

#### NIF Target Diagnostic Automated Analysis: Operations & Calibrations

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Judith Liebman, Rita Bettenhausen, Essex Bond, Allan Casey, Robert Fallejo, Matt Hutton, Amber Marsh, Tom Pannell, Abbie Warrick

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# After a NIF laser shot, analysis is automatically run on data from more than 20 target diagnostic systems



#### Novel signal & image processing is needed to turn raw diagnostic data into the key performance metrics



# Automated diagnostic analysis is used to estimate key performance metrics and enable NIF optimization



## Two critical components of automated analysis are supporting NIF operations and maintaining calibration data

#### Handling operational off-normal data

- Diagnostic raw data may be different than expected due to hardware redesigns, detector malfunctions, abnormal shot types, noise, etc.
- Review one example: Gamma Reaction History (GRH) peak suppression discrepancies between channels.

#### Calibration maintenance design

- Analysis relies on a gargantuan amount of calibration data
- Review example of oscilloscope time base calibration for DANTE
- Review scope of the maintenance feat





H Abl DT Hfoot S01b | GRH | Stitched Signals | Scope4

#### GRH automated analysis reports gamma bang time and burn width with tens of ps accuracy - fielded in 2011

**GRH** Inverse Problems Include: **Deconvolved Cherenkov Peaks** Demodulating amplitude modulated signal from Mach-Zehnder hardware **10 MeV** Fiber optic Normalized Signal (a.u. 8 MeV cable LiNbO<sub>3</sub> Mach-Zehnder Laser diode 0.5 DC Bias Stitching multiple channel data 0 22.5 22.75 23 23.25 23.5 Time (ns) GRH Summary Peak Time (ns) Peak Width (ps) Peak Area Gas Thresh (MeV) Scope Deconvolving system responses of PMT SCOPE-1 22.956 141.581 and Cherenkov Gas cells using 23.020 SCOPE-2 190.374 constrained least squares filtering in the SCOPE-3 23.039 216.940 SCOPE-4 22.974 159.349 6422.004 frequency domain  $H(f)^{-1} = X(f) \cdot Conj(Y(f))$ 

 $(Y(f)^2 + G))$ 

2.9

4.5

☆ ⊼ ∨ X

NIE

4.5 MeV

4358.268

3.601E6

3.577E5

2.9 MeV

#### GRH data on one detector scope system showed the two Mach Zehnders reporting conflicting peak levels



### Investigating causes of peak suppression in Mach Zehnder (MZ) results: MZ introduction



- MZ is used to create a continuous signal light output from a continuous voltage input signal (usually to send down a fiber optic cable)
  - Can produce continuous light signal at high speed and with accuracy.
- To do this the MZ modulates the light intensity of a constant laser source
  - Some materials can change the phase of light passing through them based on voltage level applied to the material – LiNbO3 is often used
  - Light source is split, half is phase modulated, then recombined in order to amplitude modulate the light signal, similar to an interferometer.

#### Investigating causes of peak suppression in MZ results: Dither signal used for active bias control

- Bias point drifts with changes in temperature and environment
- Active Control of the bias point can be achieved by applying a low-frequency dither signal to the control system.
  - -Second harmonic of the dither signal is minimized
  - Output data includes presence of the dither signal



### Peak suppression solution: use recorded dither signal to incorporate dither input correction into MZ demodulation equations

$$I_{out}(t) = \frac{I_{Maxhn}}{2} \left[ 1 + \sin\left(\frac{\pi V_{pnt}(t)}{V_{pnt}^{\pi}} + \frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}}\right) \right]$$
Light intensity through MZ transfer function
$$Solve \text{ for voltage entering MZ, substitute measured vars}$$

$$V_{pnt}(t) = \frac{V_{pnt}^{\pi}}{\pi} \left[ \sin^{-1} \left( \frac{V_{dig} - V_{lightExt}^{0}}{abs(V_{Dig}^{0@Q} - V_{lightExt}^{0})} + 1 \right) - \sin^{-1} \left( \frac{V_{Dig}^{0shot} - V_{lightExt}^{0}}{abs(V_{Dig}^{0@Q} - V_{lightExt}^{0})} + 1 \right) \right]$$

$$V_{pnt}(t) = \frac{V_{pnt}}{\pi} \left[ \sin^{-1} \left[ \frac{V_{Digac}(t) - baseline}{c_{ac/dc}abs(V_{Digac}^{0@Q} - V_{lightExt}^{0})} + \left( \frac{V_{Digac}^{0shot} - V_{lightExt}^{0}}{abs(V_{Digac}^{0@Q} - V_{lightExt}^{0})} + 1 \right) \right] - \sin^{-1} \left[ \frac{V_{0ignc}^{0shot} - V_{lightExt}^{0}}{abs(V_{Digac}^{0@Q} - V_{lightExt}^{0})} + 1 \right] \right]$$

### Majority of effort to develop dither correction solution is defining, storing and querying necessary data



### Dither corrected demodulation results show the effects of bias control dither related peak suppression



### Operational support projects account for one third of target diagnostic analysis team milestones



### Quality automated results require expected target diagnostic data, tested analysis software, and *accurate calibration data*



Calibration data omissions, formatting problems, and stale data are the leading cause of target diagnostic analysis failures during operations. With between 500 and 5000 calibration parameters per diagnostic, there are usually several calibration issues to follow up on every week.

## Calibration data example: Dante data is recorded on oscilloscopes that exhibit significant time-base distortion



## Formatting and naming interface documents define how analysis software reads in the calibration data

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#### Time-base calibration data is stored in Locos database associated with oscilloscope serial number and sweep speed

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C143-274-DANTE1	RACK1S04	13010107	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>52913058</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 4.5GHZ BW, 11 BIT	2009-05-01 15:30:00	9999-01-01			
C143-274-DANTE1	RACK1S02	13010111	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>53815346</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 4.5GHZ BW, 11 BIT	2009-05-01 16:44:00	9999-01-01			
C143-274-DANTE1	RACK2S08	13010148	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>53816024</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 4.5GHZ BW, 11 BIT	2009-05-01 22:24:00	9999-01-01	E		
C064-350-DANTE2	RACK1S03	13011118	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>52906419</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 7GHZ BW,13 BIT	2009-06-01 14:22:00	9999-01-01			
C064-350-DANTE2	RACK4S17	13011125	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		52906419	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 7GHZ BW,13 BIT	2009-06-01 14:22:00	9999-01-01			
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C064-350-DANTE2	RACK3S11	13011114	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>52906419</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 7GHZ BW,13 BIT	2009-06-01 14:22:00	9999-01-01			
C064-350-DANTE2	RACK1S01	13011119	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>52906419</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 7GHZ BW,13 BIT	2009-06-01 14:22:00	9999-01-01			
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C064-350-DANTE2	RACK2S09	13011128	AnalysisType=time SweepSpeed=5ns	DOCUMENT_ID	CL_SCD50		<u>52906419</u>	Dante_Scope	SCOPE, DGTZR, WAVEFORM, 7GHZ BW,13 BIT	2009-06-01 14:22:00	9999-01-01			
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#### Scale of Dante calibration: two instruments with 18 detectors each adds up to > 500 calibrated elements



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# Partnering with scientific diagnostic teams to define calibration maintenance flow and design tools



Analysis (SAVI) team is instrumental in the process of maintaining calibration data and thereby ensuring the success of target diagnostic algorithm automation and robust accurate results.

### Design of calibration report tool with recalibration notifications, high level views, and verification tracking

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TD_STREAK_CAMERA (42 items)	Dataset def	<u>inition cor</u>	nment	Last updated	d: 12/1/20	12, V1.1	Latest	t Version: V1	.2 Exp	pected F	Recalibratior	n: 12/1/2013	SAVI	Verified? YES	Dattas	et Def
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#### Supporting operations, calibration, quality assurance and new analysis automation are the foundation for successful automated target diagnostic analysis



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NIF GRH has a negative V0 with a positive going pulse, so we need to change signs from the positive baseline with positive going pulse

$$I_{out}(t) = \frac{I_{Maxhr}}{2} \left[ 1 + \sin\left(\frac{\pi V_{pmt}(t)}{V_{pmt}^{\pi}} + \frac{\pi \Delta V_{blas}}{V_{blas}^{\pi}}\right) \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1}\left(\frac{I_{out}(t)}{I_{Maxhr}/2} - 1\right) - \frac{\pi \Delta V_{blas}}{V_{bias}^{\pi}} \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1}\left(\frac{V_{dig} - 2V_{dig}^{0.bot}}{-V_{dig}^{0.bot}} - 1\right) - \frac{\pi \Delta V_{blas}}{V_{bias}} \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1}\left(\frac{V_{dig} - 2V_{dig}^{0.bot}}{-V_{dig}^{0.bot}} + 1\right) - \sin^{-1}\left(\frac{V_{Dig}^{0.bot}}{-V_{Dig}^{0.eq}} + 1\right) \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1}\left(\frac{V_{dig}}{-V_{dig}^{0.bot}} + 1\right) - \sin^{-1}\left(\frac{V_{Dig}^{0.bot}}{-V_{Dig}^{0.eq}} + 1\right) \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1}\left(\frac{V_{dig}}{-V_{dig}^{0.bot}} + 1\right) - \sin^{-1}\left(\frac{V_{Dig}^{0.bot}}{-V_{Dig}^{0.eq}} + 1\right) \right]$$

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$$V_{pmt}(t) = \frac{V_{pmt}}{\pi} \left[ \sin^{-1}\left(\frac{V_{dig}}{-V_{Dig}^{0.bot}} + 1\right) - \sin^{-1}\left(\frac{V_{Dig}^{0.bot}}{-V_{Dig}^{0.bot}} + 1\right) \right]$$

#### NIF GRH AC coupled MZ equations:

$$V_{Dig_{ac}}(t) = V_{Dig_{ac}}^{0@Q_{-}} c_{ac/dc} \left[ \sin\left(\frac{\pi V_{pmt}(t)}{V_{pmt}^{\pi}} + \frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}}\right) - \sin\left(\frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}}\right) \right]$$
where  $c_{ac/dc} \cong$  splitter ratio (~1) \*  
transmission thru bias tee (~.97)  
NIF GRH AC channel Inverted equations:  

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1} \left[ \frac{V_{Dig_{ac}}(t)}{c_{ac/dc}} + \sin\left(\frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}}\right) \right] - \frac{\pi \Delta V_{bias}}{V_{bias}} \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1} \left[ \frac{V_{Dig_{ac}}(t)}{c_{ac/dc}} + \sin\left(\frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}}\right) \right] - \frac{\pi \Delta V_{bias}}{V_{bias}} \right]$$

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1} \left[ \frac{V_{Dig_{ac}}(t) - baseline}{c_{ac/dc}} + \left(\frac{V_{Dig_{ac}}^{0@Q_{-}}}{c_{ac/dc}} + \left(\frac{V_{Dig_{ac}}^{0wot}}{D_{big_{ac}}}\right) + \left(\frac{V_{Dig_{ac}}^{0wot}}{abs(V_{Dig_{ac}}^{0@Q_{-}})} + 1 \right) \right] - \sin^{-1} \left[ \frac{V_{Dig_{ac}}^{0shot}}{abs(V_{Dig_{ac}}^{0@Q_{-}})} + 1 \right] \right]$$

With a little algebra this does simplify to the eq Kirk suggested:

$$V_{pmt}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1} \left[ \frac{V_{Dig_{ac}}(t) - baseline + c_{ac/dc}(V_{Dig_{dc}}^{0.shot} + abs(V_{Dig_{dc}}^{0.00Q_{-}}))}{c_{ac/dc}abs(V_{Dig_{dc}}^{0.00Q_{-}})} \right] - \sin^{-1} \left[ \frac{V_{Dig_{DC}}^{0.shot}}{abs(V_{Dig_{DC}}^{0.00Q_{-}})} + 1 \right] \right]$$

Where V0shotDigDC is negative

#### Example (J. Liebman):



$$\phi = \frac{\pi \Delta V_{bias}}{V_{bias}^{\pi}} = \sin^{-1} \left( \frac{V_{Dig_{dc}}^{0\,shot}}{V_{Dig_{dc}}^{0\,@\,Q_{-}}} - 1 \right) = -52.66\,mrad$$

$$V_{pmt}^{actual}(t) = \frac{V_{pmt}}{\pi} \left[ \sin^{-1} \left( \frac{V_{Dig}(t)}{V_{Dig_n}^{0@Q_{-}}} - 1 \right) - \phi \right]$$

$$V_{pmt}^{apparent}(t) = \frac{V_{pmt}^{\pi}}{\pi} \left[ \sin^{-1} \left( \frac{V_{Dig}(t)}{V_{Dig_n}^{0 \ shot}} - 1 \right) \right]$$





Good agreement! → Proceed with implementation