

Impact of of Longitudinally Tilted Beams on BPM Performance at the Advanced Photon Source

2012 Beam Instrumentation Workshop Newport News, Va. April 15-19, 2012

N. Sereno, H. Bui, G. Decker, R. Lill, X. Sun and B. Yang Advanced Photon Source Argonne National Laboratory





Outline

- Motivation: Tilted beams at the APS used to create short pulse X-rays (SPX)
- Tilted beams: Qualitative discussion
- Button signals from tilted beams
 - Delta and sum signals
 - Phase shift between buttons
- Impact on existing monopulse bpm system
- Experimental measurement of beam tilt using buttons
- Conclusion



Motivation: Short-Pulse X-ray Project at APS Using Zholents' scheme^{1,2}



Button Signal Due to Tilt: Qualitative Discussion

- Button signals to first order from offset beams
 - Large signal from beam current for a centered beam (cavity bpm signal does not have this offset)
 - Transverse beam displacement perturbs the signal with sensitivity κ = (1 5 x 10⁻⁴ $\mu m^{-1})$
 - Consider a simple tilted beam consisting of point charges



Button Signal Due to Tilt: Qualitative Discussion



 Time and frequency domain button signals for tilt = 340 mrad
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Button Signal Due to Tilt: Qualitative Discussion



Time and frequency domain button signals for tilt = 0 mrad
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Button Signal Due to Tilt

- Calculate the button signals in time and frequency domains for an arbitrary distribution
 - Construct the time domain button signals:
 - Start with expression for button signal to first order in transverse displacement
 - Integrate differential current x displacement elements along the tilted distribution
 - Convert particle position in the distribution to time by using $z=\beta ct$
 - Transform button signals to the frequency domain
 - Compute phase difference between buttons
 - Compute Delta and Sum signals
- Use these results to analyze:
 - performance of monopulse bpm system when there is beam tilt
 - Button phase measurement of a tilted beam using an Sband phase detector
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Button Signal Due to Tilt (cont.)

 $V_{T,B}(\omega) = ZQ\omega \{ iI_c(\omega)(1 \pm \kappa \,\delta \, y) \mp \kappa I_s(\omega)\theta \}$ $I_{c}(\omega) = \int_{-\infty}^{\infty} f(z) \cos(\frac{\omega z}{\beta c}) dz$ $I_{s}(\omega) = \int_{-\infty}^{\infty} zf(z) \sin\left(\frac{\omega z}{\beta c}\right) dz$ $\Delta(\omega) = \Delta_{o}(\omega) - 2ZQ\omega\kappa I_{c}(\omega)\theta$ $\Delta_{o}(\omega) \equiv 2i Z Q \omega \kappa I_{c}(\omega) \delta y$ $\Sigma(\omega) = 2iZO\omega I_{c}(\omega)$ $\frac{\Delta(\omega)}{\Sigma(\omega)} = \frac{\Delta_o(\omega)}{\Sigma(\omega)} + i\kappa \frac{I_s(\omega)}{I_s(\omega)}\theta$ $\frac{\Delta_o(\omega)}{\Sigma(\omega)} = \kappa \,\delta \, y$ $\delta \Psi \equiv \Phi_T - \Phi_B \approx 2 \kappa \frac{I_s(\omega)}{I(\omega)} \{ 1 - O(\kappa^2 \delta y^2) \}^{-1} \theta \approx 2 \kappa \beta c \omega \sigma_t^2 \theta$



Tilt Impact on Monopulse BPM System



- Converts position information in Delta signal to phase
- Compares the phase of two equal amplitude signals created from the Delta and Sum signals
- For no tilt $\theta = 0$:

$$V\left(\frac{\Delta(\omega)}{\Sigma(\omega)}\right) \approx \frac{4}{\pi} \left|\frac{\Delta_o(\omega)}{\Sigma(\omega)}\right| \cos\left(\phi_{\Delta} - \phi_{\Sigma}\right) = \frac{4}{\pi} \kappa \,\delta \,y$$
$$\phi_{\Delta} = sign\left(\delta \,y\right) \frac{\pi}{2}$$

$$\phi_{\Sigma} = \frac{\pi}{2}$$

Tilt Impact on Monopulse BPM System cont.

- XOR output
 - High state if both inputs have different states
 - Low state if both inputs have the same state
- DC component of XOR output proportional to phase
- 180 degree linear range
- Monopulse system operates near 90 degree phase point







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Tilt Impact on Monopulse BPM System cont. Im

- Phasor Diagram for delta and sum signals for no tilt ($\theta = 0$)
- Circuit measures the angle 2Ψ

 $\Delta_o(\omega)$

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$$\Psi = \tan^{-1} \frac{\Delta_o(\omega)}{\Sigma(\omega)} \approx \kappa \,\delta \, y$$

 $\Sigma(\omega) + i\Delta_o(\omega)$

 $i\Sigma(\omega) + \Delta_o(\omega)$

Ψ

 $\Delta_o(\omega)$

 $\Sigma(\omega)$

Ψ

Tilt Impact on Monopulse BPM System cont.



¹²

Tilt Impact on Monopulse BPM System cont.

$$\Psi_{1} + \Psi_{2} = \tan^{-1} \left(\frac{\Delta_{o}(\omega)}{\Sigma_{o}(\omega) + Z \,\omega \,\kappa \,I_{s}(\omega) \theta} \right) + \tan^{-1} \left(\frac{\Delta_{o}(\omega)}{\Sigma_{o}(\omega) - Z \,\omega \,\kappa \,I_{s}(\omega) \theta} \right)$$

$$\Psi_1 + \Psi_2 \approx 2 \frac{\Delta_o(\omega)}{\Sigma_o(\omega)} \left(1 + O\left(\frac{\kappa I_s(\omega)}{I_c(\omega)}\theta\right)^2 \right) = 2 \kappa \delta y \left(1 + O\left(\frac{\kappa I_s(\omega)}{I_c(\omega)}\theta\right)^2 \right)$$

- Centroid position error is second order in tilt angle
- Reduced sensitivity to tilt at the 352 MHz monopulse processing frequency due to transform ratio
- For largest SPX tilt of 340 mrad (BM source point) the beam centroid position error would be
- ~0.03 % for large aperture bpms
- ~0.75 % for small aperture bpms (P0's) (however tilt is nearly zero at the small aperture bpms





¹X. Sun, these proceedings



Button geometry used in the experiment



¹Small-gap button geometry

Tilt Measurement Using Buttons and Sband Phase Detector^{1,2}

- Experiment relies on coupling between synchrotron and betatron motion via chromaticity: $\Delta v = \xi \frac{\delta E}{E}$
 - Head of the bunch is at higher energy (tune)
 - Tail of the bunch is at lower energy (tune)
- Fast betatron frequency differs between head and tail
- After half a synchrotron period betatron phase difference between head and tail reaches maximum for maximum tilt (at least in the linear regime)
- Transient experiment: Kick the beam and observe over ~100 turns



 ¹W. Guo etal, PRST-AB, **10**, 020701 (2007)
 ²B.X. Yang etal., PAC 2005

Tilt Measurement Using Buttons and Sband Phase Detector¹



¹B.X. Yang etal., PAC 2005



Filtered and amplified S37A:P4 TI an BI button signals

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Raw phase detector phase output measured on a scope



FPGA phase detector output scaled to get tilt (final equation slide 8) and position offset (using adjacent bpms and fitting a betatron oscillation)

 $\delta \downarrow$

 \bigcirc

S37A:P4:y (mm)



 Maximum tilt and position as a function of kicker (pinger) setpoint

Table 1: APS SR machine and S37A:P4 "inner" BPM button parameters for large vacuum chamber buttons. Small gap chambers have b a factor of 5 lower.

Parameter	Value	
<i>b</i> , <i>l</i>	18.7 חוחו, 12.5 חוחו	Low chromaticity ensures linear tilt oscillations over ~100 turns
ϕ	$2 \tan^{-1} \frac{l}{25} = 0.645 \text{ rad} = 36.96^{\circ}$	
ĸ	$1.05 \times 10^{-4} \ \mu m^{-1}$	
ω	$2\pi \times 2815 \mathrm{MHz}$	
$\sigma_t = \sigma_s / \beta c$	27 ps @ 1 mA	
β	81@7GeV 🗡	
$ u_y, u_s, \xi$	0.241,0.008,4.00	
$lpha_c, \sigma_\delta$	2.82 c -4,0.00096	
$h, f_{rev}, \omega_{ m sf}$	1296, 271.555 kHz, $2\pi \times 351.9$ MHz	
(Kick angle) Θ	$\approx 0.1\mathrm{mrad}$	
$eta_{ m kicker},eta_{ m S37A:P4}$	5.4 пі, 26.7 пі	

- Performed a transient experiment where tilt was generated using a kicker to induce centroid betatron oscillations which transform in to tilt oscillations
- Tilt generated was measured using buttons and an Sband phase detector (AD8302)
- For the transient measurement, large tilt angles can be measured >~ 3-5 mrad (final calibration yet to be done using streak camera)
- Tilt measurement verified central features of tilt buildup during first ½ synchrotron period for linear theory
- For APS SPX project, will have a CW signal and ability to average up to 324 samples per turn using FPGA
- Averaging over 1000 turns could give tilt measurement resolution down to perhaps 30 μrad up to 200 Hz

Conclusion

- APS SPX project requires:
 - Evaluation of existing monopulse bpm system sensitivity in the presence of large beam tilt
 - Measurement of the beam tilt between SPX cavities
- Monopulse bpm system centroid position measurement resolution calculated to be insensitive to beam tilt
 - Centroid correction is second order in beam tilt angle
 - For largest tilt present between SPX cavities beam centroid position measurement error is 0.03 %
- Performed a transient tilt experiment by kicking a single bunch in the APS storage ring
 - Using Sband phase detector measured tilt and position for transient experiment
 - With averaging should be able to measure tilt angles down to perhaps 30 μrad up to 200 Hz
 - Phase detector can provide simultaneous tilt and position information
 - Design of a tilt measurement system based on phase
 - detector has commenced

