Abstract

surface of the cavity.

PERFORMANCE R. Eichhorn[#], J, May-Mann Cornell Laboratory for Accelerator-Based Sciences and Education, Ithaca, NY 14853-5001, USA Over the past years it became evident that the quality factor of a superconducting cavity is not only determined by its surface preparation procedure, but is also influenced by the way the cavity is cooled down. In this paper we will present results from numerical field calculations of magnetic fields produced by thermocurrents, driven by temperature gradients and material transitions. We will show how they can impact the quality factor of a cavity by producing a magnetic field at the RF

ASYMMETRIC THERMO-CURRENTS DIMINISHING SRF CAVITY

INTRODUCTION

The need to reduce the cost of the cryogenic infrastructure for future CW accelerators has driven the research on achieving high quality factor superconducting cavities. As a result, state of the art treated cavities display surface resistance approaches the theoretical limits. This allowed a deeper insight into the physics of parasitic effects, as they now become a prominent factor in limiting the performance of SRF cavities. One interesting finding, reproduced in different labs was that the quality factor of a cavity is impacted by the details of the cool-down procedure [1-3].

As of now, there seem to be two contributions resulting in the cool-down dependency of the cavity performance. One is flux pinning, the other is thermo-current.

Flux pinning describes the effect that a residual magnetic field is not fully expelled as the cavity becomes superconducting, resulting in an only partial Meissner effect. The trapped flux then concentrates in vortices which stay normal conducting and as a result, increases the losses of the cavity, denoted by a drop in the quality factor.



Figure 1: A superconducting cavity, welded into its helium vessel (dressed cavity).

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7: Accelerator Technology **T07 - Superconducting RF**

author(s), title of the work, publisher, and DOI. Thermo-currents on the other hand have no direct effect. They are a result of the Seebeck effect that exist if material joints are held at different temperatures. As shown in fig.1, a superconducting cavity, welded into its helium vessel, is essentially a Seebeck current loop. As of their nature, thermo-currents generate a magnetic fieldwhich then may be pinned during cool-down. In the past, ibution 1 an analytical analysis argued that the axial symmetry of SRF cavities leads to no (or when considering the attril potential asymmetry from vessel or cavity port: negligible small) thermo-electric induced magnetic fields in the relevant RF penetration layer at the inner cavity surface [4]. The author concluded that thermo-electric currents are not a concern for the performance of SRF cavities. must 1 However, our findings indicated early-on [5] that thermoelectric currents may have a more severe impact on the distribution of this work SRF performance as so far predicted [6].

SEEBECK EFFECT

Thermo-currents are the result of the Seebeck-effect, which is well known in physics for more than a century: Discovered in 1826, Seebeck found that a current will flow in a closed circuit made of two dissimilar metals when the two junctions are maintained at different temperatures. The voltage is dependent on the material, leading to the definition of the Seebeck coefficient S:

$$\Delta U = S \cdot \Delta T \,. \tag{1}$$

3.0 licence (© 2015). Seebeck coefficients of metals can have either sign as they are defined relative to platinum. In a single metal ВҮ arrangement, this voltage exists across the metal but does the CC not result in a current flowing other than simply building up the charges, initially. If there is a material transition, of where two different metals are joined, not only does a potential difference exist, there might also be a persistent current, driven by the temperature difference, if the loop the 1 is closed. As superconducting cavities are made out of under niobium while the helium vessel enclosing them is typically titanium this effect is relevant for accelerator physics: During the cool-down of a dressed cavity (a cavity welded into its helium vessel) it is easy to imagine that both ends of the cavity (where the Nb-Ti transition is located) have different temperatures. Seebeck coefficients are temperature dependent, as given in tab. 1 for niobium and titanium. With the more general definition of the Seebeck coefficient, the thermo-voltage becomes

$$U_{th} = \int_{T_1}^{T_2} \left(S_{Nb}(T) - S_{Ti}(T) \right) dT$$
 (2)

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Table 1: Thermoelectric Power (Seebeck Coefficient) for $\frac{1}{1000}$ in $\mu V/K$ Niobium and Titanium, Taken from [7]. Values are Given

Ξ.						
qnc		10 K	20 K	50 K	80 K	100 K
¥	Nb	0.31	0.98	2.73	3.09	3.13
NOI	Ti	N/D	N/D	-3.00	-3.00	-2.60

THERMOCURRENT SIMULATION

title of the In order to gain a better understanding, numerical s). simulations with CST® EM-Studio® were undertaken. author(We modelled a real size cavity with a simplified helium vessel (see fig. 3a). The Seebeck voltage was applied over 2 an artificial gap on the right side of the helium vessel. For o the simulation, realistic values for the expected thermovoltage and the resistivity of the materials were used and attribution the mesh was carefully adjusted to avoid numerical problems.

For the numerical simulation we assumed a Seebeck naintain voltage of 150 μ V, which corresponds to a temperature of 10 K on one side and 50-60 K on the other side (the calculation is based on experimental conditions as $\frac{1}{2}$ calculation is based on experimental conditions as $\frac{1}{2}$ published in [8]. Below 50 K the thermoelectric power of $\frac{1}{2}$ titanium is unknown. Our extrapolation is a linear dependency of the coefficient with temperature between :2 10 K and the first data point at 50 K, as our measurements $\frac{1}{2}$ in [6] suggest a rather constant value at least below 10 K.

We also assumed constant value at least below 10 k. $(5 \cdot 10^{-10} \Omega m)$ and the titanium $(2.5 \cdot 10^{-7} \Omega m)$. The below is of the titanium vessel was accounted for this simulation in terms of resistance but it was not modelled geometrically. We also assumed constant resistivity for the niobium $(5 \cdot 10^{-10} \Omega m)$ and the titanium $(2.5 \cdot 10^{-7} \Omega m)$. The bellow of the titanium vessel was accounted for this simulation in

Any Symmetric Case

2015). Even though the cavity/ helium-vessel may have nonuniform properties, symmetry exists if the properties are independent of the azimuth. In this scenario, a thermo- $\stackrel{\circ}{\stackrel{\circ}{\stackrel{\circ}{_{\sim}}}}$ independent of the azimuth. In this scenario, a thermo-current is excited if a temperature gradient exists along $\stackrel{\circ}{\stackrel{\circ}{_{\sim}}}$ the z-axis: The disparity of the temperatures at the e material transitions results in a Seebeck voltage, driving \succeq this current.

However, due to the postulated symmetry, currents in 20 the upper and the lower half are equal, resulting in a magnetic field that only exists between the outer cavity б wall and the helium vessel. This is consistent with the analytical model in [4].

We calculated the current in the thermo- loop to be 4.8 A and the maximum magnetic field to be 25 μ T. The results for the symmetric scenario are shown in fig. 3, where plot (a) gives the magnetic field configuration. The plots below give the magnetic field along a z-axis cut at Scentre of the cavity. $\exists A s extra definition of the cavity.$ the location of the equator (b) and the iris (c) near the

As expected, fields are symmetric and no field inside work the cavity exists. As a consequence of the vanishing magnetic field at the RF surface of the cavity, thermothis currents in this symmetric case do not result in any from contribution to the flux pinning at transition and thus do not influence the performance of the cavity. Content

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Figure 3: Results of the numerical field assuming azimuthal symmetry: 3-D field configuration (a), z-axis cuts along one equator (b) and at an iris (c), both locations where close to the cavity centre.

Asymmetric Case

To simulate the asymmetric scenario we applied the same conditions as described above except that we assumed the lower portion of the cavity to be a perfect conductor- representing its vanishing resistance in the superconducting state. The field configuration yielded is given in fig. 4 (a), the lower plots are z-cuts at the iris (b) and equator (c), respectively. As a result of the azimuthal asymmetry, magnetic fields are asymmetric and a reasonable large magnetic field exists inside the cavity which during transition of the upper half of the cavity through Tc could be trapped, causing an increase in the residual resistance and thus deterioration in the cavity Q.

Figure 4 also indicates that a measurable thermocurrent induced magnetic field is generated outside the titanium vessel. This explains our initial findings referred in [5] which could not be explained so far. Given the field configuration has been simulated, this allows to index the field at the cavity surface without having to place a

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Figure 4: Results of the asymmetric calculation, where the lower portion of the cavity is assumed to be superconducting while the upper half remains normal conducting: 3-D field configuration (a), z-axis cuts along one equator (b) and at an iris (c).

magnetometer inside the cavity. Thus, a magnetic field reading outside the helium vessel permit a direct distinction between the thermo-electric magnetic fields which do not affect performance (symmetric, no field inside the cavity nor outside the helium vessel) and the fields which impact the performance (asymmetric with field inside the cavity and outside the helium vessel).

CONCLUSION

Our simulations have shown that conditions can exist under which thermos-currents can contribute to the cavity performance: If an azimuthal asymmetry exists, thermocurrents can generate magnetic field at the RF layer of the cavity that is subject to flux trapping. A reason for this asymmetry can be found in the cool-down, if a transversal temperature gradient in the dressed cavity exists. This is usually the case in a horizontal test, where the cavity is cooled through a stream of cold helium entering through a

7: Accelerator Technology **T07 - Superconducting RF** cool-down port at the lower portion of the helium vessel, while the exhaust is located on the top. This results in a lower temperature of the lower portion of the cavity with decreased resistance and increased current in that region. As the resistivity of the titanium is almost constant below 50 K [9], the change of resistance has to be caused by the niobium with the most drastic change to happen as the niobium becomes superconducting.

The thermo-current effect has less influence in vertical tests for two reasons. Usually, only bare cavities are tested, but a closed current loop might exist over the cavity support frame. Longitudinal temperature gradients might be huge resulting in large thermo-current induced the magnetic fields. However, due to the mostly preserved azimuthal symmetry as a result of the only z-dependant 5 maintain attribution temperature distribution, fields are symmetric eventually generating no flux at the RF layer of the cavity.

REFERENCES

- [1] J.-M. Vogt, O. Kugeler, and J. Knobloch "Impact of cool-down conditions at Tc on the superconducting rf cavity quality factor", Phys. Rev. Sp. Top. - Acc. and Beams 16 (2013)102002.
- [2] N. Valles, R. Eichhorn, F. Furuta, G.M. Ge, D. Gonnella, Y. He, V. Ho, G. Hoffstaetter, M. Liepe, T. O'Connell, S. Posen, P. Quigley, J. Sears, V. Veshcherevich,"Cornell ERL Main Linac 7-Cell Cavity Performance in Horizontal Test Cryomodule Qualification", Proc. of the 2013 Int. Conf. on Part Acc., Shanghai, China (2013) 2459.
- [3] A. Romanenko, A. Grassellino, O. Melnychuk, D. A. Sergatskov, "Dependence of the residual surface <u>6</u> resistance of SRF cavities on the cooling rate through Tc", arXiv:1401.7747
- 0 [4] A. C. Crawford, "A Study of Thermocurrent Induced BY 3.0 licence Magnetic Fields in ILC Cavities." arXiv, (1403.7996), 2014
- [5] R. Eichhorn, et al., "High Q Cavities for the Cornell ERL Main Linac", Proceedings of SRF2013, Paris, France (2013) 844.
- 5 [6] R.Eichhorn. C. Daly, F. Furuta, А the Ganshyn, "Investigation of thermocurrents limiting the performance of superconducting cavities", of Proceedings of IPAC2014, Dresden, Germany (2014) 2621.
- [7] F. J. Blatt, P.A. Schroeder, C.L. Foiles, D. Greig, "Thermoelectric Power of Metals", Plenum Press, under 1 1976.
- used [8] D. Gonnella, R. Eichhorn, F. Furuta, M. Ge, D. Hall, V. Ho, G. Hoffstaetter, M. Liepe, T. O'Connell, S. ę Posen, P. Quigley, J. Sears, V. Veshcherevich, A. may Grassellino, A. Romanenko, D. Sergatskov, "Nitrogen-Doped 9-Cell Cavity Performance in a work Test Cryomodule for LCLS-II", J. Appl. Phys. 117, this 023908 (2015).
- from t [9] W.R.G.Kemp, P.G. Klemens, G.K. White, "Thermal and electrical conductivities of iron, nickel, titanium and zirconium at low temperatures", Austr. Jorn. Of Content Phys. 9 (1956) 180.