

Magnet Development for the LHC Accelerator Research Program (LARP)

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BNL - FNAL - LBNL - SLAC

Magnet Development for LARP



<u>Goal</u>: Demonstrate Nb_3Sn technology for the LHC Luminosity Upgrade Three main components (models series) based on shell-type coils:

- TQ (Technology Quads, 2005-07) $D = 90 \text{ mm}, L = 1 \text{ m}, G_{nom} > 200 \text{ T/m}$
- LQ (Long Quadrupoles, 2008-09) $D = 90 \text{ mm}, L = 4 \text{ m}, G_{nom} > 200 \text{ T/m}$
- HQ (High Gradient Quad, 2009-10) D = 90 mm, L = 1 m, G_{nom} > 250 T/m

In addition, three magnet series based on <u>racetrack coils</u> are used to investigate and resolve fundamental design and technology issues

Oct 25, 2005	Туре	Length	Gradient	Aperture	FY05	FY06	FY07	FY08	FY09
		[m]	[T/m]	[mm]					
MODEL MAGNETS									
Technology Quad (TQ)	cos(2θ)	1	> 200	90		3N+1R	2N+1R		
Long Quad (LQ)	cos(2θ)	4	> 200	90				1N	1N
High Gradient Quad (HQ)	cos(2θ)	1	> 250	90					2N
SUPPORTING R&D			Peak Field [⊺]					
Sub-scale Quad (SQ)	block	0.3	10-11	110	1N+1R	1N+1R	1N+1R	1N	
Short Racetrack (SR)	block	0.3	10-12	N/A		1N	1N	1N	
Long Racetrack (LR)	block	4	10-12	N/A			2N+1R		

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Quadrupole Designs for the LHC IR





<u>Objectives</u>:

- Optimize/characterize cable design and heat treatment cycle
- Evaluate conductor/cable performance and stability
- Develop and optimize coil fabrication/handling procedures
- Optimize and finalize the coil design for LQ
- Develop/calibrate FEA models (material properties, friction coefficients)
- Compare mechanical design concepts and support structures
- Compare test data with expected (design) values
- Provide experimental feedback for LQ and HQ structure selection

Implementation: two series of models with same coil design:

- TQS models: aluminum shell over iron yoke; axial pre-load
- TQC models: collar & stainless steel shell; axial support

Main parameters:

• 1 m length, 90 mm aperture, 11-13 T coil peak field



TQ Coil Design and Fabrication

Design features:

- Double-layer, shell-type
- One wedge/octant (inner layer)
- TQ01: OST-MJR strand, 0.7 mm
- TQ02: OST-RRP strand, 0.7 mm
- 27-strand, 10.05 mm width
- Insulation: S-2 glass sleeve

Winding & curing (FNAL - all coils)









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Reaction & potting (LBNL - all coils)







TQ Coil Fabrication Experience

- <u>23 TQ coils have been fabricated</u> (including 5 practice coils & 2 spare coils)
- Producing high quality coils in a reliable and consistent manner, however:
 - Some systematic asymmetries related to "2-in-1" reaction/potting
 - Some *de-bonding* in TQC instrumentation traces (minor effect in TQS)
- All coils are being wound/cured at FNAL and reacted/impregnated at LBNL
 - Decided based on existing infrastructure and to minimize tooling investment
 - Instrumental in developing and maintaining common procedures
 - Shipping of coils accomplished without damage or significant delays

Inner trace after TQC01 test



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Reaction/potting tooling

Coil measurements (TQC02)

Titanium poles (TQS02)



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TQ Performance References & Range

	Magnet	T _{op} [K]	G _{ss} [T/m]	B _{ss} ^(body) [T]	l _{ss} [kA]
$J_{c} = 2 \text{ kA/mm}^{2}$ $(12 T, 4.2 K)$ MJR strand First models	TOO	4.2	222	11.4	12.5
		1.9	239	12.3	13.6
	TOC	4.2	215	11.2	13.0
		1.9	233	12.1	14.1
	Magnet	T _{op} [K]	G _{ss} [T/m]	$B_{ss}^{(body)}$ [T]	l _{ss} [kA]
$J_{c} = 3 \text{ kA/mm}^{2}$ $(12 T, 4.2 K)$ RRP strand Final models	TQS	4.2	245	12.6	13.9
		1.9	264	13.5	15.1
	TOO	4.2	239	12.4	14.4
		1.9	255	13.2	15.5

- I_c data from <u>extracted strands determine common performance reference</u> for TQS/TQC
- Issue: relatively wide range of extracted strand I_c (TQ01: 1862-1984 A/mm² @12T, 4.2K)
- <u>Reference magnet performance limits</u> for a given test run are adjusted for measured T_{bath}
- Actual *conductor-limited quench levels* may be lower due to other degradation effects

TQS and TQC Design Concepts





TQS

- Aluminum shell over iron yoke
- Assembly with bladders and keys
- Aluminum rods for axial pre-load

TQC

- Stainless steel collars and skin
- Control spacers to limit pre-load
- End support plates, no pre-load

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Coil Stress Comparison (2D FEA)



- Main differences: warm pre-load, cool-down effect, stress uniformity (pole to mid-plane)
- Peak stresses are high & no consensus on degradation limits \rightarrow cable testing required
- Peak stress ~20 MPa difference: stress-relief slot, different G_{ss} & pole stress range at G_{ss}
- Detailed FEA shows that <u>3D effects have a significant impact</u> on actual coil stresses

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- Interfaces for integrated use of CAD, mechanical and electro-magnetic packages
- Studies of the effects of friction among interfaces (coil-pole, coil-pads, yoke-shell)
- Design goal: *maintain contact between coil and structure at all steps and locations*



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• Cable and Coil fabrication:

- 23 coils completed, 4 more spares in production
- Long TQ cable lengths (well above LQ unit length) routinely fabricated

• Model magnet assembly and test:

- TQS01 model assembled (all new coils) and tested (4.5K, LBNL)
- TQS01b assembled (1 new coil, same pre-load) and tested (4.5K, LBNL)
- TQS01c assembled (1 new coil, lower pre-load) and tested (1.9K, FNAL)
- TQS02 model assembled (all new coils) and tested (1.9K, FNAL)
- TQC01 model assembled (all new coils) and tested (1.9K, FNAL)
- TQ01 Evaluation Review (TQS01, TQS01b, TQC01) in November 2006
- In progress:
 - TQS02 analysis, TQC01b test preparations
 - Fabrication of spare coils for TQC02 and TQS02b

TQS Measured and Calculated Stresses

• Low coil stress at assembly (5-30 MPa)

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-20

-40

-60

-80

-120

-140

-160

-180

-200

(sland σ_{θ} (MPa)

- Fine tuning with bladders & key shims
- Large pre-load gain during cool-down
- 3D FEA is critical for cool-down phase
- Interfaces (friction) play significant role
- Transverse and axial effects are coupled
- Measure both transverse & axial strain
- Variations among quadrants need study





Average (4Q) σ_{θ} in support shell (TQS01, TQS01b, TQS01c)





- TQS01 achieved 87% of extracted-strand short sample limit (no stress)
- TQS01b, TQS01c: fully trained to an ~80% conductor-limited plateau
- <u>Plateau quenches occur near gaps</u> between pole parts; no end quenches



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Coil Stress near Pole Gaps in TQS

- 3D ANSYS calculations and TQS01b measurements indicate high longitudinal tension in coil across gaps, possibly leading to conductor degradation
- This effect depends on the interfaces between coil, pole (bronze or titanium) and *outer support elements*





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TQS01/b - Axial strain pole turn, µ=0.6 all, Bronze Island



TQS02 Fabrication and Test

New design features:

- First TQ test using the LARP baseline conductor (OST RRP 54/61)
- Ti poles: eliminate longitudinal stress near gaps, reduce required axial preload, improve end parts fit after reaction, reduce/eliminate gaps between pole pieces

Test results:

- Performs well above 200 T/m (4.5K & 1.9K) using RRP 54/61 conductor
- Confirms the analysis of the cause of the TQS01 limitation and its cure



TQS02a Quench History

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TQC01 Test Results

- At 1.9K, TQC01 achieved 85% of extractedstrand short sample limit (no stress)
- Highest gradient achieved was 200 T/m
- Limited to 70% of short sample at 4.2K (by different mechanism before/after 1.9K cycle)
- Most quenches before #42 occurred in the pole turn of the inner layer (all coils)
- Straight section quenches occurred in areas where the outer pole pieces were not glued
- Quenches after #42 occurred in the outer layers of coil 9 and 13:
 - Coil 13: mid-plane turn, lead side
 - Coil 9: multi-turn (up to mid-plane)
- Evidence of conductor degradation in midplane area
- Reliable results from bullet and skin gauges
- Mixed results from gauges on control spacers and on coils



Analysis of TQC01 Test Results (1/2)

Slow training/plateau observed up to quench #42 can be attributed to:

1. Low azimuthal pre-load in the straight section with respect to design targets

- Overestimation of assembly pre-load (high coil modulus applied to gauge readings)
- Longitudinal stress-relief cut was filled with epoxy, while the design assumed G10
- Implementation steps tended toward the low end of the acceptable preload window (due to fears of over-compression causing cable degradation)
- During cool-down there was some additional decrease of the pre-load

TQC01 stress analysis	Baseline			As-built			
	300K	1.9K	14kA	300K	1.9K	12kA	
Pressure at inner pole (MPa)	-100	-95	±9	-47	-53	15	
Max azimuthal stress (MPa)	162	144	146	83	67	93	

- 2. Outer pole pieces in most of the straight section not bonded to the coil
 - Due to initial plan to remove outer pole and replace with "tabbed" collar
 - Results in motion of the pole block & increase of bending due to low pre-load
- 3. Low collar-to-yoke preload ratio causing further bending in the collared area

Analysis of TQC01 Test Results (2/2)

<u>Mid-plane degradation observed after quench #42 can be attributed to:</u>

1. Axial coil motion during excitation (in turn due to low azimuthal pre-load)



- 2. Bending due to the application of local pressure at the mid-planes
 - Rigid metal parts dominate the cross-section near the coil ends
 - Ends used stainless steel yoke packs resulting in higher stresses after cool-down
 - Combined effects may have resulted in excessive coil pressure at mid-plane





New Mechanical Features in TQC02

- Warm azimuthal preload is increased to <u>150 MPa</u>, based on non-linear coil MOE
- Collared preload is increased to a peak stress of **<u>120 MPa</u>**
- Added strain gauges on the bronze poles; will be monitored during assembly
- Preload at the collared coil level is measured based on collar deflection measurements and bronze pole gauges readings, in conjunction with FEA
- Preload in the final assembly is based on readings from the skin gauges, control spacer gauges and bronze pole gauges, in conjunction with FEA
- Azimuthal gauges are placed on the coil at both the pole and mid-plane and read during all phases of assembly and testing, but are not used as the "primary" method of determining preload.
- Contact area of yoke upon collars is increased with respect to TQC01, allowing radial support over a greater azimuthal area. This should also result in a rounder final coil shape.
- The pole slot is filled with G-10 (nominal design material) instead of epoxy
- Yoke laminations will be made of iron over the entire magnet length



TQC Status and Plans

- TQC02 has been collared: results from strain gauges as well as collar deflection measurements were consistent with analysis
- However, after collaring one mid-plane shim was found to have been out of place, causing probable permanent damage to 2 coils



- Two additional coils are being fabricated to replace the damaged ones
- A new TQC test (TQC01b) was introduced using coils from TQC01 &TQS01 <u>Primary goal</u>: verify shim system and analysis with respect to preload for TQC during assembly, cool-down and excitation
- TQC01b has been fabricated and test preparations are underway
- The completion and test of TQC02 will follow shortly after TQC01b



TQ Magnetic Measurements

- Field quality measurements of TQC01 and TQS01 show encouraging results
- Normal dodecapole is large but "as built" calculated values are close to measured
- Design/fabrication/assembly need improvements to reduce non-allowed harmonics
- Alignment features and single-coil reaction/potting will be implemented in LQ
- Need AP guidance on requirements for magnetization and eddy current harmonics
- Conductor and cable choices are limited: discuss/understand options and priorities

R = 22mm	Norm	al (b _n)	Skew (a _n)		
n	TQC	TQS	TQC	TQS	
3	2.01	-1.46	-1.72	4.41	
4	-1.90	-0.52	0.62	-1.99	
5	0.58	3.06	-1.33	0.71	
6	1.71	5.40	-0.10	-0.37	
7	0.07	0.07	0.10	-0.11	
8	0.01	-0.11	-0.03	-0.18	
9	0.04	0.02	0.08	-0.02	
10	-0.06	0.02	0.00	0.00	

Harmonics at 45 T/m (average up-down ramp)



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Sub-scale Coils and Structures





Low field Low stress

SQ High stored energy High Axial forces

NMR 4-coil layout High field

SD High field High stress

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Sub-scale Quadrupole Series (SQ)

Design:

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- 4 racetrack coils in square configuration
- Coil aperture 130 mm (clear bore 110 mm)
- Similar load line as TQ (11.3 T @460 A)
- Similar coil stress as TQ (100-130 MPa)
- Similar axial force as TQ (350 kN @ Iss)

Results:

- 2 magnets, 2 tests each (LBNL/FNAL)
- Cable and MJR conductor evaluation
- Verification of heat treatment for TQ
- Verification of conductor stability
- Evaluation of stress degradation
- Analysis of quench initiation and training
- Study of the effect of axial load
- Improved assembly procedure

Next step (SQ03):

• RRP conductor evaluation, continued studies



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Long Racetrack Magnet Design

First step for scale-up, based on LBNL SC/SM coil & structure

- simple coil design \rightarrow focus on length dependent issues
- well understood SC (SM) baseline: 20+ coils tested
- common coil dipole lower forces, energy, pre-stress
- coil disassembly/reassembly in different configurations
- demonstration of bladder & key technology scale-up





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Instrumented dummy coil (6 strain gauge stations along magnet length)



Assembled shell-yoke structure with dummy coil



- LBNL: structure design, procurement & qualification; magnet design & analysis
- BNL : fabrication of short and long coils, magnet assembly, cool-down and test

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Technical approach and open issues:

- Baseline strand selected and qualified; developing improved options and qualification plans for possible use in later phases
- Present cable and insulation are working well; further developments desired to facilitate magnet production, improve radiation hardness
- Key elements of coil technology scale-up: (1) reaction/potting tooling & fabrication/handling processes; (2) pole/end parts design/materials
- LQ coil fabrication processes will be derived from TQ, LR, and core programs experience
- Alignment becomes more critical and is also needed for field quality: new features implemented in coil fabrication and magnet assembly
- Support structure performance is a key element for success: selection through LQ Design Study

High Gradient Quadrupoles (HQ)





PERFORMANCE PARAMETERS							
Parameter	Symbol	Unit	HQ1	HQ2			
Short sample gradient*	G _{ss}	T/m	308	317			
Short sample current*	I_{ss}	kA	10.7	12.6			
Coil peak field	$B_{pk}(I_{ss})$	Т	15.6	15.8			
Copper current density	$J_{cu}(I_{ss})$	kA/mm ²	2.2/2.2	2.1/2.6			
Inductance	$L(I_{ss})$	mH/m	24.5	18.0			
Stored energy	U (I _{ss})	MJ/m	1.3	1.4			
Lorentz force/octant (r)	$F_r(I_{ss})$	MN/m	1.7	1.7			
Lorentz force/octant (θ)	$F_{\theta}\left(I_{ss}\right)$	MN/m	-6.0	-6.1			
Average coil stress (θ)	$\sigma_{\theta}\left(I_{ss}\right)$	MPa	150	152			
Dodecapole (22.5 mm)	b_6		-0.2	0.0			
10-pole (22.5 mm)	b ₁₀		-0.05	-0.92			

Goals:

- Expand toward higher field/stress
- Feedback to IR optimization

The reference cross-sections were selected taking into account stress considerations:





LORENTZ STRESS AT 300 TESLA/METER (MPA)								
Coil	ANSYS (Fig 3) Mid-plane stress: ΣF_{θ} /(layer width)							
Design	L1&2	L3&4	L1	L2	L3	L4		
HQ1	176	167	139	98	179	150		
HQ2	178	131	148	143	159	114		

(*) Assuming $J_c(12 \text{ T}, 4.2 \text{ K}) = 3.0 \text{ kA/mm}^2$; operating temperature $T_{op}=1.9\text{ K}$

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<u>*Phase I*</u> (TQ and racetrack coil development)

- TQ01 prototypes fabricated and tested: achieved 200 T/m gradient
- TQ02 models test RRP conductor and optimized designs
- TQS02 performed well above 200 T/m at both 4.5 K and 1.9 K
- TQC02 was delayed due to coils damage during magnet assembly
- TQC02 and TQS02b will be tested in the coming months
- SQ models have provided and will provide key information
- Long shell-based structure fabricated and qualified for use in LR
- LR01 magnet assembly completed; test is starting

Phase II (LQ and HQ models):

- LQ coil design based on TQ; tooling/procedures under development
- LQ structure design and selection process is underway
- Good progress on HQ design, implementation depends on priorities