



Design of **Phase Feed-Forward System in CTF3** and Performance of **Fast Beam Phase Monitors**

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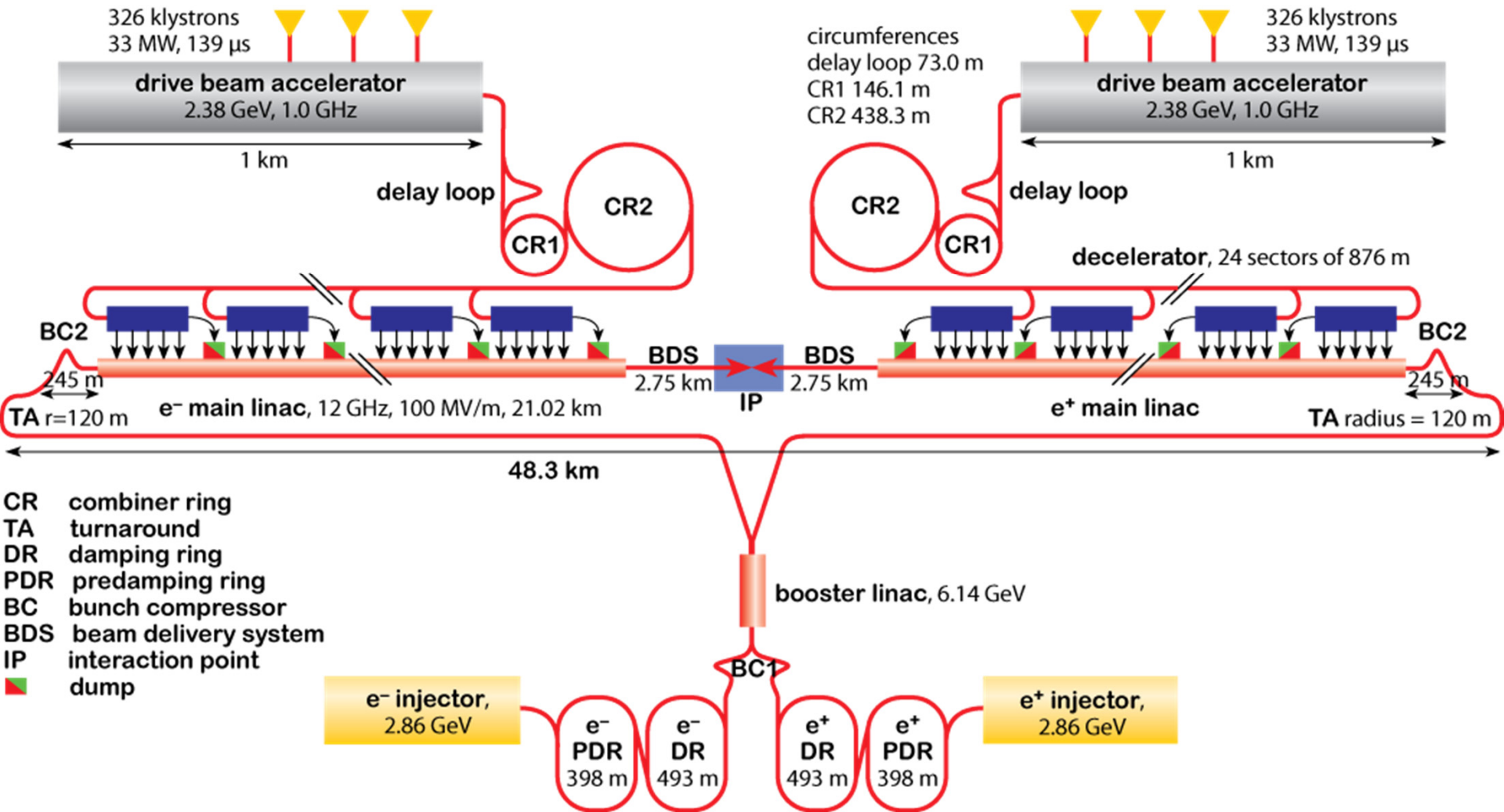
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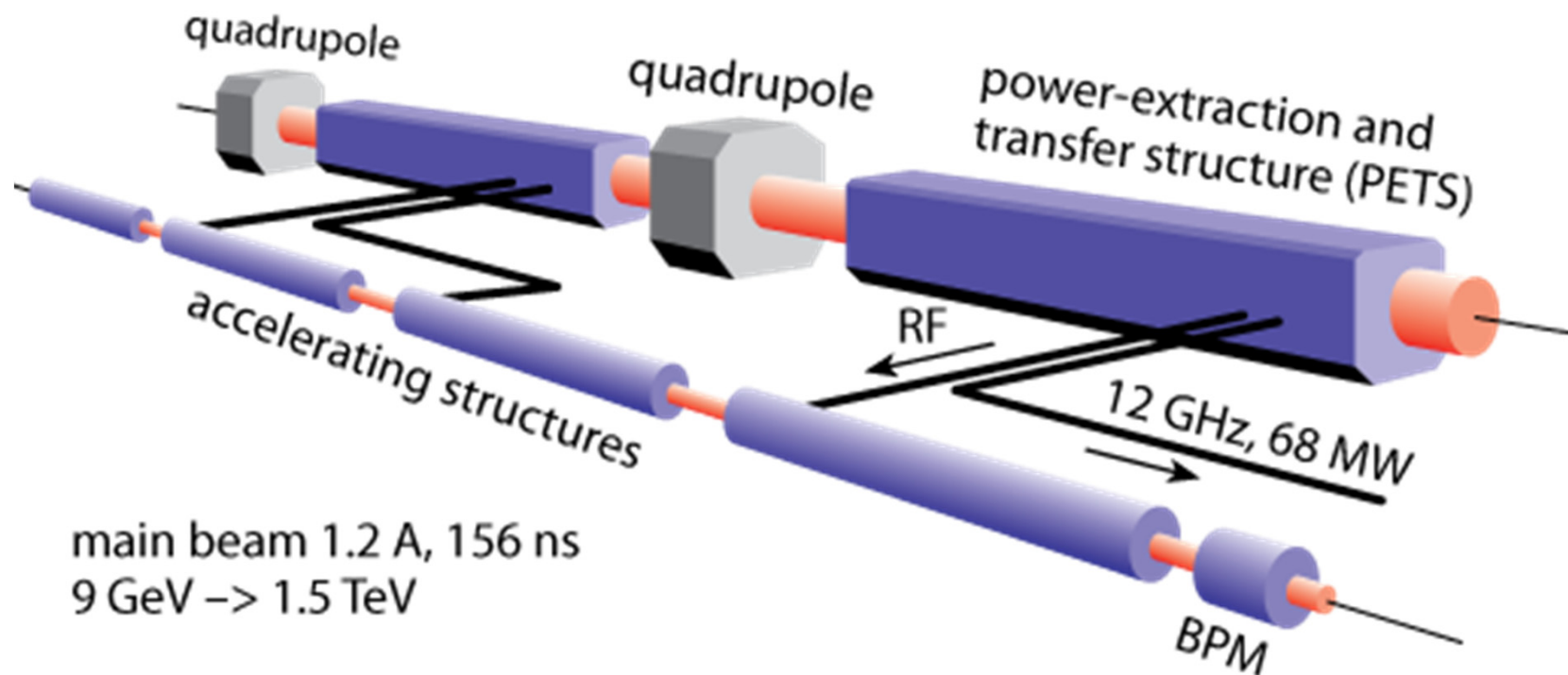


Compact Linear Collider aka CLIC



The Two Beam Acceleration

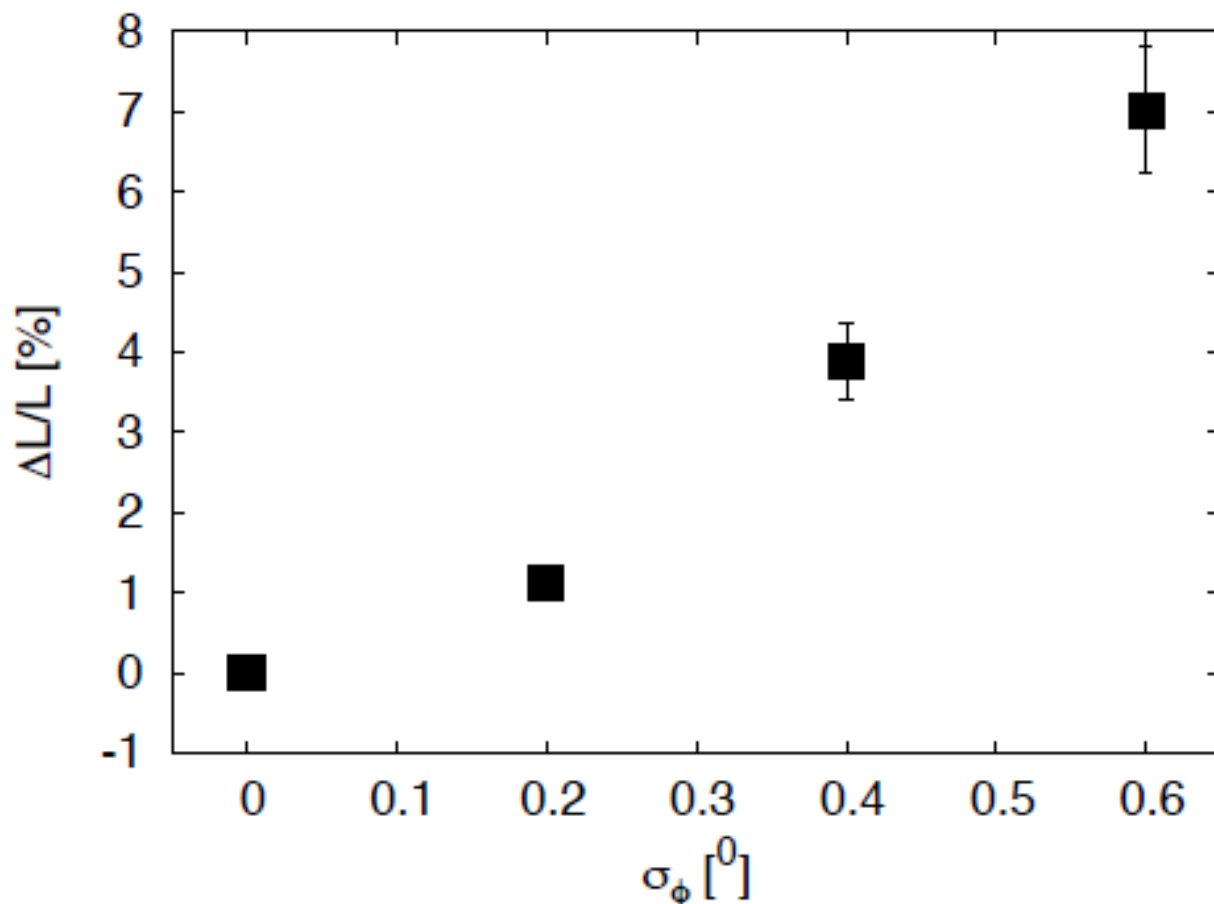
drive beam 100 A, 239 ns
2.38 GeV \rightarrow 240 MeV



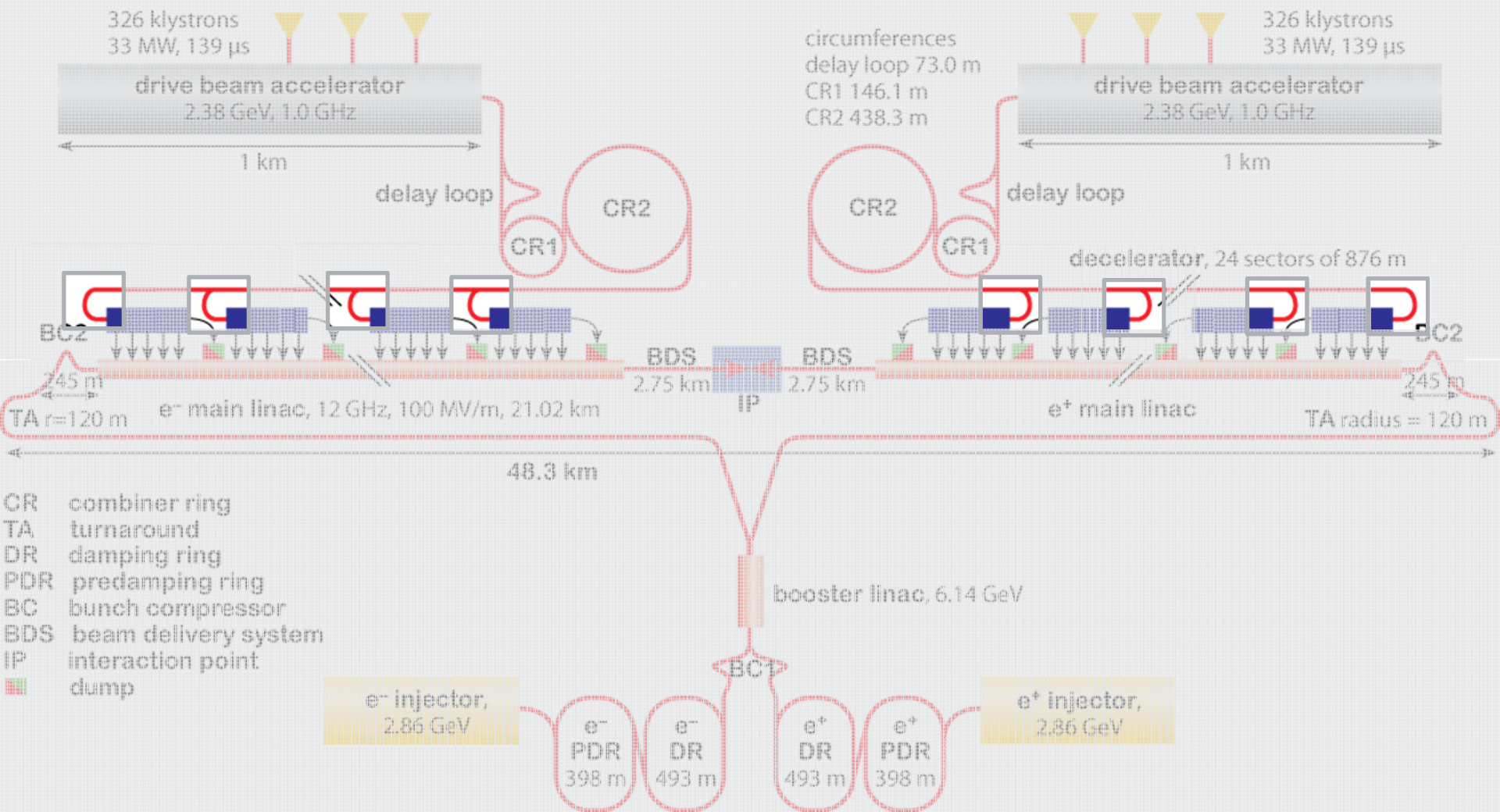
main beam 1.2 A, 156 ns
9 GeV \rightarrow 1.5 TeV

Phase Tolerance Between the two beams

- ◆ CLIC luminosity quickly drops if the RF phase jitters
- ◆ Expected (conservative) drive beam phase stability 2.5° @12GHz
→ **Must stabilize!**

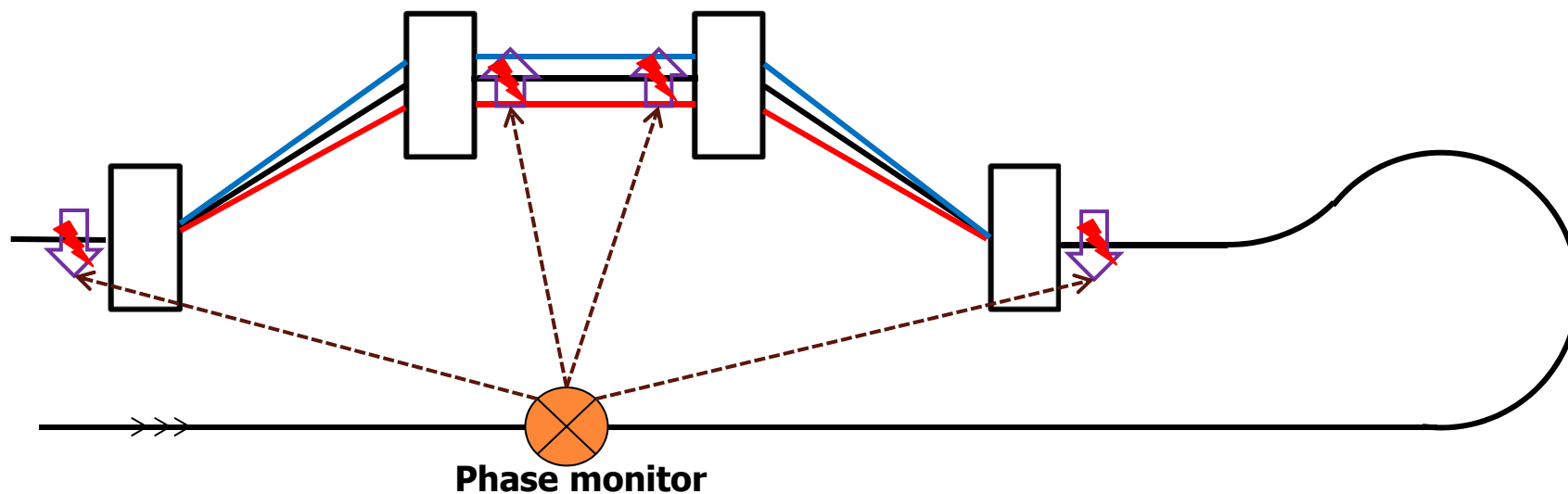


Phase stabilization in the Drive Beam Turn Arounds



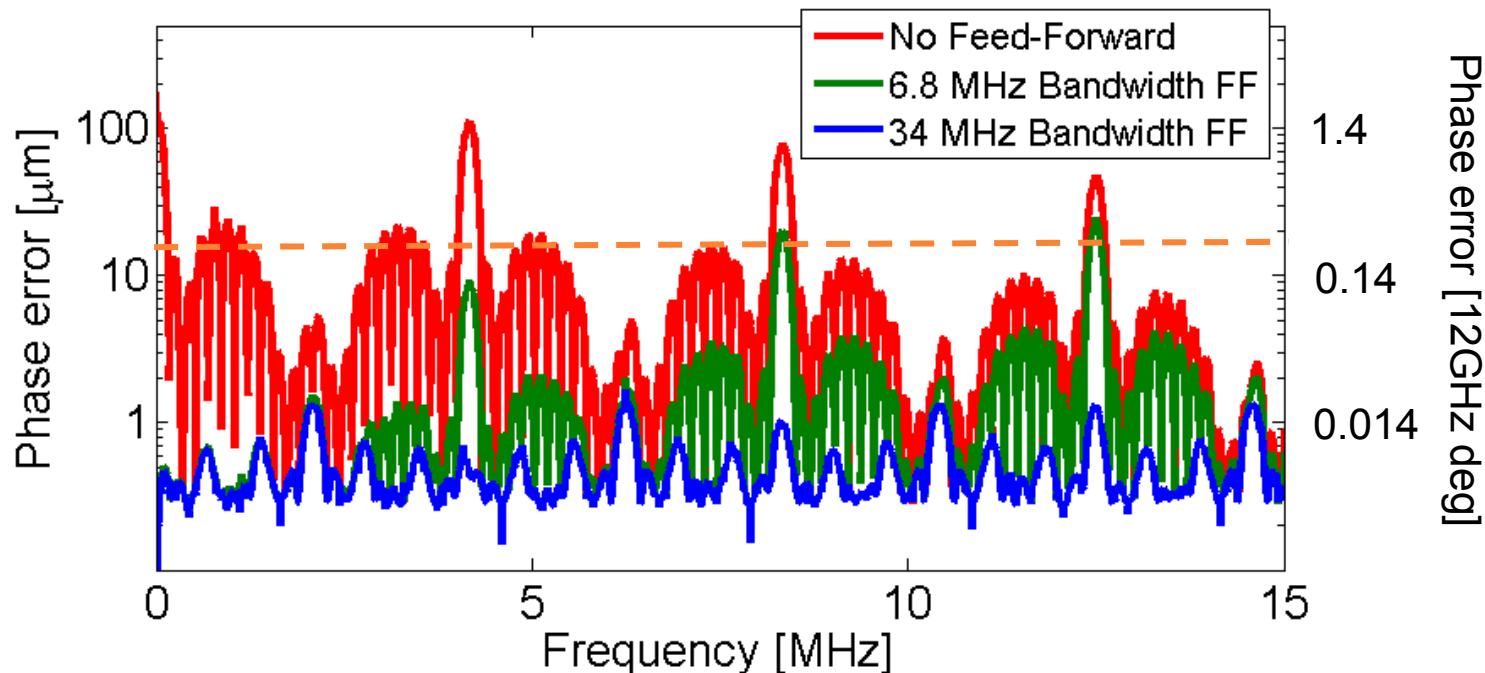
The CLIC Phase Stabilization Feed-Forward System

- ◆ It will increase the drive beam stability and correct phase variation along pulse to the required 0.2° at 12GHz
 - Measure phase offset before the turn around
 - Correct it after the turn around
- ◆ The current CLIC design based on a 4-bend chicane
 - Each bend is equipped with a fast kicker so that the time of flight though the chicane is variable, and thus the time of flight also



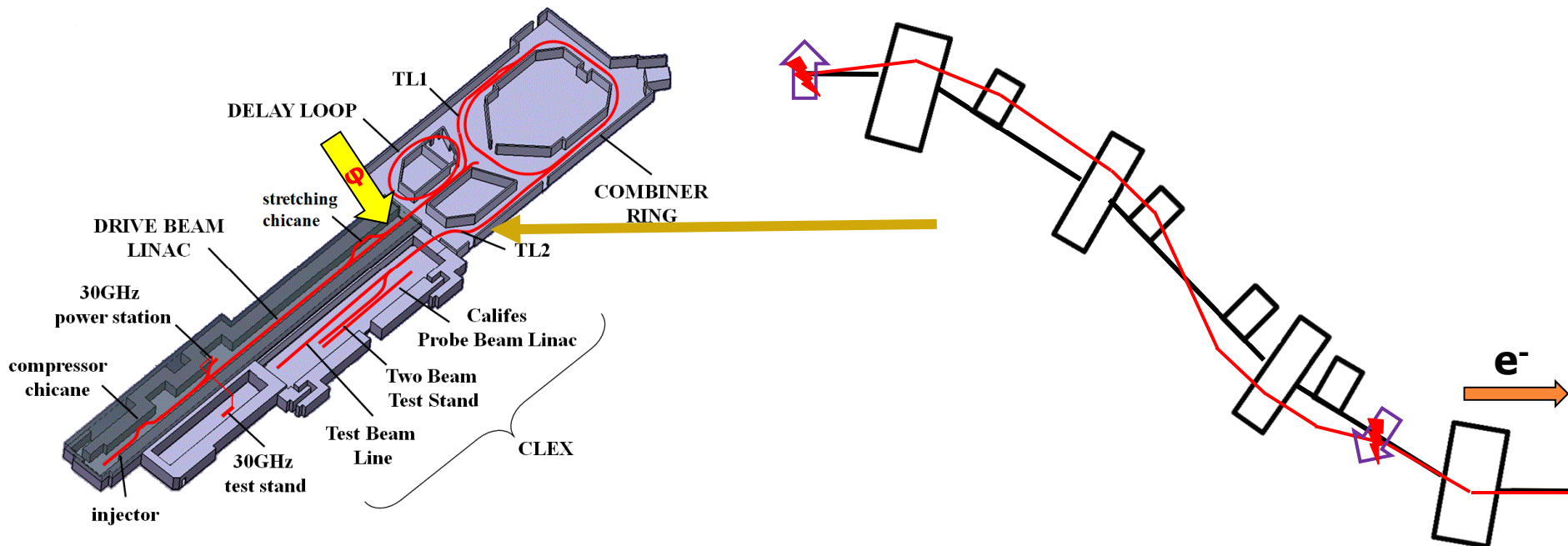
Bandwidth and amplifier power

- ◆ Naturally, the bandwidth of the system is the key parameter

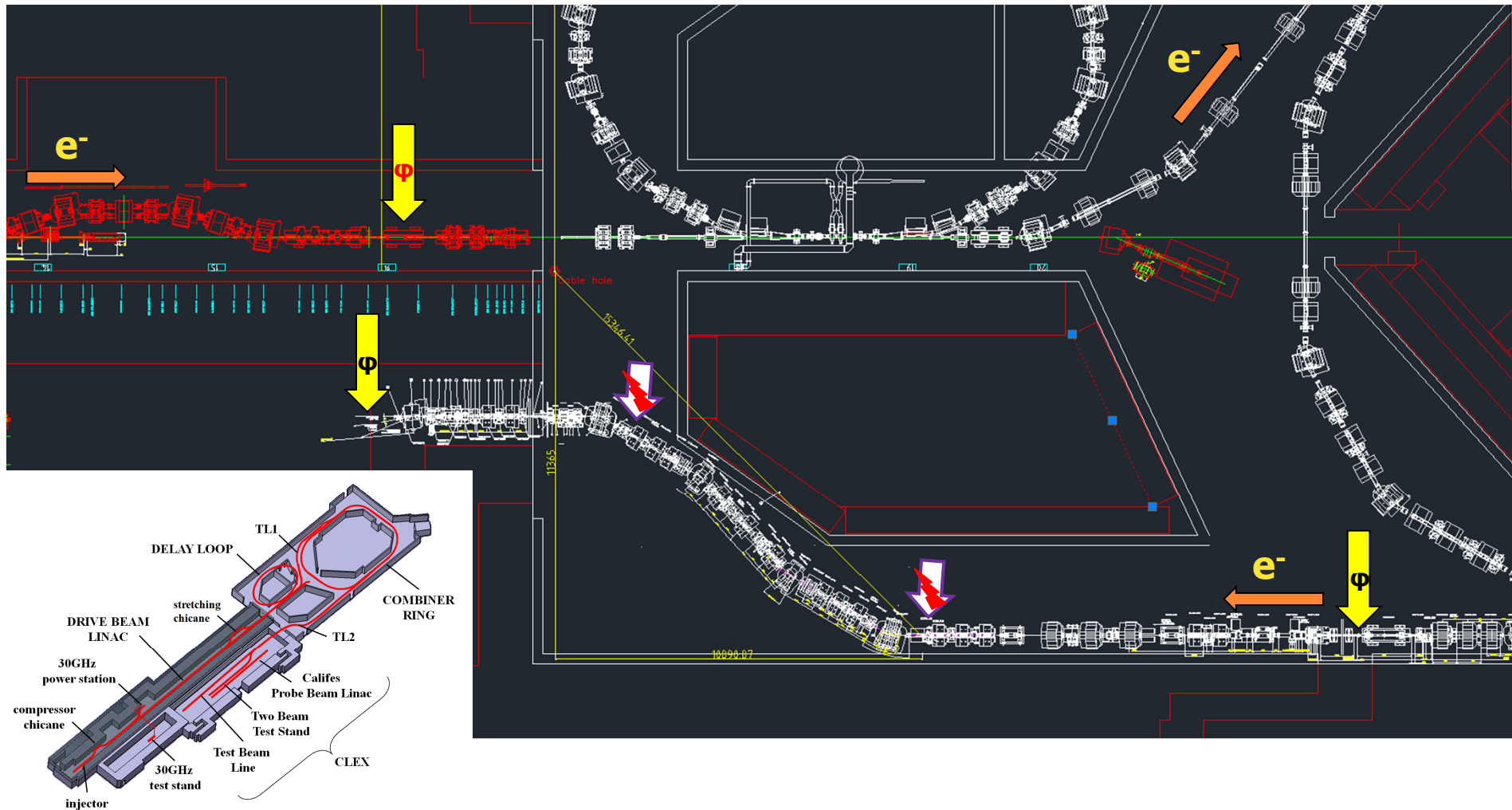


- ◆ And the amplifier power to deliver sufficient deflection angle for the 2.4 GeV beam **combined with the high bandwidth**

- ◆ A prototype system implementation in CTF3
 - Prove its feasibility
 - Test area for the R&D
 - Ultimate goal: phase stabilization to 0.2 deg @ 12 GHz
- ◆ Phase measured before the Delay Loop with a dedicated monitor
- ◆ Correction in the **dog-leg chicane** after Combiner Ring using 2 kickers
- ◆ Verification with 2 monitors installed just before and after the dogleg
- ◆ 280 ns latency



◆ A more detailed technical view



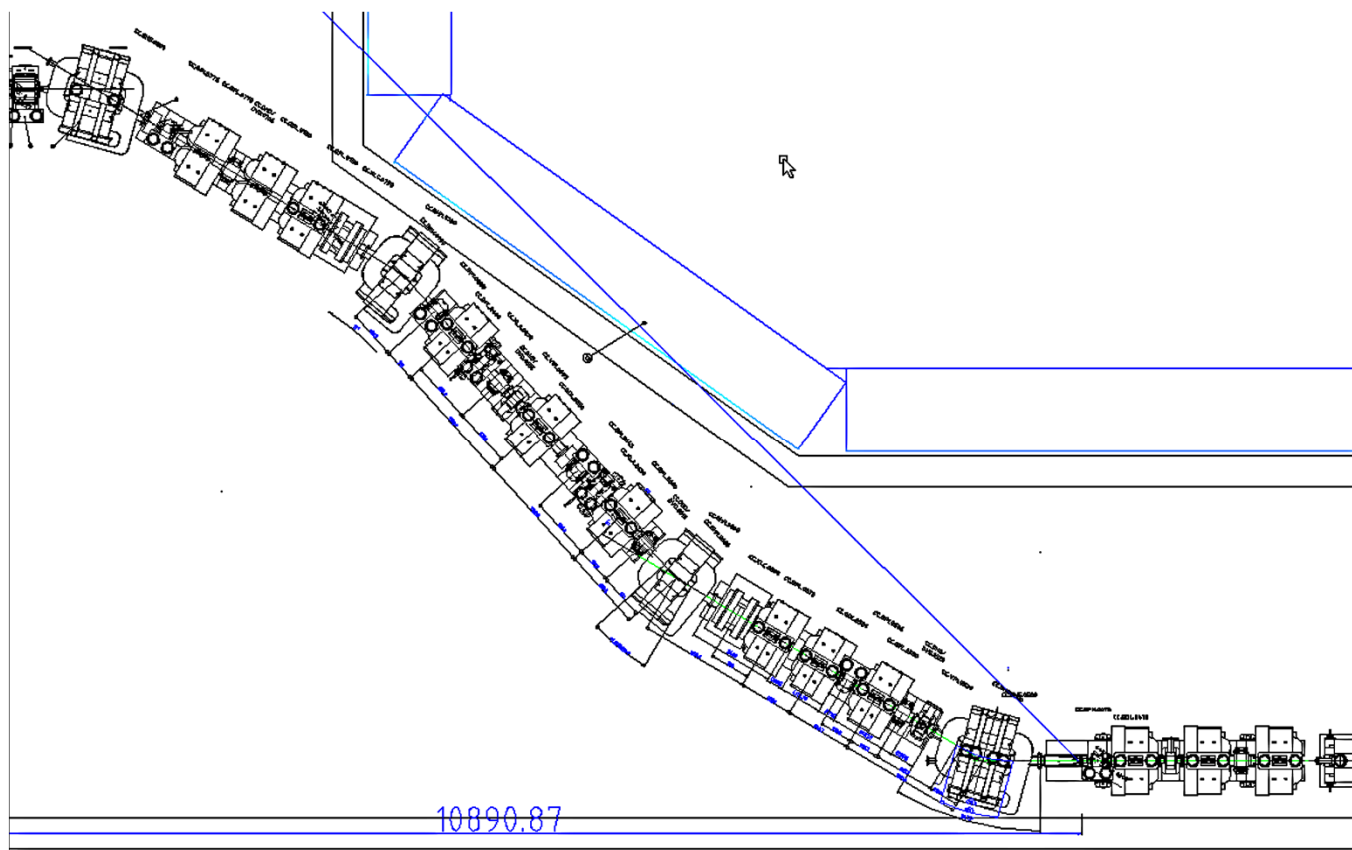


An Ideal Optics

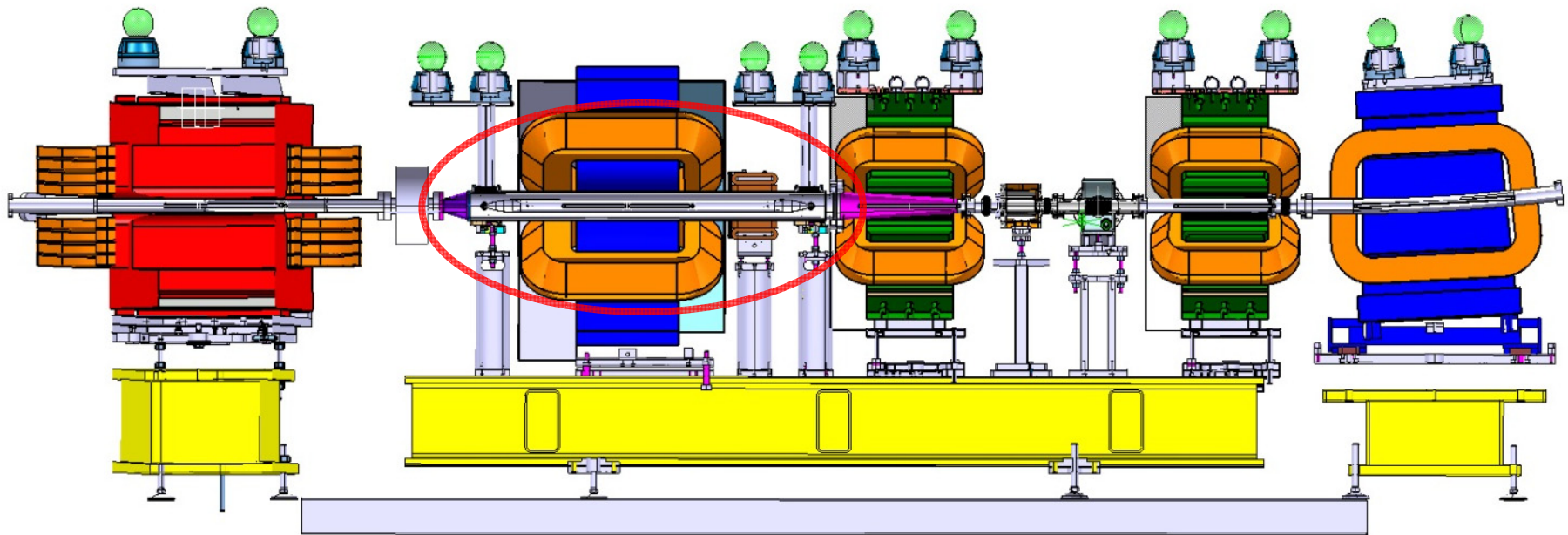


- ◆ Large R_{52} , at least 1 m
 - Defines the phase range that can be corrected with a given kick
 - ◆ $R_{52}=1$ m implies 1 mm path length change for nominal 1 mrad kick
- ◆ $R_{12} = 0$ from kicker to kicker
 - Orbit does not move after the correction
- ◆ $R_{22} = 1$ (or -1) from kicker to kicker
 - Kicker amplitude is the same (-1 means reversed polarity)
- ◆ Dispersion amplitude below 2m
- ◆ No dispersion after the dogleg
 - Including the bumped orbits
- ◆ Smooth transverse optics
 - Max betas not too big and min ones not too small
- ◆ Small R_{56} , adjustable

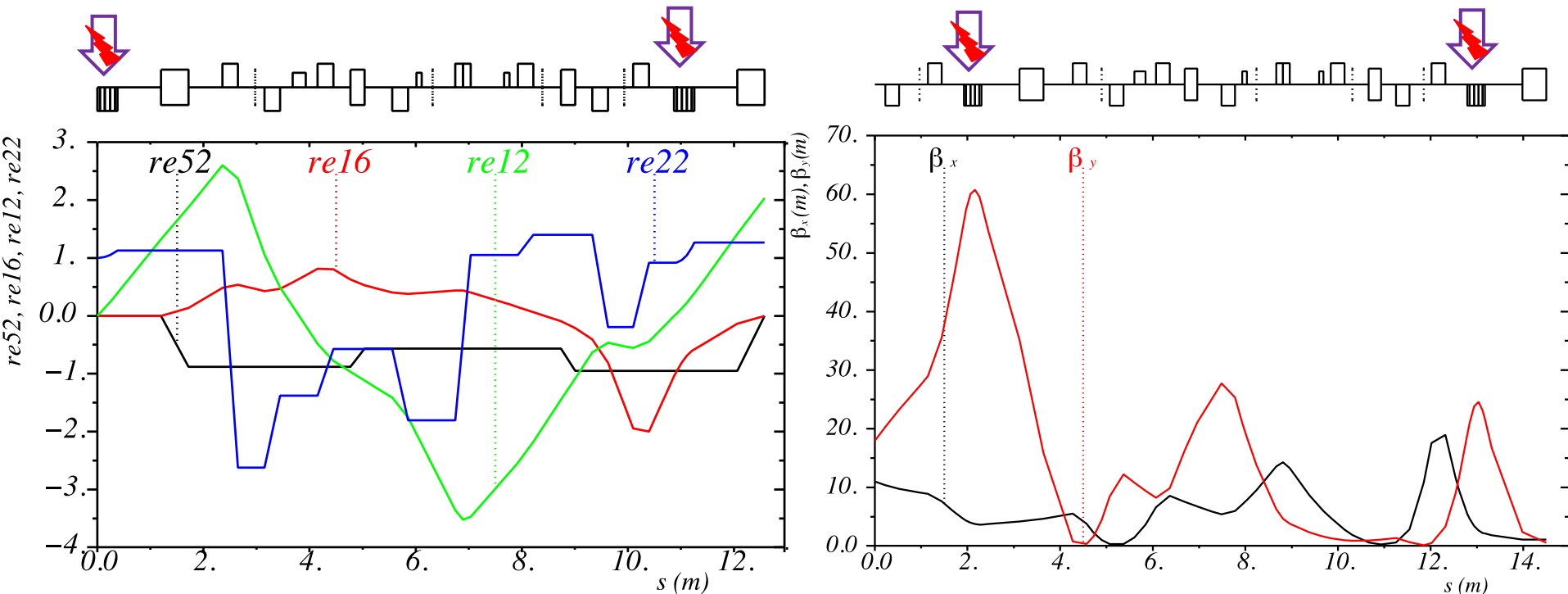
- ◆ A compromise was found between costly modifications and satisfactory performance
 - The correction chicane is implemented within an existing line
 - It is already densely packed → Kicker insertion tricky
 - For the system tests the resulting beam does not have to be perfect



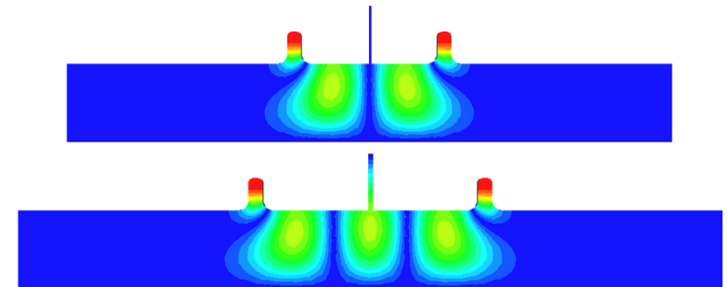
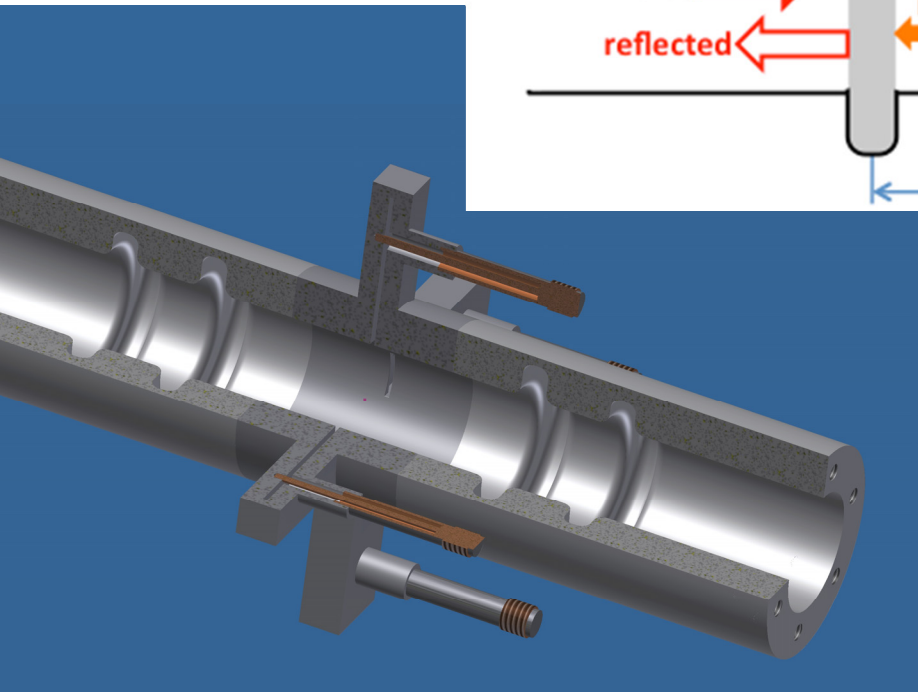
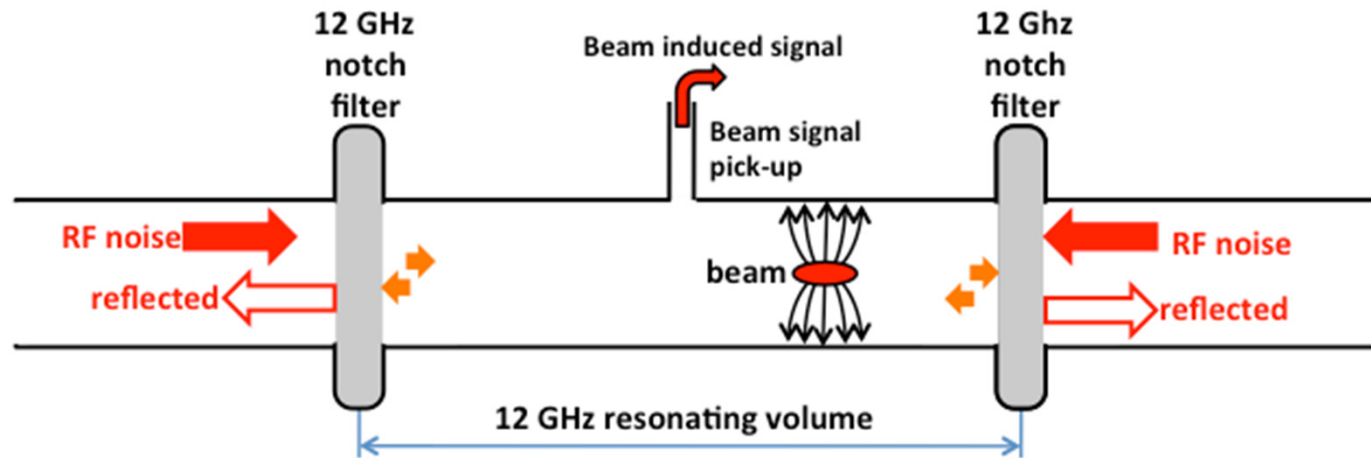
- ◆ A quadrupole and magnetic corrector around each kicker
 - The quadrupole is needed to preserve lattice functionality
 - The corrector:
 - ◆ will help in the commissioning
 - ◆ allows a slow feed-back to prevent phase drifts out of the kicker correction range



- ◆ R52=-1.05 → Correction range +/- 15° @12GHz
- ◆ The orbit bump perfectly closed
- ◆ Dispersion closed
- ◆ Maximum dispersion amplitude 2.2 m
- ◆ Spurious dispersion ~15 cm at maximum kick



- ◆ 12 GHz RF pickups using a choke mode cavity
 - 30 MHz bandwidth
 - 0.2° at 12 GHz resolution



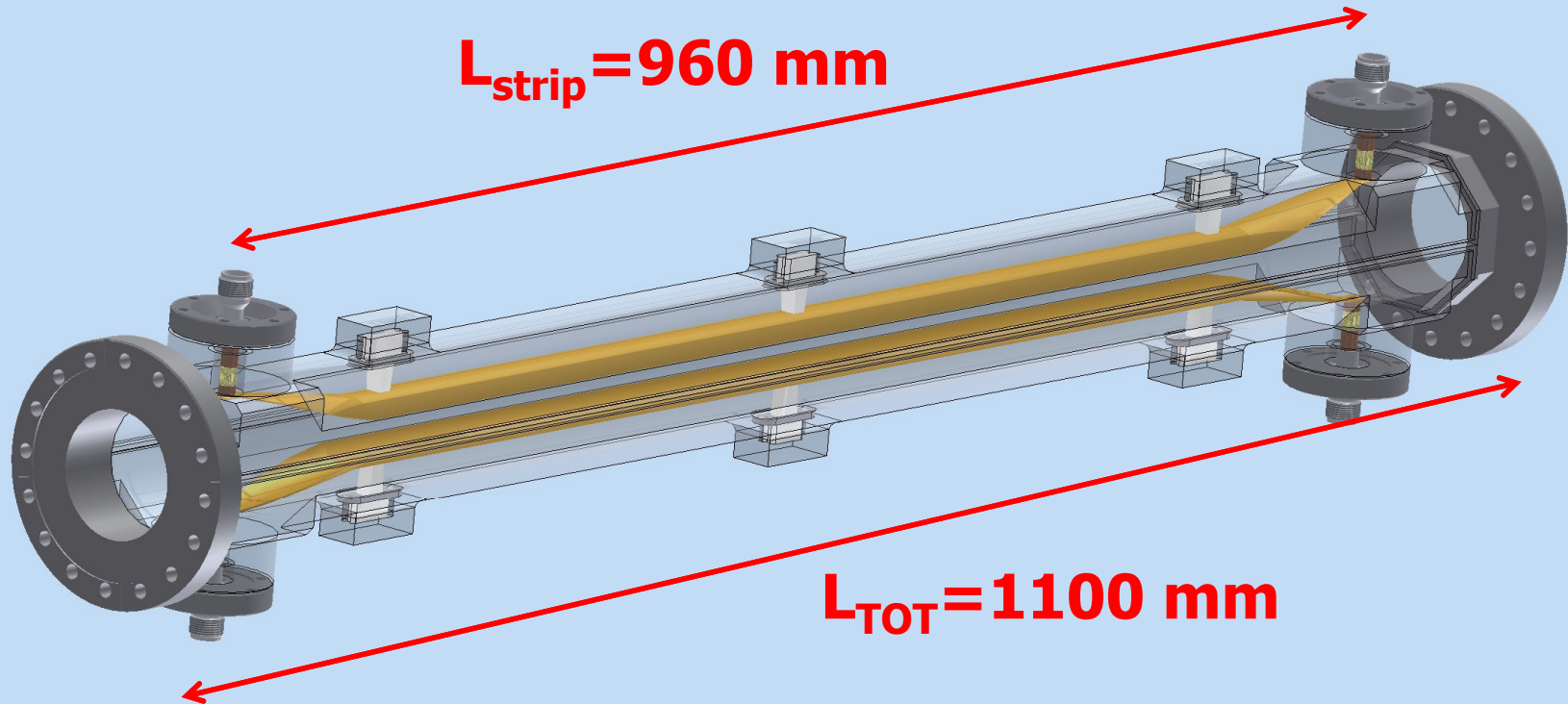
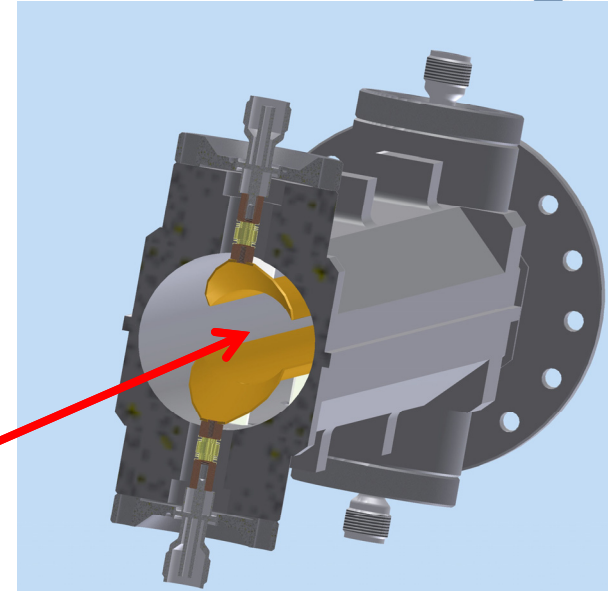


Kickers

LNF/INFN Frascati

- ◆ Strip-line kickers based on the Dafne design
- ◆ 1.1 kV for 1 mrad deflection @125 MeV
 - 100 Ω differential impedance
 - At least 50 kW drive needed

Strip-line Internal Diameter=40 mm





Amplifiers

John Adams Institute / Oxford University



- ◆ It is a major challenge: **Bandwidth and Power**
- ◆ Nominal peak power of 65 kW
- ◆ The target bandwidth is at least 50 MHz
 - But will be less for large changes in signal amplitude due to slew rate limitation
- ◆ Full performance guaranteed over a 280-420 ns range
 - 1.2 μ s pulse duration for the full uncombined CTF3 beam possible with somewhat limited performance
- ◆ 4 parallel 18 kW modules
 - Each with its own power converter and output transformer
 - The output stage of the amplifier module made of two 1200 V SiC FETs driven by low voltage Si FETs
 - Droop in the output transformers limited to 10% over 1.2 μ s
 - Each equipped with a separate drive and control module



Feed-forward processor

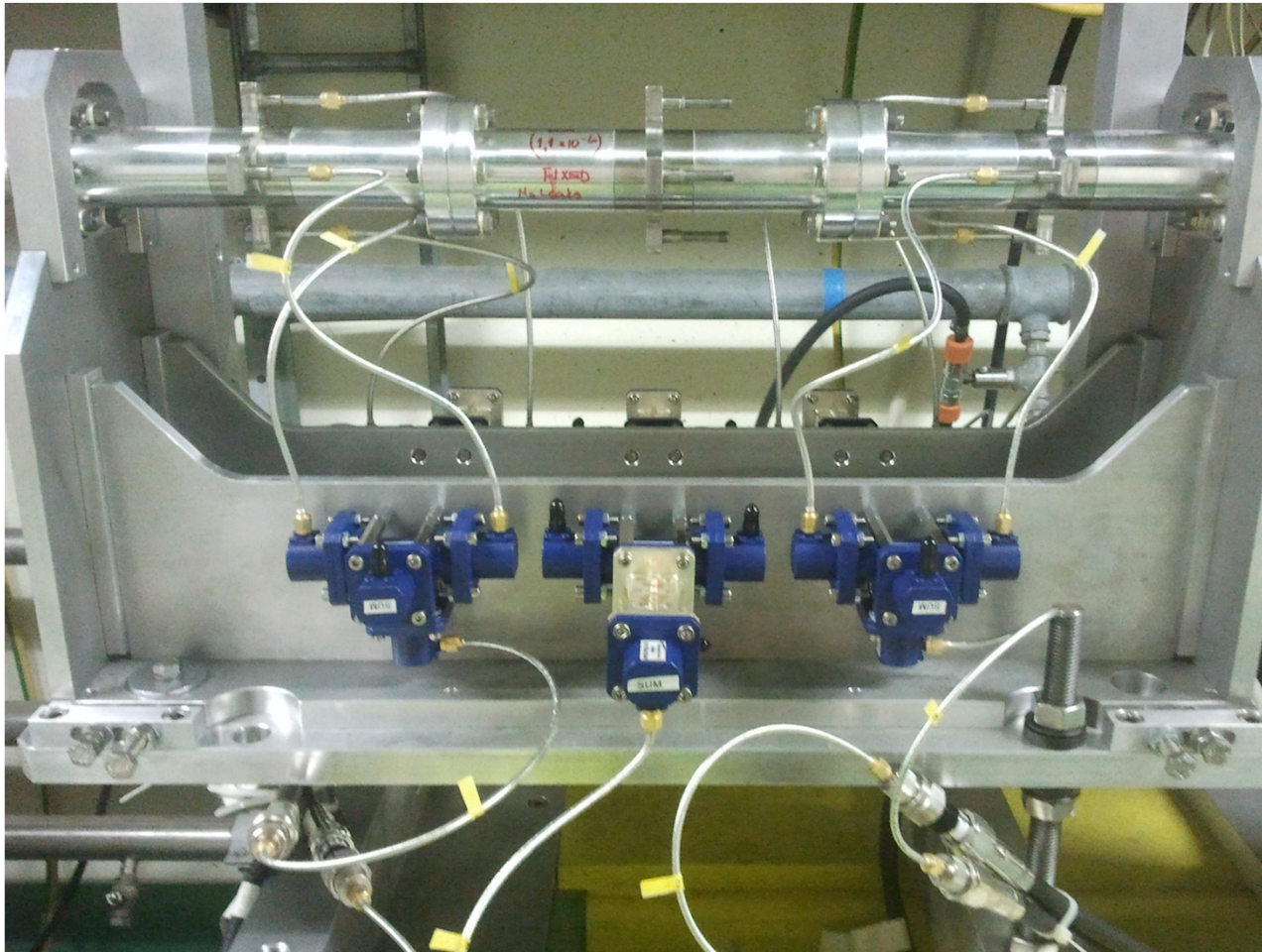
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- ◆ The brain of the system, will drive the kicker amplifiers
 - A custom digitiser and feed-forward controller based around a Xilinx Virtex-5 FPGA.
 - ◆ 9 analogue input channels, digitisation done using 14-bit 400 MS/s ADCs
 - ◆ 4 analogue output channels, using 14-bit 210 MHz DACs
 - The FPGA logic operations can be clocked in the range 200-400 MHz
 - ◆ External clock synchronized with CTF3 RF

- ◆ The feed-forward algorithm will allow for operation on both un-combined and combined beam.
 - For combined beam, measurements from corresponding sections of the different sub-pulses will be averaged together
 - ◆ This mimics the interleaving in the Delay Loop and Combiner Ring

Performance of Fast Beam Phase Monitors



The 3 monitors installed in a string for their validation



Read-out electronics

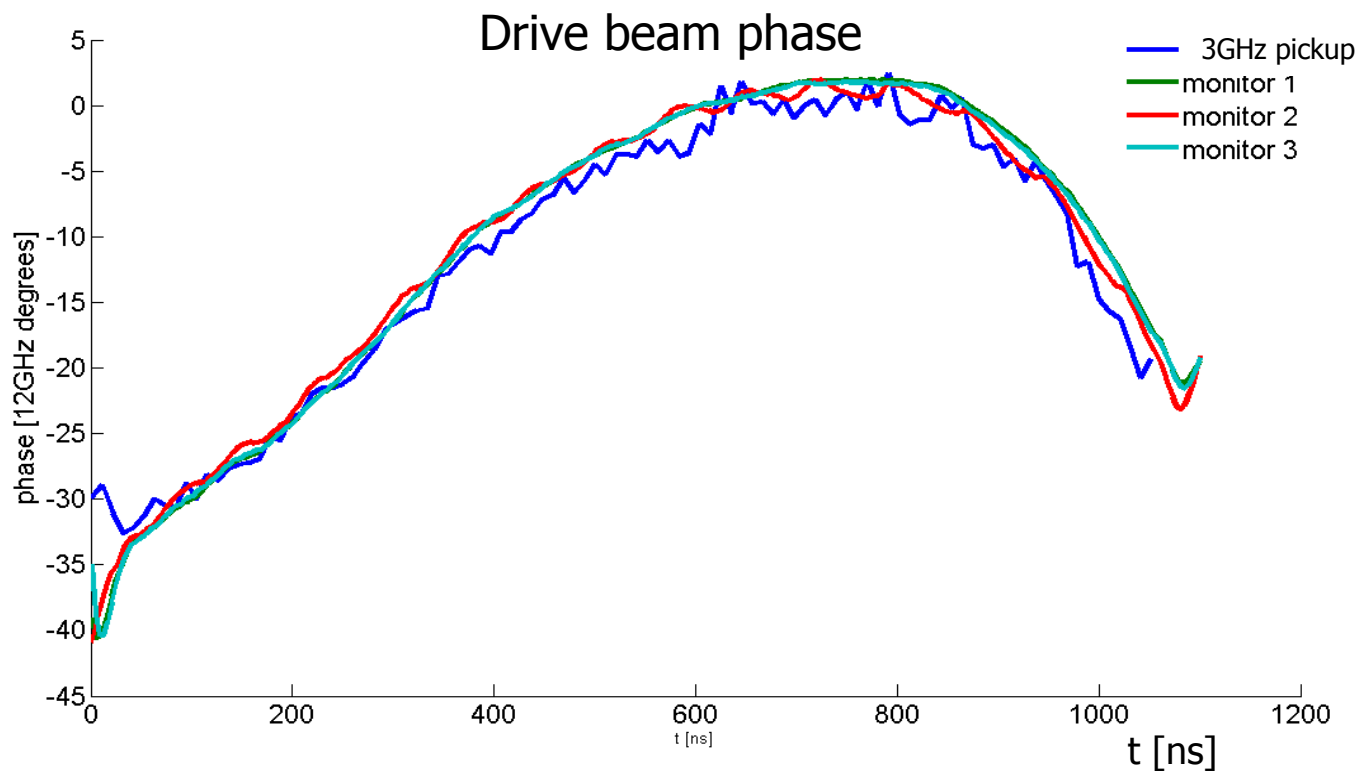


- ◆ 2 horizontal or vertical ports are connected to a hybrid
 - To remove TE11 dipole mode

- ◆ The sum signal is mixed with a 12 GHz reference producing signal proportional to $A \sin(\phi)$
 - The mixer output is amplitude dependent
- ◆ The sum amplitude is also measured with a diode
 - To resolve "A" for a given beam
- ◆ The difference signal is also measured with a diode
 - It is proportional to the beam position offset

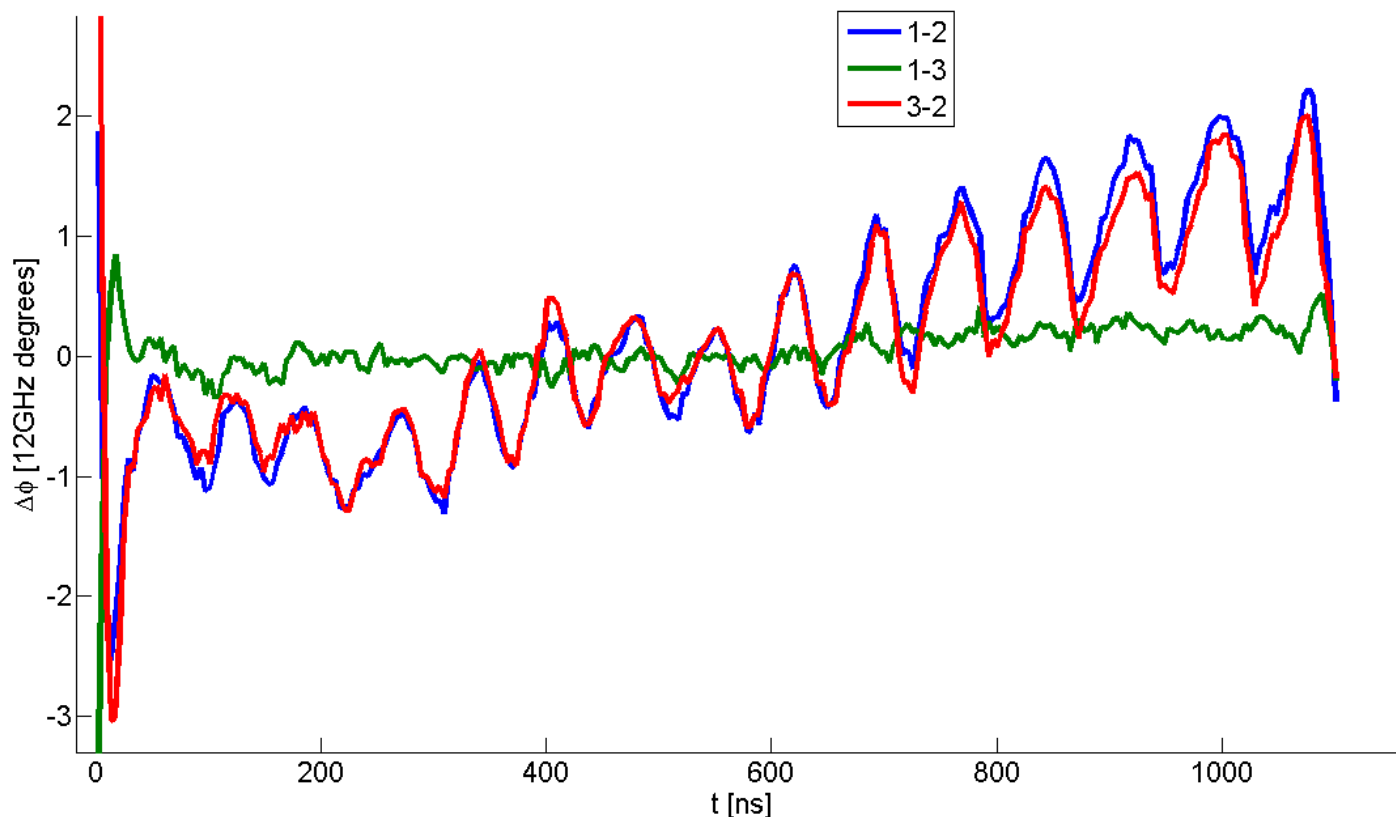
- ◆ Calibration using a synthesized signal with frequency close to the 12 GHz and with different amplitudes
 - In this way crosstalk and the all the calibration constants can be measured for the interesting range of amplitudes.

- ◆ Electronics resolution at the moment is about 0.2 degree
 - Will be soon improved with better signal and ADC level matching
- ◆ The monitors agree between each other and a 3 GHz button pickup



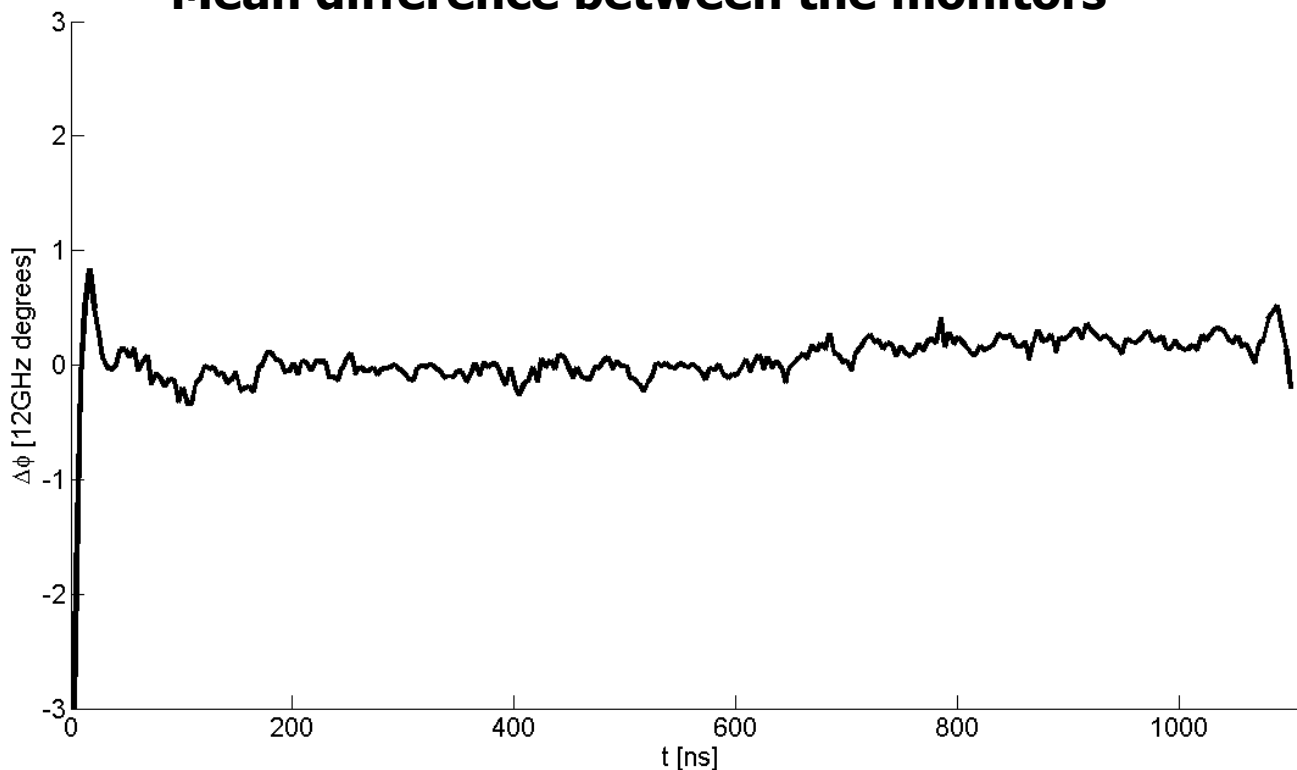
- ◆ However, monitor 2 performs not as good as 1 and 3
 - It was reported to have problems with the feed-through installation
 - It is discarded for the moment and will be repaired during shutdown

Mean difference between the monitors



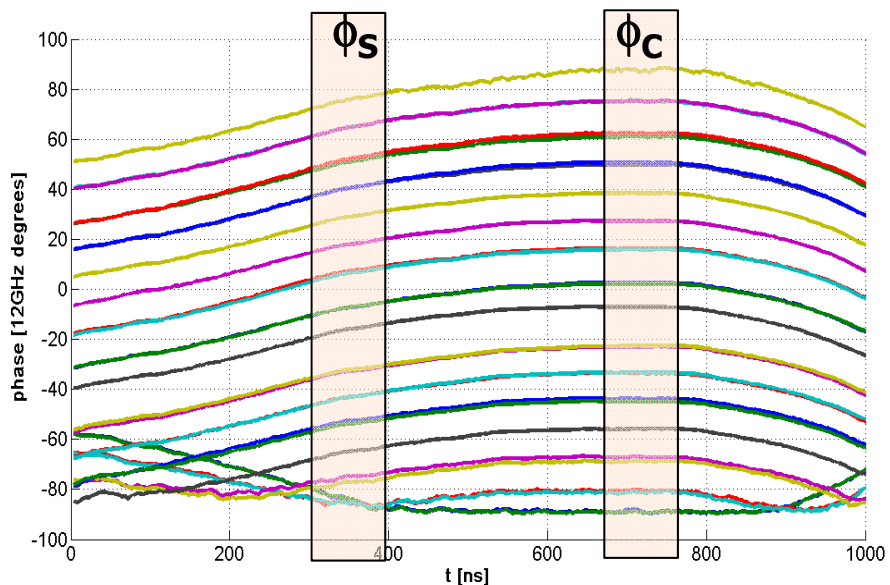
- ◆ The monitors 1 and 3 agree within 0.3 degrees
- ◆ Standard deviation of the residuals is 0.33 degrees
- ◆ The resulting resolution is 0.23 degrees
 - resolution is dominated by the electronic noise of 0.2 degrees

Mean difference between the monitors

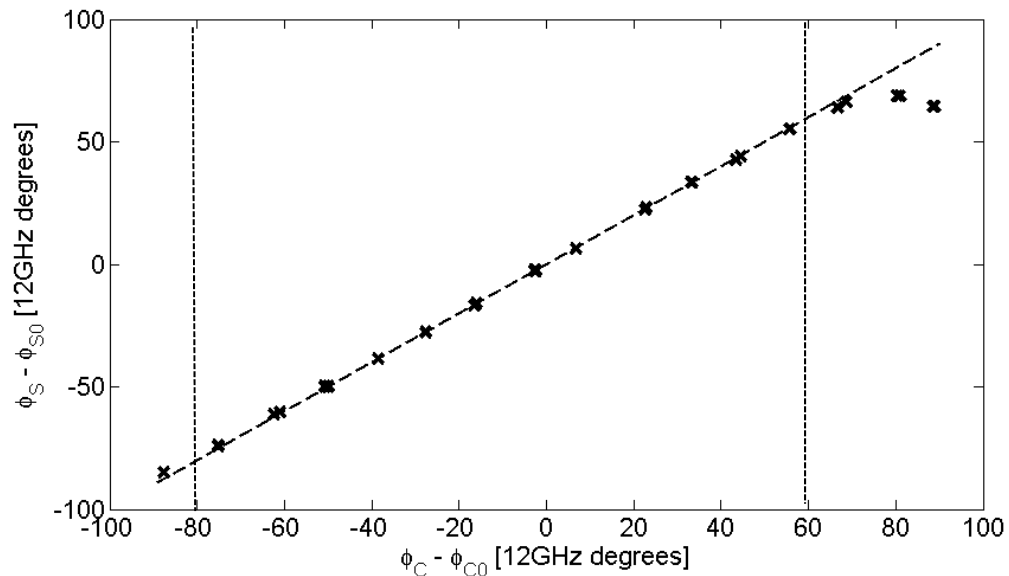


- ◆ The CTF3 beam has inherent phase sag due to the RF pulse compression system
- ◆ We observed how the measured phase sag changes for different phases of the local oscillator
- ◆ To quantify the preservation of the shape difference at 2 locations ϕ_C and ϕ_S within traces is plotted

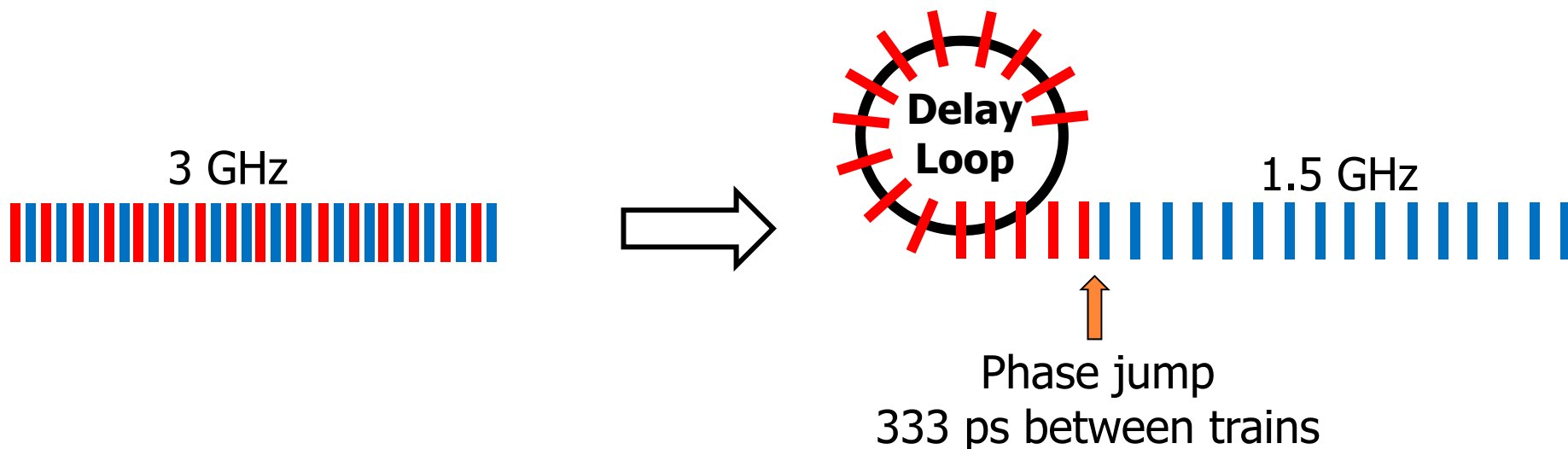
Measured beam phase for different LO phases



Linear within $\pm 70^\circ$

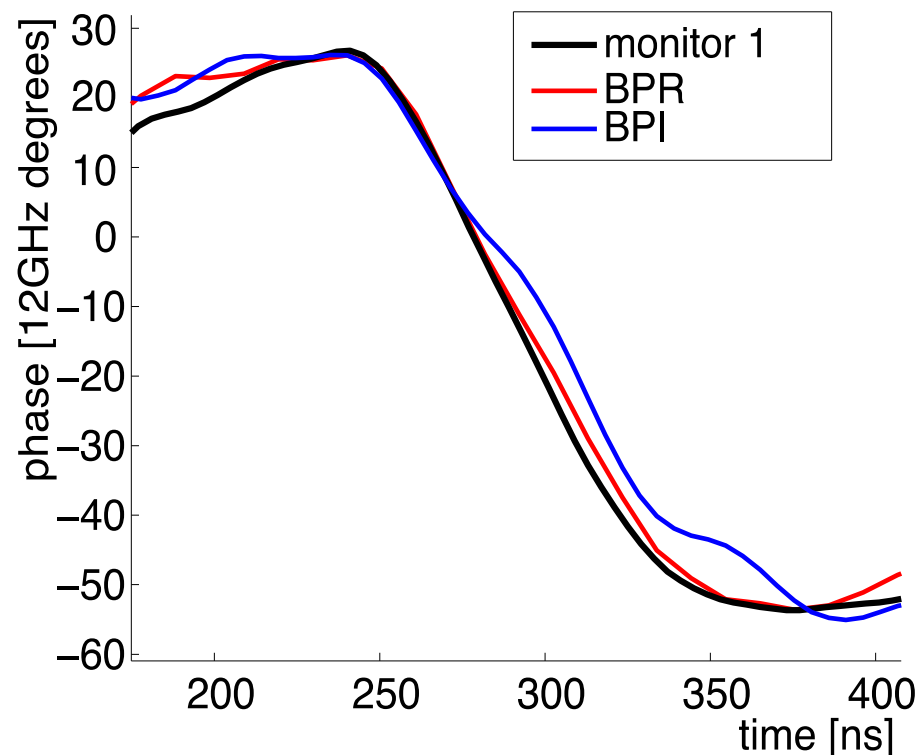


- ◆ The monitors were designed for 30 MHz bandwidth
- ◆ The final bandwidth measurement will be done only when the monitors are installed at their positions downstream of the Delay Loop
 - The Delay Loop allows us creating a train with a sharp phase jump



- ◆ A steep phase step was introduced
 - The RF pulse compression for the last station was programmed to deliver an amplitude step as sharp as possible
 - ◆ And hence the beam energy change
 - The Stretching chicane adjusted to $R56=0.45$ converted the energy change to the phase change
 - The steepness was verified using
 - ◆ A BPM (BPI) at a large dispersion location
 - ◆ A BPR - a 3GHz button phase pickup

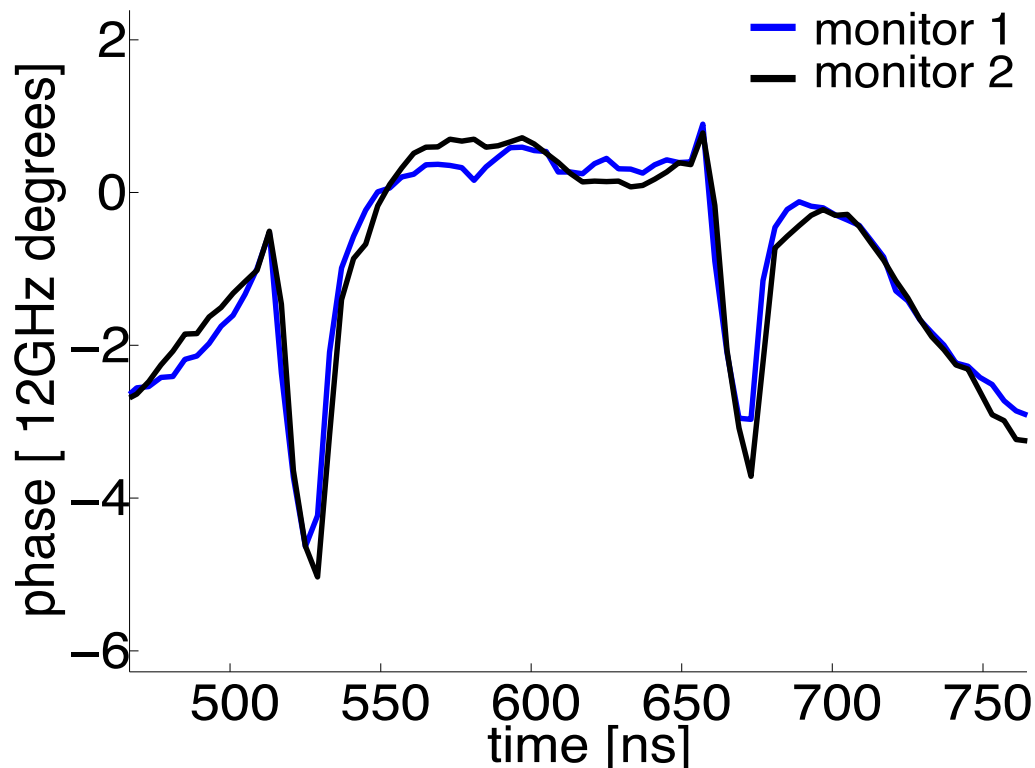
- ◆ The bandwidth is at least 3.7 MHz



Bandwidth checks

The phase switches

- ◆ Measurement of phase switches in the sub-harmonic bunchers
 - 180° phase switches needed for recombination with the Delay Loop
- ◆ Imperfect switches create discontinuity in bunch phase
- ◆ The monitors measure a 30 ns effect that implies **10MHz** BW
 - There is no independent way in CTF3 to cross-check the phase change





Beam position dependence



- ◆ A beam position offset induces dipole mode TE_{11}
 - -25dB lower than the monopole mode
- ◆ If the hybrid is perfect, it shouldn't be present in the sum
 - Hybrids are never perfect
- ◆ Direct position scans show no statistically relevant effect
 - The beam was moved ± 4 mm using 2 magnetic correctors installed just upstream of the monitors and a ballistic beam behind them was measured with 2 BPMs
- ◆ By measuring how the difference channel power changes with the beam position, we calculated the hybrid rejection level to -25dB
 - By symmetry, this must be the same in the sum (phase) signal
 - We calculated the position-to-phase crosstalk to $0.16^\circ/\text{mm}$



Conclusion



- ◆ A prototype Phase Feed Forward system is in preparation in CTF3
- ◆ It will serve as an R&D and test area for the technology development
- ◆ The fast phase monitors are operational and perform accordingly to their specification
- ◆ The full system will be operational at the end of summer 2013



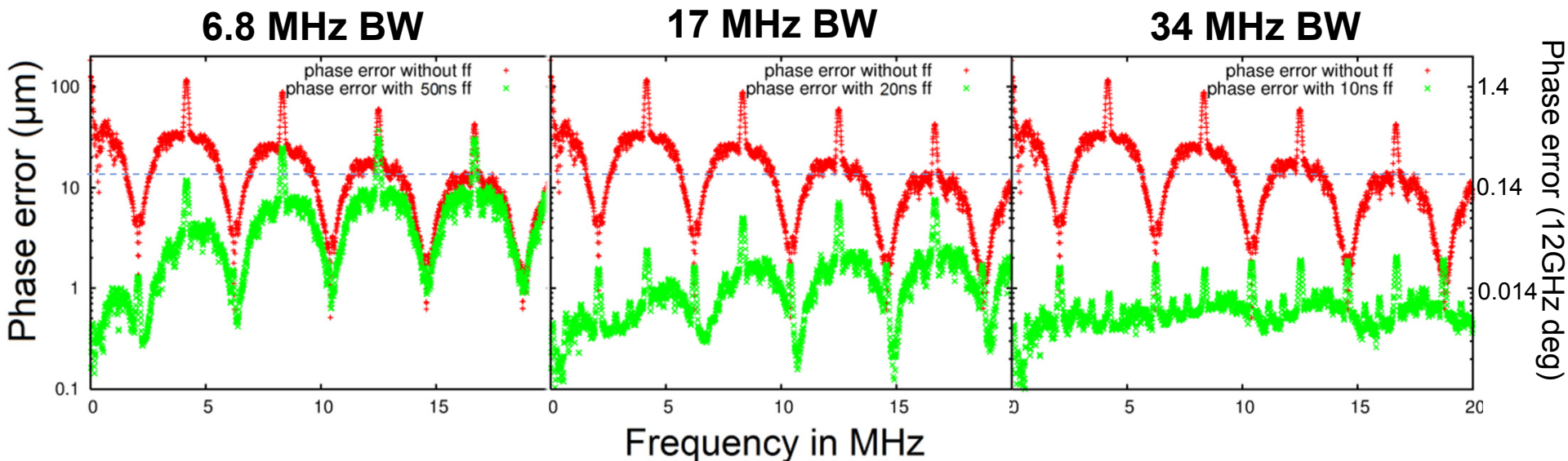
Backup slides



◆ Backup Slides

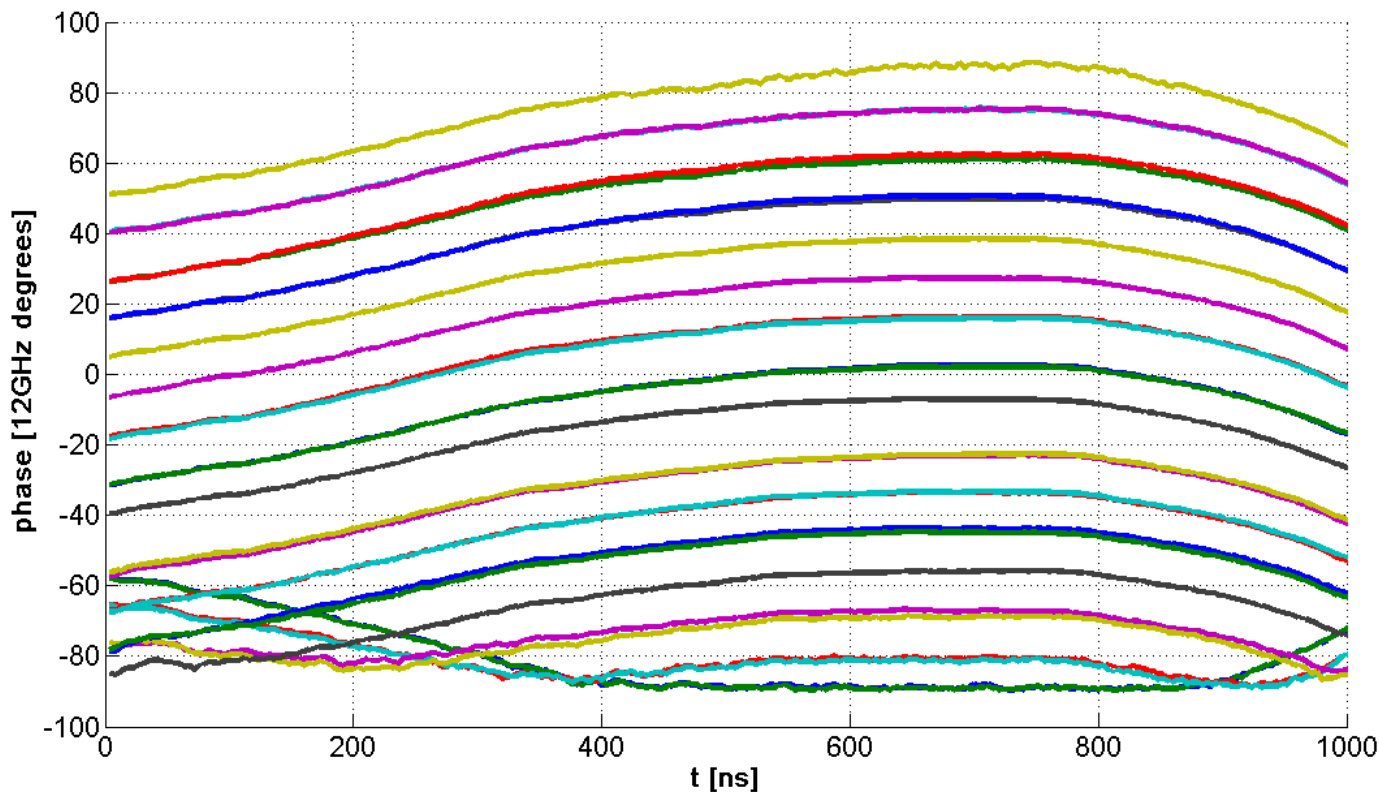
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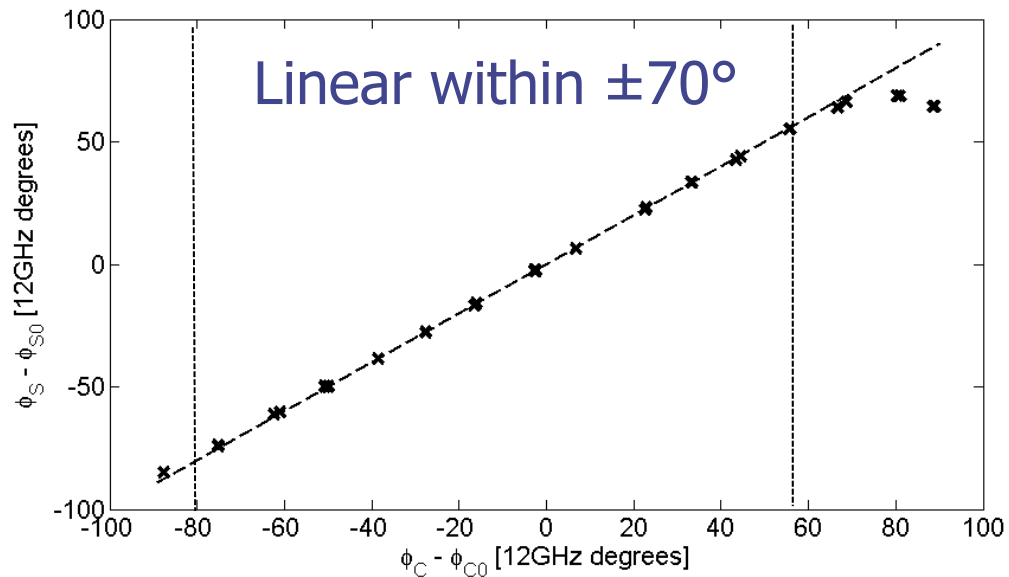
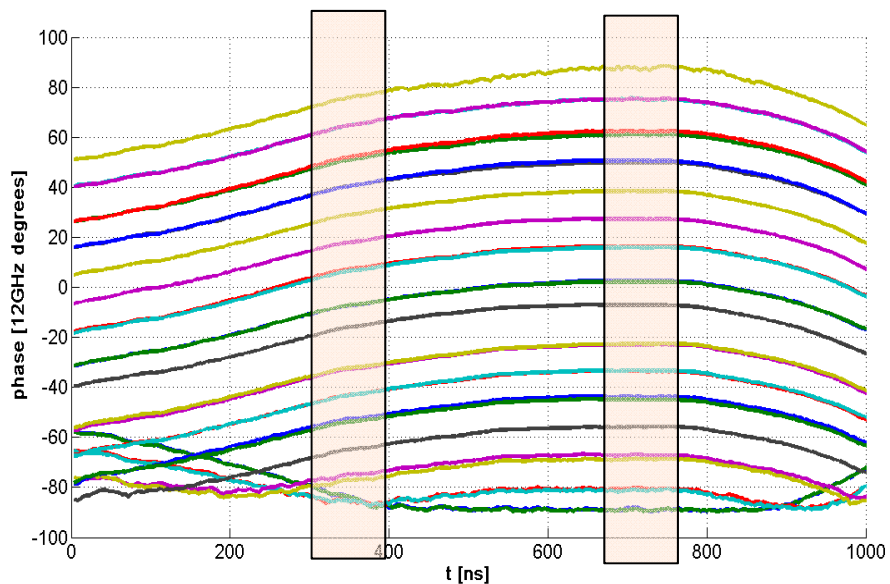


- ◆ The power of the amplifier to deliver sufficient deflection angle for the 2.4 GeV beam **combined with the high bandwidth**

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- ◆ We observed how the measured phase sag changes for different phases of the local oscillator

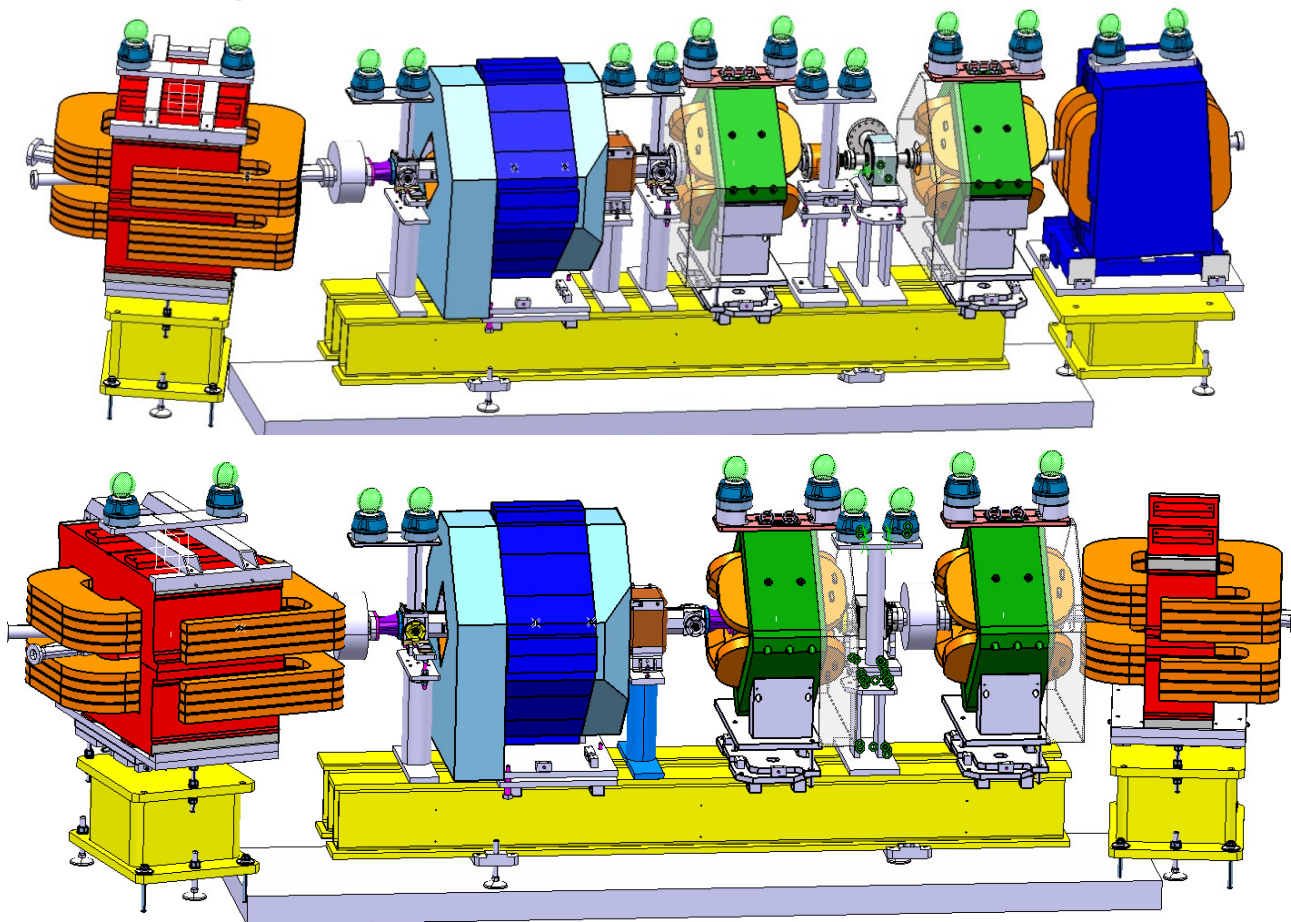


- ◆ To quantify the preservation of the shape
 - 2 values at different locations within traces are taken, ϕ_C and ϕ_S
 - One trace is taken as a reference, corresponding phases ϕ_{C0} and ϕ_{S0}
 - For each trace, the difference to the corresponding point in the reference is calculated for



Integration of the kickers

- ◆ A quadrupole and magnetic corrector around each kicker
 - Quadrupole is needed to preserve the lattice functionality
 - Corrector will help in the commissioning and allow implementation of a slow feed-back



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