

High Power Allison Scanner for Electrons

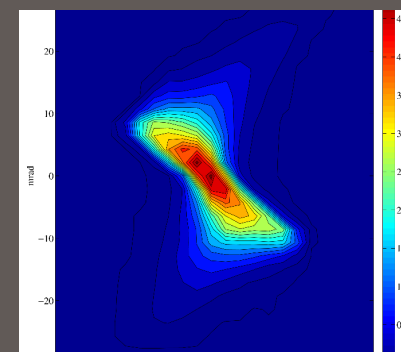
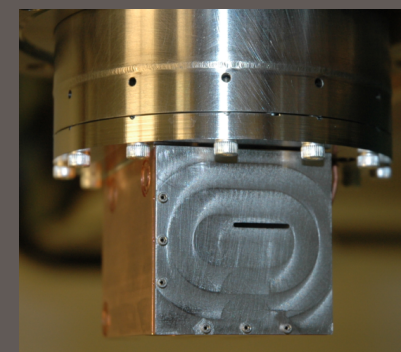
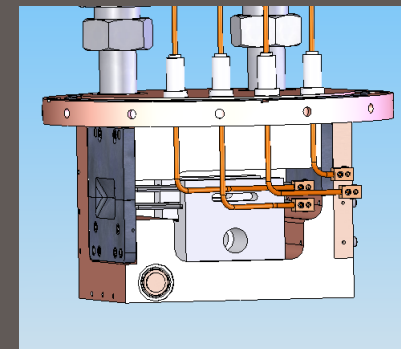
BIW12

April 17, 2012

Aurelia Laxdal TRIUMF

Accelerating Science for Canada
Un accélérateur de la démarche scientifique canadienne

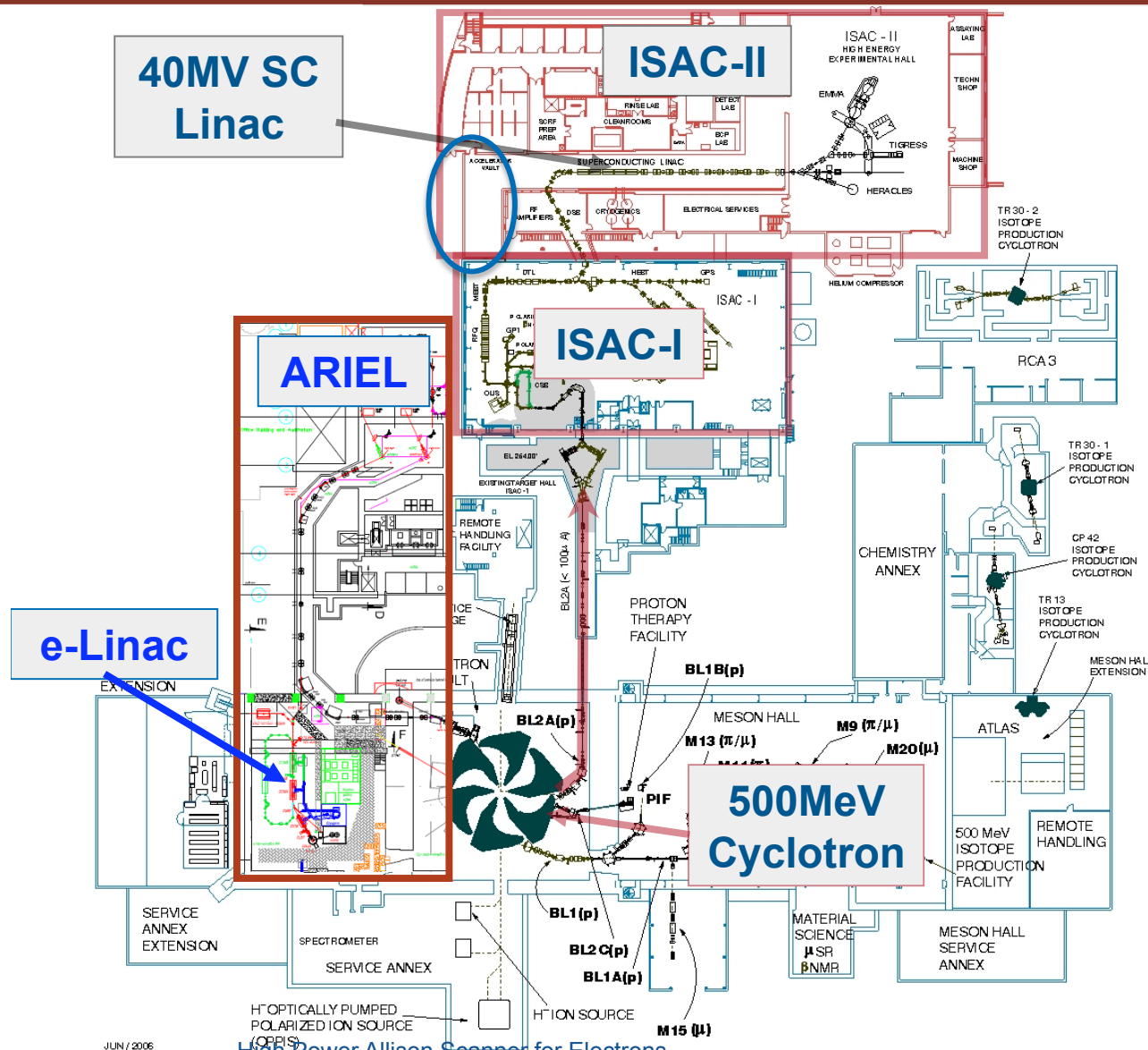
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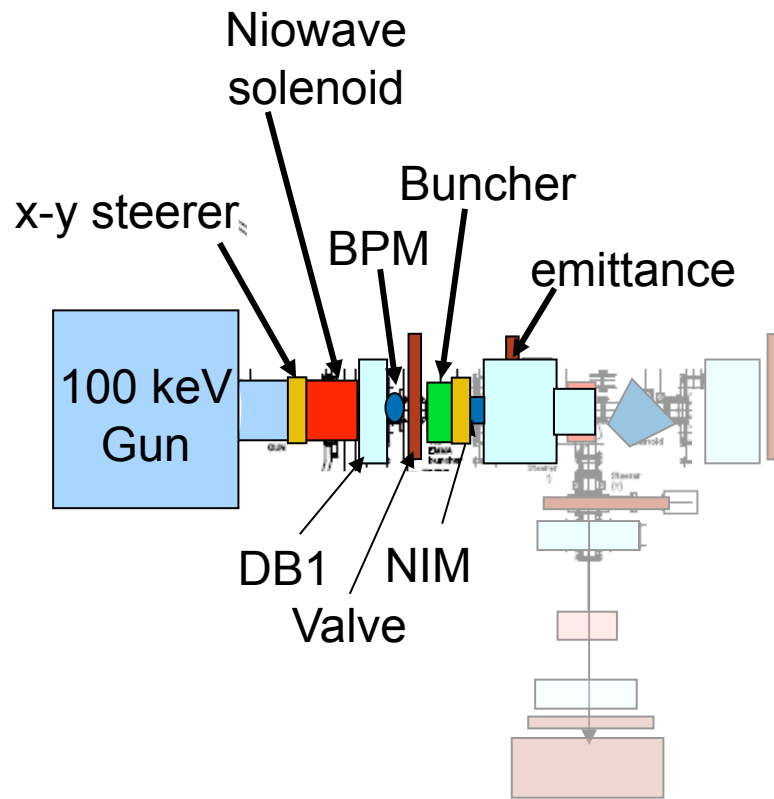
ARIEL at TRIUMF

- Now adding ARIEL to increase from one to three simultaneous beams
- Add e-Linac (50MeV 10mA cw - 1.3GHz SC linac)
- E-LINAC/VECC test area established in ISAC-II building

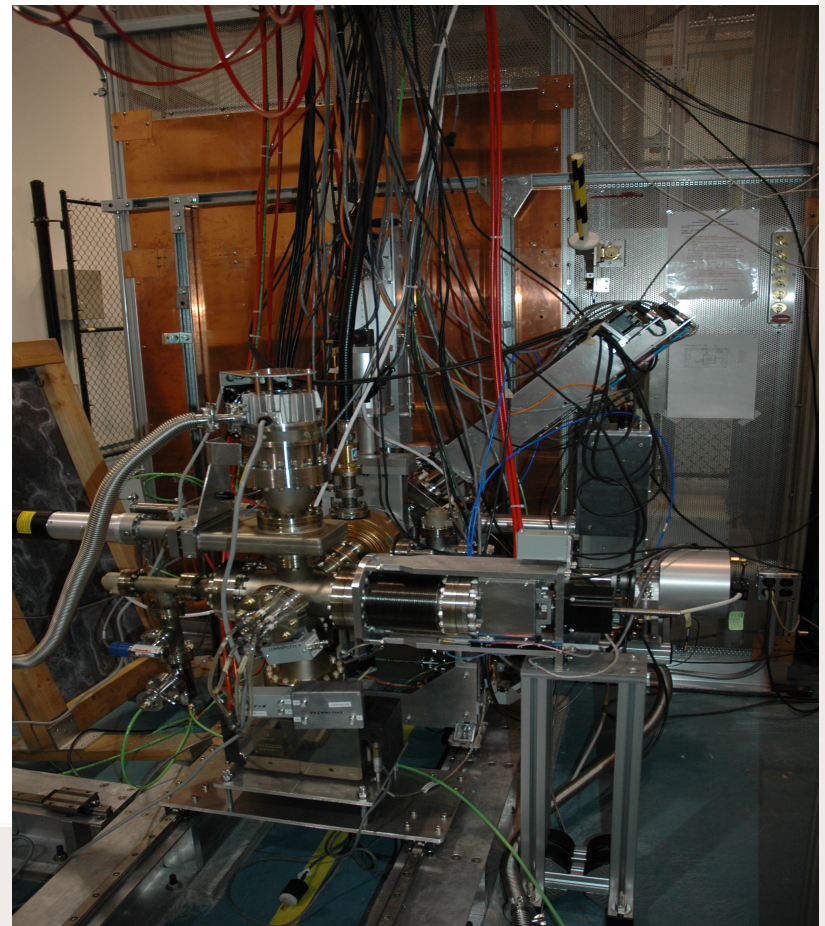


High Power Allison Scanner for Electrons

E-GUN Test Station



•100 keV e-gun test area



Overview of the 100 keV E-Gun parameters

The specifications for the 100keV electron source derived from the requirements of the e-LINAC are:

beam energy	100 keV
average current	10 mA
modulation frequency	650 MHz
bunch length	$\leq \pm 20$ deg. of 650 MHz (170 ps)
bunch charge	15.3 pC
energy spread	$\leq \pm 1$ keV
transversal emittance	≤ 30 μm normalized $2\sigma \times 2\sigma$
cylindrical beam	
UHV	10^{-9} Torr

Emittance scanner specifications

- **requirements for low energy emittance meter for the e-linac project**

beam particles	electrons
particle energy	100 – 300 keV
beam current	<10 mA
beam power	1 kW
beam size	~10 mm
vacuum	< 10^{-9} T

- **location of emittance meter**

1. directly after the electron source for initial source commissioning in E-Gun Test Station area
2. in diagnostic line of LEBT for beam characterization during operation

Overview of the Allison type emittance scanner

- At each step the beamlet selected by the front is slit swept across the rear slit with the deflecting plates and the transmitted current measured by the Faraday cup.

- The necessary voltage for an electron of energy E entering with an angle x' through the Entrance slit and exiting through the second slit is:

$$V = 4gx' E / (D - 2\delta)$$

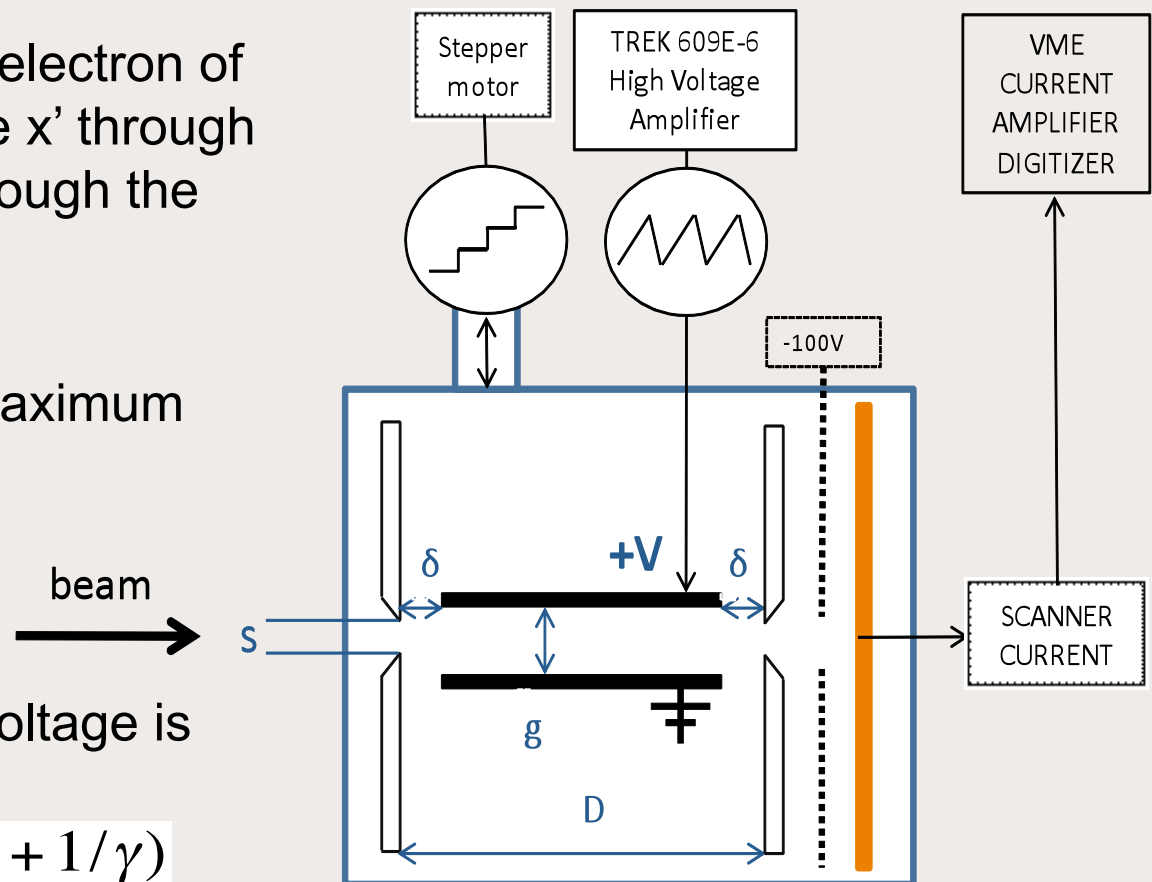
- The maximum voltage for a maximum analyzable x' angle is:

$$V_m = \pm 8Eg^2 / (D^2 - 4\delta^2)$$

$$x' = \pm 2g / (D + 2\delta)$$

- For relativistic particles the voltage is smaller by a factor k

$$V_{m-rel} = V_m / k \text{ and } k = 2 / (1 + 1/\gamma)$$



Scanner Parameters

Summary of chosen design parameters

BEAM ENERGY	60 keV	100 keV	300 keV
D (mm)	49	49	49
δ (mm)	2	2	2
g (mm)	3.5	3.5	3.5
s (mm)	0.038	0.038	0.038
K	1.06	1.09	1.23
V_{m-rel} (V)	$\pm 2,337$	$\pm 3,773.2$	$\pm 10,046$
x'_m (mrad)	± 132	± 132	± 132
Electric field (V/mm)	668	1,078	2,870

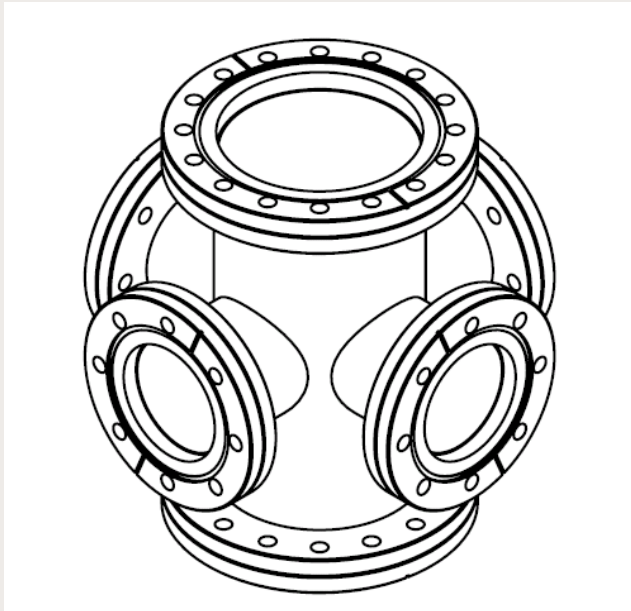
Conclusion: at these parameters the emittance scanner has **high resolution**.

Transverse phase space as large as $1600 \pi \mu\text{m}$ can be measured with a resolution of $0.03 \mu\text{m}$

MECHANICAL DESIGN

Design constraints

UHV constrains:

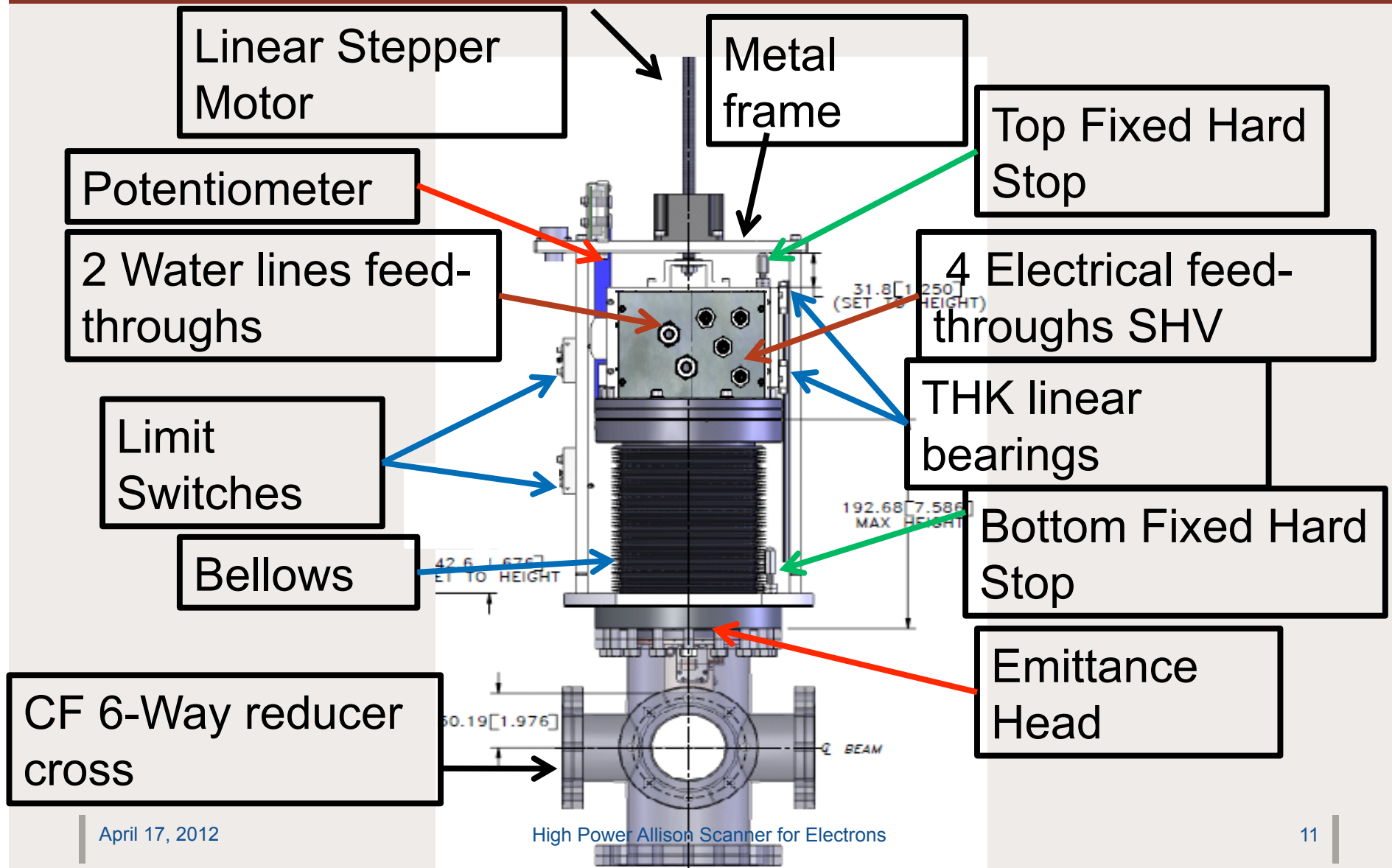


- small volumes
- UHV competitive materials

So, assembled in:

- The emittance meter is attached to a CF 6-way SS reducer cross **(2x) 6" OD (4" ID) CF x (4x) 4.5" OD (2.5" ID) CF** , clear holes rotatable.

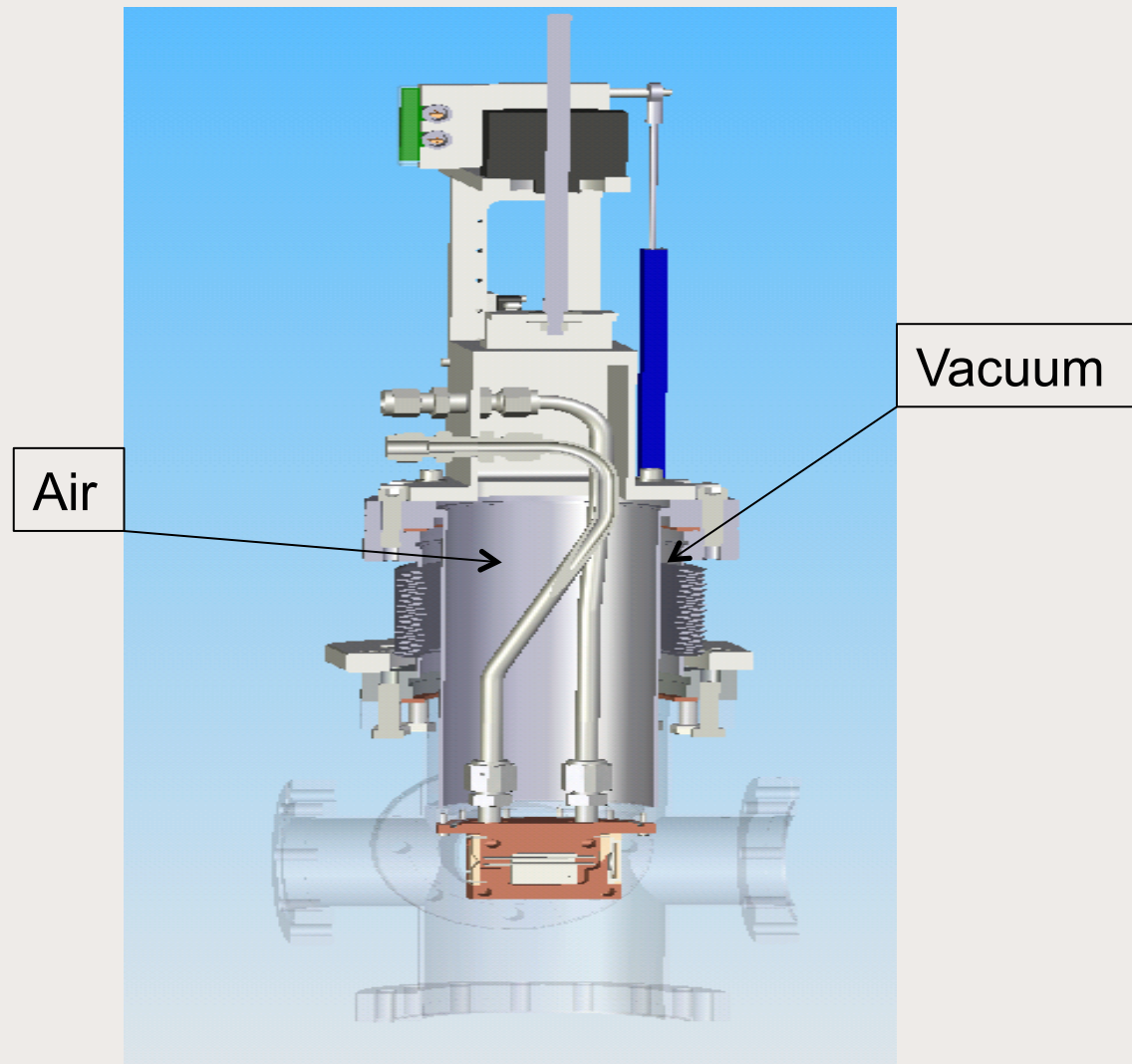
Overview of the Emittance Scanner Assembly



Design considerations (1)

In order to **preserve the UHV** and **limit the space**:

1. the **cooling lines** are placed into an inner tube, **at atmospheric pressure**.

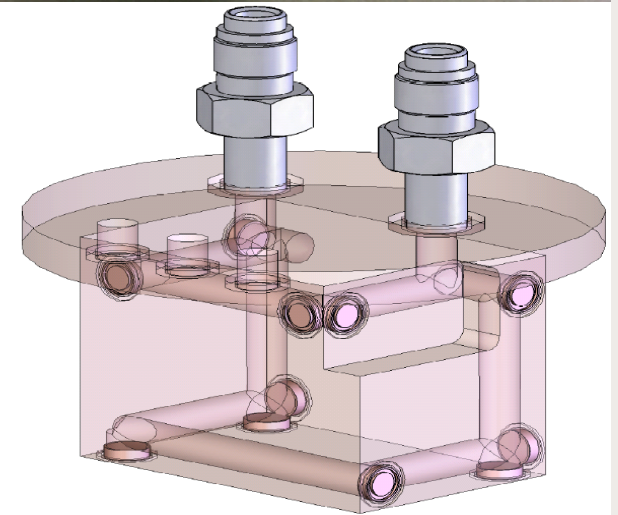
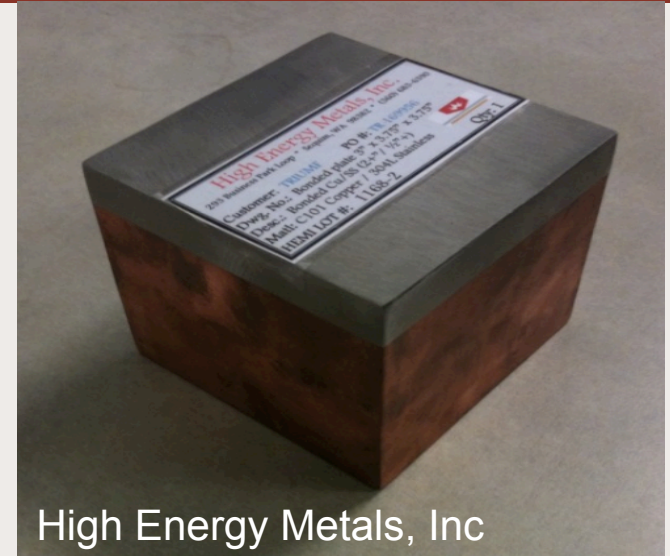


2. Flange and emittance scanner in one body AND to eliminate soldering/brazing in vacuum

Solution:

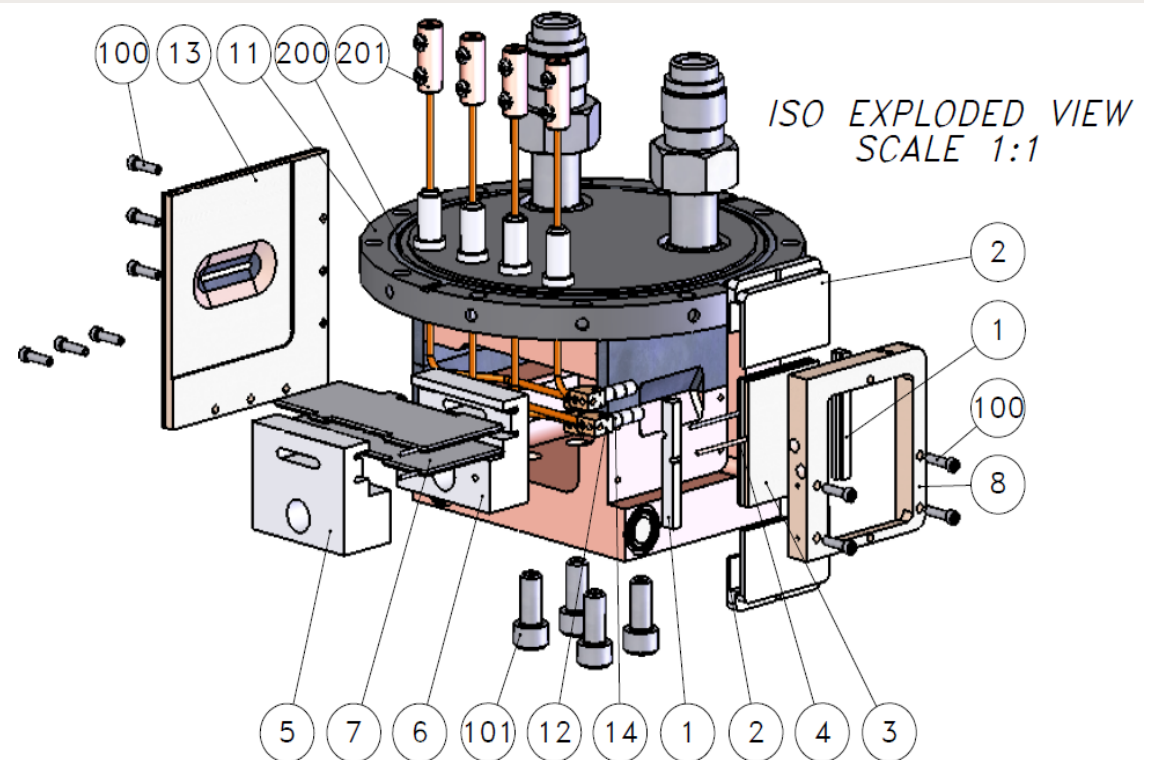
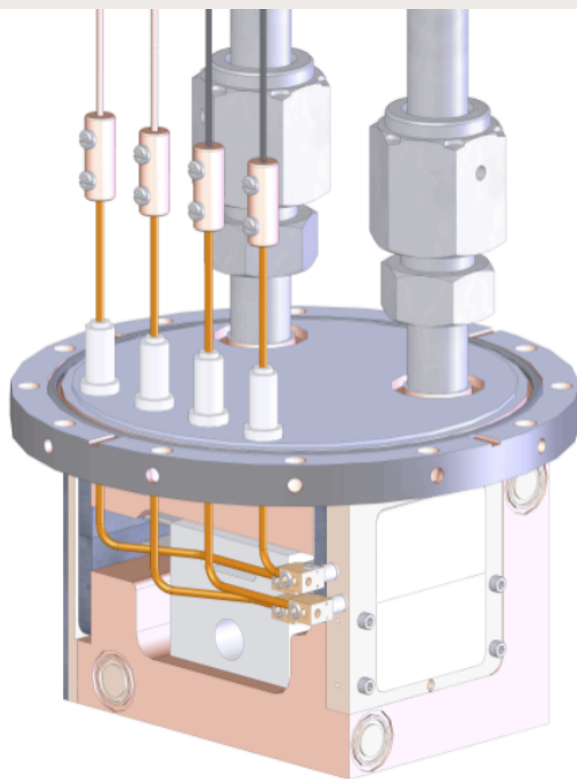
OFHC copper explosively bonded to SS to get:

- SS flange → all feedthrough can be welded (EB welding)
- emittance scanner body OFHC copper → asymmetric water cooling configuration: 2 parallel water lines, of 1/4" ID to cool the emittance head (convection) and the entrance slit (conduction).

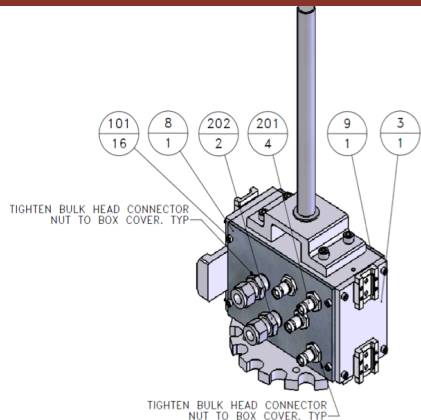


Overview of the Emittance Scanner Body design

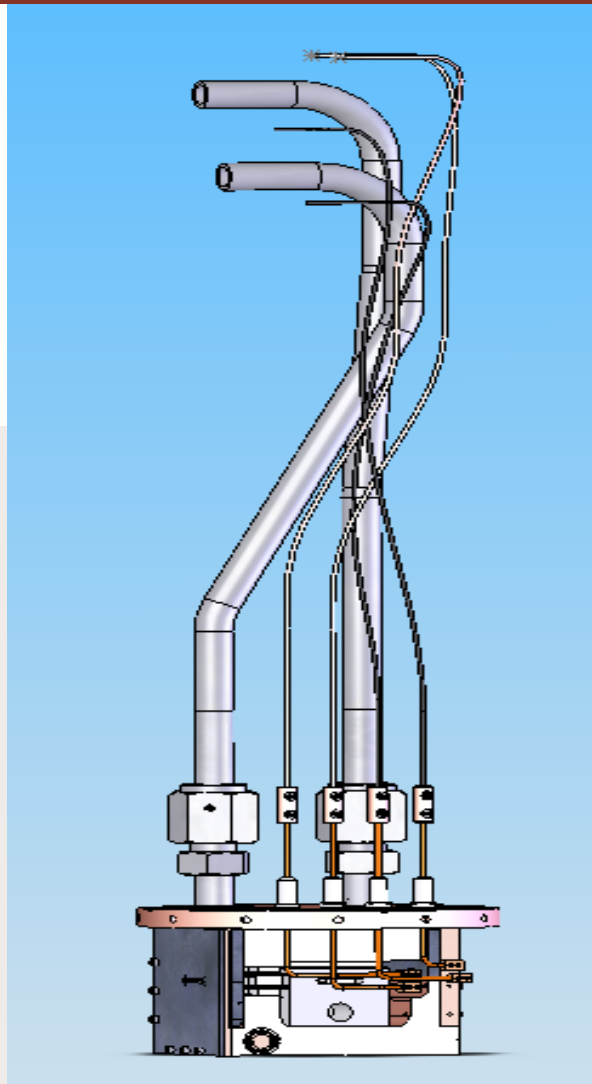
- **Dimensions:** length x width x height = 60 mm x 44 mm x 45 mm
→ Very small emittance scanner.
- Open on one side (asymmetric) → helps for vacuum pumping



Electrical Feedthroughs & Wires



- All feedthroughs are rated at 5kV and they are UHV compatible, bakeable at 250deg.
- They are EB welded on the SS flange.



There are 4 weldable single pin feedthroughs:

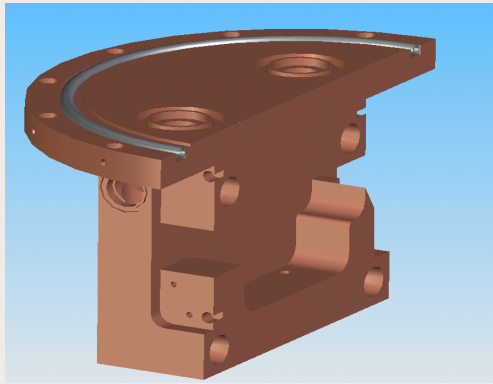
- 2 for the steering plate;
- 1 for the secondary electron suppressor;
- 1 for the Faraday cup.

The 4 wires (signal and voltage) are Kapton insulated, except for the Faraday Cup signal which is also shielded (coaxial cable).

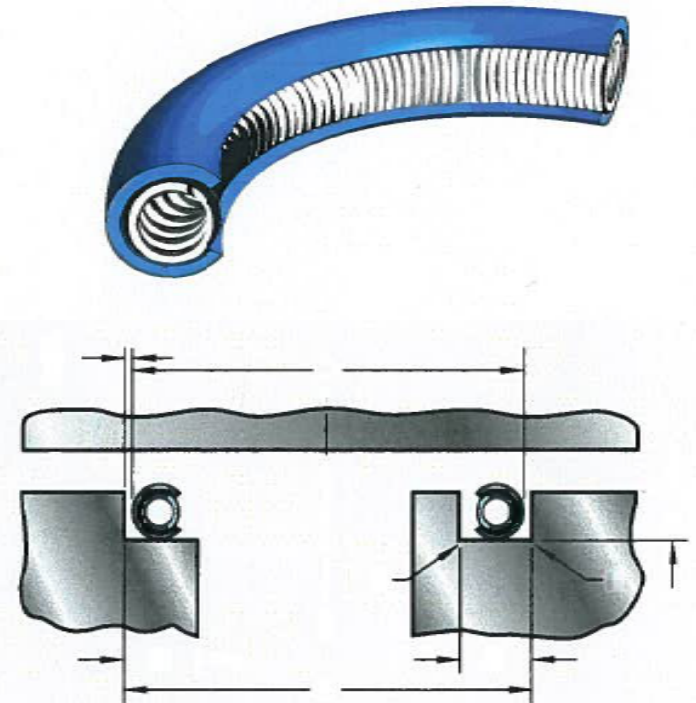
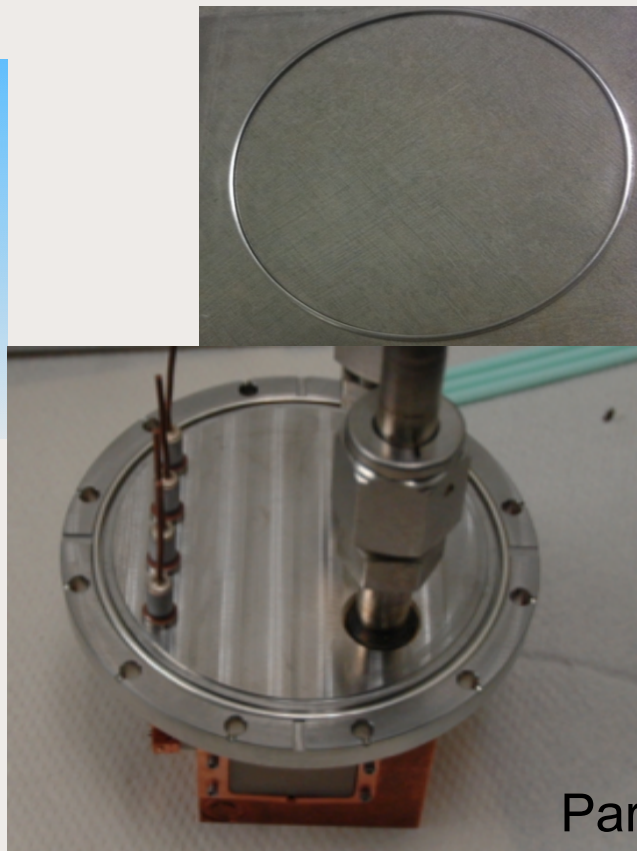
- X-Ray resistant

ESI Spring Energized Metal C-Ring

- The SS flange has an UHV compliant seal gland. The seal is a spring energized metal C-ring, made of Inconel/silver plated.
- This seal was chosen since it is UHV compatible and due to the geometry constraints.



- It takes less than 5,000 pounds clamping force.



Parker Hannifin Corporation USA

1 SS Top Steering plate

Biased plate

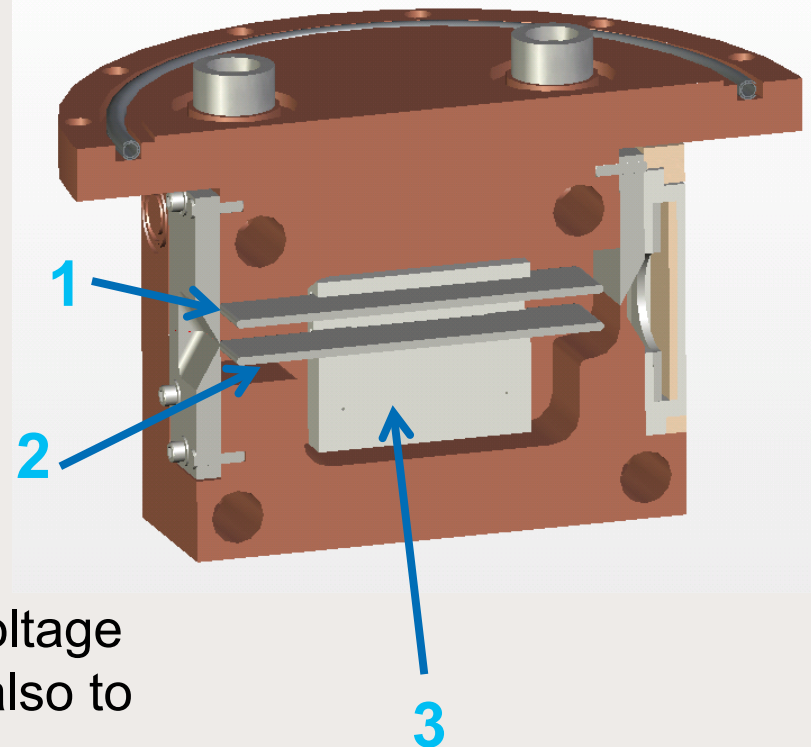
2 SS Bottom Steering Plate

This steering plate is kept grounded with the option of biasing this plate too, when used for the 300 keV e-gun, to reduce the scanning voltage.

3 Aluminum Nitride Insulators

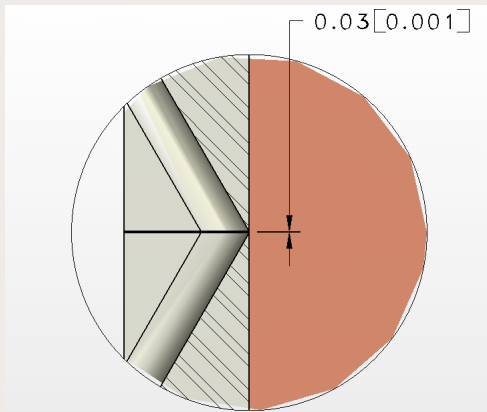
- AlN insulators are used to maintain the voltage difference across the steering plates and also to preserve the gap width between them.
- Low outgassing rate, low porosity.

Manufactured by Omley Industries Inc. - USA

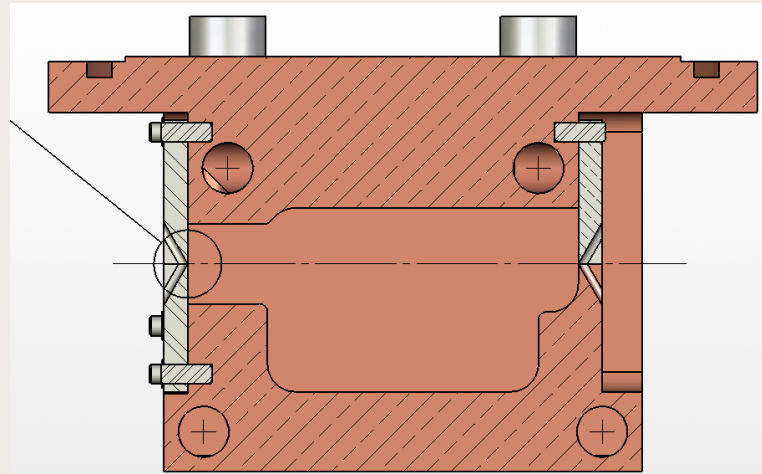


Tungsten Slits Jaws

- The entrance slit jaws are made of tungsten. This is the part of the emittance head that sees ~10% of the beam and it gets to high temperatures.



- Both slits apertures are 1.5 thou (0.038 mm)

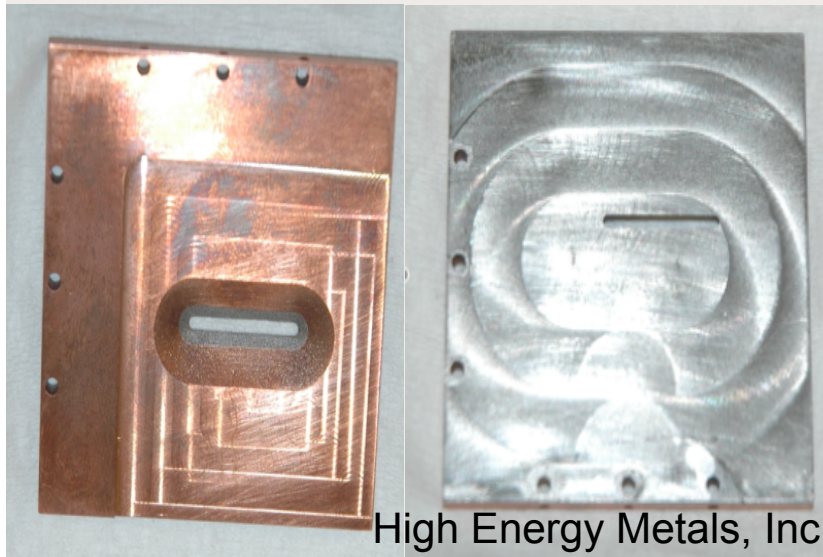
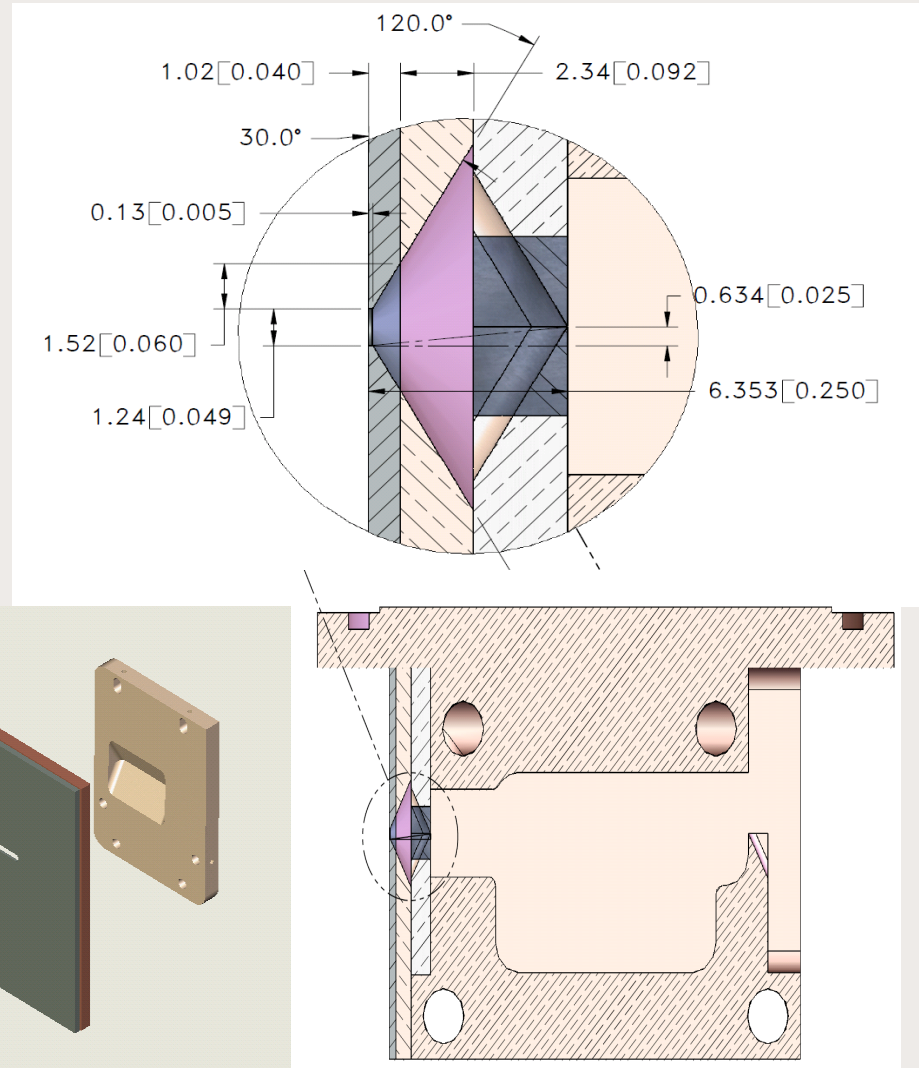


- The top slit jaws are easily removable.

The bottom slits jaws are stationary: the end one is built in, the front one is dowel pinned. To achieve alignment the bottom slit jaws were wire EDM (Innovative Tool & Die Inc. – Canada)

Tungsten-Copper Protection Plate

- For protecting the first pair of slits against the 1000 W beam power an external plate is attached in front of them. This introduces more flexibility in the design. The protective plate is made of tungsten explosively bonded to a OFHC plate for thermal conduction purposes.



Thermal considerations and ANSYS simulations

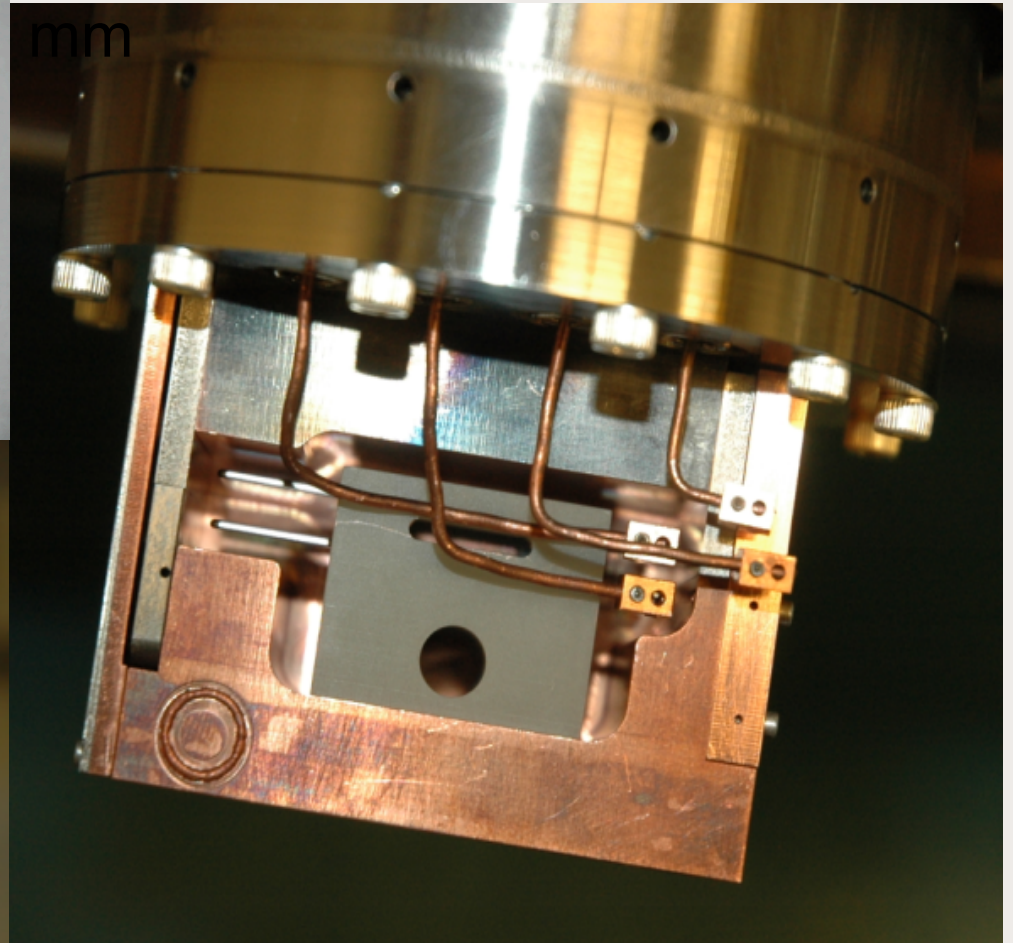
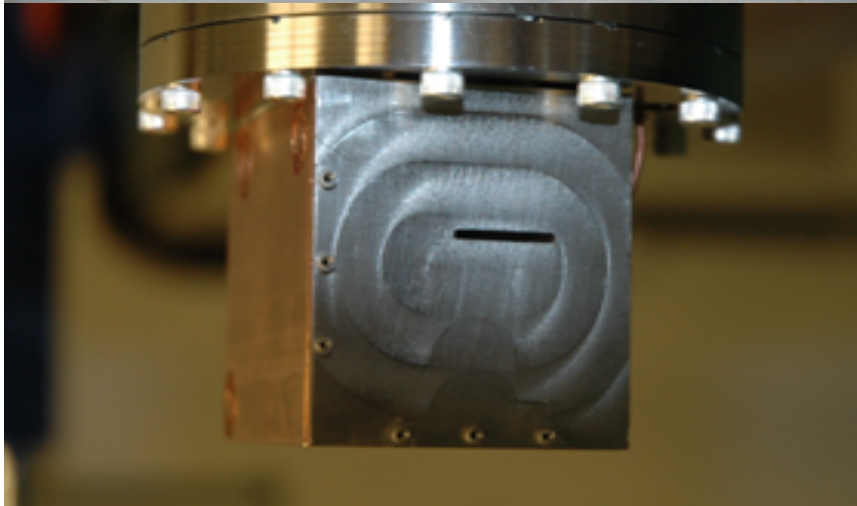
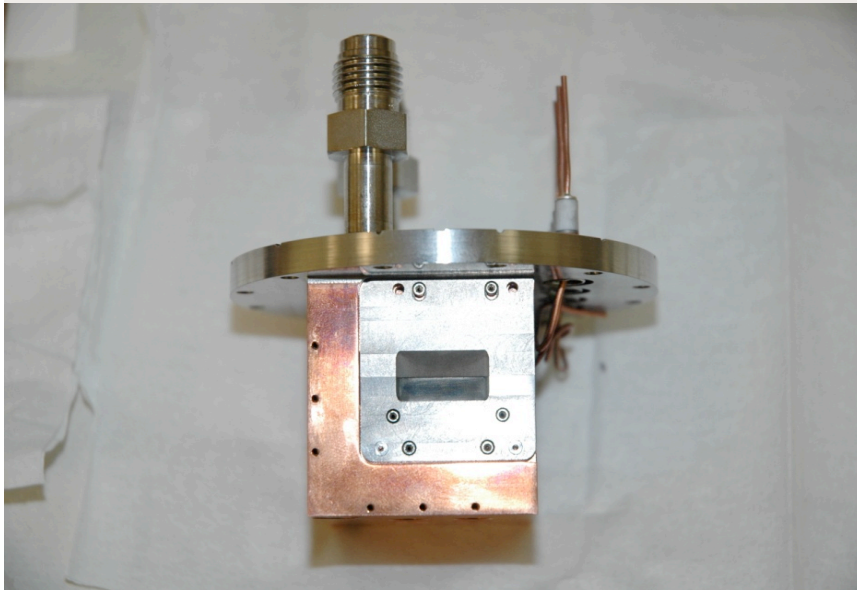
- Thermal calculations were done for the water-copper thermal convection; calculated heat transfer coefficient.
- Results were used to do thermal simplified 3D models at different homogenous beam intensities and sizes, with ANSYS, of the thermal conduction.
- The main constrain is introduced by the **power density** on the front slit: densities in excess of 115 W/mm^2 will close the slit (of 1.5 thou) through **thermal expansion**.

Beam energy [keV]	60	100
Beam diameter [mm]	2	10
Beam intensity [mA]	6	10
Power density [W/mm]	115	10
Slit Temp [deg C]	1650	300
Front plate Temp [deg C]	445	560
Thermal expansion [μm]	33	$\ll 10$

Assembly

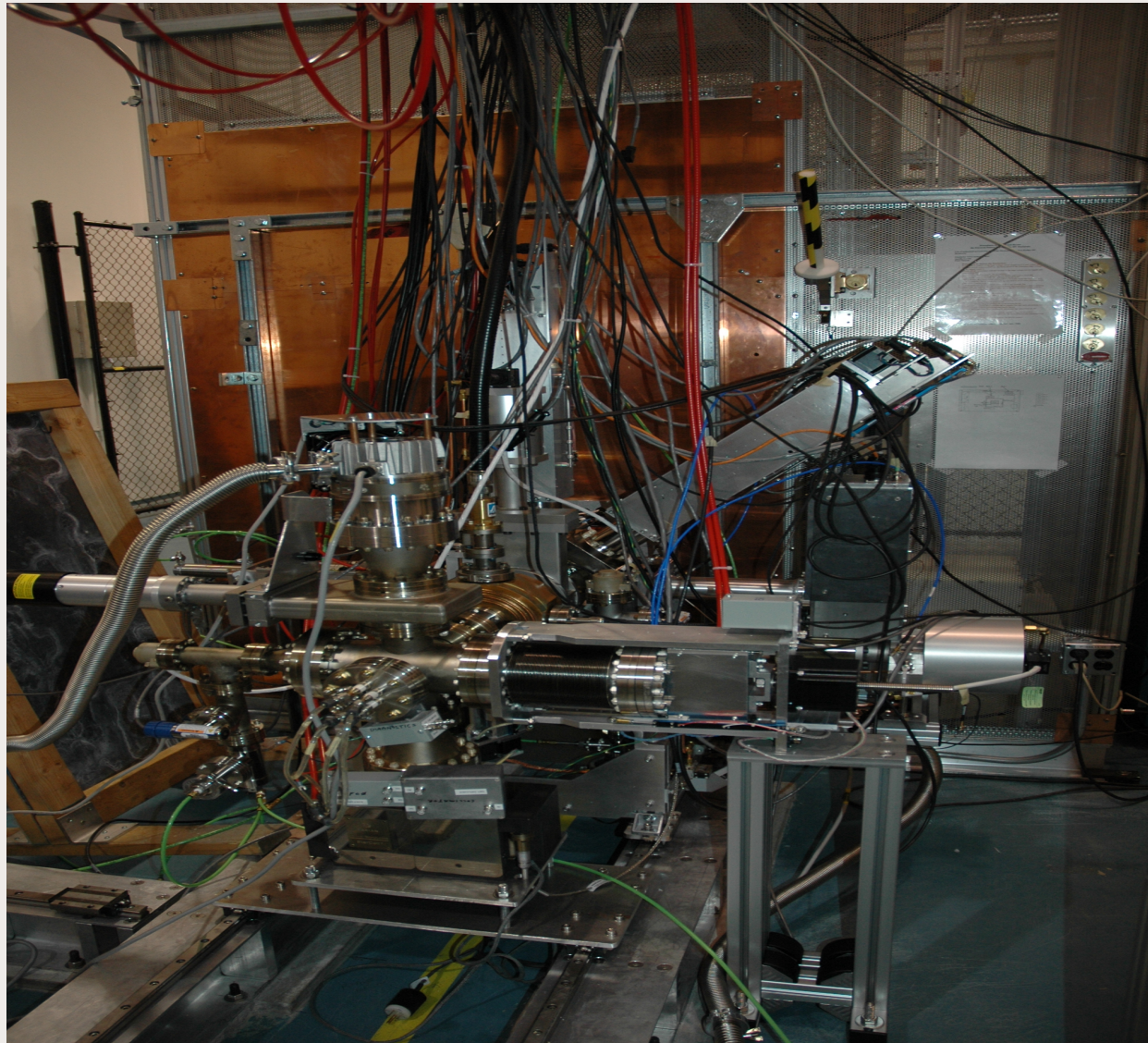
Dimensions:

$l \times w \times h = 60 \text{ mm} \times 44 \text{ mm} \times 45 \text{ mm}$



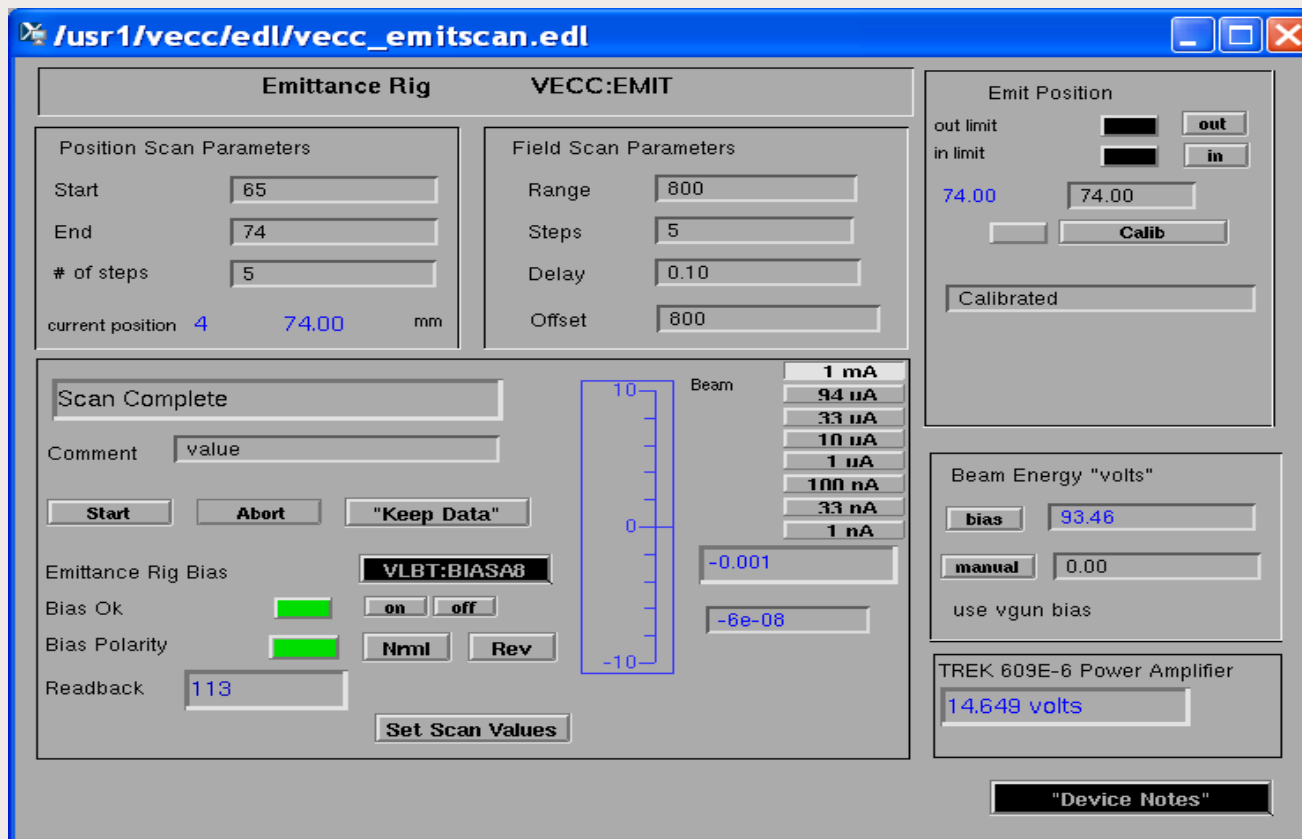
Installation & baking

- Used the cooling lines to flush hot air at 200 deg C to bake the emittance scanner head.



Controls (1)

- Scans are initiated from an EPICS GUI which communicates with the VME EPICS IOC running under Linux.

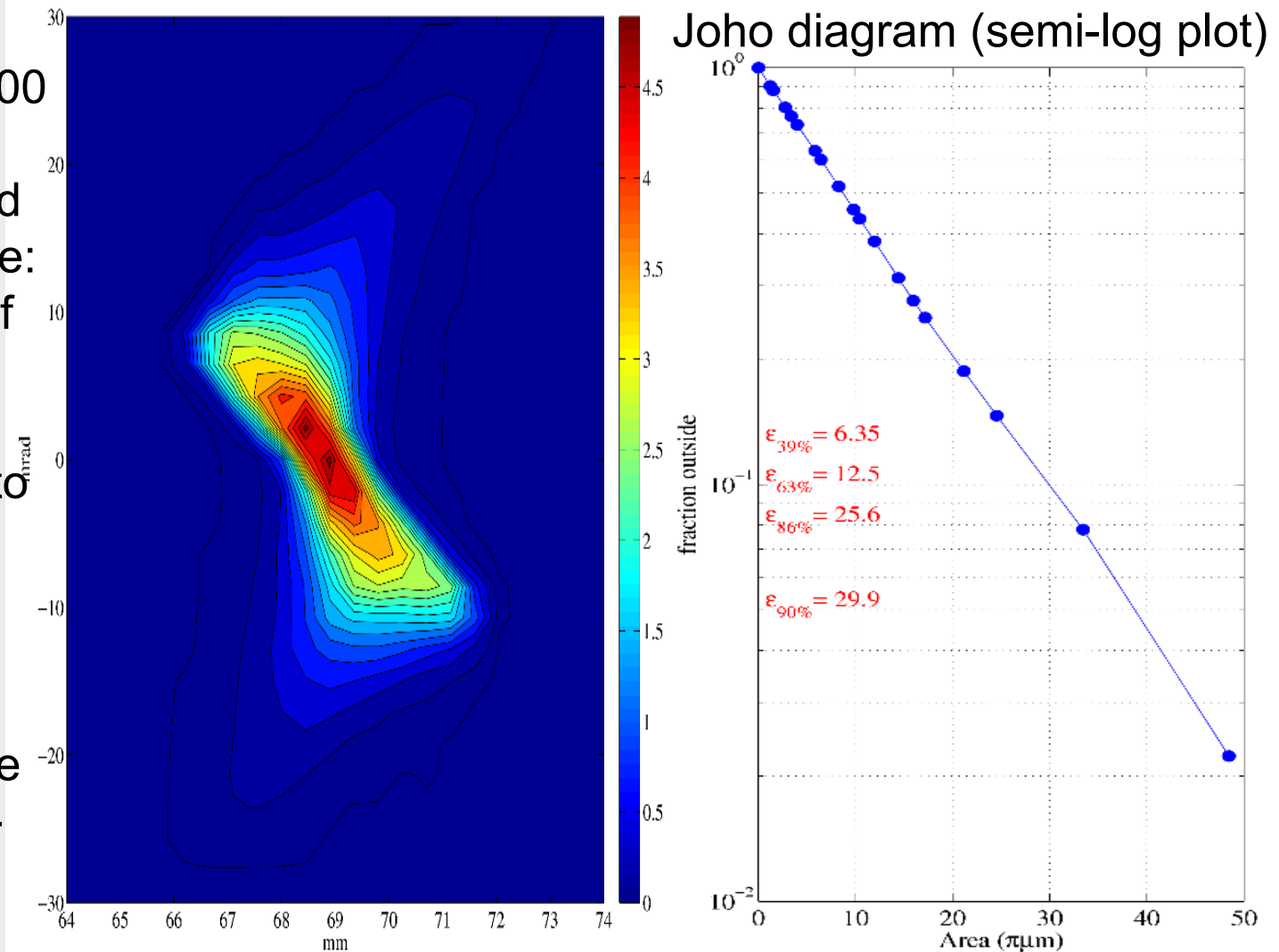


Controls (2)

- Types of VME modules:
 - stepping motor controller for positioning the slit;
 - DAC for controlling the voltage ramp;
 - variable gain current amplifier/digitizer for the current measurement.
 - The present readback device has a 10 Hz update rate;
 - Emittance scanner has a variable delay with a minimum value of 100 ms;
 - Coarse scan of 21 positions x 21 angles takes 58 seconds;
 - Medium scan of 41 positions x 41 angles takes 190 seconds;
 - Detailed scan of 81 positions x 81 angles takes 700 seconds.
-
- Data file is processed and contour-plotted using a MATLAB script.

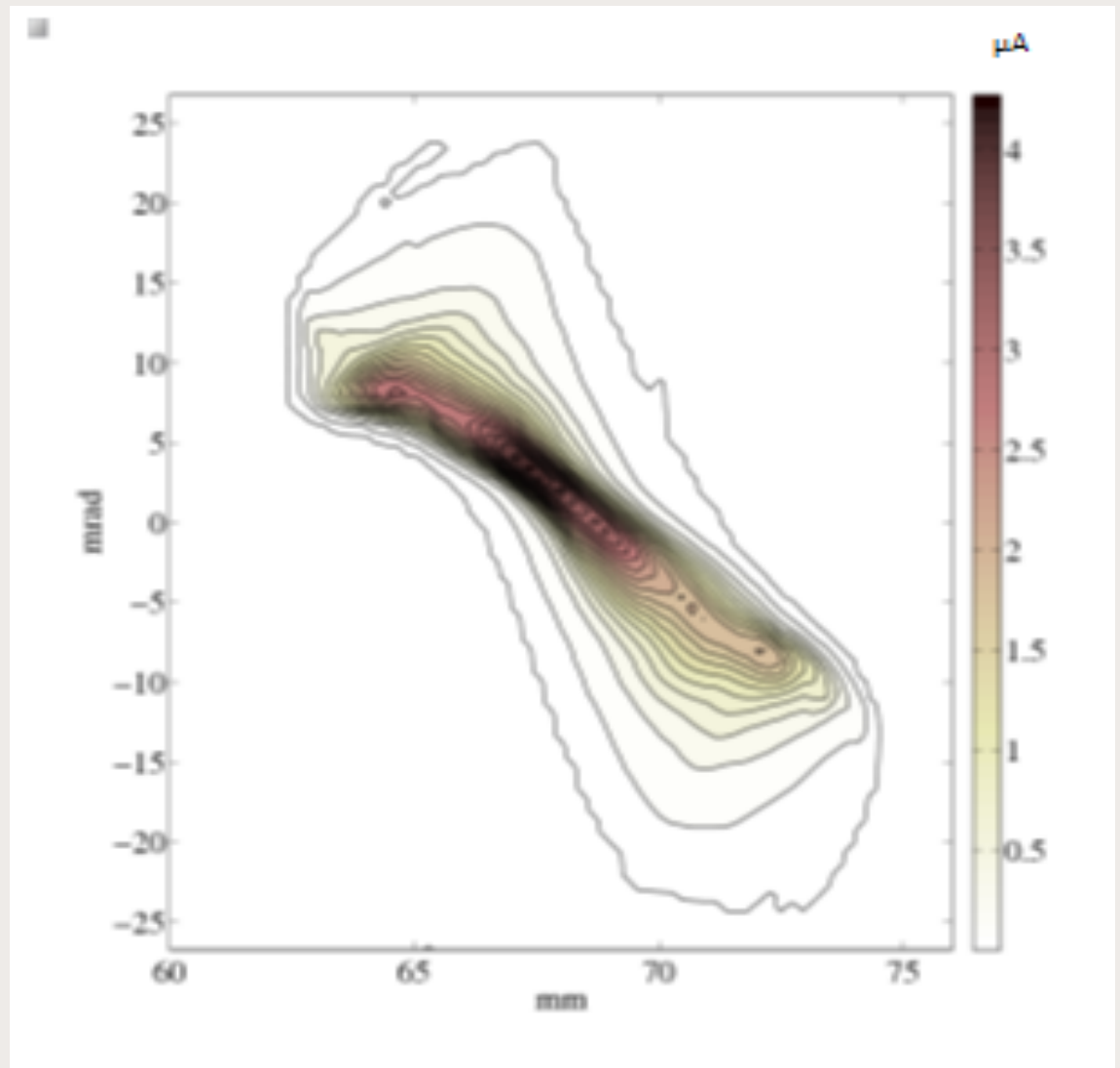
Emittance scan: 60keV 10mA 1% D.F.

- 41 x 41 readings
- Average current 100 μA
- In a 0.03 mm-mrad pixel of phase space: 50 nA at the peak of the figure;
- Noise: 10-20 pA
- This allows details to the 98% contour;
- $\epsilon_{\text{rms}} = 9.2 \mu\text{m}$
- Distortion may be due to space charge combined with non-optimal Pierce geometry angle.



Emittance scan: 60keV 11mA 99% D.F. (1)

- 81 x 81 readings
- The *rms* beam is 2.69 mm with 30 W/mm²
- Average current 100 μ A
- In a 0.03 mm-mrad pixel of phase space:
4 μ A at the peak of the figure;
- Noise: 1nA. This allows details to the 98% contour;
- $\epsilon_{\text{rms}} = 10.1 \mu\text{m}$
- $\epsilon_{39\%} = 7.1 \mu\text{m}$
- Distortion (“bow-tie”) may be due to space charge, non-optimal Pierce geometry angle and conduction angle.



Emittance scans: 60keV 11mA at WAIST

1% D.F.

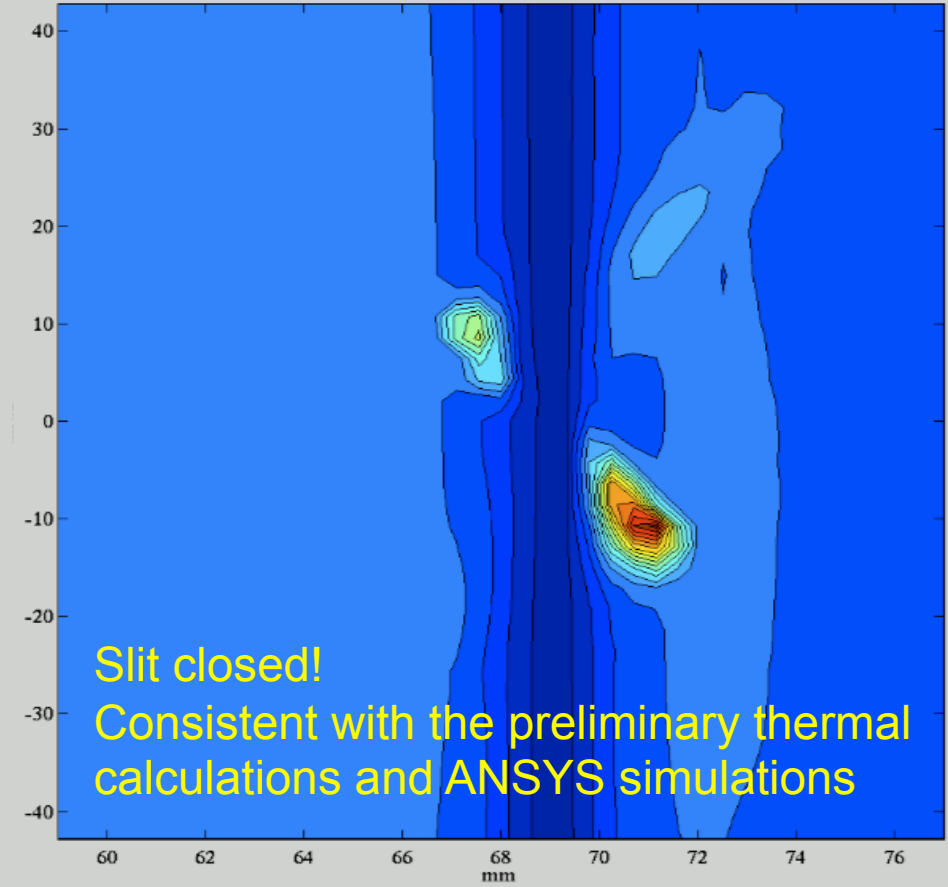
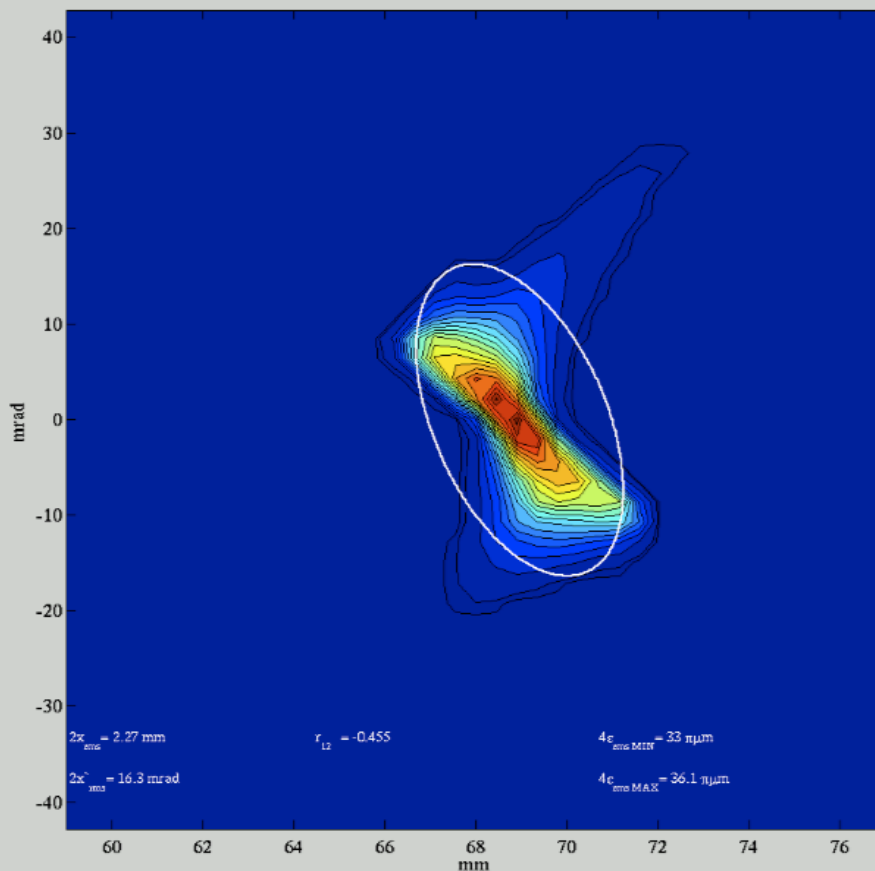
rms beam size 1.14 mm

Power Density 1.6 W/mm²

99% D.F.

1.14 mm

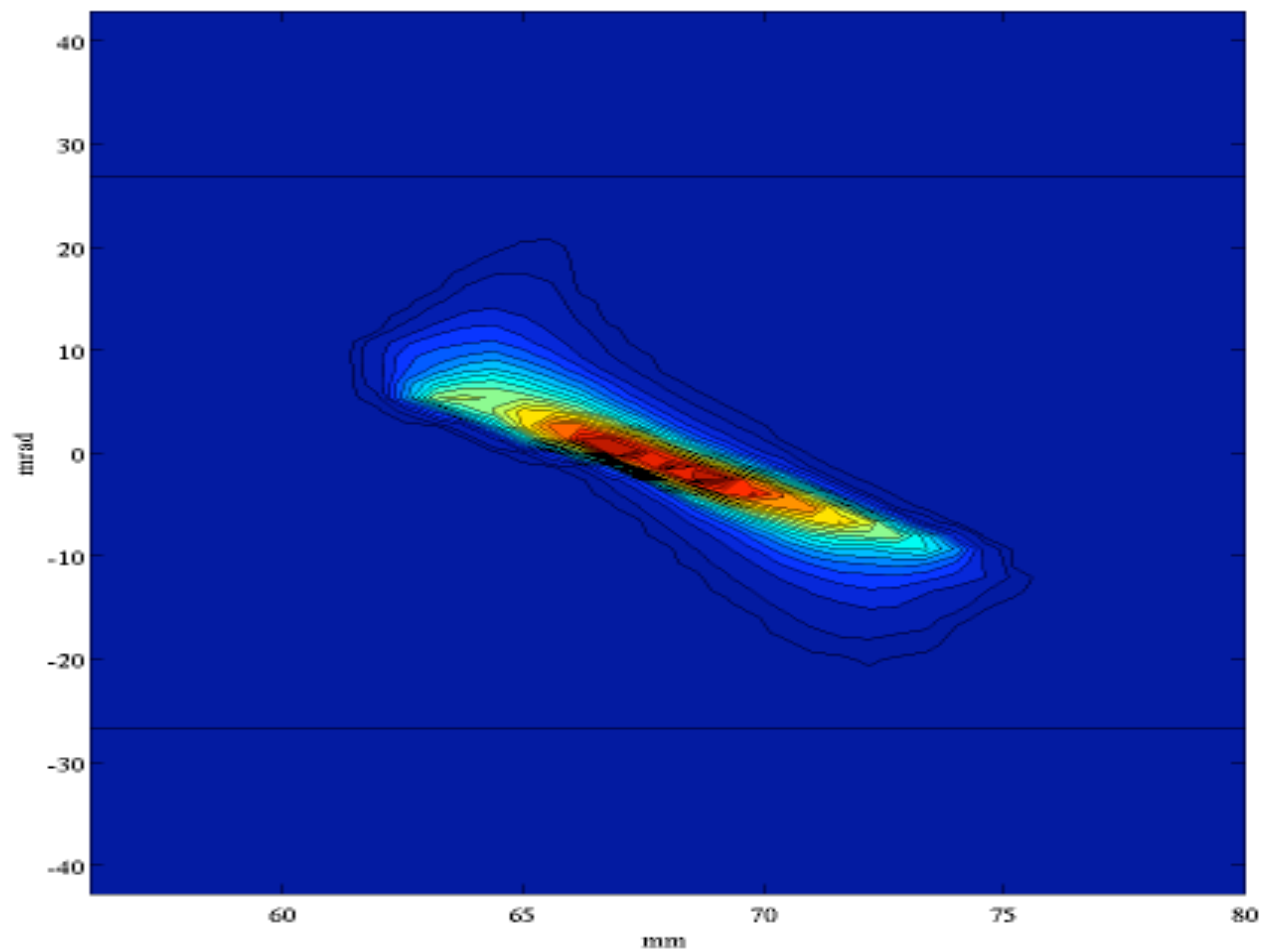
160 W/mm² → 2,300 deg C (ANSYS)



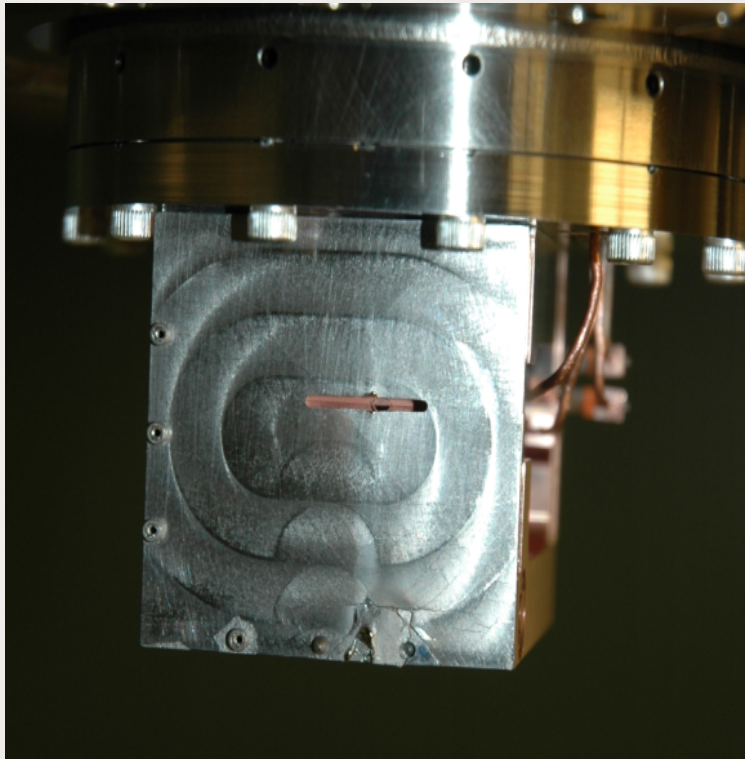
Emittance scans at different D.F.

- Took scans at different D.F. 10%, 30%, 50%, 70% and 99% for the same source parameters:
 - same RF amplitude,
 - cathode bias and
 - solenoid currents
- the emittance values were consistent;

Solenoid scans



Inspection - Front plate

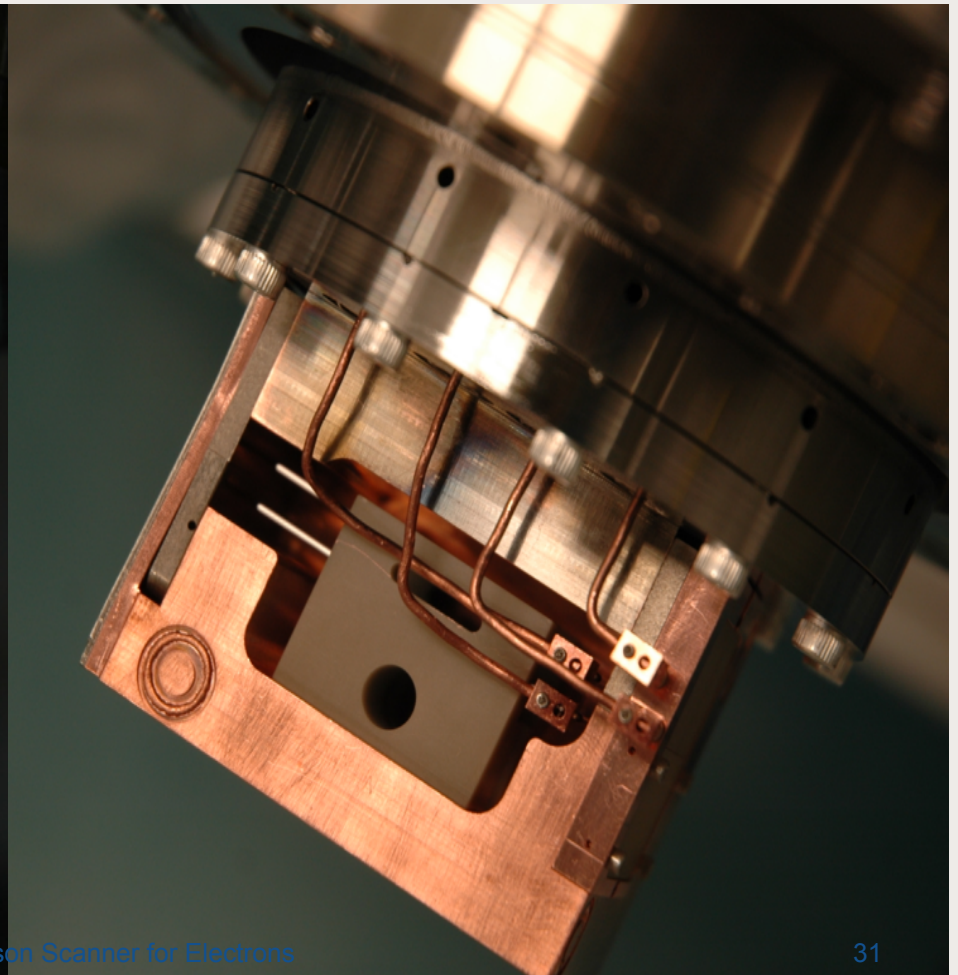
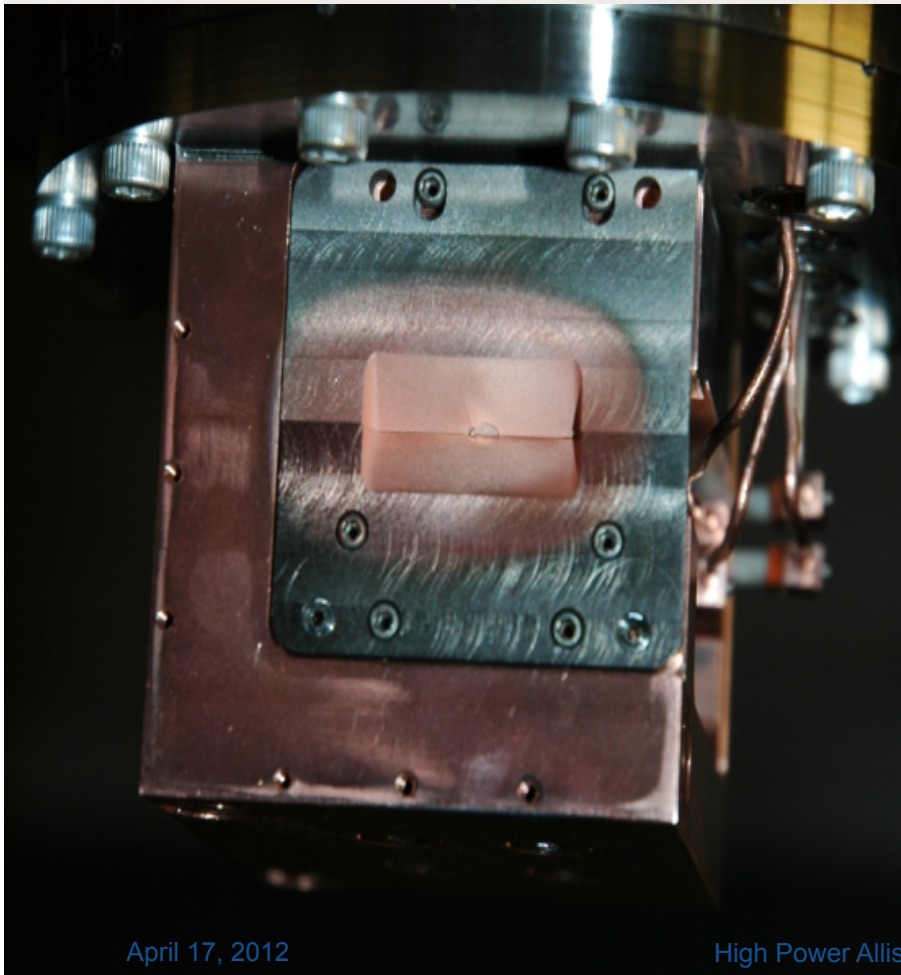


Copper vaporization from the back of the protection plate, that plated the entrance tungsten slit.



Inspection – Front slit & Emittance scanner body

- Tungsten entrance slit plated with copper.
- The emittance scanner body was not damaged.



Front slit inspection - Microscope

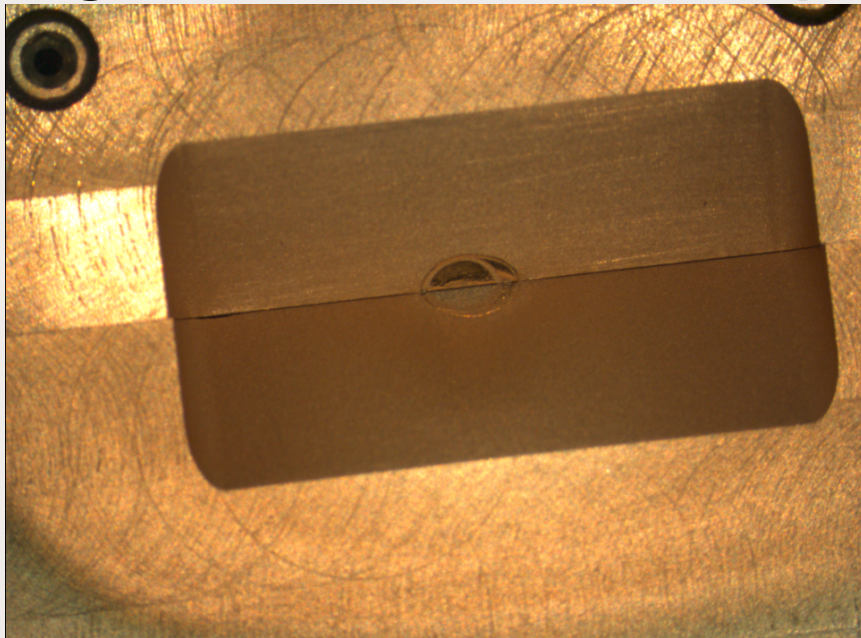
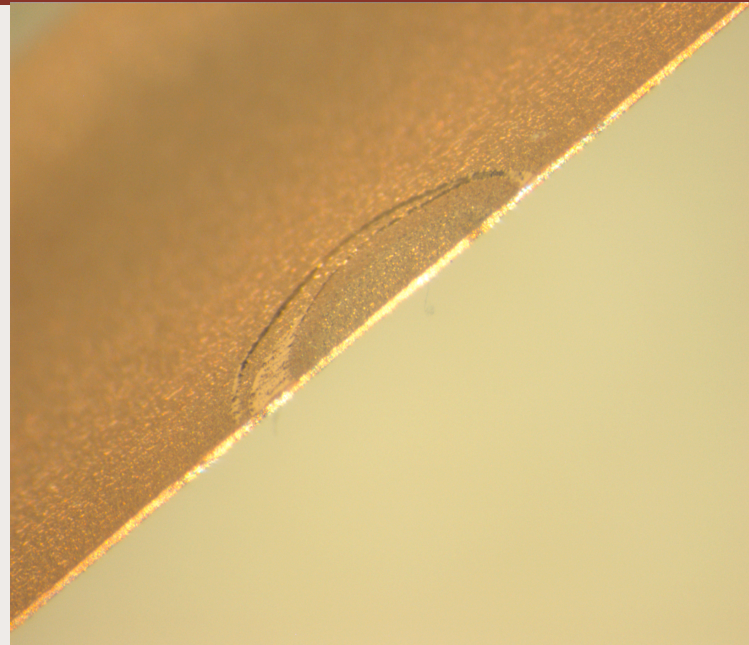
Height = 1.14 mm

Big Diameter = 2.69 mm

Small Diameter = 2.15 mm

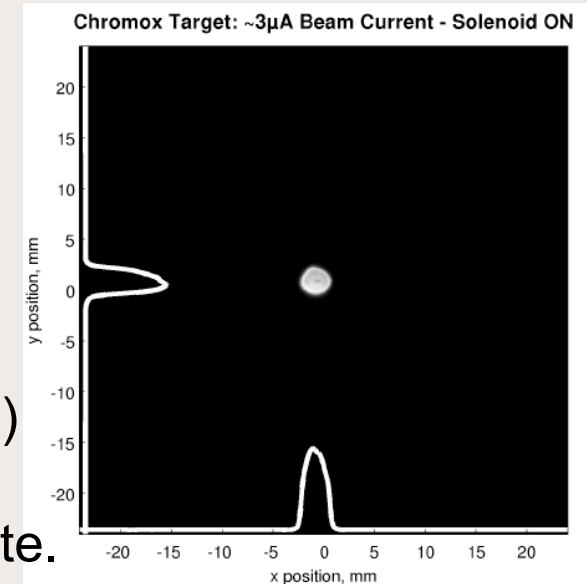
Slit gap in the center = 1.5 thou
(preserved)

Magnification: 1mm -> 365 pixels



Conclusions

1. The Allison type emittance scanner for electrons:
 - can measure a **large transverse phase space** ($1600 \pi \mu\text{m}$) at a **high resolution** of $0.03 \mu\text{m}$, in **high vacuum** 10^{-9} Torr.
 - can take **high power beams**: so far measurements were done for 660W.
2. The emittance measurements are consistent with independent measurements using a scintillator-type profile monitor, and a simple analytical model for a thermionic gun.
3. It is used for **understanding the source parameters**, at high and low D.F., and **optimizing the source**:
 - Thermal effects in the source (RF heating up);
 - Conduction angle;
 - Pierce geometry angle;
 - Space charge neutralization (changes with D.F.)
5. It can be used for the 300 keV e-gun also.
6. It can be further improved: redesigning the front plate.



Acknowledgments

TRIUMF participants:

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W. Rawnsley, P. Vincent, G. Waters, D. Yosifov

Machine shops & companies in USA and Canada:

High Energy Metals, Inc. - USA

Omley Industries, Inc. – USA

Parker Hannifin Corporation - USA

Innovative Tool & Die, Inc. – Canada

TRIUMF Machine Shop

Thank you!

Merci!

Questions?

TRIUMF: Alberta | British Columbia |
Calgary | Carleton | Guelph | Manitoba |
McMaster | Montréal | Northern British
Columbia | Queen's Regina | Saint Mary's |
Simon Fraser | Toronto Victoria | Winnipeg
| York

