# **RF PERFORMANCE OF NITROGEN-DOPED PRODUCTION SRF** CAVITIES FOR LCLS-II\*

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# Abstract

The Linac Coherent Light Source II (LCLS-II) requires 280 9-cell superconducting RF cavities for operation in continuous wave mode. Two vendors have previously been selected to produce the cavities, Research Instruments GmbH and Ettore Zanon S.p.a. Here we present results from manufacturing and cavity preparation for the cavities constructed at these two vendors for LCLS-II. We show how the cavity preparation method has been changed mid-production in order to improve flux expulsion in the cavities and maintain high performance in realistic magnetic field environments (~5 mG). Additionally, we show that the nitrogen-doping process has been carried out successfully and repeatedly on over 70 cavities.

## **INTRODUCTION**

The Linac Coherent Light Source II (LCLS-II) is a new x-ray light source being built at SLAC which utilizes the latest superconducting RF (SRF) technology. The machine will operate 280 Tesla-shape [1] 9-cell 1.3 Ghz cavities in continuous wave (CW) mode [2]. Operating in CW mode at sufficiently high gradients requires that the cavities have very low cryogenic losses in order to maintain economic viability of the machine. LCLS-II has chosen to operate the cavities at an accelerating gradient of 16 MV/m with a  $Q_0$  of 2.7×10<sup>10</sup> (~10 W of dissipated power at 2 K). The choice of these parameters enables the machine to be run with one 4 kW cryoplant. In addition to these specifications, the cavities must reach 19 MV/m in vertical test in order to account for errors in the gradient measurement and provide sufficient head room for the operating gradients in the cryomodule. Here we present on the results from the first cavities prepared an production for LCLS-II.

# **CAVITY PREPARATION**

In order to meet the ambitious  $Q_0$  specification of  $2.7 \times 10^{10}$  at 16 MV/m and 2.0 K, the SRF cavities for LCLS-II are being prepared with nitrogen-doping. Nitrogen-doping has been shown repeatably to produce  $Q_0$ 's significantly higher than with standard cavity preparation methods [3, 4].

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Nitrogen-doping typically consists of treating a niobium SRF cavity at high temperature in a low-pressure nitrogen atmosphere. It consistently produces 1.3 GHz cavities with  $Q_0$ 's on the order of  $2.7 \times 10^{10}$  or higher by lowering of the temperature-dependent BCS resistance (R<sub>BCS</sub>). Typical nitrogen-doped cavities have R<sub>BCS</sub> on the order of 4-7 n $\Omega$  at 16 MV/m.

For LCLS-II, niobium sheet was procured from two vendors, Tokyo Denkai and OTIC Ningxia. The cavities are being fabricated by two vendors, Ettore Zanon S.p.a. and Research Instruments GmbH. Thus far into cavity production, material from Tokyo Denkai has primarily been used. The cavities have been prepared with two different cavity preparation recipes as outlined in Table 1. Cavities are given a bulk electropolish (EP) (first 140  $\mu$ m and later 200  $\mu$ m) followed by a degas in vacuum at high temperature (first 800°C then 900°C). Throughout this paper, the amount of removal by EP is measured by weight. Next comes the nitrogen-doping step which is carried out at 800°C in ~25 mTorr of nitrogen gas for two minutes followed by an additional 6 minutes of vacuum annealing. Finally the cavities are given a light EP of 5-7  $\mu$ m. This recipe is known as the "2/6" nitrogen-doping recipe. The motivation for changing the recipe during production will be discussed in the next section. Results shown here will primarily focus on cavities produced at one vendor, denoted "Vendor B" from now on. A thorough discussion of vendor production and progress is presented in [5].

# **CAVITY RF RESULTS**

All production cavities for LCLS-II are tested at 2.0 K up to a maximum field of 24 MV/m, administratively limited in order to reduce the risk of field emission activation. Some cavities were tested beyond this limit. Figure 1 shows the  $Q_0$  of the first ~60 cavities tested at 16 MV/m from Vendor B. The point at which the recipe change is marked along with the LCLS-II specification of  $2.5 \times 10^{10}$  (lowered from  $2.7 \times 10^{10}$  for vertical test due to the inclusion of a stainless steel blank on one side of the cavity leading to an increase in R<sub>res</sub> of ~0.8 nΩ). A full discussion of the  $Q_0$  performance and the recipe change will be given in the following section.

Figure 2 shows the maximum gradient reach for cavities produced at vendor B. Note that all cavities shown exceed the 16 MV/m specification and all but two exceed 19 MV/m.

<sup>\*</sup> Work Supported by the DOE and the LCLS-II Project.

#### Proceedings of IPAC2017, Copenhagen, Denmark

Recipe	Bulk EP	Furnace Degas	Degas Time	N-Doping	N-Doping	N-Doping	Anneal	Final EP
		Temperature		Temperature	Time	Pressure	Time	
Original <sup>1</sup>	140 µm	800°C	3 hours	800°C	2 min	25 mTorr	6 min	5-7 μm
Revised <sup>2</sup>	$200 \ \mu m$	900°C	3 hours	800°C	2 min	25 mTorr	6 min	5-7 μm

Table 1: The nitrogen-doping recipes carried out on cavities for LCLS-II

<sup>1</sup> Original recipe on Vendor B cavities CAV0001-CAV0016 and Vendor A cavities CAV200-207.

<sup>2</sup> Revised recipe on Vendor B cavities CAV0017 and above and Vendor A cavities CAV208 and above.



Figure 1:  $Q_0$  at 16 MV/m and 2.0 K for cavities produced for LCLS-II with both recipes at vendor B. The vertical test specification of  $2.5 \times 10^{10}$  is shown as is the point where the recipe change was made. It is clear that the average  $Q_0$ improved dramatically after the recipe change. Cavities with  $Q_0$ 's of  $3.5-4 \times 10^{10}$  are now produced reliably.

Most cavities reach the administrative limit of 24 MV/m, providing significant headroom for operation in cryomodules. This also demonstrates that the "2/6" nitrogen-doping recipe used, does not lead to a reduction in quench field large enough to impact operation at medium fields.

### *Recipe Change*

RF results from the original recipe as outline in Table 1 proved good but not great. In low magnetic field environments,  $Q_0$ 's averaged below  $2.5 \times 10^{10}$  with many cavities in the region of  $2.2 \cdot 2.3 \times 10^{10}$  and a few above  $2.5 \times 10^{10}$ . This performance, while good by previous state-of-the-art cavity preparation methods is not as good as cavities in the R&D stage of the LCLS-II production and is not sufficient for the high demands of LCLS-II. Therefore a recipe change was required to improve performance. Two factors were found to be the cause of the low  $Q_0$  through studies on single-cell cavities made with production niobium sheet: insufficient bulk material removal leading to a slight increase in residual resistance (R<sub>res</sub>) and poor flux expulsion when compared with prototype material from ATI Wah-Chang.

These two effects were addressed by increasing the bulk removal from 140 to 200  $\mu$ m and increasing the furnace degas temperature from 800 to 900°C. Increasing the temperature



Figure 2: Maximum gradient reached in production LCLS-II cavities produced by vendor B. The cavities must reach a field of 19 MV/m. An administrative limit is placed on the cavity tests at 24 MV/m which has been exceeded in some cases.

has been shown to improve flux expulsion in single-cell cavities manufactured from the same production material [6]. The effect of this change can be seen in Fig. 3. At 16 MV/m, the original recipe led to an increase of ~5.5 n $\Omega$  when increasing the ambient field from 5 to 10 mG. With the revised recipe this change dropped to < 0.5 n $\Omega$ . This change is a direct result of improved flux expulsion with the revised recipe.

The change in  $\Delta R_{res}$  is translated to a dramatic improvement in  $Q_0$ . In Fig. 1, above cavity 16, the average  $Q_0$  significantly increases. Cavities now routinely exceed  $3 \times 10^{10}$ with some cavities even reaching as high as  $4 \times 10^{10}$ . It is also important to note that all cavities prepared with the original recipe were tested in ambient magnetic fields that were carefully controlled and therefore well below 5 mG. After the recipe change, cavities were tested in higher fields, upwards of 10 mG and still maintained high  $Q_0$ .

### **BCS RESISTANCE**

Nitrogen-doped cavities are characterized by improvement in their temperature-dependent BCS resistance,  $R_{BCS}$ , via two mechanisms: an overall lowering of  $R_{BCS}$  at low fields due to a lowering of the mean free path, and the introduction of an anti-Q slope which enables  $R_{BCS}$  to decrease as the accelerating gradient is raised [4].  $R_{BCS}$  is therefore



Figure 3: The change in residual resistance between cooldowns in 10 and 5 mG ambient magnetic fields with similar cool down conditions on two cavities: one with the original recipe, one with the revised recipe. At 16 MV/m, the original recipe led to an increase of ~5.5 n $\Omega$  when increasing the ambient field from 5 to 10 mG. With the revised recipe this change dropped to < 0.5 n $\Omega$ .

a good measurement of the strength of the nitrogen-doping in an SRF cavity. During the LCLS-II R&D phase, it was confirmed that  $R_{BCS}$  at 16 MV/m and 2.0 K should be on the order of 4-6 n $\Omega$  [4].

 $R_{BCS}$  is typically extracted by taking  $Q_0$  versus  $E_{acc}$  data at multiple temperatures, enabling the  $R_{res}$  component of  $R_s$  to be removed at 2.0 K. Figure 4 shows  $R_{BCS}$  versus  $E_{acc}$  for a subset of LCLS-II production cavities from both vendors which had low temperature data taken (cavities prepared with both recipes are shown). The anti-Q slope is clearly present in all cavities shown, demonstrating a decrease in  $R_{BCS}$  from 6-7 n\Omega at low fields to 4-5 n\Omega at 16 MV/m. Additionally, Fig. 5 shows  $R_{BCS}$  at 16 MV/m and 2.0 K for the same cavities. From this it is clear that  $R_{BCS}$  for the production cavities is what is expected for nitrogen-doped cavities prepared with the 2/6 recipe. This demonstrates that the nitrogen-doping was successfully transferred from the partner labs and the R&D phase to production at cavity vendors.

### CONCLUSIONS

Results from the first ~60 cavities from Vendor B are very promising. After a recipe change due to the need for more efficient flux expulsion,  $Q_0$ 's in production cavities are typically higher than  $3 \times 10^{10}$  with some reaching as high as  $4 \times 10^{10}$ . Flux expulsion was indeed improved dramatically after the furnace degas temperature was raised. Likewise, gradient reach has been fantastic, with most cavities reaching above 20 MV/m and a significant number reaching the administrative limit of 24 MV/m. Finally, the nitrogen-doping protocol was successfully transferred to both cavity vendors. Cavities reliably show a strong anti-Q slope and R<sub>BCS</sub> at

ISBN 978-3-95450-182-3



Figure 4:  $R_{BCS}$  at 2.0 K versus  $E_{acc}$  for a subset of production cavities tested at low temperatures. All cavities shown display the characteristic anti-Q slope (decreasing  $R_{BCS}$  with increasing  $E_{acc}$ ) between 5 and 20 MV/m. This demonstrates that the nitrogen-doping is being successfully carried out in production.



Figure 5:  $R_{BCS}$  at 16 MV/m and 2.0 K for cavities shown in Fig. 4. All cavities show a  $R_{BCS}$  less than 6 n $\Omega$ , consistent with expectations from R&D and prototype cavities. Nitrogen-doping has been successfully transferred to the vendors for production.

16 MV/m and 2.0 K of 4-5 n $\Omega$ , consistent with expectations from the R&D phase.

Production will continue and all cavities are expected to be received by the end of 2017. We expect to continue having great results in terms of  $Q_0$  and gradient reach. Future work will focus on ensuring  $Q_0$  performance is maintained through Vendor A.

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