

## TRANSVERSE BEAM BREAK-UP STUDY OF SNS SC LINAC\*

D. Jeon<sup>†</sup> and J. Wei, SNS/ORNL, P.O.Box 2008, Oak Ridge, TN37830, USA  
 L. Merminga, G. Krafft, B. Yunn, R. Sundelin, and J. Delayen, JLab, Newport News, VA23606

### Abstract

Numerical simulation indicates that cumulative beam breakup (BBU) instability is not a concern to SNS SC linac. First, simulation is carried out for CW operation mode where the driving harmonics are those with frequency multiples of bunch frequency 402.5 MHz. Even when the median HOM frequency is exactly on resonance with multiples of bunch frequency of 402.5 MHz, the cavity-to-cavity HOM frequency spread can ensure operation of linac. Second, in the case of pulsed operation mode, additional driving harmonics of 1 MHz and 60 Hz are added on top of those of CW mode. The shunt impedance of these additional modes is relatively small. BBU is not a concern also for pulsed mode operation, as is verified for a few most dangerous modes. More systematic analysis of BBU of pulsed mode operation is done by Sundelin *et al* [1] and presented at this conference.

### 1 INTRODUCTION

SNS H linac is different from highly relativistic electron linacs in that the beam particle velocity is significantly less than the velocity of light  $c$ . Effects of wake field and bunch energy loss of a beam with  $\beta < 1$  is relatively unknown. Recently Kurennoy did some calculation on bunch energy loss for particle beams with  $\beta < 1$  [2]. It is shown that

$$\frac{k_s(\beta, \sigma)}{k_s(1, \sigma)} = \exp\left[-\left(\frac{\omega_s \sigma}{c}\right)^2 \frac{1}{\beta^2 \gamma^2}\right] \frac{(R/Q)(\beta)}{(R/Q)(1)} \quad (1)$$

where  $k_s(\beta, \sigma)$  is the loss factor of mode  $s$  and  $\sigma$  is half of rms bunch length of a Gaussian beam. Here  $\beta$  and  $\gamma$  are relativistic factors, and  $R/Q$  is the shunt impedance. For very short bunches,  $\exp[\dots] \approx 1$ . And it is a reasonable approximation to use

$$(R/Q)(\beta) = \frac{2c^2}{\epsilon_0 \omega^3} \frac{\left| \int_0^l e^{-i\omega z / \beta c} \frac{\partial E_z(0,0,z)}{\partial x} dz \right|^2}{\int_V E^2 dV} \quad (2)$$

for H (or proton) replacing  $R/Q(1)$  of highly relativistic electron linacs.

A study is performed to investigate the effects of HOM (Higher Order Mode) of SNS superconducting (SC) linac on cumulative beam breakup. This is to provide tolerable Q value of HOM and to provide a systematic view of the dependence on parameters involved such as frequency,

\*Work supported by the DOE, under contract No. DE-AC05-00OR22725 with UT-Battelle, LLC for ORNL  
<sup>†</sup>jeond@ornl.gov

Q value, R/Q, frequency spread of HOM. For simulation, TDBBU code [3] developed at JLab is used with the relevant input of SNS SC linac.

Fundamental mode frequency of SNS SC linac is 805 MHz while bunch frequency is 402.5 MHz because beam bunch is in every other bucket. The linac bunch train is 645 ns long and the gap is 300 ns. And the macro bunch train is 1 ms long. For example, when  $Q=10^5$ ,  $\omega=2\pi \times 2400\text{MHz}$  and  $g=302.4$  ns, only 2.3% of HOM field is damped during this 302.4 ns gap because the remaining field is proportional to  $\exp(-\omega g/2Q)$ . This is a pessimistic condition from the beam breakup viewpoint.

### 2 BENCHMARKING

Benchmarking of TDBBU code is done by repeating the simulation in Gluckstern's paper [4] and by comparison with the analytical theory. The TDBBU simulation has also reproduced the Gluckstern simulation results exactly as is shown in Fig. 1.

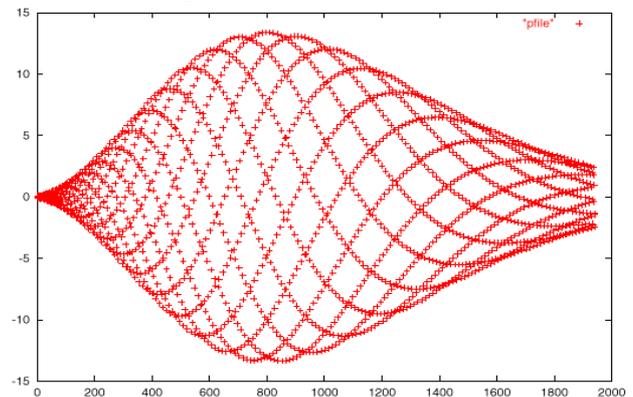


Figure 1: Plot of transverse beam centroid displacement at the end of the linac.

### 3 THRESHOLD CURRENT VERSUS Q VALUE OF HOM

The dependency of threshold current on Q of HOM is studied under pessimistic conditions. In the simulation, all the cavities both in the medium beta section and high beta section are assumed to have the same  $f_{\text{HOM}}$  of 2012.6 MHz. This is only 0.1MHz away from the resonance frequency 2012.5 MHz. Threshold beam current is defined as the beam current that produces deflecting factor of 2 at the end of SC linac during 1ms beam bunch train. When the deflection factor is larger than 2, beam loss due to the foil miss becomes a concern. The deflection factor  $D$  scales as

$$D \propto \exp[\sqrt{IQ_{\text{HOM}}R/Q}], \quad (3)$$

where  $I$  is the beam current,  $Q_{\text{HOM}}$  the quality factor of a HOM and  $R/Q$  the shunt impedance. Figure 2 shows

curves of threshold current for five different values of shunt impedance  $R/Q$ .

One interesting fact is that threshold beam current starts to saturate around  $Q=1.0 \times 10^7$  for all five values of shunt impedance. Because the "rise time" of the HOM is  $1.0 \times 10^7 / (\pi * 2.0126 \times 10^9) \sim 1.58$  ms for a 2012.6 MHz mode when  $Q$  is around  $1.0 \times 10^7$ . In other words, the instability cannot grow without a long enough pulse for the HOMs to be appreciably excited. When  $R/Q=100 \Omega$ , threshold current of 36mA corresponds to  $Q=2.5 \times 10^7$ . It should be noted that threshold current is inversely proportional to shunt impedance  $R/Q$ .

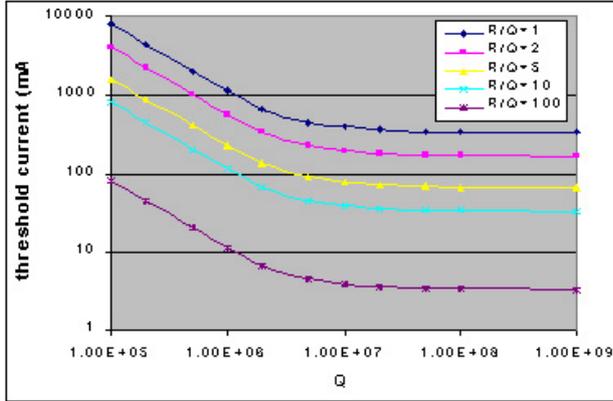


Figure 2: Plots of threshold beam current (mA) versus  $Q$  for different values of shunt impedance  $R/Q$  in Ohm.

#### 4 EFFECT OF HOM FREQUENCY SPREAD

Due to tolerances on manufacturing process of cavities, the frequency of a HOM varies from cavity to cavity. In the case of JLab FEL cavities, cavity to cavity  $f_{\text{HOM}}$  ranges from 5MHz to 30MHz. Cornell data shows that 0.38% maximum fractional  $f_{\text{HOM}}$  is measured. This HOM frequency spread effectively reduces the  $Q$  of the mode [5] and increases threshold beam current. In the simulation,  $Q=1.0 \times 10^7$  is assumed and shunt impedance  $R/Q$  is set to  $100 \Omega$  for all the cavities and the beam current  $I$  to 500 mA, more than ten times of the design current.  $Q=1.0 \times 10^7$  is chosen because threshold current starts to saturate from this value.  $100\text{-}\Omega$  shunt impedance is chosen because MAFIA study [6] indicates that biggest shunt impedance is less than or equal to about  $100 \Omega$ . Beam current is set to 500 mA to allow enough safety factors. One of resonant HOM frequencies is chosen. Median frequency of HOM is set to 2012.5 MHz.

Effect of HOM frequency spread is studied for the Lorentzian HOM frequency distribution and uniform HOM frequency distribution. The Lorentzian HOM frequency spread is given by

$$g(f) = \frac{1}{\pi} \frac{\Delta f}{(f - f_o)^2 + \Delta f^2} \quad (4)$$

where  $f_o$  is the median HOM frequency and  $\Delta f$  is frequency spread (half-width-half-maximum).

The average deflecting factor versus frequency spread (half-width-half-maximum) in MHz is displayed in Fig. 3.

HOM frequency spread dramatically reduces average deflecting factor. Average is taken over 1000 Monte Carlo linacs. 3.0MHz Half-Width-Half-Maximum Lorentzian HOM frequency spread makes linac operation possible even for 500-mA beam current under most severe resonant condition.

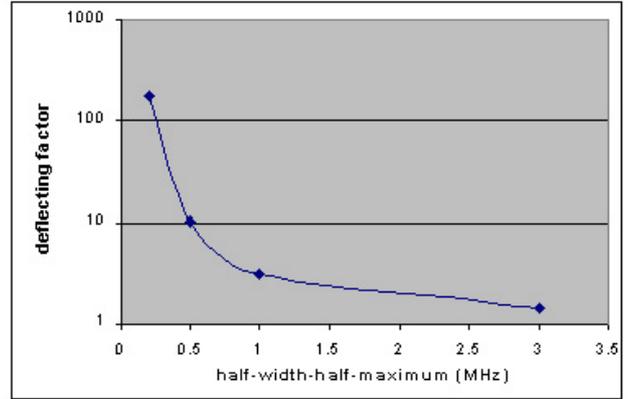


Figure 3: Plot of deflecting factor vs. HWHM (half-width-half-maximum) spread of Lorentzian HOM frequency distribution.

#### 5 EFFECT OF PULSED MODE OPERATION

There is a 300 ns gap in every 945 ns midpulse, which corresponds to 1.058 MHz spectral line. The duration of each macropulse is about 1 ms. The frequency of macropulse is 60 Hz. Preliminary transverse and longitudinal beam breakup simulation is done to estimate the effects of these time structure for a few seemingly dangerous modes. In the simulation presented in Fig. 4, modes listed in Table 1 are taken into consideration. These modes are obtained from MAFIA run. These modes have  $f_{\text{HOM}}$  quite close to multiples of bunch frequency 402.5 MHz and  $Q$  values are assumed to be  $10^8$ . One monopole mode other than the five-passband modes is taken into consideration. Maximum  $R/Q$  value is used for all the cavities instead of energy dependent  $R/Q$  values.

Table 1: HOM data used for simulation

Cavity	HOM	$f_{\text{HOM}}$ [MHz]	$R/Q$ [ $\Omega$ ]	$Q$
$\beta_{\text{med}}$	Monopole	2817.5	0.500	$10^8$
$\beta_{\text{med}}$	Dipole	1623.9	1.680	$10^8$
$\beta_{\text{med}}$	Dipole	2021.5	3.900	$10^8$
$\beta_{\text{med}}$	Dipole	2410.5	1.710	$10^8$
$\beta_{\text{med}}$	Dipole	2429.9	0.195	$10^8$
$\beta_{\text{high}}$	Monopole	2817.5	0.500	$10^8$
$\beta_{\text{high}}$	Dipole	2380.5	0.174	$10^8$
$\beta_{\text{high}}$	Dipole	2416.7	0.361	$10^8$
$\beta_{\text{high}}$	Dipole	2818.8	0.408	$10^8$
$\beta_{\text{high}}$	Dipole	2837.2	1.060	$10^8$

All bunches are transversely offset by 1 mm at injection. Figure 4 shows plots of  $x$  (mm),  $E_r$  (MeV) and  $\phi$  (deg) at the end of SC linac vs. 945-ns long midpulse number over 10 macropulses. Simulation is done with  $\pm 0.01$  MHz

and  $\pm 0.1\text{MHz}$   $f_{\text{HOM}}$  spread (monopole and dipole modes, uniform distribution). There is no sign of instability transversely and longitudinally, even though there is some fluctuation. With  $\pm 0.1\text{MHz}$  uniform  $f_{\text{HOM}}$  spread (in blue), the fluctuation is already negligible. Even with  $Q=10^8$ ,  $\pm 0.1\text{MHz}$  uniform  $f_{\text{HOM}}$  spread is sufficient. In reality,  $f_{\text{HOM}}$  spread of other SC cavities is much larger than this. So this BBU issue is not a concern for SNS SC linac.

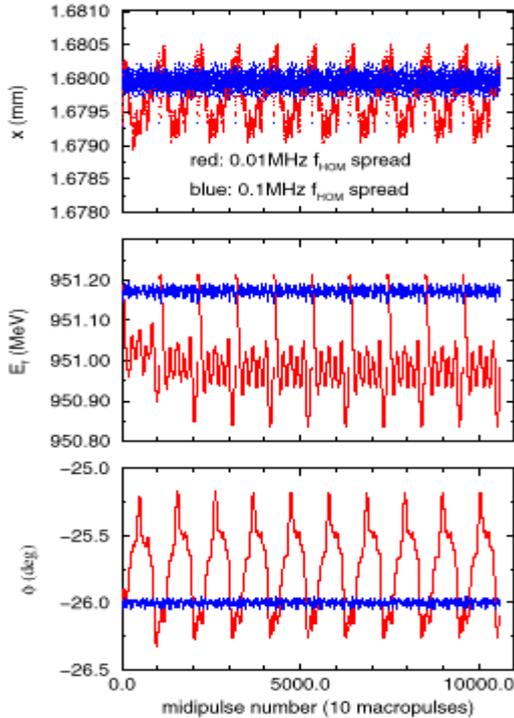


Figure 4: Plots of  $x$  (mm),  $E_r$  (MeV) and  $\phi$  (deg) at the end of SC linac for 10 macropulses. 10 macropulses are clearly shown. The gap is depicted here. With  $\pm 0.1\text{MHz}$   $f_{\text{HOM}}$  spread (uniform distribution), there is no beam breakup instability in both transverse and longitudinal motion.

Now comes the issue of HOM power dissipation in the cavities. Figure 5 shows plots of cavity heat load in W for the monopole mode in Table 1 for three different values of uniform  $f_{\text{HOM}}$  spread. This is for one Monte-Carlo machine. Cavity heat load stays below  $0.01\text{W}$  for most cavities with  $\pm 1.0\text{MHz}$  uniform  $f_{\text{HOM}}$  spread. It should be noted that usual  $f_{\text{HOM}}$  spread is much larger than the  $\pm 1.0\text{MHz}$  uniform  $f_{\text{HOM}}$  spread. Again HOM power dissipation is not dangerous with a sufficient  $f_{\text{HOM}}$  spread. More systematic analysis of cavity heat load is done by Sundelin [1] and Kim [6]. The cavities with high heat load have  $f_{\text{HOM}}$  quite close to resonances.

Figure 6 shows plots of beam energy jitter for three different  $f_{\text{HOM}}$  spread vs. pulse number. The beam energy jitter is already less than  $0.05\text{MeV}$  for  $0.1\text{MHz}$   $f_{\text{HOM}}$  spread. Slight spread of HOM frequency dramatically stabilizes the beam.

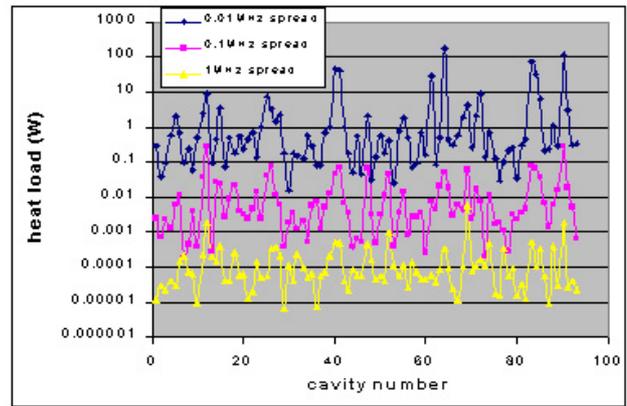


Figure 5: Plots of cavity heat load in W for the monopole mode in Table 1 for three different uniform  $f_{\text{HOM}}$  spread.

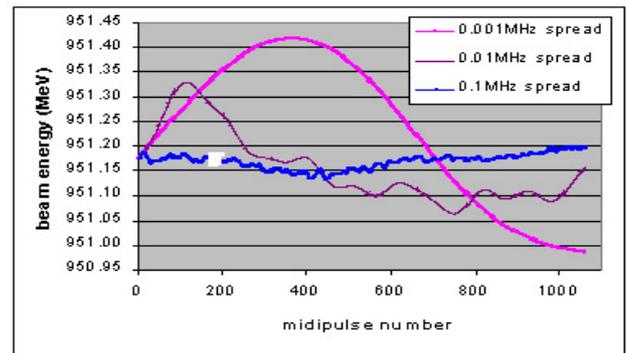


Figure 6: Plots of final beam energy jitter for three different  $f_{\text{HOM}}$  spread vs. pulse number.

## 6 CONCLUSION

Study indicates that HOM beam break-up is not a concern even for a pulsed mode operation of SNS superconducting linac. This is mainly due to the HOM frequency spread of cavities due to manufacturing tolerances. Heat load does not seem to be a concern up to  $Q=10^8$  with  $\pm 1.0\text{MHz}$  uniform  $f_{\text{HOM}}$  spread.

## 7 REFERENCES

- [1] R. Sundelin *et al*, in this conference.
- [2] S. Kurennoy, "Dependence of bunch energy loss in cavities on beam velocity", PRST-AB **2**, 032001 (1999).
- [3] G.A. Krafft and J.J. Bisognano, Two Dimensional Simulations of Multipass Beam Breakup, Proc. of the 1987 Particle Accelerator Conference, 1356 (1987).
- [4] R.L. Gluckstern, R.K. Cooper and P.J. Channel, "Cumulative Beam Breakup in RF Linacs", Part. Accel. **16**, 125 (1985).
- [5] C. L. Bohn and J. R. Delayen, "Cumulative beam breakup in linear accelerators with periodic beam current" Phys. Rev. A **45**, 5964 (1992).
- [6] S. Kim *et al*, in this conference.