TEST OF A COAXIAL BLADE TUNER AT HTS/FNAL
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Abstract
A coaxial blade tuner [1] has been selected for the 1.3GHz SRF cavities of the Fermilab SRF Accelerator Test Facility [2]. Results from tuner cold tests in the Fermilab Horizontal Test Stand [3] are presented.

INTRODUCTION
Fermilab is constructing the SRF Accelerator Test Facility [2], a facility for accelerator physics research and development. This facility will contain a total of six cryomodules, each containing eight 1.3 GHz nine-cell elliptical cavities. Each cavity will be equipped with a Slim Blade Tuner [1] designed by INFN Milan.

The blade tuner incorporates both a stepper motor and piezo actuators to allow for both slow and fast cavity tuning. The stepper motor allows the cavity frequency to be statically tuned over a range of 500 kHz with an accuracy of several Hz. The piezos provide up to 2 kHz of dynamic tuning for compensation of Lorentz force detuning and variations in the He bath pressure.

The first eight blade tuners were built at INFN Milan, but the remainder are being manufactured commercially following the INFN design. To date, more than 40 of the commercial tuners have been delivered.

CM2 Piezo Capsules
Piezo actuators can be damaged if they are subject to excessive shear forces. To limit shear, each actuator for the CM2 cavities was encased in a stainless steel capsule as shown in Figure 2.

TUNER TESTING IN THE HTS
Following installation of the tuner on each dressed cavity, the assembly is cold tested in the Fermilab Horizontal Test Stand (HTS) to ensure it meets CM2 performance requirements [4].

A dedicated HTS Tuning Control System has been developed to allow the performance of each tuner to be characterized and to provide compensation for Lorentz force detuning during other HTS operations. The compensation system can track changes in the cavity resonant frequency as operating conditions (e.g. gradient, pressure, etc.) change and can adapt the piezo drive waveform to keep the cavity on resonance. To date a total of 10 CM2 cavities have undergone testing in the HTS.

Those steps of the overall HTS test procedures related to the tuner performance evaluation are:

1. The room temperature cavity resonant frequency is measured prior to cool-down using a network analyzer.
2. The cavity is cooled to its operating temperature of 2K and the resonant frequency is again measured using a network analyzer.
3. The tuner stepper motor is exercised to ensure that the cavity can be set to any frequency within the required slow tuning band.
4. The cavity is tuned to the nominal operating frequency of 1.3GHz using the stepper motor.
5. The cavity is connected to the pulsed RF system and the maximum operating gradient is established following coupler conditioning.

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6. The cavity gradient is set to 5 MV/m and the piezo actuators are exercised to ensure the cavity can be set to any frequency within the required fast tuning band.

7. The gradient is increased in 5 MV/m steps up to the maximum gradient and the piezo actuators are exercised at each step.

8. The gradient of the cavity is set several MV/m below the maximum gradient and the piezo actuators are driven with short pulse 10 ms prior to the arrival of the RF pulse. The piezo-RF delay for the next pulse is shortened to 9.5 ms and this process is repeated until the piezo pulse arrives 10 ms following the RF pulse.

9. The results of the previous delay scan are used to calculate the piezo waveform needed to compensate for Lorentz force detuning and the fast tuning compensation system is turned on.

10. The cavity gradient is increased while the piezo compensation system remains active and the level of residual Lorentz force detuning during the RF flattop at maximum gradient is recorded.

**SLOW TUNER PERFORMANCE**

Figure 3 shows the frequency of one cavity, AES009, as the stepper motor is exercised. The response of the cavity frequency is linear to within several % as the stepper motor is rotated.

![Figure 3: Cavity frequency as a function of tuning motor steps. One turn of the slow tuner screw is equivalent to 17600 steps of the stepper motor.](image)

Table 1 provides a summary of the measured slow tuner performance parameters for all cavities tested to date.

<table>
<thead>
<tr>
<th>Cavity ID #</th>
<th>Frequency before installation (MHz)</th>
<th>Frequency after cool-down (MHz) 1 bar, 300K</th>
<th>Slow Tuner slope (kHz/turn)</th>
<th>Piezo-to-Cavity Sensitivity, Hz/V</th>
<th>Dynamic LFD Hz/(MV/m)$^2$</th>
</tr>
</thead>
<tbody>
<tr>
<td>ACC013</td>
<td>1297.385</td>
<td>1299.900</td>
<td>26.5</td>
<td>7.2</td>
<td>-970</td>
</tr>
<tr>
<td>AES009</td>
<td>1297.388</td>
<td>1299.813</td>
<td>31.2</td>
<td>6.5</td>
<td>-1240</td>
</tr>
<tr>
<td>ACCELL</td>
<td>1297.321</td>
<td>1299.750</td>
<td>-</td>
<td>8.5</td>
<td>-860</td>
</tr>
<tr>
<td>AES010</td>
<td>1297.200</td>
<td>1299.793</td>
<td>27.9</td>
<td>8.5</td>
<td>-950</td>
</tr>
<tr>
<td>AES008</td>
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<td>1299.735</td>
<td>26.5</td>
<td>7.3</td>
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<td>1299.899</td>
<td>28.1</td>
<td>10.5</td>
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</tr>
<tr>
<td>RIO29</td>
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<td>AES007</td>
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<td>10.4</td>
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<td>RIO18</td>
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<td>1299.882</td>
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<tr>
<td>Average</td>
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<td>1299.813</td>
<td>27.8</td>
<td>9.7</td>
<td>-960</td>
</tr>
</tbody>
</table>

Table 1: Summary of cavity/tuner measured performance parameters

$\sigma$ 0.116 0.065 1.7 2.8 295

As the AES009 stepper motor is driven below the nominal zero point, the cavity frequency approaches a “knee” at 1299.780MHz. At the knee, the blades no longer exert any force on the cavity. The frequency of the knee allows the piezo preload at the cavity operating frequency to be estimated. The AES009 preload of 1.1kN per piezo is within the acceptable range.

![Figure 4: Cavity frequency during the RF pulse at gradients of 8 and 28 MV/m as the piezo bias is varied.](image)
FAST TUNER PERFORMANCE

The piezo bias scans described in steps 5 through 7 of the HTS test procedure measure:
- The static sensitivity of the cavity frequency to the piezo drive voltage;
- Piezo hysteresis;
- The dynamic sensitivity of the cavity to the Lorentz force.

Error! Reference source not found. compares cavity detuning throughout the course of the RF pulse at two gradients as the piezo drive voltage is varied. In both cases, the frequency of the cavity closely tracks the piezo bias. While the cavity frequency changes very little during the RF pulse at the lower gradient, at the higher gradient the effects of the Lorentz force are clearly visible.

Figure 5 shows the hysteresis in the cavity frequency at a low gradient as the piezo bias is raised from 0V to 200V and then lowered back to the starting point.

Figure 6 shows the Lorentz force detuning of cavity ACC13 for different gradients up to the maximum of 27MV/m.

LORENTZ FORCE DETUNING COMPENSATION

The delay scan described in steps 8 and 9 of the HTS test procedure measures the response of the cavity frequency to the Lorentz force and to the piezo actuator. Using this information, the compensation system determines the piezo drive waveform required to compensate for Lorentz force detuning [5].

Figure 7: Lorentz Force Detuning compensation. The green and blue lines of the upper plot show the detuning of a cavity before and after compensation for Lorentz force detuning. The lower plot shows the piezo waveform.

Once the tuner performance has been characterized, the compensation system is routinely used to stabilize the cavity resonance during heat load measurements. These measurements can require several hours of stable operation at each load point [3].

CONCLUSION

Cavities for the CM2 cryomodule are subject to a battery of tests to verify that both the slow and fast tuners meet performance specifications.

REFERENCES