

### MAGNET DESIGN AND CONTROL OF FIELD QUALITY FOR TPS BOOSTER AND STORAGE RINGS

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IPAC15



- Introduction
- Magnet manufacture and inspection
- Mechanical error of magnet
- Magnetic field performance of magnet
- Magnet center inspection
- Permeability inspect of BR vacuum chamber
- Field distortion from the permeability chamber
- Summary





## Milestone of magnet manufacture



| 2005 |                | Preliminary design of the magnet                              |                   |
|------|----------------|---|-------------------|
| 2007 |                | <b>TPS project approved</b>                                   |                   |
| 2009 |                | Magnet prototype constructed and                              | examined in house |
| 2011 |                | <b>One-section prototype (23 magnets)</b>                     | finished          |
| 2012 |                | Mass production of magnet was beg                             | gun               |
| 2013 | Oct.           | All magnets completed   |                   |
| 2014 | Aug.           | Accelerator install completed                                 |                   |
| 2014 | mid-Dec.       | Hardware testing and improvement                              | t completed       |
| 2014 | <b>Dec. 31</b> | First synchrotron light at 3 GeV wa<br>(no corrector applied) | s observed        |



### **Overview-1/24 section (1 cell)**





<u>1/24 section (1 cell):</u>
19 magnets: DM\*2+QM\*10+SM\*7
3 girders: 4m-long/girder
1 vacuum chamber: 14m-long





# Magnet parameter

| SR magnet                                | Dipole  | Quadrupole<br>short/long | Sextupole<br>A/B/C |
|--|---------|--------------------------|--------------------|
| Quantity                                 | 48      | 192 / 48                 | 96 / 48 / 24       |
| Magnetic length (m)                      | 1.1     | 0.3 0.6                  | 0.25               |
| Field strength (T,T/m,T/m <sup>2</sup> ) | 1.191   | 17/15.63                 | 478                |
| Magnetic gap height/diameter (mm)        | 46      | 74                       | 78                 |
| Number of turns / pole                   | 36      | 54 / 48                  | 26                 |
| Conductor dimension (mm <sup>2</sup> )   | 16 x 16 | 8×8 / 9×9                | 8 × 8              |
| Coolant hole diameter (mm)               | 7       | 4 / 4.5                  | 4                  |

| BR magnet                               | Dipole<br>BD/BH   | Quadrupole<br>QF/Q1/Q2/QM | Sextupole<br>S1/S2 |
|---|-------------------|---------------------------|--------------------|
| Magnet quantity                         | 42 / 12           | 48 / 12 / 12 / 12         | 24                 |
| Magnet length (m)                       | 1.6 / 0.8         | 0.3                       | 0.2                |
| Bore diameter or gap (mm)               | 21.4~23.8         | 36                        | 36                 |
| Number of turns / pole                  | 24                | 18 / 18 / 12 / 6          | 18                 |
| Normal field (T, T/m,T/m <sup>2</sup> ) | 0.819,-1.72,-12.3 | 11.26,25.8/14.3/-9.1/-4.2 | 200                |
| Conductor dimension(mm <sup>2</sup> )   | 13×13             | 5×5                       | 3×2                |
| Coolant hole diameter(mm)               | 6.5               | 2                         |                    |

Pole profile is machined by the Computer Numerical Control Machine (CNC)
 Pole profile is machined by the Wire Electrical Discharge Machine (WEDM)

Ref: C. S. Hwang et. al., "Status of accelerator lattice magnets design of TPS project", Proceedings of PAC 09, Canada (2009).



### Magnetic field specification-SR/BR

| Storage ring         |                      |                       |                         |                      |                      |                      |                      |
|----------------------|----------------------|-----------------------|-------------------------|----------------------|----------------------|----------------------|----------------------|
| SR-dipole (SR-DM)    |                      | SR-quadrupole (SR-QM) |                         |                      | SR-sextupole (SR-SM) |                      |                      |
| n                    | $B_nL/B_1L$          | n                     | $B_nL/B_1L$ $A_nL/B_1L$ |                      | n                    | $B_nL/B_2L$          | $A_nL/B_2L$          |
|                      | [×10 <sup>-4</sup> ] |                       | [×10 <sup>-4</sup> ]    | [×10 <sup>-4</sup> ] |                      | [×10 <sup>-4</sup> ] | [×10 <sup>-4</sup> ] |
| 0                    | 10000                | 1                     | 10000                   | -                    | 0                    | ±15                  | ±10                  |
| 1                    | <u>±</u> 3           | 2                     | ±2                      | <u>±2</u>            | 2                    | 10000                | -                    |
| 2                    | <u>±</u> 3           | 3                     | <u>±2</u>               | <u>±1</u>            | 3                    | ±2                   | <u>±2</u>            |
| 3                    | ±2                   | 4                     | ±0.5                    | ±0.3                 | 4                    | <u>±3</u>            | <u>±1</u>            |
| 4                    | <u>±</u> 3           | 5                     | ±0.8                    | ±0.3                 | 5-7                  | ±0.5                 | ±0.5                 |
|                      |                      | 6-8                   | ±0.3                    | ±0.3                 | 8                    | ±0.5                 | ±0.3                 |
|                      |                      | 9                     | ±0.3                    | ±0.3                 | 9                    | ±0.3                 | ±0.3                 |
|                      |                      | 10-26                 | ±0.3                    | ±0.3                 | 10-13                | ±0.3                 | ±0.3                 |
| $\Delta b_0/b_0$     | 1×10-4               |                       |                         |                      | 14                   | ±0.3                 | ±0.3                 |
| $\Delta b_0 L/b_0 L$ | 1×10-3               |                       |                         |                      | 15-26                | ±0.3                 | ±0.3                 |

| Booster ring                      |                      |                            |                      |                      |                                |                      |                      |                      |                      |                      |
|-----------------------------------|----------------------|----------------------------|----------------------|----------------------|--------------------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| BR-dipole (BR-BD/BH)              |                      | BR-Pure quadrupole (BR-QP) |                      | BR-combin            | BR-combined quadrupole (BR-QF) |                      |                      | BR-sextupole (BR-SM) |                      |                      |
| n                                 | $B_nL/B_1L$          | n                          | $B_nL/B_1L$          | $A_nL/B_1L$          | n                              | $B_nL/B_1L$          | $A_nL/B_1L$          | n                    | $B_nL/B_2L$          | $A_nL/B_2L$          |
|                                   | [×10 <sup>-4</sup> ] |                            | [×10 <sup>-4</sup> ] | [×10 <sup>-4</sup> ] |                                | [×10 <sup>-4</sup> ] | [×10 <sup>-4</sup> ] |                      | [×10 <sup>-4</sup> ] | [×10 <sup>-4</sup> ] |
| 0                                 | 10000                | 1                          | 10000                | -                    | 1                              | 10000                | _                    | 0                    | ±45                  | -                    |
| 1                                 | -                    | 2                          | <u>±</u> 4           | ±10                  | 2                              | -                    | _                    | 2                    | 10000                | _                    |
| 2                                 | -                    | 3                          | <u>±</u> 4           | ±2                   | 3                              | ±4                   | ±2                   | 3                    | ±15                  | <u>±6</u>            |
| 3                                 | ±3                   | 4                          | ±1                   | ±1.5                 | 4                              | ±4                   | <u>±1</u>            | 4                    | <u>±</u> 9           | <u>±6</u>            |
|                                   |                      | 5                          | <u>±3</u>            | ±0.5                 | 5                              | ±2                   | ±0.3                 | 5-7                  | <u>±</u> 3           | ±1.5                 |
| b <sub>1</sub> L/b <sub>0</sub> L | -2.1043              | 6-7                        | ±1                   | ±0.5                 | 6-7                            | ±1                   | ±0.3                 | 8                    | ±10                  | ±1.5                 |
| b <sub>2</sub> L/b <sub>0</sub> L | -7.5331              | 8                          | ±0.5                 | ±0.5                 | 8                              | ±5                   | ±0.3                 | 9-13                 | <u>±3</u>            | ±1.5                 |
|                                   |                      | 9                          | <u>±</u> 4           | ±0.5                 | 9                              | <u>±2</u>            | ±0.3                 | 14                   | <u>±6</u>            | ±1.5                 |
|                                   |                      | 10-12                      | ±0.5                 | ±0.3                 | 10                             | ±4                   | ±0.3                 | 15-20                | <u>±3</u>            | ±0.6                 |
|                                   |                      | 13                         | ±1.5                 | ±0.5                 | 11                             | ±0.3                 | ±0.3                 |                      |                      |                      |
|                                   |                      | 14-16                      | ±0.5                 | ±0.3                 | 12-13                          | <u>±2</u>            | ±0.3                 |                      |                      |                      |
|                                   |                      | 17                         | ±1.7                 | ±0.5                 | 14                             | ±0.5                 | ±0.3                 |                      |                      |                      |
|                                   |                      | 18-20                      | ±0.3                 | ±0.3                 | 15-16                          | ±0.3                 | ±0.3                 |                      |                      |                      |
|                                   |                      |                            |                      |                      | 17                             | ±0.5                 | ±0.3                 |                      |                      |                      |
|                                   |                      |                            |                      |                      | 18-20                          | ±0.3                 | ±0.3                 |                      |                      |                      |



# Magnet quantity and production

| Magnet type                 | Symbol        | installation (+spare) |                                     |
|-----------------------------|---------------|-----------------------|-------------------------------------|
| SR-dipole                   | SR-DM         | 48 (+2)               |                                     |
| SR-short quadrupole         | SR-short-QM   | 192 (+3)              |                                     |
| SR-long quadrupole          | SR-long-QM    | 48 (+2)               |                                     |
| SR-sextupole                | SR-SM         | 168 (+6)              | Development and                     |
| BR-BD dipole                | BR-BD         | 42 (+1)               | Buckley System Ltd<br>(New Zealand) |
| BR-BH dipole                | BR-BH         | 12 (+1)               |                                     |
| BR-pure quadrupole          | BR-QP         | 36 (+5)               |                                     |
| BR-combined quadrupole      | BR-QF         | 48 (+1)               |                                     |
| BR-sextupole                | <b>BR-SM</b>  | 24 (+2)               |                                     |
| Double mini quadrupole-Q465 | SR-Q465       | 6 (+1)                |                                     |
| Double mini quadrupole-Q565 | SR-Q565       | 3 (+1)                | Gongin Co., Ltd.                    |
| Transfer line magnet        | <b>BTS-QM</b> | 7 (1)                 | (Taiwaii)                           |
| (LTB/BTS)                   | <b>BTS-DM</b> | 2 (1)                 |                                     |
|                             | LTB-DM/QM     | 1 (1)/11 (2)          | Danfysik A/S                        |
| Corrector                   | CV/CH and FFC | 134 and 100           | (Denmark)                           |

- ✓ 96.2% of fabricated magnets are installed. Only 3.8% of fabricated magnets for the spare (include prototype magnet).
  - $\rightarrow$  No more choice for the magnet installation



### **Field correction method**



- ✓ A feet-shim method was used to shim the<sup>™</sup> mechanical and magnetic centers of quadrupole and sextupole magnet close to the ideal center.
- ✓ A yoke-shim method was used to reduce the octupole error  $(B_3L/B_1L)$  of initial several longquadrupole magnets because the pole profile inaccurately.
- ✓ The pole-shim method was used to correct the multipole error of sextupole magnet.

Ref: J. C. Jan, et. al., "Multipole errors and methods of correction for TPS lattice magnets", IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, V24, NO. 3, 4100905 (2014).







# Magnet manufacture and inspection



CMM: 3D coordinate measuring machine RCS: Rotating coil measurement system HPS: Hall probe measurement system



# **Magnetic measurement precision**



#### HPS:

- ✓ The absolute field strength of Hall sensor has been calibrated by the Nuclear magnetic resonance & electron spin resonance system (NMR) →  $\Delta B < 0.3 \text{ G}$
- ✓ The repeatable of field strength is better than 0.01%.

#### **RCS:**

- $\checkmark$  The absolute field strength of RCS has been corrected by the HPS.
- ✓ The repeatable of main field strength of RCS is better than 0.01%.
- ✓ The repeatable of normalized multipoles of RCS is better than  $0.3 \times 10^{-4}$ . (n>2 is better than  $0.1 \times 10^{-4}$ )
- $\checkmark$  The repeatable and resolution of magnetic center offset measurement is better than 0.01 mm.



## **Mechanical error of magnet**

|   | Design               | Measure           | Different |  |  |  |  |  |  |
|---|----------------------|-------------------|-----------|--|--|--|--|--|--|
|   | (mm)                 | (mean±sd, mm)     | (mm)      |  |  |  |  |  |  |
| SR-dipole                               |                      |                   |           |  |  |  |  |  |  |
| $h_1$                                   | 45.48                | 45.484±0.070      | 0.004     |  |  |  |  |  |  |
| $DL_1^+$                                | 1026                 | 1026.228±0.460    | 0.228     |  |  |  |  |  |  |
|   | Short SR-quadrupole  |                   |           |  |  |  |  |  |  |
| SQd                                     | 74                   | 74.011±0.018      | 0.011     |  |  |  |  |  |  |
| SQg                                     | 24.6                 | 24.611±0.018      | 0.011     |  |  |  |  |  |  |
| SQL <sup>+</sup>                        | 265                  | 264.909±0.389     | -0.091    |  |  |  |  |  |  |
|   | La                   | ong SR-quadrupole | -         |  |  |  |  |  |  |
| LQd                                     | 74                   | 73.995±0.016      | -0.005    |  |  |  |  |  |  |
| LQg                                     | 24.6                 | 24.601±0.020      | 0.001     |  |  |  |  |  |  |
| $LQL^+$                                 | 565                  | 564.783±0.689     | -0.217    |  |  |  |  |  |  |
| SR-sextupole                            |                      |                   |           |  |  |  |  |  |  |
| Sd                                      | 78                   | **                | -         |  |  |  |  |  |  |
| Sg                                      | 18.3                 | 18.298±0.020      | -0.002    |  |  |  |  |  |  |
| SL <sup>+</sup>                         | 227                  | 226.997±0.315     | -0.003    |  |  |  |  |  |  |
|   |                      | BR-dipole (BD)    | -         |  |  |  |  |  |  |
| $h_2$                                   | 21.40                | 21.400±0.009      | 0         |  |  |  |  |  |  |
| $h_3$                                   | 23.84                | 23.845±0.010      | 0.005     |  |  |  |  |  |  |
| $DL_2^+$                                | 1554                 | 1553.885±0.207    | -0.115    |  |  |  |  |  |  |
|   |                      | BR-dipole (BH)    |           |  |  |  |  |  |  |
| $h_2$                                   | 21.14                | 21.148±0.008      | 0.008     |  |  |  |  |  |  |
| $h_3$                                   | 23.64                | 23.650±0.008      | 0.01      |  |  |  |  |  |  |
| $\overline{DL_2^+}$                     | 754                  | 754.159±0.320     | 0.159     |  |  |  |  |  |  |
|   | BR-quadrupole (pure) |                   |           |  |  |  |  |  |  |
| BQd                                     | 36                   | 35.997±0.017      | -0.003    |  |  |  |  |  |  |
| $BQL^+$                                 | 282                  | 282.172±0.174     | 0.172     |  |  |  |  |  |  |
| + Yoke length                           |                      |                   |           |  |  |  |  |  |  |
| ** No CMM date measured after pole-shim |                      |                   |           |  |  |  |  |  |  |



- ✓ The difference between the designed and machined values of the bore diameter (or pole high) is better than 0.011 mm.
- ✓ The difference between designed and machined value of the pole gap is better than 0.011 mm.
- ✓ The deviation of the laminate yoke length was controlled to be smaller than 0.1 % of the yoke length or one-piece thickness of lamina. Note: SR (BR) laminated by 1 mm (0.5mm) silicon steel.



### Magnetic field performance of magnet

| @3GeV   | Spec.               | Measure (mean±sd)              |  |  |  |  |  |  |
|---|---------------------|--------------------------------|--|--|--|--|--|--|
| SR-dipole   |                     |                                |  |  |  |  |  |  |
| $b_0L$ -1.3201±0.0009   |                     |                                |  |  |  |  |  |  |
|   | Short SR-quadrupole |                                |  |  |  |  |  |  |
| $b_1L$  |                     | -5.2160±0.0086                 |  |  |  |  |  |  |
| $B_2L/B_1L$   | ±2.0                | 0.1±1.1                        |  |  |  |  |  |  |
| $B_3L/B_1L$   | ±2.0                | -0.2±0.7                       |  |  |  |  |  |  |
| $B_5L/B_1L$   | ±0.8                | -0.4±0.2                       |  |  |  |  |  |  |
|   | Lon                 | g SR-quadrupole                |  |  |  |  |  |  |
| $b_1L$  |                     | -9.4438±0.0087                 |  |  |  |  |  |  |
| $B_2L/B_1L$   | ±2.0                | 0.0±0.9                        |  |  |  |  |  |  |
| $B_3L/B_1L$   | ±2.0                | -1.7±1.0                       |  |  |  |  |  |  |
| $B_5L/B_1L$   | ±0.8                | -0.3±0.3                       |  |  |  |  |  |  |
|   |                     | SR-sextupole                   |  |  |  |  |  |  |
| $b_2L$  | 120.216±0.306       |                                |  |  |  |  |  |  |
| $B_3L/B_2L$   | ±2.0                | 0.0±1.1                        |  |  |  |  |  |  |
| $B_4L/B_2L$   | ±3.0                | 0.3±1.3                        |  |  |  |  |  |  |
| $B_8L/B_2L$   | ±0.5                | 0.4±0.1                        |  |  |  |  |  |  |
|   | BR                  | -dipole (BD/ BH)               |  |  |  |  |  |  |
| $b_0L$  |                     | -1.3173±0.0019/ -0.6589±0.0007 |  |  |  |  |  |  |
| $b_1L$  |                     | 2.7719±0.0228/1.3922±0.0060    |  |  |  |  |  |  |
| $b_2L$  |                     | 9.9088±0.4514/ 4.3942±0.1146   |  |  |  |  |  |  |
| BR-quadrupole (Q1)  |                     |                                |  |  |  |  |  |  |
| $b_1L$  |                     | Q1: 4.293±0.005                |  |  |  |  |  |  |
| $B_2L/B_1L$   | ±4.0                | -1.4±3.0                       |  |  |  |  |  |  |
| $B_3L/B_1L$   | ±4.0                | -4.3±1.6                       |  |  |  |  |  |  |
| $B_5L/B_1L$   | ±3.0                | 1.9±1.0                        |  |  |  |  |  |  |
| Unit: $b_0 L$ (T·m), $b_1 L$ (T), $b_2 L$ (T/m), $B_n L / B_m L$ (×10 <sup>-4</sup> ) |                     |                                |  |  |  |  |  |  |



- ✓ The index n=0 is dipole term, n=1 is quadrupole term.
- ✓ The dispersion of the field strength is generally dominated by the error of bore diameter and the yoke length. The multipole errors are dominated by the asymmetric or machining error of the pole profile.
- ✓ The magnetic field quality of magnet is much better than the specifications.
- ✓ The SR and BR magnets have a great quality of the field because of the strict mechanical machining.

Ref: J. C. Jan et. al., "SUMMARY OF FIELD QUALITY OF TPS LATTICE MAGNETS", Proceedings of International Particle Accelerator Conference, Dresden, Germany (2014).



# **Magnet center inspection**

|  | Measurement (mean value±sd) |                   |                   |  |  |
|--|-----------------------------|-------------------|-------------------|--|--|
|  | short SR-quad.              | long SR-quad.     | SR-sext.          |  |  |
| Mechanical center offset-vertical (mm)   | -0.002±0.004                | -0.005±0.004      | -0.002±0.004      |  |  |
| Mechanical center offset-horizontal (mm) | -0.005±0.006                | -0.008±0.004      | -0.005±0.005      |  |  |
| Magnetic center offset-vertical (mm)     | $0.003 \pm 0.009$           | $0.002 \pm 0.007$ | $0.005 \pm 0.008$ |  |  |
| Magnetic center offset-horizontal (mm)   | 0.006±0.011                 | $0.007 \pm 0.009$ | $0.005 \pm 0.009$ |  |  |
| Mechanical tilt (deg.)                   | $0.00 \pm 0.00$             | $0.00\pm 0.00$    | $0.01 \pm 0.01$   |  |  |
| Magnetic tilt (deg.)                     | 0.00±0.01                   | 0.00±0.01         | 0.01±0.01         |  |  |

- ✓ The mechanical center offset was shimmed better than  $\pm 0.01$  mm in both vertical and horizontal directions.
- ✓ The magnetic center offset was measured better than  $\pm 0.02$  mm in both vertical and horizontal directions after feet-shim.
- ✓ The mechanical and magnetic tilt of magnet is better than  $0.01^{\circ}$  after feet-shim.

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# **Closed Orbit of TPS Storage Ring**

#### Without any corrector applied



- ✓ The closed orbit distortion (COD) measurement without any corrector: 1.78 mm (rms) horizontal and 1.04 mm (rms) vertical after the LOCO and BBA.
- $\checkmark$  The COD results demonstrate very high quality of magnets and the girder alignments.

Ref: C. C. Kuo et. al., "Commissioning of the Taiwan Photon Source", TUXC3, this proceeding. T. C. Tseng et. al., "The Auto-Alignment Girder System of TPS Storage Ring", THYB2, this proceeding.



### **Chamber permeability studies of Booster ring**



- ✓ Elliptical chambers are cold-drawn from circular tube of stainless steel (SUS304). The relative permeability ( $\mu_r$ ) of the vacuum chamber appeared after the drawing process.
- $\checkmark$  An annealing process was used to eliminate the permeability of the BR chamber.

Ref: I. C. Sheng et. al., "Demagnetized Booster Chambers in TPS", WEPHA049, this proceeding.



### **Chamber permeability inspection**



- ✓ A two-step test of the chamber permeability: (1) a quickly scan of the chamber by the NbFeB permanent magnet and (2) the magnitude measurement by the HPS.
- ✓ NbFeB permanent magnet:  $6 \text{ mm}(D) \times 2 \text{ mm}(t) \times 2 \text{ g}(w)$  with 0.25 T field strength.
- $\checkmark$  The relative permeability of the BR chamber is less than 1.01 after annealing.



### Field distortion from the un-annealed chamber



- ✓ An un-annealed chamber was measured to understand the field distortion in the BR dipole (combined-function) magnet.
- ✓ The field distortion increases with decreasing excitation current in the un-annealed chamber indicates that the electron beam at low energy will be perturbed seriously due to the effect of un-annealed chamber in the BR.



- ✓ The machining error of the pole profile of a TPS magnet is better than 0.02 mm as manufactured with the CNC and WEDM techniques. The multipole errors of these magnets thereby conform to the strict requirements of the spec.
- ✓ A precise mechanical and magnetic center was shimmed and measured with the CMM and RCS. The mechanical center offset was shimmed better than ±0.01 mm in both vertical and horizontal directions.
- ✓ The magnetic center offset was better than ±0.02 mm in both vertical and horizontal directions after feet-shim.
- ✓ The mechanical and magnetic tilt of magnet is better than 0.01° after feetshim.
- ✓ The permeability of the BR chamber was less than 1.01 after heat treatment.
- ✓ A serious distortion of the field from the un-annealed chamber was observed, indicates that the electron beam at low energy will be perturbed seriously due to the effect of un-annealed chamber in the BR.



The First Synchrotron Light from TPS Storage Ring December 31, 2014

# **Thanks for your attention**