IMPEDANCE STUDIES OF THE LHC INJECTION KICKER MAGNETS FOR HL-LHC

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Abstract

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title of the work, publisher, and DOI The LHC injection kicker magnets (MKIs) experienced strong heating during the first operational run, identified as being caused by power loss due to wakefields induced by circulating beam. Studies of the beam coupling impedance of the beam screen, a series of conductors embedded in a ceramic tube placed in the aperture of the ferrite voke to screen the ferrite from the beam, resulted in new design offering improved screening: this is predicted to reduce the heating to acceptable levels for operation with 25ns beam during run 2 of the LHC. However higher beam intensities proposed for HL-LHC operation are predicted to again cause strong heating to occur. Further studies have been carried out to reduce the beam induced power loss by optimising the beam screen design, some key results and findings of which are presented here.

INTRODUCTION

distribution of this work The injection kicker magnets (MKIs) are fast pulsed transmission line kicker magnets, which have a ceramic tube inserted into the aperture of the ferrite yoke: this supports a number of screen conductors, designed to provide a good conducting path for the image currents of the circulating beam. One end of the screen is directly connected to the Anv beam pipe whilst the other is capactively coupled to the beam ŝ pipe in order to preserve the fast field rise time of the magnet. 20 Beam-induced heating, due to high circulating beam current, licence (© leads to high temperatures being observed in devices in the LHC, including the MKIs [1]. In one non-conforming MKI this lead to problems as the temperature of the ferrite yoke 3.0 occassionally rose above it's Curie temperature (≈120°C) necessitating 2-3 hours waiting time between fills. Substan-B tial work has been done to reduce the power deposited by reducing the beam coupling impedance of the device - a the revised beam screen was implemented on all magnets durterms of ing long shutdown 1 (LS1) which is predicted to reduce the power loss to <52W/m (see Table 1) and the temperature is <80°C [2], comfortably below the Curie temperature.

under the The planned high luminousity upgrade of the LHC (called HL-LHC) will involve a doubling of the beam current in the LHC under current nominal parameters [3] - this is predicted used to lead again to a four fold increase in the power loss to all þe devices in the LHC unless counter-measures are taken. To nay this end further improvements to the beam screen have been studied in order to reduce the power loss into the magnet work whilst continuing to ensure both good high voltage (HV) Content from this performance and good field quality during pulsing.

Building on the previous success a new design has been proposed to satisfy competing needs of low rates of electrical

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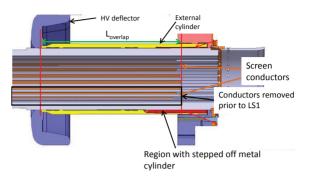


Figure 1: Cross-section of the beam screen of the MKI. Conductors circled in red weren't in place prior to longshutdown 1.

breakdown, during magnet pulsing, and a low beam coupling impedance to reduce the power lost into the structure by wakefields; in addition to meet strict requirements for magnet operation for field rise time and flat top ripple [4].

CHANGES TO BEAM SCREEN DESIGN

Past work on the beam screen of the MKI has focused on improving the screening of the ferrite yoke from the beam by increasing the number of screen conductors in the beam screen to the full compliment of 24 - during the first run of the LHC only 15 screen conductors were in place, positioned closest to the return busbar (see Fig. 1), due to issues with surface flashover during magnet pulsing [5].

A revised beam screen was designed that reduced the electric field strength during magnet pulsing sufficiently to allow 24 conductors to be installed for post-LS1 [4], shown in Fig. 1. This is predicted to substantially reduce in the power loss in the MKIs post LS1, by a factor of more than 3 relative to the non-conforming MKI pre-LS1 (≈160W/m), even accounting for the increased beam current with the change to 25ns bunch separation. However this is not expected to be sufficient for HL-LHC operation, which will see a much higher beam current than nominal LHC operation (see Table 2) and is predicted to see power losses comparable to that which caused the non-conforming magnet to heat beyond it's Curie temperature during run 1 of the LHC [6], thus necessitating further modifications.

Previous work had showed that the beam coupling impedance of the MKI with a well shielded ferrite yoke is resonant in nature, with the frequency of the resonances, f_{res} , determined by the length of the overlap between the screen conductors on the internal face of the ceramic tube

5: Beam Dynamics and EM Fields

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Table 1: Power Loss for Different Beam Screen Arrangements with Different Beam Parameters (see Table 2) in W/m.

Mode	24 Screen Cond.	15 Screen Cond.
Pre-LS1	20-35	68
Post-LS1	34-52	117
HL-LHC, 50ns	151-240	538
HL-LHC, 25ns	125-191	432

Table 2: Beam Parameters for Different LHC OperationalModes

Mode	τ_{sep} (ns)	$N_b (10^{11})$	М	t_b (ns)
Pre-LS1	50	1.6	1380	1.2
Post-LS1	25	1.15	2808	1.0
HL-LHC, 50ns	50	3.5	1380	1.0
HL-LHC, 25ns	25	2.2	2808	1.0

and the conducting pieces on the outside at the capacitivelycoupled end of the tube, given approximately by;

$$f_{res} = \frac{nc}{2\sqrt{\epsilon_r} \left(L_{overlap} + \delta_{fringe} \right)} \tag{1}$$

where n is an integer, ϵ_r the relative permitivity of the ceramic tube, $L_{overlap}$ the length of the overlap between the screen conductors and the external cylinder and δ_{fringe} the influence of the fringe fields on the effective overlap. For the post-LS1 design, $L_{overlap} = 107mm$. If we consider the general formula for power loss;

$$P_{loss} = 2 \left(f_0 e M N_b \right)^2 \sum_{n=-\infty}^{\infty} |\lambda \left(p M \omega_0 \right)|^2 \Re e \left[Z_{\parallel} \left(p M \omega_0 \right) \right]$$
⁽²⁾

where f_0 is the revolution frequency, $\omega_0 = 2\pi f_0$, *e* is the charge of an electron, N_b is the number of particles per bunch, M is the number of bunches in the machine, $\lambda(\omega)$ is the beam current spectrum, and $\Re e(Z_{\parallel}(\omega))$ is the real component of the longitudinal beam coupling impedance; we can see that the power loss can be reduced by changing either the beam profile (in this case limited as the beam profile is determined by the requirements for the physics experiments) or the beam impedance profile. Due to the approximately gaussian roll off of the beam current spectrum at higher frequencies it can be seen that shortening Loverlap would result in the resonant frequency increasing and thus a resonance sitting at a lower part of the current spectrum. This approach was thus chosen due to the relative simplicity of the change (no major redesign of the magnet would be foreseen in this case) and the system being well proven for both HV and beam impedance factors.

In addition to the reduced overlap length, further alterations to the beam screen have been proposed for HV purposes in order to reduce the rate of surface flashover during magnet pulsing, shown in Fig. 2. These modifications involve changes [7] significant for the beam coupling

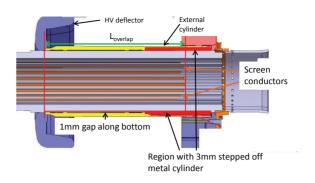


Figure 2: Cross-section of the proposed beam screen for the MKI under HL-LHC conditions.

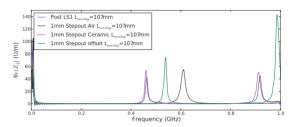


Figure 3: Real component of the longitudinal beam coupling impedance of an MKI with different beam screen arrangements. The HV deflector is not included in this model.

impedance; a small air gap is introduced around the entire ceramic tube apart from a 90° arc at the top of the cylinder, being a maximum of 1mm at the bottom of the tube and tapering to 0mm. Due to the high permitivity of the ceramic ($\epsilon_r \approx 10$) the small air gap greatly decreases the capacitance of the capactively coupled end, causing the frequency of a resonance for a fixed length of overlap to increase.

To illustrate this, simulations were carried out using CST Particle Studio [8] for the following cases, each with $L_{overlap}$ =107mm: a) as the post-LS1 setup, b) a 1mm airgap between the tube and the external cylinder, c) as for (b) but the air is replaced by ceramic, d) an offset air-gap, resulting in a gap of 1mm at the bottom and 0mm at the top. The results are shown in Fig. 3 - it can be seen that the addition of the 1mm air-gap causes the resonant frequency to increase, moving to 610MHz for the fundamental frequency, compared to 461MHz for the post-LS1 design in Fig. 1; however the reduced capacitance increases the real impedance at low frequencies (< 20MHz). It can be seen from the corresponding small shift in frequency from 1mm of ceramic that the shift is purely due to the permitivitty of the air, as the 1mm of ceramic (c above) gives a very small decrease, attributable to the increased thickness of ceramic leading to stronger influence of fringe fields. The offset air gap (d above) leads to an increase in the resonant frequency, but not as large as a uniform airgap - understandable as the capacitance does not decrease as much.

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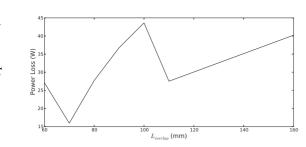


Figure 4: Power loss calculated from simulations of a reduced model of the MKI beam screen with different lengths of overlap between conductors and external cylinder.

CHANGE IN OVERLAP LENGTH

attribution to the author(s), title of the work, publisher, and DOI Initial investigations of the optimum overlap length were carried out using a reduced simulation of the MKI beam maintain screen (only considering the capacitively coupled end of the beam screen, and simulating up to 1.1GHz) - the resulting power loss (N.B. not comparable to the results given previmust ously as the magnitude of the resonances will be incorrect work and the whole frequency range is not covered, but the frequencies will be comparable) is given in Fig. 4, covering this overlaps of 60,70,80,90,100,110 and 160mm. It can be seen of that shortening the overlap to be less than 80mm in length could give substantial reductions in power loss.

Any distribution On this basis a number of overlap lengths were simulated with a full model of the HL-LHC type design and coveriing the full frequency range: in addition, parts were manufactured for measurements with an MKI magnet - this serves to verify the simulation data against measurement. \tilde{c}

Measurements are carried out using two methods as the 201 O impedance of the MKI with a complete beam screen is exlicence pected to be very low; (a) the resonant coxial wire method [9], gives very accurate measurements of the beam coupling impedance, although with poor frequency resolution, and 3.0 (b) the classical transmission method, but without matching ВҮ resistors and using time domain gating. The magnitude of 0 the impedance measured for the last method will not reprethe sent the true impedance, however the frequency resolution is of better than for the resonant method and it allows the measureterms ments to be done quickly, which making resistive matching for each does not. This method also guarantees that no resothe . nances are missed, which the resonant method may misse under due to it's poor frequency resolution.

The results of the simulations and measurements with used time-domain gating are shown in Fig. 5; the solid lines are the measurements with gating and the dashed lines the simè ulation results. It can be seen that the resonant frequency mav increases in both simulations and measurements as the overwork lap length is decreased, as expected. There is a difference in the resonant frequency given by the simulations and mearom this surements; this is attributable to simulating the full model in this case the small air gap (1mm at most) at the capacitively coupled end of the beam screen is liable to generate errors in meshing in some cases causing the model to assume

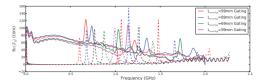


Figure 5: Comparison of the real component of the longitudinal beam coupling impedance between simulations and measurements of different overlap lengths

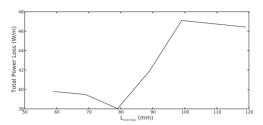


Figure 6: Power lost per metre for a number of overlap lengths, calculated assuming nominal LHC parameters using resonant wire measurements.

a metal on the surface of the ceramic as opposed to an air gap.

The power lost per metre is shown in Fig. 6 for measurements made using the resonant wire method, calculated using Eqn. 2 and nominal 25ns LHC parameters. It can be seen that the a length less than 80mm gives a substantial ($\approx 20\%$) reduction in power loss relative to lengths in the 110-120mm range, 38W/m compared to 47W/m; the corresponding power deposition for HL-LHC are 140W/m and 172W/m respectively. However as a worst case for the ferrite yoke, assuming that the 140W/m is in the ferrite yoke, the predicted maximum yoke temperature is uncomfortably close to the Curie temperature [2]. This indicates that a value of Loverlap between 70-80mm would be optimum for minimising the power loss.

SUMMARY AND FURTHER WORK

Further work to improve the impedance of the beam screen of the LHC injection kicker magnets has been carried out with a view to guarantee beam-induced heating doesn't become a problem during HL-LHC operation. It's been proposed to reduce the overlap at the capacitively coupled end to less than 80mm, preferring a value of \approx 70mm. Further work remains to be done on verifying the design for HV behaviour and it is foreseen to place a prototype MKI with this and other modifications (particularly improvements to the cooling of the ferrite yoke [10]) in the LHC verify the changes under operational conditions.

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