range wake-field is 4 times larger in a 1408 MHz multi-cell cavity. The impedance for long range longitudinal wake-fields is between 8 and 16 times larger, depending upon the mode. The impedance for transverse long range dipole modes is between 8 and 32 times larger, resulting in a reduction by the same factor of the threshold for the onset of beam break-up.

In the case of real/imperfect structures, the production scatter in the individual cell frequencies and end-cell correction for the fundamental mode disturbs the HOM field profiles. This makes their coupling and hence their damping more uncertain by a factor 2 to 4 in the 1408 MHz case.

### Impact of Frequency on RF Hardware

RF equipment is more compact at higher frequency, which increases the difficulty to dissipate the heat

generated at  $\sim 10\%$  duty cycle. 1 MW class hybrids and amplitude & phase modulators will be especially challenging to design at 1408 MHz. For klystrons, manufacturers have clearly expressed their reluctance for similar reasons.

### Cryogenics Issues

The design of the SPL cryomodule will re-use as much as possible of the state-of-the-art development made for the ILC. Static cryogenic losses are minimized using a long cryomodule with a high packing factor and containing the helium supply and return pipes. The pumping return line is also a structural element securing the alignment of the cavities and magnets. It is however impossible to duplicate exactly the ILC device because of the 1.7 % slope of the SPL (ILC: 0.6 %), and because of the 10 times higher duty factor of the SPL which imposes new designs for the RF and HOM couplers.

The quality factor  $Q_0$  estimated [9] at the indicated gradient for the different types of superconducting elliptical cavities is shown in Table 3. It is more than 20 times larger at 2 K than at 4.5 K, independently of frequency, and more than 2.5 times higher at 704 than at 1408 MHz. Taking these estimates and static loads [7] into account, the equivalent cryogenic load of the 5 GeV-4 MW SPL for the “nominal” and high frequency” options is given in Table 4. Electrical power consumption imposes clearly to operate cavities at much lower temperature than 4.5 K.

Table 4 also shows the power required by RF which is  $\sim 9$  MW larger at 704 MHz because of the larger stored energy in the cavities (see above).

Table 4: Cryogenic load and electrical consumption of the 5 GeV/4 MW SPL

Option [see Table 2]	$T_{\text{cryo}}$ [K]	$Q_{\text{eq@4.5K}}$ [kW]	$P_{\text{el}}(\text{cryo})$ [MW]	$P_{\text{el}}(\text{RF})$ [MW]
“Nominal”	2	20.8	5.2	25.5
“Nominal”	4.5	95.4	23.9	25.5
“High frequency”	2	18.3	4.6	16.3
“High frequency”	4.5	81.9	20.5	16.3

### Achievable Gradient

The performance of cavities recently built for SNS and at DESY has been analysed [10]. For a yield of 90 %, the maximum achievable equivalent gradient in  $\beta=1$  cavities is between 16 MV/m (SNS) and 23 MV/m (DESY). Higher gradients like the 25 MV/m presently assumed in the SPL can only be achieved after reprocessing a large number of cavities and/or with an improved surface treatment (electro-polishing). It is therefore important to design and build SPL-type superconducting cavities in the near future to arrive at a realistic estimate.

## CONCLUSION AND PLANS

The main advantage of the “high frequency” option is its smaller power consumption which may be balanced against its longer length and larger number of cavities and cavity types with respect to the “normal” option. For a high power proton accelerator where beam losses have to be minimized, it suffers however from less tolerance to energy/phase jitter of the Linac4 front end. Moreover, the high power RF components that it requires are much more difficult to design/build/buy. The “hybrid” option suffers from the same drawbacks, plus the need to develop an additional family of cavities (spokes). 704 MHz is hence confirmed as the correct choice for the frequency and  $\sim 2$  K for the cooling temperature of the SPL. Although valuable for the LP-SPL, these choices are mandatory for the foreseen high power/ high duty cycle extensions.

The accelerating gradient that can be expected with a reasonable yield deserves further investigation.

The main goals of the next 3 years will hence be to:

- optimize the overall design of the SPL,
- build and test 704 MHz superconducting cavities to better estimate the achievable accelerating gradient,
- design and test a solution for stabilization of the field in pulsed mode,
- progress in the development of an  $H^+$  ion source,
- design, assemble and characterize a complete high energy cryomodule.

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